DEVELOPMENT SCHEME

Prepared under Section 25 (3) of the Urban Renewal Authority Ordinance





Cheung Wah Street /Cheung Sha Wan Road (SSP-018)

Urban Renewal Authority
September 2021

PART 1 PLANNING REPORT

Urban Renewal Authority

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PLANNING REPORT

September 2021



EXECUTIVE SUMMARY

- The Urban Renewal Authority (URA) submits this planning report to seek approval of the Town Planning Board (TPB) for the draft Development Scheme Plan (DSP) No. S/K5/URA3/A. The draft DSP refers to the proposed Development Scheme (the Scheme) at Cheung Wah Street / Cheung Sha Wan Road (SSP-018).
- 2. First, a street block at Kim Shin Lane / Fuk Wa Street (namely SSP-017) comprising 90 building blocks of age over 60 with no lifts is identify as a site with imminent redevelopment needs. However, SSP-017 is undesirable for redevelopment because its existing plot ratio is as high as 8.12, hence, the residual plot ratio is 0.88 only. Multiple sub-divided units are also identified. Although SSP-017 has all the quality to demand for redevelopment, its redevelopment potential is low. In this respect, a wider area for planning opportunities have to be explored. Taking a "planning-led" approach in urban renewal works in recent years. URA has identified part of Sham Shui Po as Sham Shui Po Action Area 1 (SSPAA1) for holistic urban renewal planning. SSP-018 comprises Sites A and B, both Government land opposite each other across Cheung Sha Wan Road, is identified for redevelopment to formulate a comprehensive land-use restructuring together with SSP-017 to create more planning gains at district level. The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017.
- 3. Built in 1976, the existing Cheung Sha Wan Sports Centre at Site A of the Scheme which will be reprovisioned and upgraded at Site B up to present-day standard. Site B of the Scheme will be redeveloped to provide a POS larger than the existing Cheung Sha Wan Path Sitting-out Area and other new Government, institution and community (GIC) facilities to serve the public in a wider district. Under an integrated approach, the new GIC complex and its adjacent proposed public open space (POS) will form a larger leisure and community hub in connection with the Sham Shui Po Sports Ground for public enjoyment.
- 4. Including the reprovision of the new Cheung Sha Wan Sports Centre, to accommodate the needs of the district on social welfare and health facilities identified by relevant Government departments, not less than 38,000 sq.m. non-domestic GFA is proposed for GIC uses at both sites in the Scheme, which is more than about 33 times of the existing GIC GFA. The provision of floor space for GIC uses is in line with the promotion of the Government's policy on "Single Site, Multiple Uses".

- 5. Through re-structuring and re-planning of existing land uses, the Scheme will optimize the land uses to achieve more planning gains for the community. Apart from materializing the planning intention of current OZP in providing GIC facilities and POS without the need to divert portion of Cheung Sha Wan Road, the GIC site can be fully utilized to provide more GIC facilities under the Scheme, while Site A after redevelopment can also optimize for residential use to increase flat supply of about 830 flats.
- 6. A maximum building height of 140mPD is proposed in Site A of the draft DSP for creating 15m wide tower separation and various podium setbacks for better air ventilation and walking environment. The proposed 5-storey podium will accommodate retail uses and GIC facilities with headroom requirements.
- 7. Taking this integrated renewal opportunity, footbridges across Cheung Sha Wan Road and Cheung Wah Street are proposed to connect the open space provided in both URA projects (SSP-017 and SSP-018) to enhance connectivity of amenity features for public. The resultant all-weathered at grade and elevated pedestrian network will not only integrate various GIC facilities and POSs, but also enhance overall permeability and connectivity of a wider area of Sham Shui Po in the vicinity of the Scheme in the vicinity of the Scheme.
- 8. Under an integrated urban renewal approach, the Scheme also provides various opportunities for feasible revitalisation initiatives outside the Scheme area. With the provision of underground public vehicle park at Site A, opportunities for the replacement of some on-street parking spaces in the area will be created to make way for possible pavement widening at strategic locations. Those separate revitalisation initiatives will in particular strengthen the connector role of Cheung Wah Street to enhance the connectivity between the medium aged building cluster further north and the future leisure and community hub in the south, thus benefits a wider area. For Site B, there is a possible integration of the new POS with the existing Sham Shui Po Sports Ground in the south subject to further co-ordination with Leisure and Cultural Services Department (LCSD) on the associated revitalisation work separately, upon approval of the DSP and subject to further coordination and acceptancy of relevant Government departments.

行政摘要

- 1. 市區重建局(市建局) 向城市規劃委員會提交發展計劃草圖(編號 S/K5/URA3/A),並命名為昌華街/長沙灣道發展計劃(SSP-018) (該計劃)。
- 2. 首先,位於兼善里/福華街(SSP-017)合共 90 幢樓齡超過 60 年的樓字,均沒有升降機設施,對重建有殷切需求。唯現時 SSP-017 的地積比已高至 8.12,剩餘地積比只有 0.88,欠缺重建誘因。據現場觀察,大部分單位亦已被分間成多個劏房出租。SSP-017 雖已具備所有重建的訴求,但重建潛力很低,因此需要以整區作規劃考慮一併處理。市建局以「規劃主導」的模式,近年制定部分的深水埗區為深水埗行動區(SSPAA1),實徹以全面的規劃方式進行市區更新工作。SSP-018 包括沿長沙灣道兩旁的地盤 A 及地盤 B 的政府用地,將與 SSP-017 一併納入重建,藉著重整現有土地用途,為社區帶來更大的規劃裨益。SSP-018 地盤 A 內擬議的住宅用途亦為 SSP-017 的重建帶來契機。
- 3. 現時位於地盤 A 的長沙灣體育館建於 1976 年,將會重置至地盤 B, 並提升至現今康樂設施的規格及設計標準。地盤 B 重建後將提供比現時長沙灣徑休憩處更大的公共空間,以及全新的政府、機構或社區設施。透過整體規劃,期望將新的政府、機構或社區設施綜合大樓、擬議的公共空間,以及鄰近的深水埗運動場,融合成一個社區康樂設施集中點,將規劃裨益擴展到該計劃以外的周邊社區,以惠及更多居民。
- 4. 為配合地區對社會福利及地區康健設施的需求,該計劃建議提供不少於 38,000 平方米的非住宅樓面面積作政府、機構或社區設施用途,當中包 括重置後的長沙灣體育館,為現時政府、機構或社區設施樓面面積的 33 倍。有關建議亦切合政府現行提倡「一地多用」的政策。
- 5. 該計劃藉著重整及重新規劃現有土地,優化土地用途並為社區帶來更大的規劃裨益。該計劃無需透過部分長沙灣道改道,亦能實踐現時分區計劃大綱圖內的規劃意向,善用該計劃地盤 B 的政府、機構或社區設施綜合大樓,提供更多政府、機構或社區設施,並提供公共空間。重建後的地盤 A 亦能地盡其用,提供約 830 個住宅單位。
- 6. 發展計劃草圖建議該計劃地盤 A 土地的建築物高度限制為 140 米(主水平基準以上),為該計劃內的樓字設計提供更大彈性,包括 15 米的樓字間距及建築物部分地面後退以確保良好的空氣流通及改善行人環境。擬議的 5 層基座平台,亦可容納零售設施和有淨空高度要求的政府、機構或社區設施。

- 7. 藉此整體規劃的機會,該計劃建議提供行人天橋橫跨長沙灣道及昌華街, 以連接兩個重建項目(SSP-017 及 SSP-018) 內的公共空間,以加強擬議 社區設施的連接性。全天候的地面及高架行人網絡不單連接不同的政府、 機構或社區設施和公共空間,亦能加強深水埗區一帶的連接性。
- 8. 作為整體市區更新模式,該計劃亦希望為該計劃範圍以外的地方帶來活化更新的機遇。在地盤 A 興建的地下停車場,長遠有助提供機遇,在鄰近一些策略性的地點騰出路邊泊車位,以擴闊行人路,有助推動該項目以外的活化項目,進一步提高昌華街的暢達性,加強北面「中年」樓字群及重建後南面的社區康樂設施集中點的連接,惠及鄰近社區。市建局將與康樂及文化事務署(康文署)在細部設計階段時檢討,以活化方式進一步改善地盤 B 內的公眾休憩用地和現時深水埗運動場的連接性。然而有關工程須視乎相關政府部門的意見/許可而定。

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1. INTRODUCTION

- 1.1 The Cheung Wah Street / Cheung Sha Wan Road Development Scheme (the Scheme) (SSP-018) is located in Sham Shui Po District, comprises Sites A and B along Cheung Sha Wan Road.
- 1.2 The Development Scheme is included in the Urban Renewal Authority (URA)'s 20th Business Plan, which was approved by the Financial Secretary for commencement in 2021/22. It is proposed to be processed as a Development Scheme under section 25 of the URA Ordinance (URAO). In August 2021, the URA's Board approved the submission of the Development Scheme under section 25(5) of the URAO to the Town Planning Board (TPB). The draft Development Scheme Plan (DSP) No. S/K5/URA3/A is prepared for submission to the TPB.
- 1.3 Pursuant to section 23(1) of the URAO, the URA notified the public in the Government Gazette about the commencement of the Development Scheme on 24 September 2021. The draft DSP is now submitted under section 25(5) of the URAO to the TPB for consideration.
- 1.4 This planning report (Part 1 of the whole report) is prepared to provide the TPB with the necessary background information and the planning proposal to facilitate its consideration of the draft DSP (Part 2 of the report), submitted under section 25 of the URAO. Supplementary information, including the preliminary design of the proposed development, key technical assessments, social impact assessment (SIA) (Stage 1), and implementation approach are enclosed in Part 3 for reference.
- 1.5 First, a street block at Kim Shin Lane / Fuk Wa Street (namely SSP-017) comprising 90 building blocks of age over 60 with no lifts has been identify as a site with imminent redevelopment needs. However, SSP-017 is undesirable for redevelopment because its existing plot ratio is as high as 8.12, hence, the residual plot ratio is 0.88 only. Multiple subdivided units are also identified. Although SSP-017 has all the quality to demand for redevelopment, its redevelopment potential is low. In this respect, a wider area for planning opportunities have to be explored. Taking a "planning-led" approach in urban renewal works in recent years, URA has identified part of Sham Shui Po as Sham Shui Po Action Area 1 (SSPAA1) for holistic planning. SSP-018 comprises Sites A and B, both Government land opposite each other across Cheung Sha Wan Road, is identified for redevelopment to formulate a comprehensive land-use restructuring together with SSP-017 to create more planning.

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- gains at district level. The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017.
- 1.6 As SSP-017 conforms to the existing planning control, it will be implemented under section 26 of the URAO separately; it <u>does not</u> form part of this DSP.

2. THE DEVELOPMENT SCHEME PLAN AREA

- 2.1. The Development Scheme (the Scheme) is located in Sham Shui Po (SSP) District, comprises Sites A and B along Cheung Sha Wan Road. Plan 1 shows the location of the Scheme. Site A of the Scheme is bounded by Hing Wah Street on the southeastern boundary, Cheung Sha Wan Road on the southwestern boundary, Cheung Wah Street on the northwestern boundary, and Cheung Sha Wan Catholic Secondary School on the northeastern boundary. It is currently occupied by the Cheung Sha Wan Sports Centre and a garden both under Leisure and Cultural Services Department (LCSD). Subject to site survey upon DSP approval, the net site area used to calculate the development potential of Site A is about 5,197 sq.m.
- 2.2. Site B of the Scheme is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground to the southeast. It covers a gross site area of about 13,857 sq.m, involving the Cheung Sha Wan Path Sitting-out Area and its adjoining garden under LCSD, as well as a temporary maintenance depot of Highways Department. Subject to site survey upon DSP approval, the net site area used to calculate the development potential of the site for Government, institutions or community (GIC) facilities at Site B is about 4,212 sq.m. The Scheme Area is shown in Plan 2.
- 2.3. Site A is currently zoned for "Government, Institution or Community (G/IC)" and "Open Space (O)", while Site B is currently zoned for "Government, Institution or Community (G/IC)", "Open Space (O)", and shown as 'Road' on the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37. An extract of the OZP is shown on **Plan 3**.
- 2.4. The Scheme aims to optimise the land uses to achieve more planning gains for the community through re-structuring and re-planning. With the proposed development, more GIC facilities up to present-day standard

and a set of connected public open space (POS) will be provided for public enjoyment. The Scheme will create synergy effect with the adjoining URA redevelopment project (SSP-017) (**Plan 4** refers) and manifest the planning gains to serve a wider area of Sham Shui Po. The holistic planning driven approach and objectives of the Scheme are in line with the objectives of urban renewal under the Urban Renewal Strategy (URS) issued in 2011 aiming to:

- · Restructuring and replanning of concerned urban areas;
- Designing more effective and environmentally-friendly local transport and road networks within the concerned urban areas;
- Rationalising land uses within the concerned urban areas;
- Redeveloping dilapidated buildings into new buildings of modern standard and environmentally-friendly design;
- Providing more open space and community/welfare facilities; and
- Enhancing the townscape with attractive landscape and urban design.

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3. BACKGROUND AND EXISTING CONDITIONS

Historical Background

- 3.1 Cheung Sha Wan where the Scheme locates was named after the long beach between Sham Shui Po and Lai Chi Kok. The Scheme was at the coast in the pre-war era and to the farther southeast of the Scheme founded as a market town at around 1750-1760s. In the early 19th Century, the town was already well-established and functioned as a service centre for shipping and trade. The town grew rapidly as a primary market after the establishment of the city of Hong Kong since it was one of the best-located places for the trade in firewood and fresh food. By the end of 19th Century, certain businesses such as lime-burning, tanning, iron working, boat making and repairing, dyers, joss-stick trades and stone-cutting were well developed in Sham Shui Po. To the northwest of Sham Shui Po was a string of villages with a large piece of cultivated area are found along the coast where the Scheme locates.
- 3.2 In the early 20th Century, private developers started small-scale reclamation work in Sham Shui Po. Before the war, the Government undertook two major reclamations in 1912 and 1919 extending the reclaimed area to Tonkin Street. Historical map and aerial photo records indicate that the coast where the Scheme locates started being reclaimed and developed at around 1950-1960s to provide land for housing and factories to accommodate the flow of immigrants from China after 1949.

Existing Uses

3.3. The Scheme consists of Sites A and B along Cheung Sha Wan Road. The existing Cheung Sha Wan Sports Centre at Site A is under the LCSD. The sports centre provides basic recreational facilities for public use during the opening hours and organise various recreational activities and training courses regularly for the public. According to the LCSD's website, the sports centre provides 1 multi-purpose arena for 1 volleyball court or convert to 1 basketball court (sub-standard 5-a-side basketball court) or convert to 4 badminton courts each of which can be converted into 2 table-tennis tables on weekdays. The sports centre was built in 1976 which the design and facilities is below current standard.

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3.4. Site B of the Scheme involves the Cheung Sha Wan Path Sitting-out Area and its adjoining garden under LCSD, as well as a temporary maintenance depot of Highways Department. The existing open space at both Sites A and B are disconnected while the Sham Shui Po Sports Ground is in the south.

Surrounding Land Uses

- 3.5. The street blocks adjoining the Scheme are a mix of residential, commercial and industrial uses. The Scheme is predominately surrounded by residential buildings to the east while commercial and industrial uses are more concentrated to the west of the Scheme. Some of the industrial buildings appear not to be engaged in manufacturing activities but mainly for office, storage, workshop / showroom uses. To the east across Hing Wah Street is predominantly public housing, Un Chau Estate, while private residential buildings are found mainly to the north of the Scheme. Commercial uses such as retail shops, eateries and car repair shops are found on the ground floor of the surrounded residential buildings.
- 3.6. The Sham Shui Po Sports Ground is located to the south of the Scheme, which is a popular venue for local sports activities and events.

Existing Traffic Network

3.7. The Cheung Sha Wan Road in between Sites A and B of the Scheme is a primary distributor forming the major traffic road connecting east and west with high traffic flow. To the east of the Scheme is Hing Wah Street is a district distributor which is a key traffic road connecting north and south. Cheung Wah Street, Fuk Wa Street and Fuk Wing Street are local distributors locating to the northwest of Site A of the Scheme. Some of the local roads are frequently occupied by road-side parking, storage and loading/unloading activities.

Existing Pedestrian Network

3.8. The Scheme is located between Lai Chi Kok and Cheung Sha Wan MTR Stations. Cheung Sha Wan Road in between Sites A and B of the Scheme is the major pedestrian corridor in the vicinity. Many residents from Un Chau Estate locating at the east of the Scheme and nearby residential developments locating at the north of the Scheme walk to Cheung Sha Wan Road for public transport services. At present, long

- queuing at the bus stops often appear along the pavement of Cheung Sha Wan Road, resulting in a crowded condition along the pavement.
- 3.9. Residents from the nearby residential developments often walk through three inner streets in the vicinity of the Scheme for daily activities, i.e. Cheung Wah Street, Fuk Wa Street and Fuk Wing Street. However, the current pedestrian environment may be unwelcoming as the car repairing activities, dumping and roadside storage often occupied the pavement of these streets.
- 3.10. The existing temporary maintenance depot of Highways Department at Site B is not accessible by public and acts as a major blockage of the pedestrian network. The existing Cheung Sha Wan Sports Centre and Garden at Site A is disconnected from the existing Cheung Sha Wan Path Sitting-out Area at Site B and the Sham Shui Po Sports Ground in the south. Local residents in the north of the Scheme has to pass through the Cheung Sha Wan Path Sitting-out Area to reach the Sham Shu Po Sports Ground for sports activities.

Environmental Condition

3.11. The Scheme is along the heavily trafficked Cheung Sha Wan Road between Site A and B and Castle Peak Road to the further northwest. The Scheme is envisaged to be subject to severe traffic noise and air pollutants generated from the heavy traffic along these major roads.

4 PLANNING AND LAND USE PROPOSALS

Development Intensity

- 4.1. Under the draft DSP, the scheme area in orange colour is proposed to be zoned "R(A)", which is primarily for residential use, with the lowest three floors or in the purpose-designed non-residential portion of a building for commercial use as stipulated in the proposed Notes of the "R(A)" zone. The scheme area in green is proposed to be zoned "O" while the scheme area in blue is proposed to be zoned "G/IC".
- 4.2. In the Notes of "R(A)" zone, the proposed plot ratio (PR) is 7.5 for domestic building or 9.0 for a building that is partly domestic and partly non-domestic, which is in line with the development intensity of "R(A)" zone under the prevailing Cheung Sha Wan OZP. It is proposed to include a clause in the "Remarks" of the proposed Notes of "R(A)" stating that "any floor space that is constructed or intended for use solely as GIC facilities, as required by the Government, may be disregarded from PR calculation".
- 4.3. A maximum building height of 140mPD is proposed at Site A under the draft DSP to enable a higher podium design to mitigate the severe traffic noise generated from the surrounding road traffic (details on technical assessments described in paragraph 4.14 to 4.24). This will not only allow for accommodating GIC facilities with appropriate headroom in the podium, but will also opportune for creating 15m tower separation and various podium setbacks, including about 15-20m ground floor setback from Cheung Wah Street for better air ventilation and providing opportunities to preserve existing trees. It is considered compatible with the nearby built environment, which includes Un Chau Estate (120mPD) and The Sparkle (152mPD) to the southeast of the Scheme.
- 4.4. For Site B, a maximum building height of 95 mPD is proposed for the GIC complex.
- 4.5. The proposed development parameters of the Scheme are shown in **Table 4.1**, which will be subject to adjustments in the detailed design stage after DSP's approval.

 Table 4.1
 Proposed Development Parameters of the Scheme

Parameters (Site A)	Details
Gross Site Area	About 5,197 sq.m.
Site Area for PR Calculation	About 5,197 sq.m.
	(subject to survey and detailed design)
Proposed Zoning	"R(A)"
Proposed Maximum Building Height	Not more than 140mPD
Proposed Maximum Domestic GFA (PR)^	About 38,978 sq.m. (PR = 7.5)
Proposed Maximum Non-domestic GFA (excluding GIC Provision (PR)) ^A	About 5,197 sq.m. (PR = 1.0)
Proposed Non-domestic GFA for GIC Provision (PR) ^ (proposed to be exempted from GFA calculation under DSP)	Not less than 5,197 sq.m. (PR = 1.0)
Total GFA	Around 49,372 sq.m.
No. of Flats®	About 830 flats
Average Flat Size@ (GFA)	About 46 sq.m.
Internal Transport Facilities for the proposed development (including the proposed provision for GIC facilities)*	Basement ancillary car park to accommodate: - 142 nos. private car parking spaces - 12 motor-cycle parking spaces - 9 nos. L/UL bays
Public Vehicle Park*	Basement public vehicle park to accommodate about 50 private car parking spaces
Proposed Public Open Space	About 750 sq.m.

Parameters (Site B)	Details
Gross Site Area	About 13,857 sq.m
Net Site Area (for G/IC)	About 4,212 sq.m.
	(Subject to site survey and detailed
	design)
Proposed Zoning	"G/IC", "O"
Proposed Maximum Building	Maximum 95 mPD
Height (for G/IC)	
Proposed Maximum G/IC GFA	About 33,696 sq.m. (8.0)
(PR)^	
Proposed Public Open Space	About 9,645 sq.m.
Internal Transport Facilities for the	Basement ancillary car park to
proposed development*	accommodate:
	- 65 nos. private car parking spaces
	- 3 nos. L/UL bays

Notes:

- ^ The exact GFA and PR are subject to TPB approval, detailed design and prevailing First Schedule of Building (Planning) Regulations (B(P)R).
- @ Indicative only, subject to detailed design at project implementation stage.
- * Subject to liaison and agreement with Transport Department.

Conceptual Layout

4.6. As shown in the indicative block plan and the section plan of the notional design for the Scheme in (Appendix 1), the proposed development at Site A comprises two residential towers (T1 and T2) on top of a commercial/retail/GIC podium, an open space, and a basement car park for public and ancillary parking spaces. Site B comprises of a GIC complex building and a POS.

Re-provision and new provision of GIC facilities for the community

4.7. To accommodate the needs of the district on social welfare and health facilities and align with "Single Site, Multiple Uses" principle promoted by Government, it is proposed to provide about 38,893 sq.m. non-domestic GFA is proposed for GIC uses at both sites in the Scheme, which is more than 33 times of the existing Cheung Sha Wan Sports Centre of about 1,170 sq.m. at Site A.

4.8. The existing Cheung Sha Wan Sports Centre at Site A, built in 1976, will be reprovisioned at Site B and be upgraded to prevailing standard and continue its operation for public enjoyment. The proposed GFA of the reprovisioned sports centre at Site B will be about 9,100sq.m. which will be about 8 times of the existing sports centre at Site A. A multi-purpose air-conditioned main games arena which can used for 1 netball court/ 2 basketball courts/2 volleyball courts/8 badminton courts will be provided in the proposed GIC complex at Site B. In addition, a multi-purpose activity room, dance room, fitness room, table-tennis room, children's play room, etc. will be provided in the new Cheung Sha Wan Sports Centre subject to further liaison with LCSD. The actual uses of the new GIC provision in the Scheme will be subject to liaison with Planning Department, other relevant Government departments as well as the views from the relevant stakeholders.

Re-structuring of POS and provision of all-weathered at-grade and elevated pedestrian network to enhance walkability and connectivity

- 4.9. Under the proposed Scheme, a POS of not less than 9,645 sq.m is proposed at Site B and a POS of not less than 750 sq.m. is proposed at Site A along Cheung Sha Wan Road. The restructured POS provision will not be less than the area of existing POS provision of about 10,382sq.m at Sites A and B and provide better integration. According to the consultation with LCSD, LCSD agreed to take up the management and maintenance of the proposed POS at Site B. LCSD proposed the POS at Site A under planning to be under ownership and management of URA or its future joint-venture partner(s), or its assignee, as it will be fronting the retail facilities of Site A, subject to further liaison with relevant Government departments upon DSP approval. It is envisaged that the proposed POS at Site A will be open to public during reasonable hours.
- 4.10. Taking this redevelopment opportunity, footbridges across Cheung Sha Wan Road and Cheung Wah Street are proposed to connect up the POSs at the Scheme and an adjoining URA project (SSP-017). The resultant all-weathered at-grade and elevated pedestrian network will not only integrate various GIC facilities and POSs, but will also enhance connectivity of a wider area of Sham Shui Po. Proper paving and landscaping, where appropriate, will be provided at the pedestrian walkways to create a safe and pleasant walking environment. Given the

- proposed footbridges are outside the DSP boundary and do not form part of the DSP, the URA will liaise with relevant Government departments on the proposal via a separate revitalisation initiatives subject to the approval of DSP and detailed technical feasibility.
- 4.11. To further enhance the walkability of the Scheme Area, ground floor setbacks will be provided along Cheung Sha Wan Road, Cheung Wah Street and Hing Wah Street to create a wider pavement for a better walking environment. With an integrated urban renewal approach, the provision of underground public vehicle park at Site A would create opportunity for the replacement of some on-street parking spaces in the area. It will make way for possible pavement widening under separated revitalization work at strategic locations. For Site B, there is a possible integration of the new POS with the existing Sham Shui Po Sports Ground in the south subject to further co-ordination with LCSD on the associated revitalization work.

Proposed building height to enhance flexibility in building design

- 4.12. A maximum building height of 140mPD is proposed in Site A of the Scheme Area, which can enable a slimmer building form and wider building separation to enhance building permeability of the local area. Despite not less than 750 sq.m of open space will be provided at Site A, ground floor setbacks (15-20 m along Cheung Wah Street) are also proposed for pavement widening to create better walking environment and provide opportunities to preserve or transplant trees at Site A.
- 4.13. Given the Scheme adjoins to the Cheung Sha Wan Road which is a heavy traffic road, a 5-storey podium is proposed at Site A, with an aim to raise the residential floors to higher levels to mitigate noise impacts according to the respective technical assessments (Details on technical assessments provided in para. 4.16 to 4.26). The 5-storey podium will also allow for accommodating GIC facilities with headroom requirements to serve a wider district. With the proposed building height of 140mPD, the two proposed residential towers in Site A can adopt more flexible design on block size, disposition and layout to provide sufficient building separation as recommended in the Sustainable Building Design (SBD) Guidelines to improve permeability.

Greenery and Landscaping

4.14. A total of 294 nos. of trees (with 95mm Diameter at Breast Height (DBH) or above) were identified within the Scheme Area. The majority of the

- existing trees were found to be in fair form, fair health and fair amenity value. No old and valuable trees (OVTs) are recorded on site. All the existing trees will be retained or transplanted as far as practical.
- 4.15. The proposed development will follow the SBD Guidelines as far as practicable to provide greenery to enhance the built environment. Greenery will be provided at pedestrian level, podium edge as well as roof top where appropriate and applicable, to create a visual relief and enhancement of the built environment. A tree survey was conducted and a compensation planting proposal was prepared together with a preliminary design concept to address the conditions of the existing vegetation on site (see **Appendix 2**). Mitigation measures are proposed for the trees affected by the proposed development of the Scheme. Detailed landscape design, layout arrangement and proposed tree treatment of the POS at Site B will be further liaised with LCSD upon DSP approval.

Technical Assessments

Visual Impact

4.16. A Visual Impact Assessment (VIA) was conducted (see Appendix 3) to study the potential visual impact with the implementation of the Scheme. Visual appraisal has made reference to the Town Planning Board Guidelines No. 41 and been carried out at locally viewpoints. The proposed building height of not more than 140mPD at Site A respects and complements the building height profile of the surrounding context. The study has demonstrated that the proposed development was visually compatible with the surrounding built environment and planned developments, and would not create significant visual impact in general.

Social Impact

4.17. In accordance with the URS, a non-obtrusive SIA (Stage 1) has been conducted and the report is included as **Appendix 4**. The report includes the local profile of the Scheme, which will need to be prepared for and borne in mind during the implementation of the Scheme. The Stage 2 SIA report is under preparation based on factual data, which has been conducted on the commencement of the Scheme. The Stage 2 SIA report will be submitted to TPB separately. The SIA reports are to assess the likely effect of the implementation of the Scheme and to propose mitigation measures to minimise any social impact.

Traffic Impact

4.18. A TIA (see Appendix 5) has been conducted to assess the traffic impact of the Scheme and the proposed provision of internal transport facilities of the proposed development. The TIA demonstrated that the Scheme (together with the proposed public vehicle park) has no adverse traffic impact on the local traffic network and the pedestrian walking environment. The proposed parking provision and the internal transport facilities aligns with the requirements in the latest HKPSG and are acceptable from traffic engineering point of view.

Environmental Aspect

- 4.19. An Environmental Assessment (EA) (see **Appendix 6**) was conducted to study any potential environmental impact/benefits associated with the implementation of the Scheme. The study concluded that the impact on air quality, noise impact, land contamination and waste management were not insurmountable with mitigation measures adopted if necessary.
- 4.20. Air quality impact assessment (AQIA) indicated that in view of the local air quality condition, fresh air intake and residential units for the proposed development in Site A of the scheme area shall be located at minimum about 6.35mAG (i.e. about 11mPD) above ground to meet the air quality requirement under AQOs.
- 4.21. On noise assessment, with appropriate noise mitigation measures implemented during the construction period, no adverse impact arising from the construction activities is expected. Based on the notional layout and adoption of mitigated measures such as acoustic fins, acoustic balcony/window, the road traffic noise will be minimized and a noise compliance rate of 80% by flat could be achieved. The potential noise impact from the fixed noise sources has also assessed and no adverse noise impact is anticipated with mitigated measures adopted.
- 4.22. Land Contamination appraisal was made for the Scheme area. It is considered that potential land contamination is very low as the site has been occupied mainly for residential purposes for decades and there was no dangerous good license issued for any activity in the Scheme in EPD's records.
- 4.23. In terms of waste management, appropriate sustainable measures/approaches to waste management are proposed to produce less waste and reuse or recover value from waste, no adverse environmental impacts arising from handling, storage, transportation or

disposal of the wastes generated the construction and operation stage of the Scheme are envisaged.

Air Ventilation

4.24. An Air Ventilation Assessment (AVA) has been conducted to assess the ventilation performance of the area surrounding the Scheme (see Appendix 7). A comparison of air ventilation was made between the notional design under the OZP-compliant Scheme (the Baseline Scheme) according to the consultation with Planning Department and the notional design under the draft DSP (the Proposed Scheme). It is concluded that no adverse air ventilation impact is anticipated for the Proposed Scheme as compared to the Baseline Scheme.

Drainage and Sewerage Impact

4.25. A Drainage and Sewerage Impact Assessment (DSIA) was conducted (see Appendix 8). The DSIA report concluded that the impact on the capacities of the existing drainage and sewerage system due to the increase of population from the proposed development will be acceptable. With the provision of new drainage and sewerage pipes and upgrading / diversion of a few sections of existing drainage and sewerage pipes connecting with the proposed development, the discharge generated from the proposed development in the Scheme will be within the capacities and will not have adverse impact to the existing drainage and sewerage systems.

Water Supply Impact

4.26. A Water Supply Impact Assessment (WSIA) was also conducted (see Appendix 9). Findings of WSIA concluded that there would be no adverse impact to the water supply due to the proposed development.

5 PLANNING AND DESIGN MERITS

- 5.1 The Scheme will provide the following planning and environmental benefits:-
 - Provision of about 38,000 sq.m. GIC GFA for re-provisioning of existing Cheung Sha Wan Sports Centre to be upgraded to prevailing standard and for provisioning of new social welfare and health facilities to address community needs. The total floor area of GIC provision of the Scheme will be about 33 times of the existing GIC provision (ie. Cheung Sha Wan Sports Centre at Site A)
 - Re-structuring and rationalising the land uses in the Scheme to optimise the land uses to achieve more planning gains for the community;
 - The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017 which has pressing redevelopment need and contribute to flat supply;
 - Creation of an all-weathered at-grade and elevated pedestrian network with proposed footbridges across Cheung Sha Wan Road and Cheung Wah Street to enhance connectivity for the benefit of a wider area of Sham Shui Po;
 - Provision of no more than 50 underground public car parking spaces and create opportunities for possible pavement widening under URA's separated revitalization initiatives at strategic locations;
 - Possible integration of the new POS at Site B with the existing Sham Shui Po Sports Ground in the south under separated associated revitalization work subject to further co-ordination with LCSD; and
 - Enhancing the townscape, urban design and environment through sensible building layout and design.

6 IMPLEMENTATION OF THE DEVELOPMENT SCHEME

- 6.1. The URA does not own or lease any land within the boundaries of the Scheme, both Sites A and B are currently owned by the government. Close liaison on land matters and construction will be carried out with relevant government departments upon DSP approval.
- 6.2. Supplementary documents detailing the implementation programme for the Scheme is attached in **Appendix 10**. The URA may implement the Scheme in association with one or more parties or implementing the Scheme by itself alone.

URBAN RENEWAL AUTHORITY

September 2021

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PART 2 THE DRAFT PLAN

DRAFT URBAN RENEWAL AUTHORITY CHEUNG WAH STREET / CHEUNG SHA WAN ROAD DEVELOPMENT SCHEME PLAN NO. S/K5/URA3/A

(Being a Draft Plan for the Purposes of the Town Planning Ordinance prepared by the Urban Renewal Authority under section 25 of the Urban Renewal Authority Ordinance)

NOTES

(N.B. These form part of the Plan)

- (1) These Notes show the uses or developments on land falling within the boundaries of the Plan which are always permitted and which may be permitted by the Town Planning Board, with or without conditions, on application. Where permission from the Town Planning Board for a use or development is required, the application for such permission should be made in a prescribed form. The application shall be addressed to the Secretary of the Town Planning Board, from whom the prescribed application form may be obtained.
- (2) Any use or development which is always permitted or may be permitted in accordance with these Notes must also conform to any other relevant legislation, the conditions of the Government lease concerned, and any other Government requirements, as may be applicable.
- (3) (a) No action is required to make the existing use of any land or building conform to this Plan until there is a material change of use or the building is redeveloped.
 - (b) Any material change of use or any other development (except minor alteration and/or modification to the development of the land or building in respect of the existing use which is always permitted) or redevelopment must be always permitted in terms of the Plan or, if permission is required, in accordance with the permission granted by the Town Planning Board.
 - (c) For the purposes of subparagraph (a) above, "existing use of any land or building" means
 - (i) before the publication in the Gazette of the notice of the first statutory plan covering the land or building (hereafter referred as 'the first plan'),

- a use in existence before the publication of the first plan which has continued since it came into existence; or
- a use or a change of use approved under the Buildings Ordinance which relates to an existing building; and
- (ii) after the publication of the first plan,
 - a use permitted under a plan which was effected during the effective period of that plan and has continued since it was effected; or
 - a use or a change of use approved under the Buildings Ordinance which relates to an existing building and permitted under a plan prevailing at the time when the use or change of use was approved.
- (4) Except as otherwise specified by the Town Planning Board, when a use or material change of use is effected or a development or redevelopment is undertaken, as always permitted in terms of the Plan or in accordance with a permission granted by the Town Planning Board, all permissions granted by the Town Planning Board in respect of the site of the use or material change of use or development or redevelopment shall lapse.
- (5) Road widths, road junctions and alignments of roads may be subject to minor adjustments as detailed planning proceeds.
- (6) Temporary uses (expected to be 5 years or less) of any land or building are always permitted as long as they comply with any other relevant legislation, the conditions of the Government lease concerned, and any other Government requirements, and there is no need for these to conform to the zoned use or these Notes. For temporary uses expected to be over 5 years, the uses must conform to the zoned use or these Notes.
- (7) The following uses or developments are always permitted on land falling within the boundaries of the Plan except where the uses or developments are specified in Column 2 of the Schedule of Uses:
 - (a) provision, maintenance or repair of plant nursery, amenity planting, open space, rain shelter, refreshment kiosk, road, bus/public light bus stop or lay-by, cycle track, Mass Transit Railway station entrance, Mass Transit Railway structure below ground level, taxi rank, nullah, public utility pipeline, electricity mast, lamp pole, telephone booth, telecommunications radio base station, automatic teller machine and shrine; and

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- (b) geotechnical works, local public works, road works, sewerage works, drainage works, environmental improvement works, marine related facilities, waterworks (excluding works on service reservoir) and such other public works co-ordinated or implemented by Government;
- (8) Unless otherwise specified, all building, engineering and other operations incidental to and all uses directly related and ancillary to the permitted uses and developments within the same zone are always permitted and no separate permission is required.
- (9) In these Notes, "existing building" means a building, including a structure, which is physically existing and is in compliance with any relevant legislation and the conditions of the Government lease concerned.
- (10) Any development not compatible with the Urban Renewal Authority's Development Scheme for the area is prohibited by virtue of section 25(4) of the Urban Renewal Authority Ordinance.

S/K5/URA3/A

DRAFT URBAN RENEWAL AUTHORITY CHEUNG WAH STREET / CHEUNG SHA WAN ROAD DEVELOPMENT SCHEME PLAN NO. S/K5/URA3/A

Schedule of Uses

	<u>Page</u>
RESIDENTIAL (GROUP A)	1
OPEN SPACE	5
GOVERNMENT. INSTITUTION OR COMMUNITY	6

RESIDENTIAL (GROUPA)

Column 1	Column 2
Uses always permitted	Uses that may be permitted with or without conditions on application to the Town Planning Board Commercial Bathhouse/ Massage Establishment
Ambulance Depot	
Flat	
Government Use (not elsewhere specified)	Eating Place
House	Education Institution
Library	Exhibition or Convention Hall
Market	Government Refuse Collection Point
Place of Recreation, Sports or Culture	Hospital
Public Clinic	Hotel
Public Transport Terminus or Station (excluding open-air terminus or station)	Institutional Use (not elsewhere specified)
Residential Institution Public Vehicle Park (excluding container vehicle)	Mass Transit Railway Vent Shaft and/or Other Structure above Ground Level other than Entrances
School (in free-standing purpose-designed	Office
building only)	Petrol Filling Station
Social Welfare Facility	Place of Entertainment
Utility Installation for Private Project	Private Club
	Public Convenience
	Public Transport Terminus or Station (not elsewhere specified)
	Public Utility Installation
	Religious Institution
	School (not elsewhere specified)
	Shop and Services (not elsewhere specified)
	Training Centre

(Please see next page)

RESIDENTIAL (GROUP A) (Cont'd)

In addition, the following uses are always permitted (a) on the lowest three floors of a building, taken to include basements; or (b) in the purpose-designed non-residential portion of an existing building, both excluding floors containing wholly or mainly car parking, loading / unloading bay and / or plant room:

Eating Place
Educational Institution
Institutional Use (not elsewhere specified)
Off-course Betting Centre
Office
Place of Entertainment
Private Club
Public Convenience
Recyclable Collection Centre
School
Shop and Services
Training Centre

Planning Intention

This zone is intended primarily for high-density residential developments. Commercial uses are always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of an existing building.

Remarks

- (1) No new development, or addition, alteration and/or modification to or redevelopment of an existing building shall result in the plot ratio for the building upon development and/or redevelopment in excess of 7.5 for a domestic building or 9.0 for a building that is partly domestic and partly non-domestic, or the plot ratio of the existing building, whichever is the greater. Except where the plot ratio is permitted to be exceeded under paragraphs (7) and/or (8) hereof, under no circumstances shall the plot ratio for the domestic part of any building, to which this paragraph applies, exceed 7.5.
- (2) For a non-domestic building to be erected on the site, the maximum plot ratio shall not exceed 9.0 except where the plot ratio is permitted to be exceeded under paragraphs (7) and/or (8) hereof.

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- (3) For the purposes of paragraph (1) above, no addition, alteration and/or modification to or redevelopment of an existing building shall result in a total development and/or redevelopment in excess of the relevant maximum domestic and/or non-domestic plot ratio, or the domestic and/or non-domestic plot ratio or the existing building, whichever is the greater, subject to, as applicable
 - (i) the plot ratio of the existing building shall apply only if any addition, alteration and/or modification to or redevelopment of an existing building is for the same type of building as the existing building, i.e. domestic, non-domestic, or partly domestic and partly non-domestic building; or
 - (ii) the maximum domestic and/or non-domestic plot ratio stated in paragraph (1) above shall apply if any addition, alteration and/or modification to or redevelopment of an existing building is not for the same type of building as the existing building, i.e. domestic, nondomestic, or partly domestic and partly non-domestic building.
- (4) In determining the relevant maximum plot ratio/GFA for the purposes of paragraph (1) and (2) above, any floor space that is constructed or intended for use solely as car park, loading/unloading bay, plant room, caretaker's office, or caretaker's quarters and recreational facilities for the use and benefit of all the owners or occupiers of the domestic building or domestic part of the building, provided such uses and facilities are ancillary and directly related to the development or redevelopment, may be disregarded. Any floor space that is constructed or intended for use solely as Government, institution or community facilities, as required by the Government, may also be disregarded.
- (5) An at-grade Public Open Space of not less than 750m² shall be provided.
- (6) The provision of underground public car parking spaces will be exempted from GFA calculation.
- (7) No new development, or addition, alternation and/or modification to or redevelopment of an existing building shall result in a total development and/or redevelopment in excess of the maximum building height in terms of metres above Principal Datum (mPD) as stipulated on the Plan, or the height of the existing building, whichever is the greater.

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- (8) Where the permitted plot ratio as defined in Building (Planning) Regulations is permitted to be exceeded in circumstances as set out in Regulation 22(1) or (2) of the said Regulations, the plot ratio for the building on land to which paragraphs (1) and (2) applies may be increased by the additional plot ratio by which the permitted plot ratio is permitted to be exceeded under and in accordance with the said Regulation 22(1) or (2), notwithstanding that the relevant maximum plot ratio specified in the paragraphs (1) and (2) above may thereby be exceeded.
- (9) Based on the individual merits of a development or redevelopment proposal, minor relaxation of the plot ratio and building height restrictions as stated in paragraphs (1), (2) and (6) above may be considered by the Town Planning Board on application under section 16 of the Town Planning Ordinance.

OPEN SPACE

Column 1	Column 2
Uses always permitted	Uses that may be permitted with or without conditions on application to the Town Planning Board
Aviary	Eating Place
Barbecue Spot	Government Refuse Collection Point
Field Study/Education/Visitor Centre	Government Use (not elsewhere
Park and Garden	specified)
Pavilion	Holiday Camp
Pedestrian Area	Mass Transit Railway Vent Shaft and/or
Picnic Area	Other Structure above Ground
Playground/Playing Field	Level other than Entrances
Public Convenience	Place of Entertainment
Sitting Out Area	Place of Recreation, Sports or Culture
Zoo	Private Club
	Public Transport Terminus or Station
	Public Utility Installation
	Public Vehicle Park(excluding container vehicle)
	Religious Institution
	Service Reservoir
	Shop and Services
	Tent Camping Ground
	Utility Installation for Private Project

Planning Intention

This zone is intended primarily for the provision of outdoor open-air public space for active and/or passive recreational uses serving the needs of local residents as well as the general public.

GOVERNMENT, INSTITUTION OR COMMUNITY

Column 1	Column 2
Uses always permitted	Uses that may be permitted with or without conditions on application to the Town Planning Board
Ambulance Depot	Animal Boarding Establishment
Animal Quarantine Centre (in Government building only)	Animal Quarantine Centre (not elsewhere specified)
Broadcasting, Television and/or Film Studio	Columbarium
Eating Place (Canteen, Cooked Food Centre only)	Correctional Institution Crematorium
Educational Institution	Driving School
Exhibition or Convention Hall	Eating Place (not elsewhere specified)
Field Study/Education/Visitor Centre	Flat
Government Refuse Collection Point	Funeral Facility
Government Use (not elsewhere specified)	Helicopter Fueling Station
Hospital	Helicopter Landing Pad
Institutional Use (not elsewhere specified)	Holiday Camp
Library	Hotel
Market	House
Place of Recreation, Sports or Culture	Mass Transit Railway Vent Shaft and/or
Public Clinic	Other Structure above Ground
Public Convenience	Level other than Entrances
Public Transport Terminus or Station	Off-course Betting Centre
Public Utility Installation	Office
Public Vehicle Park (excluding container	Petrol Filling Station
vehicle)	Place of Entertainment
Recyclable Collection Centre	Private Club
Religious Institution	Radar, Telecommunications Electronic
Research, Design and Development Centre School	Microwave Repeater, Television and/or Radio Transmitter
Service Reservoir	Installation
Social Welfare Facility	Refuse Disposal Installation (Refuse
Training Centre	Transfer Station only)
Wholesale Trade	Residential Institution
	Sewage Treatment/Screening Plant
	Shop and Services (not elsewhere specified)
	Utility Installation for Private Project Zoo

(Please see next page)

Planning Intention

This zone is intended primarily for the provision of Government, institution or community facilities serving the needs of the local residents and/or a wider district, region or the territory. It is also intended to provide land for uses directly related to or in support of the work of the Government, organizations providing social services to meet community needs, and other institutional establishments.

Remarks

- (1) No new development, or addition, alteration and/or modification to or redevelopment of an existing building shall result in a total development and/or redevelopment in excess of the maximum building heights in terms of metres above Principal Datum (mPD) as stipulated on the Plan, or the height of the existing building, whichever is the greater.
- (2) Based on the individual merits of a development or redevelopment proposal, minor relaxation of the building height restrictions stated in paragraph (1) above may be considered by the Town Planning Board on application under section 16 of the Town Planning Ordinance.

DRAFT URBAN RENEWAL AUTHORITY CHEUNG WAH STREET / CHEUNG SHA WAN ROAD DEVELOPMENT SCHEME PLAN NO. S/K5/URA3/A

EXPLANATORY STATEMENT

DRAFT URBAN RENEWAL AUTHORITY

CHEUNG WAH STREET / CHEUNG SHA WAN ROAD

DEVELOPMENT SCHEME PLAN NO. S/K5/URA3/A

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DRAFT URBAN RENEWAL AUTHORITY CHEUNG WAH STREET / CHEUNG SHA WAN ROAD DEVELOPMENT SCHEME PLAN NO. S/K5/URA3/A

(Being a Draft Plan for the Purposes of the Town Planning Ordinance prepared by the Urban Renewal Authority under section 25 of the Urban Renewal Authority Ordinance)

EXPLANATORY STATEMENT

Note: For the purposes of the Town Planning Ordinance (the Ordinance), this statement shall not be deemed to constitute a part of the Plan.

1. <u>INTRODUCTION</u>

This explanatory statement is intended to assist an understanding of the draft Urban Renewal Authority (URA) Cheung Wah Street/ Cheung Sha Wan Road Development Scheme Plan (DSP) No. S/K5/URA3/A. It reflects the planning intention and objectives of the Town Planning Board (the Board) for the area covered by the Plan.

2. <u>AUTHORITY FOR THE PLAN AND PROCEDURES</u>

- 2.1 In the URA's 20th Business Plan (2021/22) which was approved by the Financial Secretary, the Cheung Wah Street/ Cheung Sha Wan Road Development Scheme (SSP-018) was proposed to be processed as a Development Scheme (the Scheme) under section 25 of the URA Ordinance (URAO).
- 2.2 On XX September 2021, pursuant to section 23(1) of the URAO, the URA notified in the Government Gazette the commencement of implementation of the Cheung Wah Street/ Cheung Sha Wan Road Development Scheme.

- 2.3 On the same day of commencement (i.e. 24 September 2021), the URA submitted the draft URA Cheung Wah Street/ Cheung Sha Wan Road DSP to the Board under section 25(5) of the URAO.
- 2.4 On XXXX, the Board, under section 25(6)(a) of the URAO, deemed the draft URA Cheung Wah Street/ Cheung Sha Wan Road DSP as being suitable for publication. Under section 25(7) of the URAO, the draft DSP, which the Board has deemed suitable for publication, is deemed to be a draft plan prepared by the Board for the purposes of the Town Planning Ordinance (the Ordinance).
- On XXXX, the draft Cheung Wah Street/ Cheung Sha Wan Road DSP No. S/K5/URA3/1 (the Plan) was exhibited under section 5 of the Ordinance. By virtue of section 25(9) of the URAO, the Plan has from the date replaced the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37 in respect of the area delineated and described herein.

3. OBJECT OF THE PLAN

The DSP comprises two Sites, with Site A at the north of Cheung Sha Wan Road and Site B at the south of Cheung Sha Wan Road. The Plan illustrates that the Development Scheme Area (the Area) in orange colour is designated as "Residential (Group A)" ("R(A)"), the Area in blue colour is designated as "Government, Institution or Community" ("G/IC"), and the Area in green colour is designated as "Open Space" ("O"). It is planned to be developed by means of the Development Scheme prepared under section 25 of the URAO. Site A of the DSP intends to be primarily for a high-density residential development with commercial uses are always permitted on the lowest three floors of an existing building or in the purpose-designed non-residential portion of a building. Site B of the DSP intends to be primarily for Government, Institution or Community (GIC) uses and Public Open Space.

4. NOTES OF THE PLAN

- 4.1 Attached to the Plan is a set of Notes which shows the types of uses or developments which are always permitted within the Area in this zone and which may be permitted by the Board, with or without conditions, on application. The provision for application for planning permission under section 16 of the Ordinance allows greater flexibility in land use planning and control of development to meet changing needs.
- 4.2 For the guidance of the general public, a set of definitions that explains some of the terms used in the Notes may be obtained from the Technical Services Division of the Planning Department and can be downloaded from the Board's website at http://www.info.gov.hk/tpb.

5. AREA COVERED BY THE PLAN

- 5.1 The Development Scheme boundary which is shown in heavy broken line on the Plan. Site A is bounded by Hing Wah Street on the southeastern boundary, Cheung Sha Wan Road on the southwestern boundary, Cheung Wah Street on the northwestern boundary, and Cheung Sha Wan Catholic Secondary School on the northeastern boundary, with a gross site area of about 5,197 m². Site B of the Scheme is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the southeastern boundary, with a gross site area of about 13,857 m².
- On the Approved Cheung Sha Wan OZP No. S/K5/37, Site A is zoned "Government, Institution or Community (G/IC)" and "Open Space (O)", while Site B is currently zoned for "Government, Institution or Community (G/IC)", "Open Space (O)", and an area shown as 'Road' before the exhibition of the Plan.

6. EXISTING CONDITIONS

6.1 Site A of the Area is currently occupied by the Cheung Sha Wan Sports Centre and a garden both owned and managed by Leisure and Cultural Services Department (LCSD). The sports centre was built in 1976 of which the design and facilities are below current standard. Site B involves the Cheung Sha Wan Path Sitting-out Area and part of Sham Shui Po Sports Ground owned and managed by LCSD and a temporary maintenance depot occupied by Highways Department.

7. PLANNING AND LAND USE PROPOSALS

7.1 On the Plan, Site A of the Area is zoned "R(A)" and Site B of the Area is zoned "G/IC" and "O". The Notes of the Plan indicated broadly the intended land uses within the Area.

Uses

- 7.2 The "R(A)" zone is intended primarily for a high-density residential development. Commercial uses are always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of an existing building.
- 7.3 The maximum plot ratio within the "R(A)" zone is 9.0, or the plot ratio of the existing building(s), whichever is the greater. Except where the plot ratio is permitted to be exceeded under the Notes of the Plan or under Building (Planning) Regulations 22(1) or (2), under no circumstances shall the plot ratio for the domestic part of any development exceed 7.5. The "R(A)" zone is also subject to a maximum building height of 140 metres above Principal Datum (mPD).
- 7.4 The "G/IC" zone is intended primarily for the provision of GIC facilities serving the needs of the local residents and/or a wider district, region or the territory. It is also intended to provide land for uses directly related to or in support of the work of the Government, organizations providing social services to meet community needs, and other institutional establishments. The "G/IC" zone is subject to a maximum building height of 95 mPD.

- 7.5 The "O" zone is intended primarily for the provision of outdoor openair public space for active and/or passive recreational uses serving the needs of local residents as well as the general public.
- 7.6 To provide design flexibility, minor relaxation of the plot ratio and building height restrictions may be considered by the Board on application under section 16 of the Ordinance taking into account its individual planning and design merits.

Government, Institution or Community (GIC) Facilities

7.7 Subject to confirmation of operational needs and detailed design, about 38,700 m² non-domestic GFA would be proposed for GIC uses at the Scheme Area, with about 5,100 m² within the non-domestic portion of Site A and about 33,600 m² non-domestic GFA at Site B. The existing Cheung Sha Wan Sports Centre at Site A which was built in 1976 will be reprovisioned at Site B up to prevailing standard and continue its operation for public enjoyment. The intended use of new GIC provision would be subject to further liaison with relevant Government departments as well as views from local stakeholders. In determining the relevant maximum plot ratio of the development and/or redevelopment in Site A, any floor space that is constructed or intended for use solely as GIC facilities, as required by the Government, may be disregarded.

Public Open Space

7.8 Subject to detailed design, a POS of not less than 9,645 m² is proposed at Site B and a POS of not less than 750 m² is proposed at Site A along Cheung Sha Wan Road. According to the consultation with LCSD, LCSD agreed to take up the management and maintenance of the proposed POS at Site B. LCSD proposed the POS at Site A under planning to be under ownership and management of URA or its future joint-venture partner(s), or its assignee, subject to further liaison with relevant Government departments. The proposed POS at Site A will be open to public during reasonable hours.

Provision of all-weathered at-grade and elevated pedestrian network

- 7.9 Subject to Roads (Works, Use and Compensation) Ordinance, footbridges across Cheung Sha Wan Road and Cheung Wah Street are proposed to connect up the POSs at the Scheme and an adjoining URA Development Project (Kim Shin Lane / Fuk Wa Street (SSP-017)). The resultant at grade and elevated pedestrian network will not only integrate various GIC facilities and POSs, but will also enhance connectivity of a wider built environment of Sham Shui Po. Proper paving and landscaping, where appropriate, will be provided at the pedestrian walkways to create a safe and pleasant walking environment. Given the proposed footbridges are outside the DSP boundary and do not form part of the DSP, the URA will liaise with relevant Government departments on the proposal via a separate revitalisation initiatives subject to the approval of DSP and detailed technical feasibility.
- 7.10 To further enhance the pedestrian circulation and pavement environment, appropriate podium setbacks of the proposed development along Cheung Sha Wan Road, Cheung Wah Street, and Hing Wah Street, where appropriate, would be explored in the Area. There is also a possible integration of the new POS with the existing Sham Shui Po Sports Ground in the south subject to further co-ordination with LCSD on the associated revitalization work.

Underground Public Vehicle Park

7.11 For public benefits, no more than 50 underground public car parking spaces will be provided in a basement car park at Site A according to consultation with Transport Department. Such provision will create opportunity for the replacement of some on-street parking spaces in the area. It will make way for possible pavement widening under separate revitalization initiatives at strategic locations. The provision of underground public car parking spaces will be exempted from GFA calculation according Joint Practice Note No. 4.

Internal Transport Facilities

7.12 Ancillary car parking spaces and loading/unloading bays will be provided in a basement car park at Site A to serve the proposed residential development with non-domestic podium in the Development Scheme. To serve the proposed GIC facilities at Site B, loading/unloading bays and ancillary car parking spaces will be provided on the ground floor and at basement levels, respectively, of the proposed GIC complex. The number of car parking spaces, loading/unloading bays will be based on the relevant requirements under the current Hong Kong Planning Standards and Guidelines (HKPSG) and subject to agreement with Transport Department.

Air Ventilation

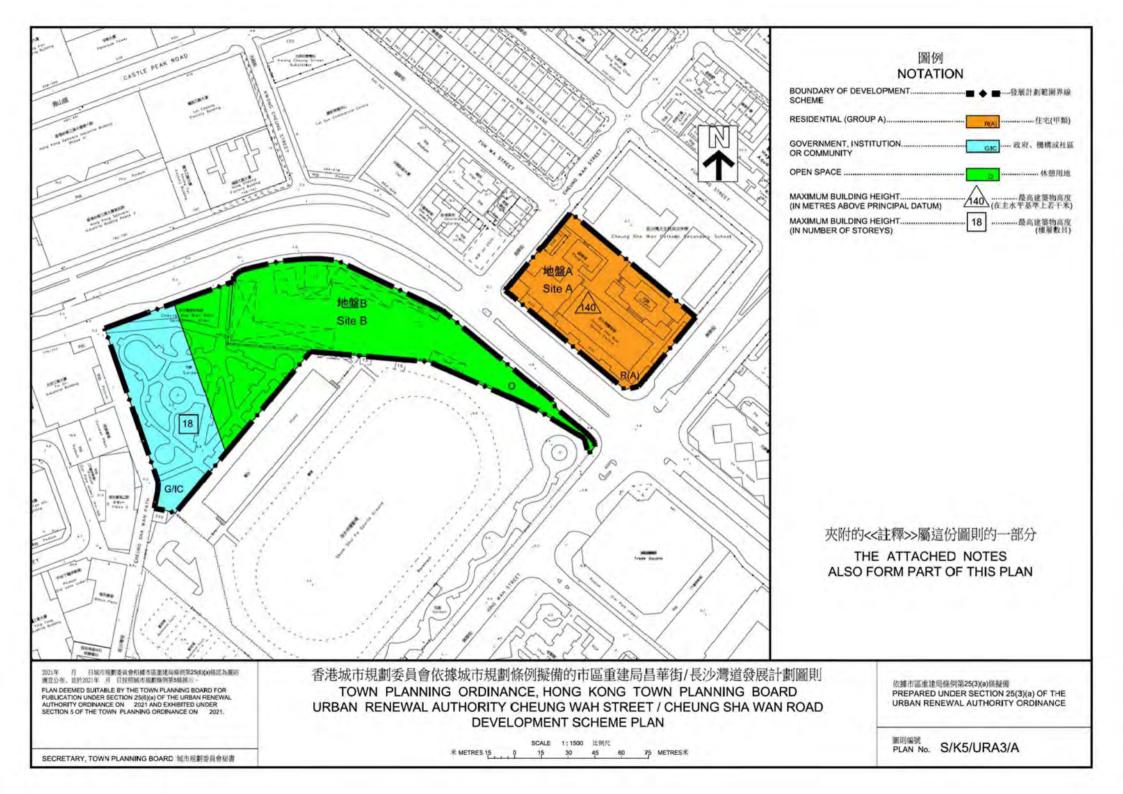
7.13 As identified in the air ventilation assessment report, Cheung Wah Street and Fuk Wing Street could be better benefited by the north-south direction wind breezeway with "Good Design Features" (i.e. ground floor setbacks along Cheung Sha Wan Road, Cheung Wah Street and Hing Wah Street and residential towers separation at Site A) in the proposed development. The proposed development will also meet the requirements under Sustainable Building Design Guidelines (SBDG).

8. IMPLEMENTATION OF THE DEVELOPMENT SCHEME

- 8.1 The proposals set out in the Plan form an integral part of the Development Scheme for the Area.
- 8.2 The URA does not own or lease any land within the boundaries of the Scheme; both Sites A and B are currently owned by the Government. Close liaison on land matters and construction will be carried out with relevant Government departments upon DSP approval. The proposed GIC facilities within the Area and POS at Site B will be handed over to Government for future ownership, management and maintenance, subject to liaison with relevant Government departments.

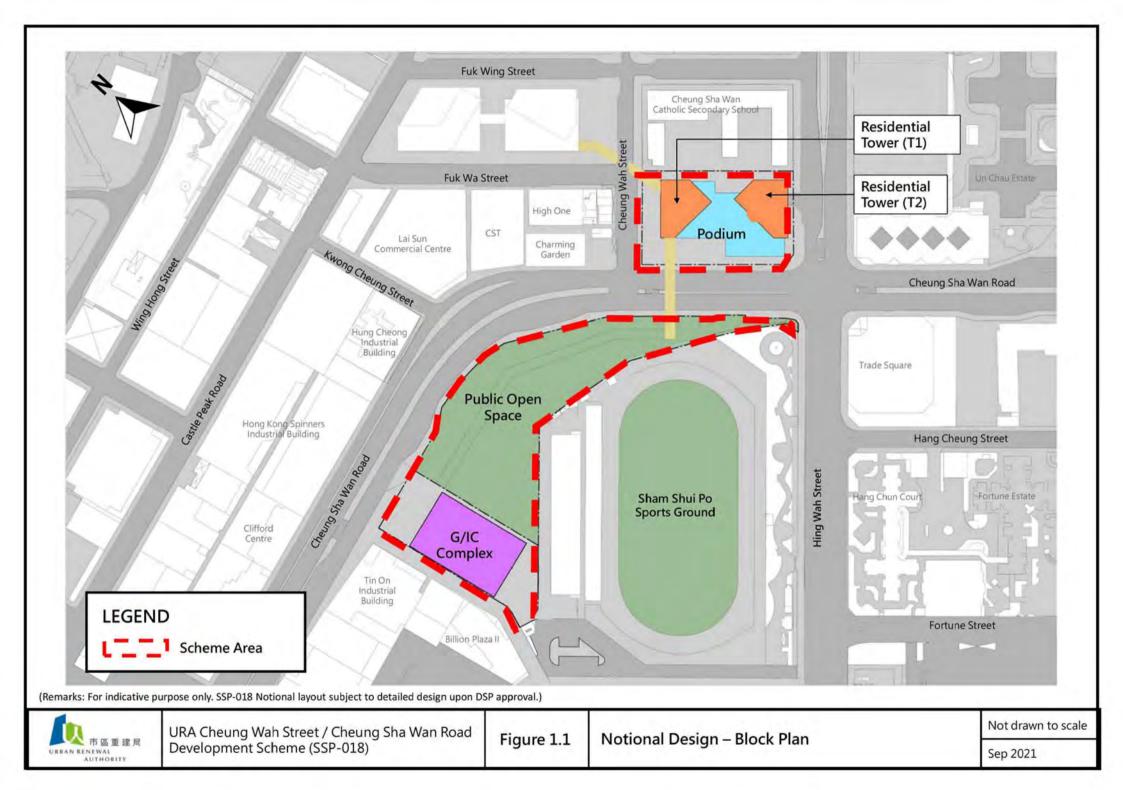
8.3 The URA may implement the Development Scheme on its own or in association with one or more partners.

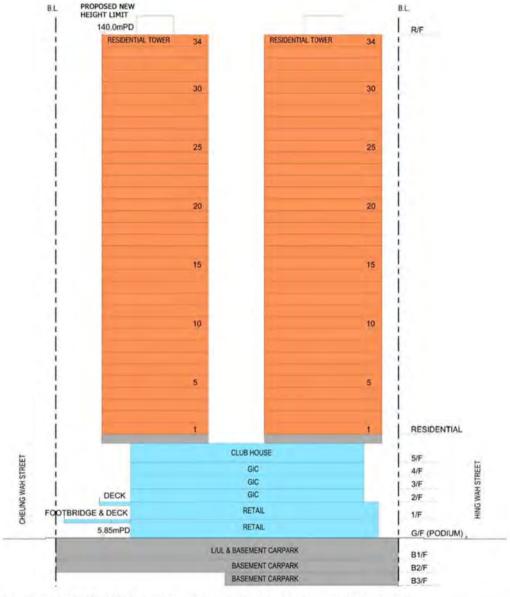
TOWN PLANNING BOARD September 2021

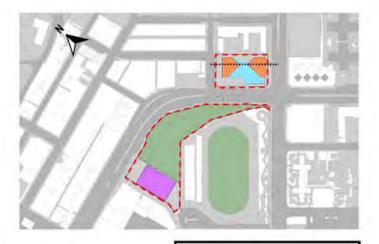


PART 3 SUPPLEMENTARY INFORMATION

Appendix 1
Preliminary Design







LEGEND
The Scheme

(Remarks: For indicative purpose only. SSP-018 Notional layout subject to detailed design upon DSP approval.)



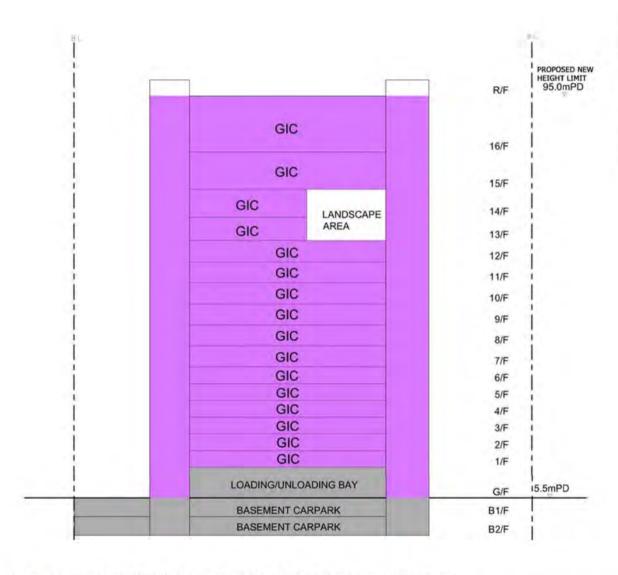
URA Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018)

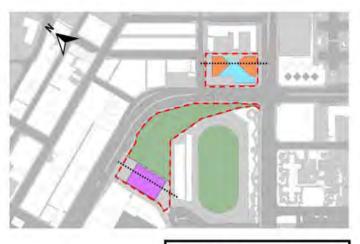
Figure 1.2

Notional Design – Schematic Section at Site A

Not drawn to scale

Sep 2021





LEGEND
The Scheme

(Remarks: For indicative purpose only. SSP-018 Notional layout subject to detailed design upon DSP approval.)



URA Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018)

Figure 1.3

Notional Design – Schematic Section at Site B

Not drawn to scale

Sep 2021

Appendix 2

Preliminary Landscape Design and Tree Survey Report

Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018)

Preliminary Landscape Design and Tree Preservation Proposal

24th September 2021

Prepared By:

SCENIC Landscape Studio Limited



Project Title	Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018)
Report Title	Preliminary Landscape Design and Tree Preservation Proposal

Revision	Date	Complied by:	Checked by:	Approved by:	Description
-	20210802	Various	Fiona Yu	Chris Foot	Draft to Client
Α	20210805	Various	Fiona Yu	Chris Foot	Draft to Client
В	20210827	Various	Fiona Yu	Chris Foot	Draft to Client
С	20210920	Various	Fiona Yu	Chris Foot	Draft to Client
D	20210924	Various	Fiona Yu	Chris Foot	Final to Client

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1.0 Introduction

- The Urban Renewal Authority (URA) has proposed Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). SCENIC Landscape Studio Limited have been commissioned to prepare the Tree Preservation Proposal for a development scheme ("the Proposed Development") at Sham Shui Po ("the Application Site"). The Application Site comprises of site A and B, which fall within areas zoned Open Space (O), Government, Institution or Community (G/IC) and Road on the Approved Cheung Sha Wan (KPA 5) Outline Zoning Plan ("OZP") No. 5/K5/37.
- 1.2 The Tree Preservation Proposal outlines the approach and findings of the tree survey and describes the type, number and condition of the existing trees found within the site. The proposal also identifies the trees found to be in conflict with the Proposed Development and makes recommendations for their proposed treatment and provides an indication of the number of new trees required to compensate for the loss of existing trees.
- 1.3 This tree preservation proposal has been prepared in broad accordance in broad accordance with DEVB TC(W) No. 4/2020 "Tree Preservation" and DEVB TC(W) No. 2/2020 'Tree Preservation and Tree Removal Application for Building Development in Private Projects'. The survey approach is presented as Annex I – Tree Survey Methodology.
- 1.4 The tree survey was undertaken in June 2021.

2.0 Existing Site Description

2.1 The Application Site (site A and site B) covers a total land area of 19,054m². Site A is a sitting out area southwest to Cheung Sha Wan Catholic Secondary School and is bounded by Cheung Sha Wan Street, Cheung Sha Wan Road and Hing Wah Street. Site B, situated opposite to site A along Cheung Sha Wan Road and at northwest to Sham Shui Po Sports Ground, consists of Cheung Sha Wan Path Sitting Out Area at the west and a temporary work site of HyD at the east. Tree and shrub plantings are found throughout site A, Cheung Sha Wan Path Sitting Out Area and along the edge of the temporary work site of site B.

3.0 Project Description

- 3.1 The Proposed Scheme in site A consists of a commercial and G/IC complex building with 2 residential towers with maximum building height of 134.95m. The proposed development provides 838 nos. of household units. Vehicular access will be located at eastern corner of the site where it meets Hing Wah Street.
- 3.2 A G/IC building not exceeding a building height of 90.5m is proposed at the western part of site B. Vehicular access will be located at northern and southern ends of the G/IC building to provide connections between Cheung Sha Wan Road and Sham Shui Po Sports Ground.
- 3.3 The Proposed Scheme will be landscaped to provide quality public open space for enjoyment and a landscape buffer along the periphery of the development to form an effective screen between the proposed development and the traffic. Footbridge connection between site A and site B across Cheung Sha Wan Road will be provided to enhance accessibility.

4.0 Existing Vegetation

- 4.1 A total of 294 nos. trees were identified within the Application Site boundary and immediately adjacent to it. As shown on **Annex II Tree Location Plan** the tree growth is found within a series of areas both within and at the periphery of the Application Site Boundary.
- 4.2 The existing tree locations are illustrated on **Annex II Tree Location Plan** and **Annex III Tree Survey Schedule** provides an identification of numbers of tree species, an assessment of their condition and recommendations for the treatment of the trees and **Annex IV** Tree Photographic Record provides a visual reference for the assessments.
- 4.3 **Table 4.1** below lists the tree species surveyed and their relative abundance and describes their conservation value (native or exotic).

Table 4.1 Existing Tree Species Summary

Botanical Name	Chinese Name	Overall No. of Trees within Survey Area	Native (N) Exotic (E)	Conservation Status in Hong Kong
Acacia confusa	台灣相思	3	E	Common
Ailanthus fordii	常綠臭椿	9	N	Common
Albizia lebbeck	大葉合歡	1	E	Common
Aleurites moluccana	石栗	73	E	Common
Araucaria heterophylla	異葉南洋杉	1	E	Common
Bauhinia variegata	宮粉羊蹄甲	1	E	Common
Bauhinia x blakeana	洋紫荊	1	N	Common
Bombax ceiba	木棉	7	E	Common
Callistemon viminalis	串錢柳	7	E	Common
Caryota mitis	短穗魚尾葵	2	E	Common
Caryota ochlandra	魚尾葵	3	E	Common
Celtis sinensis	朴樹	5	E	Common
Choerospondias axillaris	南酸棗	1	N	Common
Corymbia torelliana	毛葉桉	12	E	Common
Dypsis lutescens	散尾葵	1	E	Common
Elaeocarpus obtusus subsp. Apiculatus	長芒杜英	1	E	Common
Ficus benjamina	垂葉榕	20	E	Common
Ficus elastica	印度橡樹	2	E	Common
Ficus microcarpa	細葉榕	3	N	Common
Ficus virens	大葉榕	1	N	Common
Garcinia subelliptica	菲島福木	1	E	Common
Grevillea robusta	銀樺	2	E	Common
Jacaranda mimosifolia	藍花楹	1	E	Common
Juniperus chinensis `Kaizuca`	龍柏	11	E	Common
Lagerstroemia speciosa	大花紫薇	15	E	Common
Leucaena leucocephala	銀合歡	1	E	Common

Botanical Name	Chinese Name	Overall No. of Trees within Survey Area	Native (N) Exotic (E)	Conservation Status in Hong Kong
Litsea glutinosa	潺槁樹	1	N	Common
Livistona chinensis	蒲葵	14	E	Common
Macaranga tanarius var. tomentosa	血桐	12	N	Common
Melaleuca quinquenervia	白千層	5	E	Common
Melia azedarach	苦楝	18	E	Common
Michelia x alba	白蘭	1	E	Common
Morus alba	桑	2	N	Common
Murraya paniculata	九里香	1	E	Common
Phoenix roebelenii	日本葵	14	E	Common
Podocarpus macrophyllus	羅漢松	5	N	Common
Ravenala madagascariensis	旅人蕉	14	E	Common
Roystonea regia	大王椰子 (王棕)	9	E	Common
Senna siamea	鐵刀木	6	E	Common
Spathodea campanulata	火焰木	1	E	Common
Sterculia lanceolata	假蘋婆	1	N	Common
Syzygium jambos	蒲桃	3	E	Common
Terminalia catappa	欖仁樹	1	E	Common
Terminalia mantaly	小葉欖仁	1	E	Common
Dead trees		0		
Total		294		

- 4.4 The most numerous of the existing trees are Aleurites moluccana (73 nos.), Ficus benjamina (20 nos.) and Melia azedarach (18 nos.). Most of these trees exist along application boundary of site A, site B and at the periphery of Cheung Sha Wan Path Sitting-Out Area of Site B. Other species include Corymbia torelliana, Lagerstroemia speciosa, Livistona chinensis and Phoenix roebelenii etc. Other species identified are generally present in quantities of less than 10 nos. with no trees found dead within of the Application Site Boundary. The photographs in **Annex IV** clearly shows the condition of the surveyed existing trees.
- 4.5 The average trunk diameter at breast height (DBH) is 0.35m. The average tree height is 8.16m and the average crown spread is 4.16m.
- 4.6 A high percentage of trees exhibit a fair existing form and condition. This assessment and photographic record show that many of the trees are growing in close proximity to one another or structures resulting in leaning main stem and asymmetrical canopies. The table also shows a high percentage of trees surveyed have fair amenity value. This includes a large proportion of the trees which have a spindly, contorted and often leaning form with asymmetrical canopy growth due to their close proximity to one another and the competition for light. Annex III Tree Survey Schedule provides further information of the form and condition of individual trees, indicating the range of characteristics observed.
- 4.7 Nine nos. specimen of *Ailanthus fordii* were identified by the survey. This species is protected under Forestry Regulations (Cap. 96. sub. leg.) It is also listed as "Near Threatened" in Rare and Precious Plants of Hong Kong (Status in China). However these specimens have been planted as part of the development of the existing open space rather than being naturally growing specimens; and so therefore not considered to be protected.

- A number of specimens (15 nos) of Lagerstroemia speciosa were identified as part of the survey. Lagerstroemia speciosa are generally protected in Hong Kong under the Forestry Regulations (Cap. 96. sub. leg.) except for "plants grown outside Hong Kong or on any land held from the Government under a lease, licence or permit or by virtue of an Ordinance". Since all the recorded Lagerstroemia speciosa were found within landscaped areas it is likely that they have been planted as ornamental shrubs and therefore not protected under Cap. 96 and not considered as a floral species of conservation interest for this Project (Hong Kong Herbarium and South China Botanical Garden eds., 2007)
- 4.9 There are no trees within the Application Site registered as Old and Valuable Trees (DEVB TC(W) No. 5/2020 Registration of Old and Valuable Trees (OVT), and Guidelines for their Preservation). Two trees T143 and T203 are mature specimens with good value.

5.0 Recommendations

- 5.1 Of the 294 nos trees surveyed some 146 nos trees are recommended for retention in-situ/ transplantation. The proposed tree protection measures are indicated in Annex VII - Tree Protection Measures.
- 5.2 Approximately 31 nos trees are recommended for transplantation and a further 117 nos. for transplantation / felling as they are conflict with the proposed notional design of the Scheme. The locations of the trees to be transplanted / felled are shown in Annex V Tree Recommendation Plan.
- 5.3 The feasibility of transplanting the affected trees has been reviewed. The affected trees will be transplanted as far as practicable subject to the agreement of relevant government departments. The permanent receptor sites for the transplanted trees shall be located, as far as possible, within the Application Site. If this is not possible offsite receptor sites shall be identified preferably within the same area so that the trees will continue to contribute to the landscape and visual amenity of the locale. If transplanting is found to be not feasible / appropriate at the detailed design stage, tree felling will be proposed and the loss of trees shall be compensated. Table 5.1 provides a summary of the recommendations for the treatment of the existing trees.

Table 5.1 Summary of Tree Recommendations

Recommendation	Approximate Number of Trees	% Trees
Trees to be retained / transplanted	146	50%
Trees to be transplanted	31	10%
Trees to be transplanted / felled	117	40%
Total number of trees	294	

Note: The preliminary tree treatment proposal is not deemed to be final, subject to detailed design and government's agreement.

5.4 The recommendations for tree retention and felling are provided in **Annex III - Tree Survey Schedule** and their proposed status recorded on photographic Records of Existing Trees are presented as **Annex IV**. Their proposed status recorded on plans is presented on **Annex V - Tree Recommendation Plan**.

6.0 Preliminary New Tree Planting Proposal

- 6.1 The new tree planting proposals will be based on a compensatory ratio of 1:1 in number. These will be in compensation for the felled trees in the existing Cheung Sha Wan Road Sitting-out Area and Sham Shui Po Sports Ground. The new tree planting will utilise heavy standard trees (min 75mm DBH) with an approximate spacing of 5000 mm and will be planted within new residential Sites A and B and the new extension to the Sham Shui Po Sports Ground.
- 6.2 A summary of the preliminary new tree planting proposals is provided in **Table 6.2** below and shown in Annex VI New Tree Planting Plan.

Table 6.2: Preliminary New Tree Planting Proposals

Botanical Name	Chinese Name	Native / Exotic	Tree Size
Tree Species			
Adenanthera microsperma	海紅豆	N	Heavy Standard
Ailanthus fordii	常綠臭椿	N	Heavy Standard
Bauhinia purpurea	紅花羊蹄甲	E	Heavy Standard
Bischofia javanica	秋楓	N	Heavy Standard
Bixa orellana	紅木	E	Heavy Standard
Libidibia ferrea	巴西鐵木	E	Heavy Standard
Chukrasia tabularis	麻楝	E	Heavy Standard
Cinnamomum camphora	樟	N	Heavy Standard
Cleistocalyx nervosum	水翁	N	Heavy Standard
Ehretia longiflora	長花厚殼樹	N	Heavy Standard
Elaeocarpus japonicus	日本杜英	N	Heavy Standard
Ficus subpisocarpa	筆管榕	N	Heavy Standard
Ficus virens	大葉榕	N	Heavy Standard
Garcinia subelliptica	菲島福木	E	Heavy Standard
llex rotunda var. microcarpa	小果鐵冬青	N	Heavy Standard
Jacaranda mimosifolia	藍花楹	E	Heavy Standard
Juniperus chinensis 'Kaizuka'	龍柏	E	Heavy Standard
Koelreuteria bipinnata	複羽葉樂樹	E	Heavy Standard
Liquidambar formosana	楓香	N	Heavy Standard
Machilus breviflora	短序潤楠	N	Heavy Standard
Plumeria rubra	雞蛋花	E	Heavy Standard
Polyspora axillaris	大頭茶	N	Heavy Standard
Pongamia pinnata	水黃皮	N	Heavy Standard
Pterocarpus indicus	紫檀	E	Heavy Standard
Radermachera hainanensis	海南菜豆樹	E	Heavy Standard
Tabebuia chrysantha	黃鐘木	E	Heavy Standard
Terminalia mantaly	小葉欖仁	E	Heavy Standard
Xanthostemon chrysanthus	金蒲桃	E	Heavy Standard

Note: The species selection above is based on the Greening Master Plan for the Sham Shui Po District. The final selection will evolve during the detailed design stage of the project and is subject to the agreement of relevant government departments.

7.0 Relevant Recognised Standards for Tree Preservation and Protection

- 7.1 The tree preservation, protection and transplanting proposals will be undertaken in accordance with the following:
 - BS 3998: 2010 Recommendations for Tree Work;
 - BS 4043: 1989 Recommendations for transplanting root-balled trees;
 - BS 4428 1989 Code of practice for general landscape operations (excluding hard surfaces);
 - BS 5837: 2012 Trees in relation to Construction;
 - ArchSD General Specification, Section 25 (2017 edition); and
 - Handbook on Tree Management prepared by the Greening, Landscape and Tree Management Section of Development Bureau (http://www.greening.gov.hk/en/tree care/Handbook on Tree Management.html)

8.0 Conclusion

- 8.1 The Application Site contains some 294 nos, specimens, largely comprising of common tree species with a small number of common native species.
- 8.2 Some specimens of Ailanthus fordii and Lagerstroemia speciosa were identified and whilst these species are normally protected under Cap. 96 both were planted as part of the development of the existing open space rather than being naturally growing specimens and are therefore not protected.
- 8.3 There are no trees within the Application Site registered as Old and Valuable Trees (DEVB TC (W) No. 5/2020 Registration of Old and Valuable Trees (OVT), and Guidelines for their Preservation). Two trees T143 and T203 are mature specimens with good value.
- 8.4 Based on the proposed notional architectural layout, approximately 146 nos. of trees are recommended for retention in-situ/ transplantation, 31 nos. of tree are recommended for transplantation and a further 117 nos. for transplantation / felling.
- 8.5 Should any of the trees be felled the new tree planting proposals will be based on a compensatory ratio of 1:1 in number, using heavy standard trees (min 75mm DBH) Both the new (compensatory) trees and transplanted trees shall be planted within residential Sites A and B and the new extension to the Sham Shui Po Sports Ground as far as practicable. As a whole, the proposed tree preservation and removal proposal shall meet the minimum requirements for compensatory planting as stipulated in DEVB TC(W) No. 5/2020.

Annexes

Annex I

Tree Survey Methodology

Tree Survey Methodology

1.0 Tree Survey

1.1 Definitions

- 1.1.1 Scope of Survey: To survey all 'trees' within the Application Site Boundary and the intermediate adjacent area where trees are possibly be affected by proposed road widening works.
- 1.1.2 Tree: A woody plant with a stem diameter over 95mm measured at a point 1300mm above the root collar (DBH),
- 1.1.3 DBH: Diameter at Breast Height as defined in the Practice Note Issue No. 2/2006 issued by AFCD.

1.2 Site Survey

1.2.1 The tree locations were recorded by visual assessment and subject to verification by topographic surveyor. Measurements of tree size (DBH, Height and Crown Spread) were primarily measured by Tree Surveyor. Photographs to show the whole tree, tree trunk, tree base are taken for each tree during the tree assessment survey. Topographic plans are attached in Annex VI for reference.

1.3 Basic Tree Information in Tree Survey Schedule

- 1.3.1 The tree survey schedule includes the following information for each tree or group of trees surveyed:
- 1.3.2 Tree Number Each tree is allocated a tree number and clearly marked on site with an identity label showing the tree number and its position plotted on topographic Tree Location Plan(s) (Annex III). The numbering is to follow a logical sequence in numerical order say from north to south.
- 1.3.3 Species Name (Botanical Name) All trees are identified by species, or in some cases by genus if full identification is not possible. Species names currently adopted by AFCD take precedence over other scientific publications.
- 1.3.4 Jurisdiction Authority providing expert advice in vetting of Tree Removal Application for particular trees.
- 1.3.5 Tree Dimensions The following dimensions are to be recorded for each tree:
 - · Overall Height (in metres);
 - . Trunk DBH (in metres / millimetres; refer to schedule);
 - Overall Crown Spread (in metres);
 - . Height at the base of the tree: In metres above principal datum (mPD); and
 - Location: On a slope or flat ground
- 1.3.6 Measurements of tree dimension and location are recorded by topographical surveyor

1.4 Photographic Record

1.4.1 Photographs to show the whole tree, tree trunk, tree base are taken for each tree during the tree assessment survey. Four photographs per A4 sheet.

1.5 Tree Health and Condition

1.5.1 Factors considered include both functional health and structural stability, which is evaluated with reference to the following criteria:

Foliage Condition

- Insect and fungal infections. Colour and small size indicating possible damage to roots;
- Crown density and foliage colour in consideration of normal species performance, seasonal and climatic effect;
- Evidence of insect, bacterial or fungal infections;
- Mechanical damage (e.g. typhoons, insect consumption and vandalism).

Branch Condition

- Poor shoot growth and die-back in the crown are often symptoms of root problems caused by a change in the water table level or soil compaction resulting from site development work.
- · Dead or crossing branches.
- Heavy horizontal branches [which] may make the tree unstable" (Ref. R.Webb).
- The presence of broken damaged or cut branches to be noted as a possible site for infections, calluses may protect the wounds.
- Damaged branches which make the tree unbalanced or unstable;
- Location of decay and/or voids in the branches.
- Whether the tree is "an edge tree exposed as a result of the removal of adjacent trees [which]
 often has an unbalanced crown and may be hazardous" (Ref R.Webb).

Trunk Condition

- Tightly forked trunks which may be a source of weakness in the tree and in high winds can be torn apart.
- Inspect for "cavities or internal rot [which] can be revealed by discoloured bark, moisture seeping through the bark or bracket fungi" (Ref R.Webb).
- Co-dominant stems with included bark.
- · Open cavities, cracks and bark damage.

Root Condition

- Damaged surficial roots.
- · Ground heave evident in cracks in the soil around root zone.
- Branch die-back.

Miscellaneous

- Occurrence of aggressive climbers or parasitic plants.
- Asymmetrical crowns and leaning due to intense competition between adjacent trees.
- · Tangled branches or roots.
- · Adjacency of underground structures.
- 1.5.2 Ratings for tree health and condition:

Definition

- G Trees with a low incidence of less serious defects are graded as good;
- F Trees with a higher incidence of less serious defects are graded as fair;
- P Trees with more serious defects are graded as poor; or
 - D Trees that are dead or irretrievably unhealthy are graded as dead.

1.6 Tree Form

1.6.1 Assessment of tree form following inspections are classified as follows with reference to the overall tree size, shape and any special features:

G	Good - trees with well-balanced form, upright, evenly branching, well-formed head and generally in accordance with the standard form for its species
F	Fair - Trees with less balanced crowns which are mildly distorted due to competition with neighbouring trees or structures, or which have suffered minor damage or which have leaning trunks for example are graded as average
P	Poor - trees with very unbalanced form, distorted crowns, severely leaning, suffering loss of major branches with general damage; unstable and growing close to adjacent trees.

1.6.2 Terms used to describe tree form:

- Forked: a tree with a division in the main stem or having major branches that divide near ground level.
- Topped: a tree that has had its main trunk severed drastically reducing and distorting its crown development.
- · Multi-stem: a tree with more than one main stem or trunk

1.7 Tree Condition

1.7.1 Assessment of tree health and condition involves inspections for the above features and classification as follows:

G	Good - trees with a low incidence of the less serious features listed above and a high chance of a fast recovery from such features.
F	Fair - trees with a higher incidence of the less serious features and a medium chance of recovery.
P	Poor - trees with more serious health features and with a low chance of recovery, even with remedial measures.
D	Dead - no signs of life or irretrievably unhealthy

1.8 Amenity Value

1.8.1 Amenity value is graded as "Excellent", "Good", "Fair" or "Poor". The grading indicates the following qualities in trees or groups of trees:

Excellent	Important trees where species may be of fung shui significance
	which should be retained by adjusting the design layout accordingly

Good	Common species and good health, good condition and good form.
Fair	Common species and average health, average condition and average form.
Poor	Common species and little or no functional or visual value and poor health, poor condition and poor form.

1.9 Structural Condition

1.9.1 Assessment of tree structural condition involves inspections for the overall tree structural system features and classification as follows:

G	Good - trees with good structural system and robust form with low risk of structural failure.
F	Fair - trees with overall robust structure despite some minor structural problems and risk of structural failure is medium.
P	Poor - trees with more serious structural problem and with high risk of structural failure.

1.10 Suitability for Transplanting

1.10.1 This assessment is based on the health of the tree and the practicalities of transplantation. Some species are much more tolerant of the stress of transplantation than others. The assessment of the survival rate of a species after transplantation is based on the observed performance of that species in previous transplantation programmes. Species with insufficient transplantation data are assumed to have a low survival rate. Grading are given as follows:

High - very likely to survive transplantation;

Medium - likely to survive transplantation;

Low - unlikely to survive due to poor health/species/form or difficult to transplant.

1.11 Conservation Status

1.11.1 Assessment of conservation status indicates rarity and protection status under relevant ordinances of a species in Hong Kong. References such as Rare and Precious Plants of Hong Kong, the IUCN Red List of Threatened Species and the Forests and Countryside Ordinance (Cap. 96) may be used.). The categories include very common, common, rare, rare and protected.

1.12 Remarks

1.12.1 Notes will be made about the condition of the tree including any defects, whether it is leaning or not, asymmetrical canopies, the presence of cavities, tree form issues such as forked main stem, included bark, decay, growth of sprouts; and/or growth of climbers. The schedule shall also record any trees with high conservation values such as rare or protected species, old and valuable trees etc.

2.0 Effects of the Development on Existing Trees

2.1 Treatment of Trees

2.1.1 First priority to retain trees and then if this is not possible transplant trees to new location. Trees in direct conflict with proposals which are necessary to be felled shall be confirmed on site by the Architect's / Engineer's Representative. Existing trees to be retained will be protected during construction.

2.2 Assessment

2.2.1 The assessment leading to the recommendation for the treatment of the tree is based on the following:

Retain

- 2.2.2 The preferred option for all trees is to be retained in-situ unless they pose a threat to the public or the trees are nuisance species (e.g. Leucaena leucocephala). In case a tree group processes significant value in the landscape or to the ecosystem, it should be retained as a whole even when the individual components are not outstanding aesthetically.
- 2.2.3 The feasibility of retaining trees has been considered with regard to the following:
 - · Potential damage to trees as a result of proximity to the works.
 - Changes to ground level on a macro scale which affects the ground water table and may cause severe stress.
 - Special constructions to maintain the existing ground level are also considered.
 - · Conflict between tree roots and the proposed works.

Transplant

Statutory Guidelines

- 2.2.4 The recommendation of Transplanting makes reference to paragraph 7[b] of the DEVB TC(W) No.4/2020 which states '...transplant the affected tree(s) to other permanent locations within the project site or the maintenance area to minimise the loss of vegetation in the local environs'. This should be considered as far as possible unless the trees affected are of low conservation and amenity value, or have a low chance of surviving or recovering to its normal form after transplanting'.
- 2.2.5 In situations where it is impossible to retain trees then transplanting them is the first consideration. The criteria upon which the assessment of transplanting trees is based includes the following:
 - Variety of species, rare Hong Kong species are particularly important.
 - Condition of the tree, especially trees with balanced form, in good health and with high amenity value.
 - Size and maturity, small and younger trees have a better chance of surviving transplanting
 while larger, mature trees are difficult to transplant both logistically and in terms of survival
 rate.
 - Species, different tree species have differing rates of survival and are better suited to transplanting than others.

- Access, large machinery may be required to lift the trees, steep slopes and rocky terrain therefore make it difficult to access trees.
- 2.2.6 A recommendation to transplant a tree will be made only when:
 - It is impossible to retain the tree in-situ due to the unavoidable proximity of proposed retaining walls, viaducts, roads or other structures, including their foundations, which pose major conflicts with its branches, root system or the tree in its entirety.
 - It is impossible to retain the tree in-situ due to changes to surrounding ground levels on a macro scale which affect the ground water table thereby severely stressing the tree or where large areas of proposed cut and fill unavoidably affect the tree.
 - Transplantation of the tree is feasible and is positive to the landscape and environment for the public.
 - The Overall Value of the tree justifies transplanting.

Fell

Statutory Guidelines

- 2.2.7 The recommendation of Felling makes reference to paragraph 9 of the DEVB TC(W) No. 4/2020 which states '...Tree removal arising from government projects shall only be considered and approved under the following circumstances -
 - (a) preservation or transplanting is unsuitable or impracticable;
 - (b) the tree has been irreparably damaged by inclement weather;
 - (c) dead tree(s); or
 - (d) any other justifications or circumstances'
- 2.2.8 Expanding on this the following shall also be considered:
 - Tees in direct conflict with the proposals; changes of level etc., trees which cannot be transplanted
 - There is no practical alternative and the tree to be felled is neither included in the Register of Old and Valuable Trees under DEVB TCW No. 05/2020 nor potentially eligible to be registered as such.
 - The tree has an unrecoverable health problem and is in poor condition;
 - The tree has a low amenity value;
 - · Dead, damaged, hazardous or trees with contagious diseases are also proposed to be felled or
 - Trees which are unsuitable for the proposed development. For example poisonous species within a public open space;
 - Woodland trees which have had adjacent trees removed and have an unbalanced form or which are at risk of being blown over due to loss of supporting trees are considered for felling; or
 - Other justifications provided by the project proponent.
- 2.2.9 Where it is possible neither to retain trees in-situ nor transplant them to other permanent locations within the site or off-site, felling is recommended. The felling of a tree must be justified by the following criteria:
 - No irreplaceable, rare or protected species (under Forestry Regulation Cap.96) is felled.
 - The felling would not cause a serious loss of species diversity in the subject area.
 - A genuine development or traffic need exists, which cannot be reasonably overcome.
 - Adequate compensatory tree planting is to be implemented, or replacement with a new nursery grown specimen of the same species and comparable size is deemed more cost effective than transplanting, particularly in the case of common pioneer or cultivated species

(e.g. Acacia confusa).

- · The tree is not an unusually large or fine example of its species.
- The tree has a low amenity value, poor health, and structure or form;
- The tree is in poor condition or is unsuitable for transplanting due to its low survival potential.
- The tree is not in the list of Champion Trees (Ref: Jim, C.Y. 1994. Champion Trees in Urban Hong Kong. Urban Council, Hong Kong) nor Unusual Trees (Ref: AFCD's Register of Unusual Trees in Rural Areas), nor registered Old and Valuable Tree.
- . The tree is neither a significant landmark tree nor of special fung shui or cultural significance.
- Existing site conditions are such that transplantation would be hazardous to the public.
- The tree is dead, hazardous or diseased.
- A tree that has been rendered unstable because of the removal of neighbouring trees may be considered for felling.
- The tree possesses invasive habits. According to DEVB TC(W) No. 4/2020 section 8 (e) this
 includes Leucaena leucocephala is identified as an undesirable species with aggressive growth
 characteristics which prevent natural succession of indigenous species and so is not controlled
 by the same preservation requirements as other more valuable tree species. Therefore, this
 weed species should be replaced with native tree species.

2.3 Tree Photography

- 2.3.1 With respect to the objectives of photo recording and the possible function of the photographs, shot of each tree follows the standards set out below:
 - Where practical (within reasonable distance and within a safe location), the whole form of an individual tree will be shown;
 - Where obstacle(s) are present (e.g. structures, other trees / nearby vegetation, dense climbers covering, etc.), the main tree trunk(s) from the base level to at least 3m in height will be shown;
 - Picture to show the full extent of the canopy (may include more than one shot) and the base of the tree including the adjacent ground conditions;
 - Where special feature(s) at the trunk base present (e.g. exposed roots, special rooting medium, etc.), the photo shot of a tree is taken from the location where such feature as well as the largest possible part of the tree can be displayed.

2.4 References

Ordinances, Circulars and Practice Notes

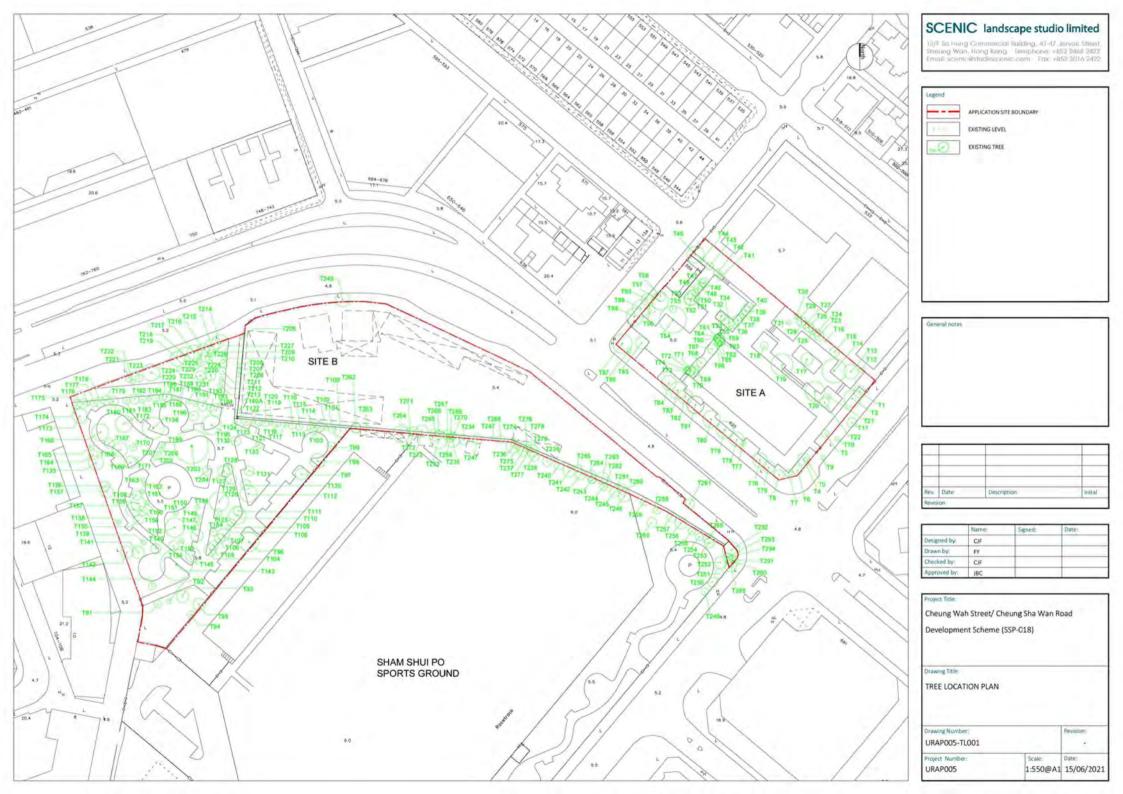
- Chapter 96. Forest and Countryside Ordinance;
- Chapter 586. Protection of Endangered Species of Animals and Plants Ordinance;
- DEVB TC(W) No. 05/2020, Registration of Old and Valuable Trees, and Guidelines for their Preservation;
- DEVB TC(W) No. 04/2020, Tree Preservation;
- DEVB TC(W) No. 2/2020 Tree Preservation and Tree Removal Application for Building Development in Private Projects;
- AFCD Conservation Practice Note No. 2, Measurement of Diameter at Breast Height (DBH); and
- · AFCD Conservation Practice Note No. 3, The Use of Plant Names.

Publications

- HU, Q. et al (2003) Rare and Precious Plants of Hong Kong, AFCD, Hong Kong;
 - Leisure and Culture Services Department. Register of Old and Valuable Trees. Website: http://ovt.lcsd.gov.hk/ovt/
 - Webb, R. (1991). Tree Planting and Maintenance in Hong Kong. Standing Interdepartmental Landscape Technical Group, Hong Kong Government, Hong Kong.

Annex II

Tree Location Plan



Annex III Tree Survey Schedule

Tree Survey Schedule

Address: Sham Shui Po Prepared by a Certified Arborist (Ray Luis) Field Survey conducted on [05/06/2021] To be read in conjunction with drawing number: URAPO05-TL001

ree Ne.	Photo No.	Botanical Name	Chinese Name	Jurisdiction (AFCD, HyD,	11	Survey So	av .		Form		Health	Canditio	an.	Struct	walCondi	alan.	Ann	mity Valu	**	3	Suitability Transplant	for ting	Conservation	Prog	onsed Treatm	nwint	Within	Justification	Nemerks
es No.	Phote No.	Botanical Name	Chinese Name	LCSD/RGD)	DBH (m)	Height (m)	Spread (m	6		0 0	,	,	D	ď	1	R	£ 6	ø	P	.0		ı	Status	Betain /. Trans	Irans	Trans/ Felt	Site	Justification	Methanix
Ti	101	Acquia confusa	台灣相思	LCSD	0.570	13	\$	П		1	1		П	П	1			1	1				Kommon			1.	1	B/C/D/F	Significant pruning in the past
12	T02	Acaaa confusa	台灣相思	LCSD	0,830	13	7		1		1				1			1				Ŷ.	common			1.	1	B/C/D/F	Asymmetric crown; leaning
13	703	Ficus benjamina	被禁机	LCSD	0.290	5.	- 3	1	1.		1				t			.00	111		4		common			X-	£	B/F	Major pruning and decay
T4	T04	Aleurités moluc cond	石栗	LCSD	0.510	8	- 5		1		- 1				Ŧ			1				1	common	1			4:	N/A	Co-dominant branches; Cavity on trunk; Wound on branch
75	TOS	Éicus benjamina	美型板	LCSD	0,100	2	2		1		1				1			1.0	111		11		common	- 3 =			3.	14/16	N/A
76	105	Aleuntes malus cand	5.00	LCSD	0.480	8	- 3		1	11 (.)	L.t				101			130		101		10	commen	3.			4.	N/A	Co-dominant branches
77	T07	Aleuntes moluceuna	EM	UC30	0.460	8	1		1.		1				-(1.				0.	converen				10.0	N/A.	N/A.
Tā	108	Alkurites moluccana	2500	LCSD	0.400	6	4		1-		1				-1		-1	10				4	common	- 1			545	N/A	Cavity on trunk; Exposed roots
19	T09	Вотьак сепья	中格.	LCSD	0.300	5	- 4		1		1				3		1 7	10	1		1		common	2.				N/A	Deformed canopy
T10	Tio	Stercullia lancrolota	644	LCSO	0,160	5	2		1		1			1		-		1			1		common	- 3 -				N/A	N/A
7(1	- DI	Barnhax ceiba	水棚	rczo	0.300	7	4		-) -	-	1				-(10				-4-	Common			1		C/D/F	Leaning contorted form; canopy damaged
712	712	Grevillea robusta	2004	LCSO	0,120	3	ž.		3		i				4			1				1	common			41	1	00	N/A.
T13	713	Ficus benjamina	通常桁	LCSD	0.680	10	-6	\Box	1		9				1			1				-it	ESONOSION			1	11	C/D/F	Co-dominant trunks
114	T14	Ficus benjamins	200	LCSD	0.910	14	10		1		1		П		1	1		1				1.	common		1		1	B/C/D/F	Multiple trunks; Stub
715	Tis	Murraya paniculata	71.00	LCSD	0.200	3	4			1	1				1			11			1	-	common			i	. 1	COM	Mature specimen; trunk stub
T16	716	Foducarpus macrophylius	MI M Et:	LCSD	0.130	4	Т.	\vdash	3		1				'n			1				10	common			A.	Τ	C/D/F	N/A
T17	T17	Caryotamitis	知他负压英	icso	0.110	6	5		1.		1				1.			-0			1.1		common			1	1	C/D/F	N/A
T18	TIB	Livistona chinensis	3834	LCSD	0.490	17.	3	\vdash	1		1	+	Н	1		\forall	+	10				1	common			-35	1	C/D/F	N/A
T19	T19	Ficus microcorpa	GEM RO	LCSD	1.160	19	9		1		1		Н		1			1				T.	common			4	T	C/D	Co-dominant trunks
T20	T20	Michelia x alba	自開	LCSD	0.710	21	8		1		1		Н		1		_	1	+			1	common			1	- 1	B/C/D/F	Co-dominant trunks; leaning; pruning wound healed
T21	T21	iun perus chinensis. Kaltuca	配伯	LCSD	0,110	4	2	+	1	+	1	+	Н	\dashv	1	+	+	100	+		1		common			1	1	B/C/D/F	Mature specimen
T22	T22	Dypsis lutescens	ROTES I	LCSD	0.110	\$	4		1	-	1	+			10	\rightarrow	+	1			1		common			1	13	B/C/D/F	N/A
T23	T23	Podocurpus macrophyllus	ALMO:	LCSD	0.160	7	4		1		1				1		-	100	1	-		1	common			1	1.	C/D/F	N/A
T24	124	Acacia confusa	企業相型	ICSO	0.270	7	3	1	1	_	1	+	Н	\dashv	1	+	+	1	1			1	common	1		1	1	C/D/F	Co-dominant trunks; Included bark
T25	T25	Рососатры тактру, ис-	位 重性	LCSD	0.210	5	1	\vdash	1	-	1	-		-	1	-	+	1	+		-	-	common			1	-	C/D/F	N/A
T26	126	Ficus benjamina	688	icso	0,100	5	4	\vdash	1	-	1	+	Н	-	Y	-	_	1	1			-	ronmon	_		· ·	4	C/D/F	Co-dominant trunks
127	127	Padacarpus macrophylus	2.80	LCSD	0.170	,		\vdash	1	-	1		Н	\dashv		+	+	1	1		-		bommon			-1	4	C/D/F	N/A.
T28	T28	Fixes benjamina	が	icio	0.150	6	4		1	-	1	+			1	+	+	1	+			-6	common			1	1	C/D/F	N/A
T29	T29	Fodocarpus macrophy Fus	四连也:	LCSD	0.140	4	2	\vdash	0	+	1	+	\vdash	-	1	-	_	1	+	-	-	4	Lightman	1		1	4	C/D/F	N/A
T30	T30	Ficus benjamina	要集化	UCSD	0.110	4	1	\vdash	1	+	1	+	Н	-	1	+	+	1	1	-	-	1	common	1		1		C/D/F	N/A
131	Tai	Garcinia subelliptica	芝島福木	icsp	0.200	5	2	+	1	+	1	+	\vdash	-		+	+	1	+		1	-	common		1	1	1	C/D/F	N/A
T32	T32	Livistona chinerish	場場	LCSD	0.250	5	4	1	4	+	1	+		,	_	+	+	1	+		-	-1	common	-	14		14.	B/C/D/F	N/A
133	T33	Livistona chinema	26	LCSD	0.170	7	4		1	+	1	+		,		-	+	1	+		1	10	common	1	-1		11	B/C/D/F	N/A
134	734	Livitona chinemia	96	icso	0.250	7	5		1	+	1	+		+		+	+	1	+				Common		1		1	B/C/D/F	N/A
T35	T35	Livitina chinensit		tCSD	0.240	4	1	\vdash	7	-	+ '	+	\vdash	-		+	+	1	+		-	1	tommon		-	1	4:	B/C/D/F	Leaning
T36	T36		(株) (株)	LCSD	0.260	7	4	+	4	-	1	+	\vdash	1		-	+	1	-		-	-	common	-			1	B/C/D/F	N/A
137	T37	Divistona chinensis		LCSD	0.250	6	1	1		+	1	+				+	+	1	+	-	-		common				1.6	B/C/D/F	N/A
T38	-		36			-	-	++	1	-	1	+		-		+	+	1	+	-	-	- A)		-	1	-	1	B/C/D/F	
	T38	Livistona chinensa	建筑	LCSD	0.250	4	3	\vdash	4	-	1	+	\vdash	-		+	+	1	+			1	common		-		7	-	N/A.
T39	T39	Elvistona chinensis	309	LCSD	0.240	7	4	1		-	1	+		-		+	+	1	+	-	-	-	(CORPORAL)		- 1	1-		B/C/D/F	N/A
T40		Livistona chinensis	389	LCSD	0.210			1	1	+	1	+	\vdash	+	-	+	+	1	+	-	-	1	common	-	- 27	-	1	B/C/D/F	Leaning
T91	T41	Livintona chinensii	38	LCSD	0.240	*	. 1		7	+	+ '	+	\vdash	1.5	-	\dashv	+	-	+	-	-		Economica		- 5			B/C/D/F	N/A
T42	T42	Livisiona chinerisis	300	LCSD	0,220	4.	1		.1		1	-	\vdash	1		-		1	-		-	10	common		1.		-6	B/C/D/F	N/A

				Juradiction	1.5	Survey Sit	ir		Form		Healt	th Cond	ition	Strue	turalCor	dition	An	menity V	alue		Soitabili Transpla		Conservation	Proj	pesed Treatm	ent	Within	1,225	- E
ree No.	Photo No.	Botanical Name	Chinese Name	LCSD/RGDI	DBH Imi	Height (m)	Spread/m	G			6		P D	G	F	P	€ 6	4	1		1	1	Status	Retain/	Trans	Trans/	Site	Justification	Remarks
T44	T44	Callistemon vimicalis	中級個	LCSD	0.110	3	2		1			1			1						1	1	common		1 4	1-	. 1	C/D/F	Leaning
TAS	T45	Aleurites moluccond	578	LCSD	0.590	111	7		3			1		1		\Box						30	commen			AL	TI	C/D/F	Restricted roots
T46-	146	Allanthus forail	五件条件	UCSD	0,490	12	4	7	1			1			1.			110	0		+	1.	near threatened	-		17	1	B/C/D/E/F	Protected under Cap. 96
T42	T47	Allanthus faraii	常趋发按	LCSD	0.330	9	- 3		1			1		1	T.				15			1 1	near threatened			45	11	B/C/D/E/F	Protected under Cap. 96
T48	T49	Allanthus fortil	京田共格	LCSD	0,350	7	3	П	9			1			1.3	П		= 10				10	near direstered			Ť,	T	B/C/D/E/F	Protected under Cap. 96
T49	T49	Allanthus fordii	23/3/86	ucso	0,480	-07	- 6		1			1			Y	П		- 10				Υ.	near threatened			Y	Y	B/C/D/E/F	Protected under Cap. 96
T50	750	Allamhus faraii	双热条6	rcso	0.650	17			1			1			1				10	1		-1	near firestened			1.	141	B/C/D/E/F	Protected under Cap. 96
T51	751	Allanthus foraii	安存在被	LCSD	0,310.	8	5		3			1			3			1	1		1	19.	near threatened			4	11	B/C/D/E/F	Protected under Cap. 96
T52	TSZ	Allanthus fordii	常组风格	LCSD	0.460	17.	- 6	-	3.	-		1			· T			- 1	0.		1 10	-1	near dynamical		-	1.	4-	B/C/D/E/F	Co-dominant branches; protected under Cap. 96
133	T53	Allanthus fordii	示线与特	UCSD	0.370	14	5		4			1			÷¥.		-	10				1	near fire-steroed			1-	4:	B/C/D/E/F	Protected under Cap. 96
T54	T54	Ficus benjamins	9.400	LCSD	1.240	14	18		1			1		1				1				1	common		1		3.1	B/C/D/E/F	Wound on trunk; Co-dominant branches
TSS.	755	Caryoto ochlundra	0.00.0	LCSD	0.100	4.	3		2			7			Α.	\Box		10	0.1		1 0		tommon			1	1	B/C/D/E/F	Large specimen; pruning wound for primary branch
156	T56	Callisemon viminali:	明規修	ucso	0.140	7	8			1		1				1.1		1	(I		11/12	1	contrion			11	4.	B/C/D/F	Cracks on trunk base; Leaning: Uprooted
T57	757	Syzygium jambas	500	icsp	0.360	13	2			4.		1			1							1	common			Ť		C/D/E/F	Bending trunk: Cavity on trunk: Leaning; Exposed roots
T58	759	Syzygium jambas	1600	LCSD	0.380	8	4			1	10	1				1		0	0 1		1 10	10	tommon			A.	14	C/D/E/F	Dead wood on trunk Leaning, Exposed mots
T59	T59.	Ravenala madagascariensu	他人概	UCSD	0.160	9	- 4	\Box	1			,		1		\top		1				10	-bammon			1	9.0	C/D/E/F	N/A
760	760	Naverala madayascan ensis	原人類	LCSD	0.310	8	4		1	- 1	1	,		1		Н		1		1	-	1	common			1	4.	B/C/D/E/F	N/A
Tot	761	Ravenala madagascarieras	版人框	LCSD	0.250	6	1		1		+	,		1				-				7	common			141	9	B/C/D/E/F	N/A
T62	T62	Ravenaja madagascariensis	泰人东	LCSD	0.250	5	4	\Box	1			,		1					1			10	common			1	1	B/C/D/E/F	N/A
T63	763	Ravennia madagascoriensis	版人家	UCSD	0.210	6	4	Н	4			1		1		†				+		1	common			1	140	B/C/D/E/F	R/A
T64	T64	Rovenala madagascar eros	在人板	LCSD	0.290	6	1	1	7		+	,		1						+		1	common	1		1	1	B/C/D/E/F	N/A
T65	765	Navenala madagascariersis	版人概	LCSD	0.280	6	3		,			1		1			-					1	common			1	1	B/C/D/E/F	N/A
T66	166	Raverola madagascariensis	版人能	LCSD	0.230	6	- 3	1	1			,	+	1			+	1		+	1	1	common			1	- 6	B/C/D/E/F	N/A
T67	767	Livitona chinensa	384	LCSD	0.280	8	4	+	· ·	-	+	1	+	1		+	+			+	1		common		1		1	B/C/D/E/F	N/A
T68	768	Livotona chinensh	309	LCSD	0.290	8	- 4	\vdash	,	-				1		+	+	-		+	1	+	tommon	1			1	B/C/D/E/F	N/A
T69	769	Raverala madagasconersis	北人斯	UCSD	0.220	7	1	\vdash	1	-	-		+	1	_	+	+			+	+	1	common	1		1-	- 1	B/C/D/E/F	N/A
T70	770	Ravenala madagascarienso	野人所	LCSD	0.240	7	4	\vdash	1	-	+	1	+	1		+	+		-	+	+	1	common	1		1	1	B/C/D/E/F	N/A
T71	171	Ravenala madayascarieres	原人鄉.	ICSD	0.610	7	4	\vdash	,	-	+	1	+	1	_		-		-	+	+	10	termos	1		1	1	B/C/D/E/F	N/A
172	T72	Ravenala madaga con erais	BAR	ucso	2.216	7	4		1	-			+	1		1		+		+	+	1	common	1		-	-	B/C/D/E/F	N/A
171	773	Ravevala madagascariens-s	原人族	LCSD	2.220	7	1	+	-	-	+		+	1	-	\vdash	-	+	-	+	+-	ài.	EMPHORA	-		-	-	B/C/D/E/F	N/A
T74	174		版人施	LCSD	2550	6	1	\vdash	1	-	+		+	1		+	-		-	+	-	1	common			1	-	B/C/D/E/T	N/A
_	175	Ravenala madagascaneros		LCSD	0.380	9	5	\vdash	3	-	+	,	+	+	1	+	+	+	-	+	+	1	icommon	1	_	· ·	1	N/A	
T75		Akuntes moluccuna	7.17		0.510	-	_	1	-	-	+	+	+	+	1	+	+	+	-	+	+	1	Laminan	1			1		Co-dominant branches N/A
176	176	Albuntes maluccana	15W	LCSD	0.130	5	2	-	+	-	+	-	+	-	1	\vdash	-	+ '	-	+		1	1	1			1	N/A N/A	N/A
_		Caryota ochlandra				-		-	,	-	+		+	1	-	+	-		-	+	+	1	common	1			10		
178	T78	Alkumes maluccana	579	LESD	0.510	-0	ě .	-	7	-	+	1	+	+	1	+	-	+	-	+	+	1	Estretion	1			4	N/A	N/A
179	179	Aleurines maluccinna	100	LCSD	0,470	10	7	-	40	-	+	1	+	+	2.7	+	-	+	+	+	-	1	-ponition				-1	N/A	Co-dominant branches; Cavity on branch
180 Tes	780	Alkuntes moluccuna	200	LCSD	0510	11	7	\vdash	7	-	+	-	+	+	. L	+	-	+		+	+	1	nommon	1			3.	NIA	Co-dominant branches
THE	781	Aleuntes muluccond	Ping.	LCSD	0.450	12			2	-			+	+	1	+	-	1		+	+	1	temmen	3			1	N/A	Cavity on trunk
782	T82	Aleurites molucçuna	石栗	LCSD	0,470	13	6		1.1	-	+	1	-	-	1	\vdash	-	-	-	+	-	10	countaiou				1	N/A	N/A
785	783	Aleurites maluccina	57	LCSD	0.590	10	2		1	-	+	-	+	-	1	\vdash	-	-		-	-	1	Example	1			14.	N/A	Co-dominant branches
TB4	T84	Aleurites moluctona	行権	ricad	0.470	10	6		2	-	+		+	+	1	+	-	1		+	-	1	tommon	1			4	N/A	Co-dominant branches; Cavity on trunk
T85	T85	Choerospondias axiliam	向数值	LCSO	0.400	2)	-5		1	-	-	Till I	+	-	1	\vdash	1	- 1	-	-	-	1	Lommon	1			11	N/A	Co-dominant branches
TBS:	186	Allanthus farais	常性為格	rczo	0.250	-17	-2		1		-	1	+	-	1		-	1	-	-	-	1	Lummun	1-			-4:	N/A	N/A
Te2	T87	Aleurites moliciona	石棚	LCSD	0.570	12	В		1	-	-	1	+	-	1	\perp		1		-	-	Y	continion	1			14	NA	Co-dominant branches
J88	788	Вотрах серь	水板	LCSD	0.460	15	7		2		-	1			- 3		-	1				- 0	Estatement	3.				N/A	N/A
THP	T89	Bombax cerbs	3/8	LCSD	0.370	15	7		1		1		1		1			0		1	-	1	-pommon	1				N/A	N/A
T90	190	Вотрах сеіва	木橋	LCSO	0.340	14	5		1		-	1			1			ť in			1, 1	. 1	common	1				N/A	Leaning
19)	T91	Mélalèuca quinquenervia	日千届	TC2D	0.500	9	3		3			1			1.30	1 1	1		0.1		1117	1	termos	1		4	TY	C/D/E/F	Co-dominant branches

aute.	NG CO		46.00	Jurisdiction		Survey Sit	Ter .		Form		Hei	elth Con	dition	Stru	ctural Cor	dition	Am	senity Val	lue		Soitability Transplan		Conservation	Pro	posed Treatm	sent	Within	LONG CO.	9 Lane
red No.	Photo No.	Botanical Name	Chinese Name	LCSD/RGDI	DBH Imi	Height (m)	Spread/m	6	r.	ė	6		P (G		R	€ 6	1	P	н		L.	Status	fleteln/	Thems	Trans/	Site	Justification	Remarks -
192	T92	Grevillea robusta	300	LCSD	0.480	16	2		1			1			1			1				1	common		1	1	1.1	C/D/E/F	Slightly leaning
91	T93	Melaleuça quinquenerva	百千加	LCSD	0.490	14	5					t			L.b.			1	4 1 1			10	commen			A.	TX.	C/D/E/F	N/A
194	T94	Logerstroemio spécioso	大花養養	UCSD.	0.220	6	. 5		1			1			1.			100			. 7		common	- 7			1	N/A	Asymmetric canopy; contorted
T95	T95	Spathodea campanulata	火焰木	LCSD	0.450	-ir	5		. 1			1		1	1			11				-0.	common	- 40			19	N/A	Co-dominant branches
T96	T96	Ficus virens	大監修	LCSD	0.430	15	8		3			i			1.			1.3				10	common	1			T	N/A	N/A
T97	T97	Logerstroemia speciosa	大花繁寶	UCSD	0,370	- 8	7		1			Y		Y		П		10				у.	common	- 1			Y.	N/A	N/A
T98	798	Logerstroemia speciosa	大花繁新	LCSD	0.220	8	ā		1		П	1		- 1				1			1		gamman	1			141	N/A	N/A
T99	799	Ficus benjamina	越車 位	LCSD	0,320	1	- 4		114	1.		1			3			1	1		1	19	common	1			111	N/A	Wound on trunk
T100	T100	Alcuntes moluccana	石原	LCSD	0.530	9	- 6	-	-2	-		1			T			-1	1			-10	common	1 -			4.	N/A	Heavy crown load; Wound on trunk; Leaning
T101	T101	Aleantes makes and	音楽	UCSD	0.450	9	- 3		1			1.			ΞŤ.		-	11				- 11	common	1			4	N/A	N/A
T102	T102	Aleumin moluccona	25.00	LCSD	0.330	9	2		Ŏ.			1			1			1				-1	common	- 1			3.	N/A	N/A
T103	7103	Aleuntes moluccana	FEMP	LCSD	0.320	317	*		0		\top	Y	\neg		T	П		100				τ	common	7.0			7	N/A	Gall
T104	T104	Servici slames	鐵力本	ucso	0.430	15	5		1		1	1			-1	\Box		11			-	- 6	contract			111	9.1	B/C/D/E/F	Epicormics
T105	T105	Servia slamea	観力水	LCSD	0.350	16			Ť			1			1	Ħ		1			-	- 1	common			i.	1/1/	B/C/D/E/F	N/A
T106	7106	Senina liamed	銀刀北-	LCSD	0.350	15	1.4		1		1	i	+		1			1				1	tommon			i.	- 4	B/C/D/E/F	Epicormics; Wound on Trunk
T107	T107	Senna samea	#12 %	LCSD	0.340	15	-5		1			1	+	+	1	\Box		1	1			10	-bammon			1	3.0	C/D/E/F	Epicormics; Wound on trunk Cavity on trunk
T108	TIOR	Collisterion vimicalis	*120	LCSD	0.100	5	2		1	=	7	1	+	+	1	+		1	1		1	1	common	1.1			14	N/A	N/A
Tiú9	7109	Callisterron viminalis	小河田	LCSD	0.150	- 6	1		4		+	4	+	-	P			1				7	common	1			- 14	N/A	N/A
T110	7110	Senna slamea	推力未	LCSD	0.330	17.	7		1		+	1	+		1	Н		1	+		+	10	common	Υ.			1	N/A	Wound on trunk
mi	TILL	Carymbia tarelliana	毛唇按	UCSD	0.330	10	4		4		+	1	+	+	1	+		1	+		1	1	common	1			14	N/A	N/A
T112	7112	Corymbia rorelliana	E整位	LCSD	0,440	12	7	+	1		-	ī	+	+	1	+	-	1	+	+	-	1	common	1			1	N/A	Contorted trunk
T113	7)13	Ficus benjamina	直整板	LCSD	0.420	7)	6	-	,		-	1	+	+	ì	+	-	1	+	+	+	1	common	7			1	N/A	Heavy crown load; Asymmetric crown; Epicormics
T114	7114	Albumes moluccona	音楽	LCSD	0.360	9	3	+	3		-	1	+	+	1	+	-	11	+	+	+	1	common	1			- 1	N/A	N/A.
_	_		_	_	0.420	8		+	,	\rightarrow	+	1	-	+-	1	+	+	+	+	+	+	1	_	1	-		1		
T115	7115 T116	Alcuntes maluccona	石榴	LCSD	0.360	0	3	-	,		-	1	+	+	7	+	-	+	+	+	+-	1	common	-			1	N/A	Co-dominant branches; Dieback twigs
T116		Alkuntes maluccond	石原		0.340	-	3	-	4	-	-	-	-	+	-	+	-	+ '	+	+	-	-	CONTROL	1	-			N/A	N/A
1917	T117	Aleurites malucçuna	行際	LCSD	-	8	- 2	-	-1	\rightarrow	+	1	+	+-	1	+	+	1 1	+	+	+	1	common	1		-	1.	N/A	N/A
7118	3118	Aleuntes moluccana	2519	LCSD	0310	6	2	-	11 3 11		-	,	+	-	1	+	-	+	+	-	-	,	commod	1			1	N/A	N/A
1119	7119	Aleustes muluccond	石幣	LCSD	0.290	9	Z		,		-	1	-	-	1.0	\mathbf{H}		1			-	. 10	tommon	1			T	N/A	Dieback twigs
T120	1120	Aleurites moliccond	石棚	UCSD	0,326	11	J.		1		-	1	-	-	1			1			-	1.	countried	- 1			+4	N/A	N/A
1121	7121	Aleuntes moluccana	5799	LCSD	0.310	9	1	-	1		-	1	-	-	-4-	\vdash		1	+	-	-	- 1:	Entwiness	1-1-		-	1	N/A	N/A
T122	1122	Aleuntes moluccana	石原	LCSD	0.310	7	1	-	1		-	1	-	_	1	\perp		,	-	-	-	10	common	.1			7.	N/A	Co-dominant branches; leaning
T123	7123	Aleuntes moluceura	7.19	LCSD	0.320	9.	3		4		4	1	-	1	-1			-1	-			1.	nommon	-	1		111	C/E/F	Co-dominant branches: Dieback twigs
T)24	1124	Aleurités maluceana	D#	rcso	0.250	6	- 3		i.∄≡		-	1	-	-	1			1.1	-			-1	Fausting		-1		-4-	C/E/F	Dieback twigs; leaning how shaped stem
1125	T125	Citrymbia foreillana	毛量核	LCSO	0.410.	13	1	-	1		-	1		-	1			1	-	-		1.3	common	1			1	N/A	N/A
T126	T126	Corymbia tavilliana	EMR	LESD	0.460	15	8		7		1	1	-	-				1			100	=1:	Estation				10	N/A	Co-dominant branches; asymmetric canopy; leaning
T127	1127	Corymbia torelliana	EWIX	VCSD	0,440	- 18	- 8		-1-			1.		-	- 1			1	-			-1	-common	- 1			4	N/A	Leaning: asymmetric canopy
T128	7128	Corymbia torelliana	毛並佐	LCSD	0.330	10	4		dr.			1		_				1				1	common	1			3.	N/A	N/A
1129	7129	Carymbia torelliana	主黨標	LCSD	0.470	17	2		4			1		-	1	\perp		-1				1.40	termen	1.31			1	N/A	N/A
T130	1130	Carymbia torelliona	毛幣按	ucsp	0.570	17	4		1.1			1			1			1.1				16.	convinor	1			13.1	N/A	N/A
T)31	7131	Logerstroemia speciosa	大花繁菱	LCSD	0.160	4	4		11	-		1		1				1			1		Economical	-4-			4.1	N/A	Leaning
T132	7132	Corymbia torelliana	毛無夜	LCSD	0,510	16	5		7	11		1			Ť			1				1.0	tommon	7.7	14		40	C/E/F	Contorted stem
T133	T133	Bauhinia x blakeana	沙梨族	LCSO	0.200	8	3			1		1			1			1				- 1	icommon	(1)			11	N/A	Bending trunk; Wound on trunk
T134	T134	Joeanunda mimesilolis	- 軽花椒	rczo	0.130	\$			1	-		1			1			14				-8-	Emmino			1-	14:11	B/C/D/E/I	Leaning
1135	7135	Melio amdorach	古柳	LCSD	0,660	14	9		1			1			1			-1				Y	common	1	J. T	1	1.	B/C/D/E/F	Leaning, asymetric caonpy
T)36	#136	Melia azedarach	810	UCSD	0.650	14	В	100	101	1		1			1		3	1	1		11.11	1	common	111		1	-1	B/C/D/E/F	Co-dominant trunk; Cavity on trunk; Cracks on trunk; learning
T137	T137	Melia andorach	389	LCSD	0.520	12	- 6		3			7			1			10	/ 10			-0	parvison			1.	4.1	B/C/D/E/F	Co-dominant branches
T138	T138	Collistenon viminalis	40段個	LCSD	0.126	3	2		1			1			1	\Box		1			1		pommon		1		- (B/C/D/E/F	N/A

n her	la com			Jurisdiction	14	Survey Sit	le .	15	Form		Hee	lth Con	dition	Stra	etural C	ondition		Amenity	y Value		Soi	itability ansplant	far ing	Conservation	Ргор	esed Treatm	rnt	Within	. George	\$ E50.X
Tree No.	Photo No.	Botanicai Name	Chinese Name	LCSD/RGD)	DBH Imi	Height (m)	Spread (m)	a	*		6		P (G	,		ε	6	Œ	P	8		4.	Status	Retain/. Trans	Trans	Trans/ Fell	Site	Justification	Remarks
1139	7139	Callisterion vimicalis	中級個	LCSD	0.110	3	2		1			1			-)				10			1		common		3.		.11	B/C/D/E/F	N/A.
140	7140	Meialeura quinquenerna	H-FM	LCSD	0.330	70	14		Э.,			i.			İ				1).				10	sommeri			- F	TY	B/C/D/E/F	Leaning co-dominant, forked stem
141	T141	Logestroemia speciosa	大花葉板	üsb	0.160	6.	5		7.	-		1		1					υC.	11		-76		common			1	0	B/C/D/E/F	Contorted stem.
142	T142	Melia azedaroch	1611	LCSD	0.580	-14	2		1		Т	1			1				10				31	common			4	17	B/C/D/E/F	Mature specimen
1143	T143	Flous microcorpa	医 重化	LCSD	1,130	17	13		7			1		1				7					10	common		1		1	B/C/D/E/F	Mature specimen; leaning
T184	7144	Ficus benjamina	MININ.	LCSD	0,100	3	3		7			1			T				1			7	-	common			T	Y.	B/C/D/E/F	Mature specimen; leaning
1145	7145	Coryribia torelliana	EMIT	LCSD	0.490	10	- å		-1			1			. 1	-			11				-t	common			-1-	- C-	B/C/D/E/F	Co-dominant branches; leaning
1146	T146	Corymbia toretliana	6.50	LCSO	0.480	12	5		1			9			1				10.				-0	common			4.	1	B/C/D/E/F	Leaning
147	T147	Melaleuca quinquenervia	日午線	LCSD	0.270	7	2		. 1			Y			ì	1			0.	м			. 1	common			1.	4.	B/C/D/E/F	Leaning
T148	7148	Phoenis rombelenii	日本資	LCSD	0.110	- 2	-2		1			1		1					1			1		common		-1		1	B/C/D/E/F	N/A
T149	T149	Phoeniu torbelenii	日本質	LCSD	0,110	2	- 2		Ť.			1		,1					1			1		common		4		(0.1	B/C/D/E/F	N/A
1150	T150	Phoenix roebelenii	日本祭	LCSD	0.110	3			7			τ.,		. Y.	Т				0			1		common		Tr.		4.	B/C/D/E/F	N/A
T151	T151	Phoenix roebelenii	HAN	U30	0,130	3	2		1.			1		1					1.			1		contrion		-(4.1	B/C/D/E/F	Transplant
1152	1152	Melia azedarozh	344	LCSD	0.550	9	8		1		1	1			- 1		-		(-)				1	common			1	140	B/C/D/E/F	N/A
T153	7153	florrhax cerba	中級	LCSD	0.180	9	2		1			9			3	1			10			100	10	common			4	. 1	B/C/D/E/F	Contant main stem
T154	T154	Meleleuca quinqueneryis	0.78	LCSD	0,400	13	4		1			1			1				1				10	common	11.1		1.	14.	6/C/D/E/F	N/A.
T155	TISS	Lagerstraeniki speciasa	大花素數	LCSD	0.210	7	4		-1-	1	1	1		1					-)-				-1-	Xemmon			1	-(-	B/C/D/E/F	N/A
T156	7156	Layerstroemia specioso	大龍軍政	LCSD	0,240	-6			- p			4		1					1			- 1		Common			11	-1	B/C/D/E/F	Leaning
T157	T157	Logerstroemia speciosa	大花紫葡	LCSD	0.160	7	- 6		3.		+	1		1					1			1		ESONOSO			1.	-1	B/C/D/E/F	Leaning
1158	T158	Logerstruenia speciosa	大花繁噩	LCSD	0.276	8	6	Н	1		+	1	1	1	1	1			1			1		common			1	14	B/C/D/E/F	N/A
1159	7159	Lagerstroemia speciosa	大花繁新	LCSD	0.160	5	4		14		+	1		1		1			1			1	_	common			1	71	B/C/D/E/F	N/A
T160	7160	Phoenix roebelens	日本原	LCSD	0.110	3	2)		+	1		1					1		_	,		common			4	1	B/C/D/E/F	Leaning low stem
T161	T161	Phoenia roebelenii	HAR	icsb	0.110	5	2		4		+	1	_	1		+		\vdash	-01			.9.1		common			1	- 6	B/C/D/E/F	Leaning contorted stem
1162	7162	Phoenix roebelenii	日本製	LCSO	0,110	4	2	\vdash	1	\rightarrow	+	1	_	1	\vdash	+	+	\vdash	-		_	1		common	1		1	1	B/C/D/E/F	Leaning contorted stem
T163	T)63	Phoenix roebelenii	日本発	LCSD	0.110	5	2		,	_	+	1	+	1	1	+	1	\vdash	-		\neg	,		common			1	1	B/C/D/E/F	Leaning contorted stem
1164	T164	Mella azedovach	200	LCSD	0.390	8	4		1		+	,	-	+	1			\vdash	1				1	convince			Y	1	B/C/D/E/F	Leaning
T165	T165	Bombaxcelba	木橋	LCSD	0,130	5	2	+	1	\rightarrow	+	1	+	+	1	+	+	\vdash	-1		\rightarrow		1	common	1-		1	1	B/C/D/E/F	Leaning
T166	7166	Lagerstmenta speciesa	大花里面	LCSD	0.260	11	7		1	-	+	,	+	1	1	+	+		1		_	,		common			1	1	B/C/D/E/F	N/A
T167	7167	Lageritroemiii speciosa	大花紫朝	LCSD	0.250	4	4			7	+	7	+	+	+	1			6		-	1		-common	-		1	10	B/C/D/E/F	Wound on trunk
1168	7168	Lagerstroonia speciesa	大花紫觀	LCSD	0.290	7	.6	\vdash	1		+	1	+	1	+	+	+	\vdash			-	1	-	common	1		1.	4	B/C/D/E/I	Tree support
1169	T169	Logerstroemia speciora	大花葉霞	LCSD	0.220	6	ś		4	-	+		+	1	+	+			1			1		common			4	1	B/C/D/E/F	N/A
T170	7170	Juniperus chinensis "Kaizuca"	服相	LCSD	0.140	3	3	\vdash	1	-	+	1	-	÷	1	+	+	-	1	-	-	1		common	1		1	1	B/C/D/E/F	N/A
1771	1171	Elaeocarpus obrusus subsp.		UCSD	0.440	15	2	+		-	+	•	-	+	1	+	+	\vdash	,	-	-	,		common			-1	1	B/C/D/E/F	Fig. 1 - 1 - 1
1172	7172	Apigulatus Lagentroemia speciosa	是否杜斯 大花香蘭	LCSD	0.210	8	7		1	-	+	1	+	+	-	+	1	+	+	-	-	1		common			1	4	B/C/D/E/F	Slightly leaning N/A
1173	1173			LCSD	0.340	9	6	\vdash	,	1	+	÷	+	+	1	+		1	-	-	-	-	1	common	1		A	1.0	B/C/D/E/F	
T174	1174	Baufiria variegna	SECTION.	LCSD	0.540	10	4		1	1	+	-	+	+	1	+		\vdash	÷	-	-			common			1	4	B/C/D/E/F	Bending trunk; cavity an trunk; contorted
T)75	T175	Aleurites moluccina Aleurites moluccina	1200 A200	LCSD	0.480	12	4		1	-	+	,	+	+	-	+	\vdash	+	1	-				countries			1	4	C/D/E/F	Co-dominant branches, asymmetric canopy N/A
	7176		59	LCSD	0.280		2	\vdash	4	-	+	1	+	+	1	+		+	1	-	-		4		1		- to	-	C/D/E/F	
T176		Alternative and	5章			12			90	-	+	:	+	+	-	+		-	7/	-	-		40	common	1			1		Dieback twigs; leaning low stem
	7177	Aleurites molucciona	石幣	LCSD	0.340	11.	3		- 5	+	+	1	+	+	1	-		+	-		-		1	common			4	1	C/D/E/F	Cavity on trunk
178	7178	Aleurites moluccona	石原	1CSD	0.350	13	4		11	-	+	1	+	+	1	+	\vdash	H	-1-	-	-		1	Ebtamina	-		1	14.	C/D/E/F	Co-dominant branches N/A
	1, 90000 0	The second Printing Lines	五章	- Spiller	4,465	- 11	4		7	-	+	1	+	+	1	+			0	-	\dashv	_	- 1	common	-		1	11	C/D/E/F	
Tied	T180	Aleuntes maluccona	石棚.	read	0.390	9	4		1.	-	-	T.	+	+	- 1	-		\vdash	1.	-	\dashv		1.	tommon			10	1.	C/D/E/F	Co-dominant branches
1001	T181	Aleurités maluciona	V5/M	LCSD	0.340	12			1	-	+	1	+	+	- 1	-	\vdash	\vdash	11	-	+	-	1	bonimon	-		1	A	C/D/E/F	Cavity on trunk
1162	T182	Alvantes moliciona	77.00	LCSO	0.390	-01	4		. 1	-	-	1	+	+	1	-		-	= t) .				1	Commod			1	1.	C/D/E/F	Dieback twigs
183	T183	Alkurites moluccond	万里.	LCSD	0.350	10	3	\vdash	7	-	-	1	+	+	,	-	\vdash	Н	-	-	-		10	Convenion			1.	I.V.	C/D/E/F	Diebisck twigs
184	T184	Aleurites maluccuna	石庫	LCSD	0,320	10	2		1	-	-	1	+	+	1	\rightarrow		\vdash	-11	-	-		-1	common			1	1	C/D/E/F	Cavity on trunk
TIRS	T185	Alcuntes maluccana	5.0	LCSD	0.410	tg.	3		. 1		-	1			- 1	-			ıήτ		-	100	1	toward			1	JP.	C/D/E/F	Cavity on trunk
1186	7186	Albuntes maluczona	68	LCSD	0.370	10	3		7			1			. 3				10			12.	10	common			1	TX.	C/D/E/F	Dieback twigs

			1.00	Jurisdiction	137	Survey Six		×	Form		He	elth Co	ndition	St	outher.	Condition	on	Amen	nity Valu	•	5	oitability ransplant	for ting	Conservation	Prop	esed Treatm	ent	Webbe	1	
Tree No.	Photo No.	Bosanical Name	Chinese Name	(AFCD HyD, LCSD/RGD)	DBH Imi	Height (m)	Spread (m)	G	i.		6	ē	p	D 6	5	•	P E	6	4	P	8	4	L	Status	Retain /. Trans	Trans	Trans? Fell	Site	Justification	Remarks
T187	T187	Alcumes moluccana	石原	LCSD	0.350	10	4		3.			1				i i			Œ				i	common			i.	144	C/D/E/F	Dieback twigs; cavity on trunk, primary branch stub with decayed surfa
T188	7188	Alewites maluccana	5.00	LCSD	0.330	8	2		9	11		1				t			. 1				10	common			1	1.	C/D/E/F	Dieback twigs
T169	T189	Alcurites moluccuna	石里	LCSD	0.340	9	2		.1.			1				1			1				10	common			1	14.0	C/0/E/F	Dieback twigs; cavity on trunk; lowered stem
T190	T190	Aleurites moluccana	- BM	LCSD	0.400	10	2		1			1			1	1			-).			-	-10	common			1	-(-	C/D/E	Dieback twigs; co-dominant branches with forked stem
Ti91	T191	Aleurites moluccina	200	LCSD	0.340	12	2		1			1				1			1	11	100	1	- 1	common			1	1.	C/D/E	Dieback twigs
T192	7192	Alcuntes moluccana	石原	LCSD	0.360	10	- 4		3			1.				1			.0.				10	Esmmon			1	1.	C/D/E	Wound on trunk
T193	T193	Aleuntes moluccana	行業	LCSD	0.340	10	- 1		1			1				1			-0				1.	common	1			16	N/A	N/A
T194	T194	Aleumes moluccana	279	LCSD	0.450	9	5		1	100		1				1			1		-1		- 10	common	- 1 =				16//6	Co-dominant branches: Wound on branch
T195	T195	Terminalia catappa	(唯仁相)	LCSD	0.470	10	6		2			ĭ				T			1				Ť	Eartmoh	1			4	N/A	Co-dominant branches; leaning; asymmetric canopy, bow shaped mair stem
T196	T196	Ficus benjarnins	25年	LCSD.	0.110	-4	4		10			1				1.			10			4	_	Common	1			10	N/A	N/A
T198	7198	Ficus elastica	印度橡板	LCSO	0.400	15	140		1			1				1			10	1			÷γ	common			1	141	B/C/D/E/F	Restricted roots
T199	T199	Phoenix roebelenii	日本英	LCSD	0.120	2	2		1	H		1		1	C ii					14		1		common	1	1		Tr.	B/C/D/E/F	N/A.
T200	T200	Phoenis roebelenii	日本保	LCSD	0.110	2	-2		1			1							1	H		1		common		1.1		4	B/C/D/E/F	N/A
1201	T201	Phoenix rozbelenia	日本英	LCSD	0,130	2	2		1	7.4		1		- 1		-1	-		10	73	41	1		promotor		1		JT:	B/C/D/E/F	N/A
T202	T202	Phoenix roebelenii	日本質	LCSD	0.130	2	2		1			1							13	1		. 1		common				Tr	B/C/D/E/F	N/A
T203	T203	Ficus elastics	印度物植	ÚCSD.	2,500	17	14		1	14		1				1		10		1.1			1	common		11		1	B/C/D/E/F	Dieback twigs; Dead branch
1204	7204	Corymbia torelliana	€MEC	LCSD	0.620	13	2		4			1				1			1				11	common	1			4	N/A	Co-dominant branches
T205	T205	Iomperus chinemus Kazuca	70/40	LCSD	0.130	6	2		15			i				3		\top	. 1				10	common	1				N/A	N/A
T206	T206	Jumperus chinenta Kolauca	Tické	LCSD	0,120	5	2		1			1		+		ì	1	1	10				· v	common	- 1			1	N/A	Tree-support
T207	7207	Jumperus chinemis 'Kolzuca'	WHO .	LCSD	0.140	4	-2		1			1				Y			1				-):	Kemmen	1			4	N/A	Tree support
T208	T208	Jumpenis chinemis Kozuco	凝粒	LCSO	0,120	4	2		1			1		1		1	1		1	-			- 9	common	- 1			1.	tv/A	Tree support
T209	T209	Suspenschinenin Kolauca	凝拍	LCSD	0.110	4	2		4	11		1			1	1			-0	100		A.		common	3 -			+	N/A	Leaning
1210	T210	Josepenis chinemia 'Kouruca	粗柏	LCSD	0.170	- 4	1		1			1		+	1	T	1		1			1		common	1			4	N/A	N/A
T211	T211	Jumperuschinemia Kazuca	麗柏	LCSD	0.120	5	1		dr.	HT.		1				1			11	111		1		common	1			1	N/A	N/A
T212	7212	Jumperus chinensis "Kalauca"	旅伯	LCSD	0.170	4.	1		.0			1		1	+	Ť			1			4		common	1				N/A	Leaning
1213	T213	Jun perus chinensia "Katruca	原相	LCSD	0.140	-4	2		4			1		+	+	1	1		1			1		common	1			4	N/A	Leaning
T214	T214	Ficus benjamina	更新板	LCSD	0,440	10	7		1			1		1	+	1	1		1				1	common	1			197	N/A	Epicormics; slightly leaning form
1215	7215	Ficus benjamina	0.00	LCSD	0.510	31	6	\vdash	.0		\vdash	Tr.	\vdash	+	+	T	+		110				1.0	common	3.			- 6	N/A	Epicormics
T216	T216	Ficus benjamina	点面物	LCSD	0.430	ű.	5					1			+	1	+		1					common	1			1	N/A	Epicormics.
7217	T217	Ficus benjamins	多数的	LCSD	0.550	12	6		1		\vdash	1		+	+	1	+	+	10				1	Erammigh	1			14.	N/A	Epicormics; co-dominant trunks; leaning form
1218	T218	Ficus benjamina	6.50	LCSD	0.340	12	7		1			1		+	+	1	+		10				1	common	3			1	N/A	Epicormics
T219	T219	Ficus benjamina	西兰布	LCSD	0,370	12	6		1			1		+	+	1							-10	common	1			11	N/A	Epicormics
1220	T220	Ficus benjamina	500	ICS0	0.260	12	7		1		\vdash	1		+	1	1	+	1	16		-		1	common			1	16-	C/D/E/F	Epicormics; multiple trunks; leaning form
T221	T221	Roystonea regia	大王椰子(王牌)	LCSD	0.440	12	- 1		1.3			1				1			13				¥	common			1		C/D/E/F	N/A.
T222	T222	Terminalia mantaly	小旗權仁	LCSD	0.130	3	1		1		\vdash	Y		1		r	1					1		common			1	.1.	C/D/E/F	Sightly leaning
1223	7223	Roystonea regia	大主都子(主称)	LCSD	0.440	n	1		Y			1		1		1	+		1				11:	benimen		η.		-(-	C/D/E/F	N/A
1224	T224	Aroucaria heterophylla	以 国用:3443	LC(0)	0,160	6	2		1			1	1	+	+	ì	1		1	1.0		1		common	1			1	N/A	N/A
T225	7225	Phoenix roebelensi	日本祭	LESD	0.110	3.	2		7			i		1		1			7			1		common	1			y	N/A	N/A
1226	T226	Roystónea regia	大王椰子(王财)	UCSD	0,440	10	4		1			1	1	1		+	+		11				1	common	1			- (N/A	N/A
1227	T227	Roystonea regia	大王椰子(王烷)	LCSD	0.500	to	3		1			1		1	1	1	+		1				1	pommon	- t			. 1	N/A	N/A
1228	T228	Roystonea regia	大王椰子(王際)	LESD	0.440	10	3		1			4	1	1	1	1			1				9	territion	1			TE	N/A	N/A
T229	T229	Phoenix roebderai	日本身	ücso	0,120	3.	1		-1		\vdash	1	1	1		\dashv	1		1			.1.		common	1			1	N/A	NA
T210	T230	Roystonea regia	大王帽子(王叔)	FCZO	0.410	13	4		1		\dashv	1		-	+	_	+		-1				1	common	1			-1	N/A	N/A
T231	T231	Roystonea regia	大王椰子(正焊)	LCSD	0.500	12	4		1			1			-	-	+		1				10	common	1			1	N/A	N/A
T232	T232	Royatonea regia	大王都行(五祖)	icso	0,470	11	4		3		+	1	+		+	+	+	+	-6				1	Edutation	1			14	N/A	N/A
1733	T233	Aleurites malus cona	4500	ICID	0.590	9 -	7		7		\forall	1	+	+	+	Y	+		1				1	common	1				N/A	N/A
T234	T234	Aleuntes moluccunia	GW	LCSO	0.390	8	4		1		+	1	-	+	-	1	+	1					-40	common	1				N/A	N/A

auter	bear of		***	Jurisdiction		Survey Sin			Form		Health	Çonditio	n	Structue	ra (Condit	on	Ameni	ity Value			oitability (c ansplanti		Contervation	Prop	esed Treatm	nent	Within	LONG CO.	- Land
Tree No.	Photo No.	Botanical Name	Chanase Hame	LCSD/RGD	DBH Im)	Height (m)	Spread (m)	a	ř.			P	D	G		P E	6	Œ.	P	8	4	£.	Status	fleteln/. Trans	Tions	Trans/	Site	Justification	Remarks
1235	T235	Aleumes molucciona	208	LCSD	0.490	9	6		1.		1				7			1				1	common	1				N/A	Co-dominant branches; cavity on trunk; pruning wound
T236	T236	Alcuntes multiceand	6/8	LCSD	0.390	_ X:			5		1	7 7	=		t.			1.6	1.1		=	10	common	3				N/A	Co-dominant branches, Wound on branch
1237	T237	Aleuntes motucquad	石橋	UCSD.	0.240	7	4		1		1				1.			W.			7.4	1	common	7				N/A	Co-dominant branches, slightly leaning
1238	7238	Alcurites molucciona	西鄉	LCSD	0.290	6	4		.1		1			\neg	1			=1				4.	common	10				N/A	Leaning low stem
T239	T239	Aleurites molluccuno	50	účsti	0,300	7	4		3		1				1			0		П		1	common	1				R/A	Co-dominant branches; dead branches, pruning scars on primary branches
T240	T240	Aleumes maluccana	88	LCSD	0,340	6	4		3		. 1				3.			JAI.			rail	30.7	common	1.3.				N/A	Co-dominant branches, wounded roots; included bark
T241	T241	Aleurites maluccana	708	UCSD.	0.240	5	-5		1		1				1			100			10.0		-bamman	. 7				N/A	N/A.
T242	7242	Aleurites maluccana	129	LCSD	0.280	5	4		1		1			7	V-			1				100	common	1				N/A	Leaning form
T243	T243	Aleumies molluciona	500	LCSO	0.226	6	1		3	- 1	,		-		4			1.				9.	common	1				N/A	N/A
T244	T244	Alcuntes moluccina	石學	LCSD	0.240	5	3		2	10	. 1				7			- U		- 1	10,11	1	common			-		N/A	Leaning form
1245	T245	Aleantes malucçuna	- 石庫	VCSD	0.370	6	4		1		1				1			(1)				1	common	1				N/A	Co-dominant branches; Included bark
1246	T246	Aleuntes moluccana	GR.	LCSD	0.440	7	5		1		1				1			11.				10	common	- 4				NA	Co-dominant branches; included bark
T247	T247	Aleumes malustand	59	LCSD	0.340	6.	4		1	14	1	1		\top	t-	-		0	-			F .	termin	2 -			1	N/A	Co-dominant trunks
1248	T246	Celtis sinensis	1149	CCSD	0.580	6	. 0			4	1			1	Ĺ			1		- 1		1	common	31				N/A	Co-dominant branches; bending trunk; restricted roots; contorted for asymmetric canopy
T249	T249	Alcuntes moluccona	- BM	UC30	0.350	7	- 3		1.		1				(1.				0	conmon					N/A	Wound on trunk
1250	7250	Aleurites maluccina	599	LCSD	0.330	6	4		3	-1	1				1			1				- 6	common	-1-				N/A	Wound on trunk
T25.7	T251	Aleumes maluccana	2個	LCSD	0.410	7	4		5		1				1			1				7	common	7				N/A	Wound on trunk
T252	T252	Ficus benjamina	商益物	LCSD	0.250	8	5		1.		1				4			1.1				0.	common	1.34				N/A	N/A.
T253	7253	Aleurites maluc cana	1509	FC20	0.390	-7	4	-1	-1-	-1-	1		-		1	-		-)-				-1-	Датитион	1				N/A	N/A
T254	T254	Aleumes monuceana	250	LCSO	0,250	6	4		1		1				1			1				Ÿ	common	3				N/A	Leaning asymmetric canopy
T255	T255	Яви тістрапра	組幣物	LCSD	0.250	5	3		3		1		4	-	7			10				0.	Eservision	3.1				N/A	Asymmetric canopy
1736	T256	Albarites maluccond	石栗	LCSD	0,446	10	- 5			4	1				1.			1				1.	common	1				N/A	Co-dominant branches; Wound on branch
1257	T257	Syrygium jambas	38%	LCSD	0.150	6	4	-	Ť	10	. 1		-		1			11	1		h 1	-i	common	1		-	-	tuh	N/A
T258	T258	Aleuntes moluceana	石原	LCSD	0,420	11	- 6		1		1				7			1.				80	common	3				N/A	N/A.
1259.	T259	Albizia lebbesk	大師多數	LCSD	0.190	7:	1		T.		1				1		П	=1				8-	bonimon	1)				N/A	Asymmetric carriopy
T260	T260	Roystoned regia	大王原刊(王栋)	LCSD	0.290	9	4		1		1			i				U.				1	common					NA	N/A
T261	7261	Melia azedarach	378	LCSD	0.600	2	34.		4		1				3			101				31	common	11			17	N/A	Restricted roots
1262	T262	Leucaena leucocephala	930	HyD	0.230	6	4			1	1				1				1			-1	common			1	14	6	Unble to label; included bank leanig form
1263	T263	Morus alba	9	Hyo	0 350	4	2	П		1	1			T	1		П	1				1	towwood	Ŷ			70	N/A	Unble to label: Topped
1204	T264	Mélia azedarach	音棟	LCSD	0.400	- 11	7		7		1	11			it.			11.47			17,271	10	territion	10.7				N/A	Unble to labely Rooting area cannot be reached
T265	T265	Critis sinerals	科数	Hyb	0,190	5	5		1	- 1		1			1		1 =	10		11	15.1	1	- barrimon	1			110	N/A	Unble to label; contorted; severely leaning
1266	T266	Macarangu tanarius vac Jerannosa	加料	HyO	0.150	41	4			1	1				1			1				-1-	common				1	N/A	Unble to label
T267	T267	Caryota mitis	短標的能源	Hyp	0.150	6	4		A.	100	1				1.00			10	147	3.1		10	common	1			3	N/A	Unble to label

				Jurisdiction		Sorvey S	ite		Form		He	elth Çor	sdition	Sto	uctura	Condition	in	Ameni	ity Valu	•		loitability ransplant		Conservation	Prop	geed Treatm	ment	Within	land.	
ié No.	Photo No.	Botunical Name	Chinese Name	LCSD/RGDI	DBH Im)	Height (m)	Spread/m	a a	*		6	ē	P	D 6	1			6	Œ.	P	н		L.	Status	fletein/ Trans	Tions	Trans/	Site	Justification	Remarks
268	T268	Macaranga tavarlus var. tomentosa	mile	Hyp	0,390	5	3		J.	T.		1				1			30				1.	common	DO:				N/A	Unble to label
T269	T269	Macaranga tananus var. Terrumtosa	migra	HyD	0.130	4	z			1		i				t .			100				10	common	1.1			TX	N/A	Unble to label
T270	T270	Mocoranga tanànas var. tomentosa	inst	HyD.	0.140	3	. 5		ir ii	1		1				1.			W		7+		1.	common	7			10	N/A	Unble to label
1271	7271	Macaranga tunarius var. tomentoja	10.64	HD	0.170	4	3			1		1				1			1				=1"	common	15			17	N/A	Unble to label; flooting area cannot be reached
1272	T272	Celtis simensis	RW.	HyD	0.180	5	- 4		5	П		1				Ť						7.0	30	common	7			T	N/A	Unble to label; Rooting area cannot be reached
1273	7273	Cultis sinensis	作棚	150	0.300	9	5		1	-		Y				Y			3				- Y-	common	- Y			Υ.	N/A	Unble to label: Rooting area cannot be reached
T274	T274	Macaranga tanarius yar, tementosa	面侧	HyD	0,140	4				1		1			Т	1	T		-)				-11	gamman	1				N/A	Unble to label; Multiple trunks: Epicormics
T275	T275	Macalunga tananus var. tomentosa	血網	нур	0,150	5	4		= 1	1		1				1			10	111	9.1	-	1	common	7			1.	N/A	Unble to label
1276	T276	Mocaranga fanarius var. fornimto ja	Finit	HyD	0.260	3.	3	100	p 4	4		1			4	T			×Đ.	$i \in \mathcal{C}$	0.1	10, 11	-10	EDENMON	1 -			4.	N/A	Unble to label
1277	1277	Macaranga tanarius var. lumentosa	mee	Hyp	0.140	- 3	2			1		1				Ť.			1		14		1	common	1			-4	N/A	Unble to label
1278	T278	Macraranga fanarius var. tomentosa	m#	Hyp	0.150	5	5		i ja	1.		1				1			10				-1/	common	1			7.	N/A	Unble to label
T279	T279	Macaronga tananus var. Tomentosa	抽槽	190	0.120	Z	7			1.		Ť				t-			10			N/V	1	common	3.0			1.	N/A	Unble to label
T260	T280	Monusalba	- 6	HyD.	0.350	4	.4		100	1-		1				1			T)		4		- 15	countaion	1			18.7	N/A	Unble to label: Restricted roots
1261	T281	Caryota ochlandra	MMM	Hyb	0.110	3	2		1			1				1.			1			7.1	-Á	tommon	1			1/1/	N/A	Unble to label
12R2	7282	Utsea glutinasa	高标图	Hyp	0.140	6	- 4		1			1				T.			(3)	14	114	100	10.	temmon	3				N/A	Unble to label Restricted roots
T263	T283	Melia azedorach	2.8	150	0.270	6	-5)	-		1				1			1	H	1.4		1.0	-bamman	- V			9.0	N/A	Unble to label; Restricted roots
T284	T284	Melia azedarachi	38	Hyb	0.290	5	4		1)			1				t	T						$-A \vdash$	annman	t			1407	N/A	Unble to label, Restricted roots
T265	T285	Melia azedaroch	- 39	150	0,390	8	1	-	1			1				P			$= f_{\mathcal{S}}$		+-	plot	T.	common	1			3.	NA	Unble to label; Restricted roots
T256	T286	Melia azedarach	38	HyD	0.300	7	3		1	Н.,		1				1			10	14		10	10	pommon	3			1	N/A	Unble to label
T287	T287	Melia azedorach	898	HyD	0.180	3	-2		-1			1				1.			=).				=1.	common	11			14	N/A	Unble to label
1268	T288	Macaranga fanarius var. tomentosa	m#i	Hyp	0,160	4	4			4.		1				1			1	Н	34		1	common	1				N/A	Unble to label; Wound on trunk
T289	T289	Celtis sinersis	15-80	HyD	0.230	\$	S		3	I.		i				ti I						1.1	36.	tommon	- T-			. 1	N/A	Unble to label; Asymmetric crown; Climber
1290	T290	Melia azedorach	安原	HyD	0.220	5	- 5		1			1				1			1				1.	countries	1			(1)	N/A	Unble to label; Climber; leaning form; asymmetric canopy
1291	T291	Melia azedoroch	2.9	Hyp	0.250	9	4		3-			1				1			1				1.	common	Υ			71	N/A	Unble to label; Climber
T292	T292	Melia azedarach	省標.	нур	0.440	10	7		2	10		1				1			00	11			10.	toomon	0.1			T.E.	N/A	Unble to label
1293	T293	Melia azedorach	811	Нур	0.120	5	- 2		1			1				1:			=12				1.	common				f.	N/A	Unble to label; climber; asymmetric canopy
T294	T294	Melia apedoroch	XW	њо	0,140	6	4		1			1				1			1				1.	common	1			TV.	N/A	Unble to label; climber, asymmetric carropy
180A.	T180A	Servici Scimed	B0738	НуΩ	0,300	6	3		10.11	Y		1				1			0			112	30.	termon		1		T	C/D/E/F	Unble to label; Asymmetric crown
		1					1	0	265	29	0	293	1	0 67	2	24 3		6	287	1	0	52	242		146	31	112	255		
								0%	90%	10%	0%	100%	0%	25	6 7	6% 1	90 09	25	97%	1%	0%	18%	82%		50%	10%	40%	87%		294
								G			a	F	р	0 6		, ,	2 6	G	100	P	(8)		X,	Conservation Status	Artain/	Trans	Trans i	Within Site		Surveyed Total no. of trees.

Legend

Tree Condition / Health		Tree Form		itural lition	Suitability for Transplantation
6	Good		G	Good	Hig
F	Fair		F	Fair	Med
P	Poor.		P	Poor	Low Survival Rate expected after
D	Dead				2000 000 000000000000000000000000000000
Amenity Value					
E	Excellent				
G	Good				
F .	Fair				
P	Poor				
		poor health, poor	condition a	nd poor for	TL.

Conservation Status

Conservation status (indicates rarity and protection viatus under relevant ordinances of a species in Hong Kong, References such as Rare and Percious Plants of Hong Kong, the IUCN Bed List of Threatened Species and the Forests and Countrylide Ordinance (Gas. 96) are used.)

Justification of Tree Transplanting / Felling

- A Existing dead tree .
- B. Existing tree is in conflict with the proposed scheme
- C Existing tree is in conflict with the proposed internal circulation and EVA
- Recommend to fell as the existing tree has an anticipated low survival rate if transplanted.
- E Tree growing in close proximity to other trees, asymmetrical roots and accessibility.

 F Existing tree has leaning form and broken or damaged branches and trunk.
- Existing tree has leaning form and broken or dama
 Existing tree is invasive weed species.

Top of Soil Level at the base of the tree

This figure refers to the soil level at the base of the tree to be maint. This figure refers to the soil level at the base of the tree to be maintained following the development of the The future soil level should not cover the root collar of the tree.

Tree Girth

- * Girth of a tree refers to its trunk circumference at breast height (i.e. measured at 1.3m above ground level)
- ** Girth of a tree refers to its trunk chumference at breast height (i.e. trees with multitrunk branching were all measured seperately at 1m above ground level). The collective girth was then calculated using the methodology set Conservation Practice Note No. 02/2003, Measurement of Diameter at Breast Height (DBH).

Annex IV

Photographic Record of Existing Trees



T01 (Acacia confusa)Photograph showing the overall form of the tree.



T02 (Acacia confusa)Photograph showing the overall form of the tree.



T03 (Ficus benjamina)Photograph showing the overall form of the tree.



T04 (Aleurites moluccana)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T05 (Ficus benjamina)Photograph showing the overall form of the tree.



T06 (Aleurites moluccana)Photograph showing the overall form of the tree.



T07 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T08 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV







T11 (Bombax ceiba) Photograph showing the overall form of the tree.



T10 (Sterculia lanceolata) Photograph showing the overall form of the tree.



T12 (Grevillea robusta) Photograph showing the overall form of the tree.

07/06/202

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T13 (Ficus benjamina)
Photograph showing the overall form of the tree.



T14 (Ficus benjamina)
Photograph showing the overall form of the tree.



T15 (Murraya paniculata)
Photograph showing the overall form of the tree.



T16 (Podocarpus macrophyllus)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T17 (Caryota mitis)
Photograph showing the overall form of the tree.





T19 (Ficus microcarpa)
Photograph showing the overall form of the tree.



T20 (Michelia x alba)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV







T23 (Podocarpus macrophyllus) Photograph showing the overall form of the tree.



T22 (Dypsis lutescens) Photograph showing the overall form of the tree.



T24 (Acacia confusa) Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T25 (Podocarpus macrophyllus)
Photograph showing the overall form of the tree.



T26 (Ficus benjamina)Photograph showing the overall form of the tree.



T27 (Podocarpus macrophyllus)Photograph showing the overall form of the tree.



T28 (Ficus benjamina)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T29 (Podocarpus macrophyllus)Photograph showing the overall form of the tree.



T30 (Ficus benjamina)
Photograph showing the overall form of the tree.



T31 (Garcinia subelliptica)
Photograph showing the overall form of the tree.



T32 (Livistona chinensis)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REY





T33 (Livistona chinensis)
Photograph showing the overall form of the tree.



T35 (Livistona chinensis)
Photograph showing the overall form of the tree.



T34 (Livistona chinensis)Photograph showing the overall form of the tree.



T36 (Livistona chinensis)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T37 (Livistona chinensis)Photograph showing the overall form of the tree.



T38 (Livistona chinensis)
Photograph showing the overall form of the tree.



T39 (Livistona chinensis)Photograph showing the overall form of the tree.



T40 (Livistona chinensis)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T41 (Livistona chinensis)Photograph showing the overall form of the tree.



T43 (Callistemon viminalis)Photograph showing the overall form of the tree.



T42 (Livistona chinensis)Photograph showing the overall form of the tree.



T44 (Callistemon viminalis)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T45 (Aleurites moluccana)Photograph showing the overall form of the tree.





T47 (Ailanthus fordii)Photograph showing the overall form of the tree.



T48 (Ailanthus fordii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T49 (Ailanthus fordii)Photograph showing the overall form of the tree.



T51 (Ailanthus fordii)
Photograph showing the overall form of the tree.



T50 (Ailanthus fordii)
Photograph showing the overall form of the tree.



T52 (Ailanthus fordii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T53 (Ailanthus fordii)Photograph showing the overall form of the tree.



T55 (Caryota ochlandra)Photograph showing the overall form of the tree.



T54 (Ficus benjamina)
Photograph showing the overall form of the tree.



T56 (Callistemon viminalis)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T57 (Syzygium jambos)Photograph showing the overall form of the tree.



T58 (Syzygium jambos)
Photograph showing the overall form of the tree.



T59 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T60 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.

	SCALE	N.T.S.	DATE	Jun 2021
Γ	CHECKED	CJF	DRAWN	FY
F	FIGURE NO.	URA	AP005 TSR	REV





T61 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T62 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T63 (Ravenaia madagascariensis)
Photograph showing the overall form of the tree.



T64 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T65 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T66 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T67 (Livistona chinensis)Photograph showing the overall form of the tree.



T68 (Livistona chinensis)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T69 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T70 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T71 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T72 (Ravenaia madagascariensis)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T73 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T74 (Ravenaia madagascariensis)Photograph showing the overall form of the tree.



T75 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T76 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T77 (Caryota ochlandra)Photograph showing the overall form of the tree.



T78 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T79 (Aleurites moluccana)Photograph showing the overall form of the tree.



T80 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	RE





T81(Aleurites moluccana)Photograph showing the overall form of the tree.



T82 (Aleurites moluccana)Photograph showing the overall form of the tree.



T83 (Aleurites moluccana)Photograph showing the overall form of the tree.



T84 (Aleurites moluccana)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T85 (Choerospondias axillaris)Photograph showing the overall form of the tree.



T87 (Aleurites moluccana)Photograph showing the overall form of the tree.



T86 (Ailanthus fordii)
Photograph showing the overall form of the tree.



T88 (Bombax ceiba)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T89 (Bombax ceiba)Photograph showing the overall form of the tree.



T91 (Melaleuca quinquenervia)Photograph showing the overall form of the tree.



T90 (Bombax ceiba)Photograph showing the overall form of the tree.



T92 (Grevillea robusta)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T93 (Melaleuca quinquenervia)Photograph showing the overall form of the tree.



T94 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T95 (Spathodea campanulata)Photograph showing the overall form of the tree.



T96 (Ficus virens)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T97 (Lagerstroemia speciosa)Photograph showing the overall form of the tree.



T98 (Lagerstroemia speciosa)Photograph showing the overall form of the tree.



T99 (Ficus microcarpa)Photograph showing the overall form of the tree.



T100 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV







T103 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T102 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T104 (Senna siamea)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T105 (Senna siamea)
Photograph showing the overall form of the tree.



T106 (Senna siamea)
Photograph showing the overall form of the tree.



T107 (Senna siamea)
Photograph showing the overall form of the tree.



T108 (Callistemon viminalis)
Photograph showing the overall form of the tree.

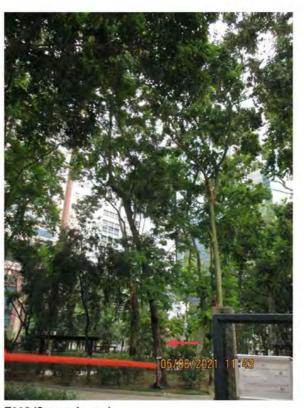
SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV







T111 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T110 (Senna siamea)
Photograph showing the overall form of the tree.



T112 (Corymbia torelliana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	RE





T113 (Ficus benjamina)
Photograph showing the overall form of the tree.



T114 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T115 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T116 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T117 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T118 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T119 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T120 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T121 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T122 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T123 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T124 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T125 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T126 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T127 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T128 (Corymbia torelliana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T129 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T130 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T131 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T132 (Corymbia torelliana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T133 (Bauhinia x blakeana)
Photograph showing the overall form of the tree.



T135 (Melia azedarach)
Photograph showing the overall form of the tree.



T134 (Jacaranda mimosifolia)
Photograph showing the overall form of the tree.



T136 (Melia azedarach)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T137 (Melia azedarach)
Photograph showing the overall form of the tree.



T138 (Callistemon viminalis)
Photograph showing the overall form of the tree.



T139 (Callistemon viminalis)
Photograph showing the overall form of the tree.



T140 (Melaleuca quinquenervia)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T141 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T142 (Melia azedarach)
Photograph showing the overall form of the tree.



T143 (Ficus microcarpa)
Photograph showing the overall form of the tree.



T144 (Ficus benjamina)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T145 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T146 (Corymbia torelliana)
Photograph showing the overall form of the tree.



T147 (Melaleuca quinquenervia)Photograph showing the overall form of the tree.



T148 (Phoenix roebelenii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T149 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T150 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T151 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T152 (Melia azedarach)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T153 (Bombax ceiba)
Photograph showing the overall form of the tree.



T154 (Melaleuca quinquenervia)
Photograph showing the overall form of the tree.



T155 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T156 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	RE





T157 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T158 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T159 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T160 (Phoenix roebelenii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T161 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T162 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T163 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T164 (Melia azedarach)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV



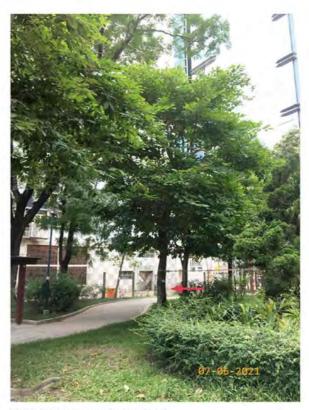




T167 (Lagerstroemia speciosa) Photograph showing the overall form of the tree.



T166 (Lagerstroemia speciosa) Photograph showing the overall form of the tree.



T168 (Lagerstroemia speciosa) Photograph showing the overall form of the tree.

05/06/2021 12:15

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T169 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.



T170 (Juniperus chinensis 'Kaizuca'
Photograph showing the overall form of the tree.



T171 (Elaeocarpus obtusus subsp. Apiculatus)
Photograph showing the overall form of the tree.



T172 (Lagerstroemia speciosa)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T173 (Bauhinia variegata)
Photograph showing the overall form of the tree.



T174 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T175 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T176 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T177 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T178 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T179 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T180 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T181 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T182 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T183 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T184 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T185 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T186 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T187 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T188 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T189 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T190 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T191 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T192 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T193 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T194 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T195 (Terminalia catappa)
Photograph showing the overall form of the tree.



T196 (Ficus benjamina)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T198 (Ficus elastica)
Photograph showing the overall form of the tree.



T200 (Phoenix roebelenii)Photograph showing the overall form of the tree.



T199 (Phoenix roebelenii)
Photograph showing the overall form of the tree.



T201 (Phoenix roebelenii)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T202 (Phoenix roebelenii)Photograph showing the overall form of the tree.



T203 (Ficus elastica)
Photograph showing the overall form of the tree.



T204 (Corymbia torelliana)Photograph showing the overall form of the tree.



T205 (Juniperus chinensis 'Kaizuca')Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV

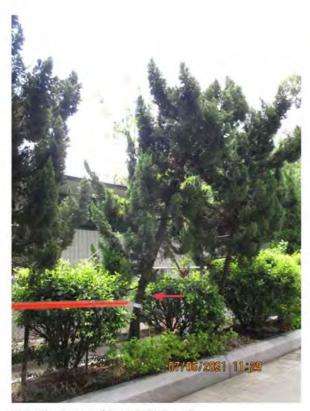




T206 (Juniperus chinensis 'Kaizuca')Photograph showing the overall form of the tree.



T207 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.



T208 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.



T209 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T210 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.



T211 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.



T212 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.



T213 (Juniperus chinensis 'Kaizuca')
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





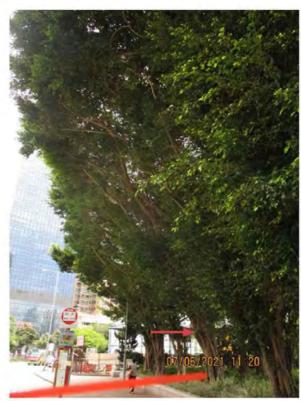
T214 (Ficus benjamina)Photograph showing the overall form of the tree.



T216 (Ficus benjamina)Photograph showing the overall form of the tree.



T215 (Ficus benjamina)
Photograph showing the overall form of the tree.



T217 (Ficus benjamina)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T218 (Ficus benjamina)Photograph showing the overall form of the tree.



T219 (Ficus benjamina)
Photograph showing the overall form of the tree.



T220 (Ficus benjamina)
Photograph showing the overall form of the tree.



T221 (Roystonea regia)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T222 (Terminalia mantaly)Photograph showing the overall form of the tree.



T223 (Roystonea regia)
Photograph showing the overall form of the tree.



T224 (Araucaria heterophylla)Photograph showing the overall form of the tree.



T225 (Phoenix roebelenii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T226 (Roystonea regia)Photograph showing the overall form of the tree.



T227 (Roystonea regia)
Photograph showing the overall form of the tree.



T228 (Roystonea regia)
Photograph showing the overall form of the tree.



T229 (Phoenix roebelenii)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T230 (Roystonea regia)Photograph showing the overall form of the tree.



T231 (Roystonea regia)Photograph showing the overall form of the tree.



T232 (Roystonea regia)
Photograph showing the overall form of the tree.



T233 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T234 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T235 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T236 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T237 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR		EV





T238 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T240 (Aleurites moluccana)Photograph showing the overall form of the tree.



T239 (Aleurites moluccana)Photograph showing the overall form of the tree.



T241 (Aleurites moluccana)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T242 (Aleurites moluccana)Photograph showing the overall form of the tree.



T243 (Aleurites moluccana)Photograph showing the overall form of the tree.



T244 (Aleurites moluccana)Photograph showing the overall form of the tree.



T245 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T246 (Aleurites moluccana)Photograph showing the overall form of the tree.



T247 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T248 (Celtis sinensis)Photograph showing the overall form of the tree.



T249 (Aleurites moluccana)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	RE





T250 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T252 (Ficus benjamina)
Photograph showing the overall form of the tree.



T251 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T253 (Aleurites moluccana)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR	REV	





T254 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T255 (Ficus microcarpa)
Photograph showing the overall form of the tree.



T256 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T257 (Syzygium jambos)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T258 (Aleurites moluccana)
Photograph showing the overall form of the tree.



T259 (Albizia lebbeck)
Photograph showing the overall form of the tree.



T260 (Roystonea regia)Photograph showing the overall form of the tree.



T261 (Melia azedarach)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR	REV	





T262 (Leucaena leucocephala)Photograph showing the overall form of the tree.



T263 (Morus alba)Photograph showing the overall form of the tree.



T264 (Melia azedarach)Photograph showing the overall form of the tree.



T265 (Celtis sinensis)
Photograph showing the overall form of the tree.

	SCALE	N.T.S.	DATE	Jun 2021
CI	HECKED	CJF	DRAWN	FY
FIG	URE NO.	URA	AP005 TSR	REV





T266 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T267 (Caryota mitis)Photograph showing the overall form of the tree.



T268 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T269 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.

	SCALE	N.T.S.	DATE	Jun 2021
CI	HECKED	CJF	DRAWN	FY
FIG	URE NO.	URA	AP005 TSR	REV





T270 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T271 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T272 (Celtis sinensis)Photograph showing the overall form of the tree.



T273 (Celtis sinensis)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR	REV	





T274 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T275 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T276 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 202	1
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR		REV





T278 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T279 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T280 (Morus alba)
Photograph showing the overall form of the tree.



T281 (Caryota ochlandra)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR	REV	





T282 (Litsea glutinosa)Photograph showing the overall form of the tree.



T283 (Melia azedarach)
Photograph showing the overall form of the tree.



T284 (Melia azedarach)Photograph showing the overall form of the tree.



T285 (Melia azedarach)
Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021	
CHECKED	CJF	DRAWN	FY	
FIGURE NO.	URA	AP005 TSR	RE	





T286 (Melia azedarach)Photograph showing the overall form of the tree.





T288 (Macaranga tanarius var. tomentosa) Photograph showing the overall form of the tree.



T289 (Melia azedarach)Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T290 (Melia azedarach) Photograph showing the overall form of the tree.



Photograph showing the overall form of the tree.



T292 (Melia azedarach) Photograph showing the overall form of the tree.



T293 (Melia azedarach) Photograph showing the overall form of the tree.

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV





T294 (Melia azedarach)Photograph showing the overall form of the tree.



T180A (Senna siamea)
Photograph showing the overall form of the tree.

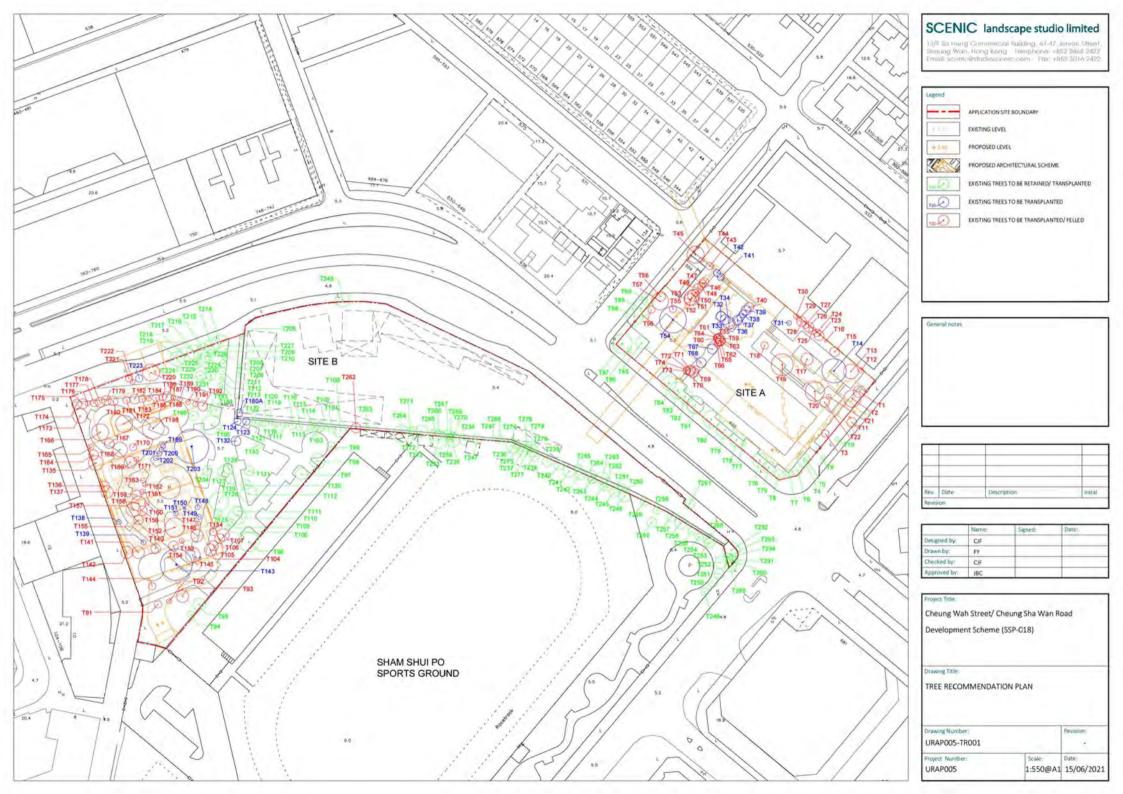
Cheung	Wah	Street/	Cheung	Sha	Wan	Road
De	velor	oment!	Scheme	SSP.	-018)	

SCALE	N.T.S.	DATE	Jun 2021
CHECKED	CJF	DRAWN	FY
FIGURE NO.	URA	AP005 TSR	REV

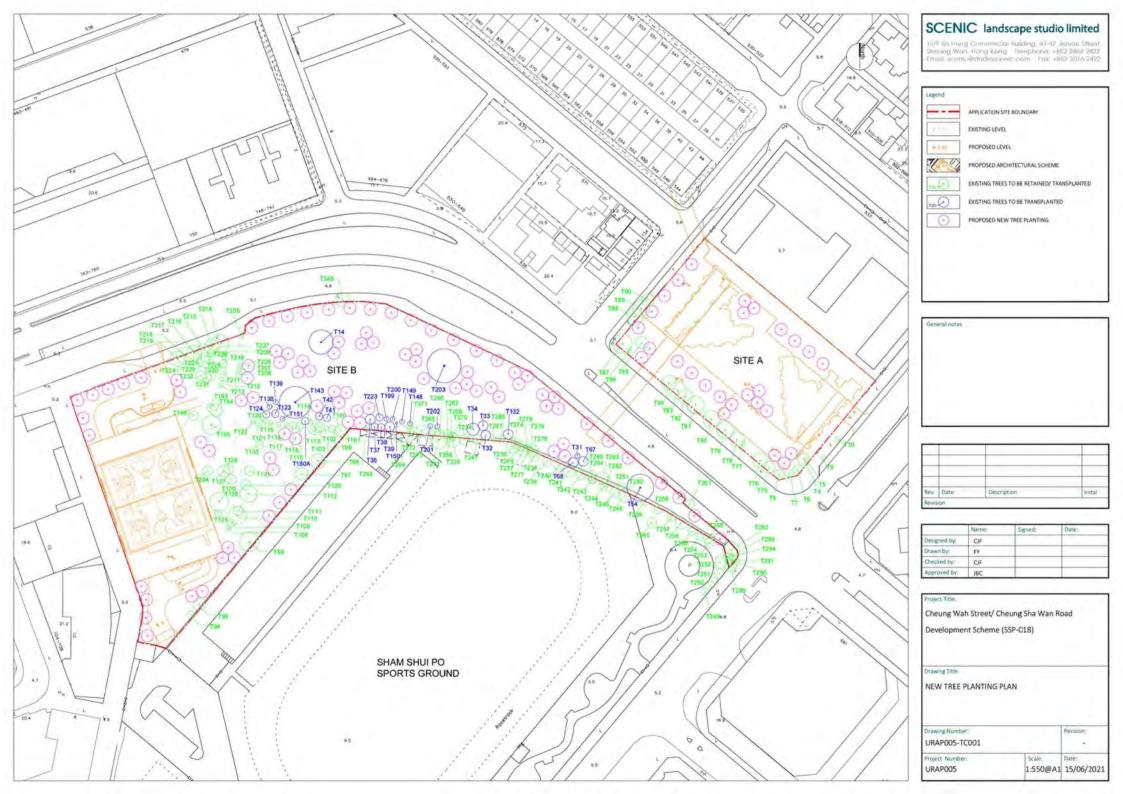


Annex V

Tree Recommendation Plan

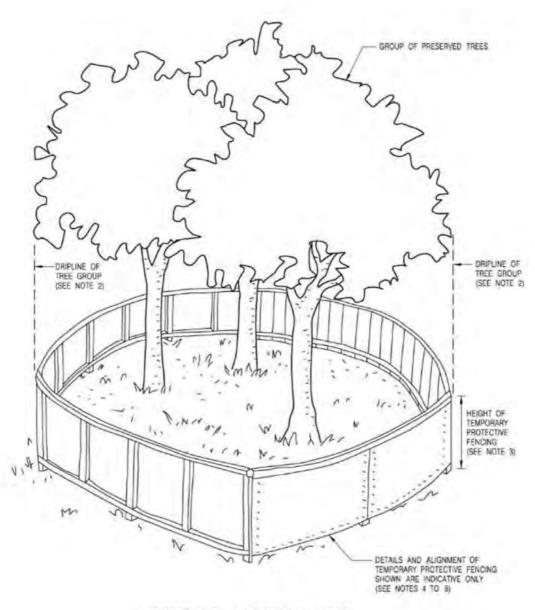


Annex VI New Tree Planting Plan



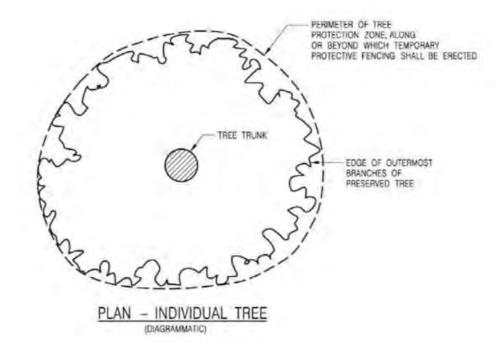
Annex VII
Tree Protection Measures

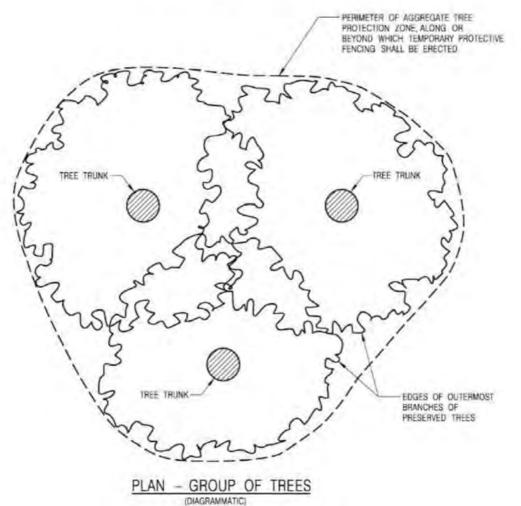
Tree Protection Measures

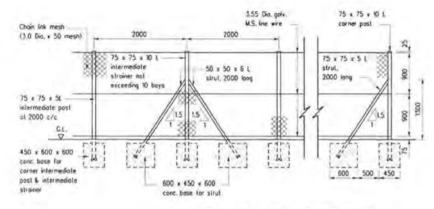


PERSPECTIVE - GROUP OF TREES

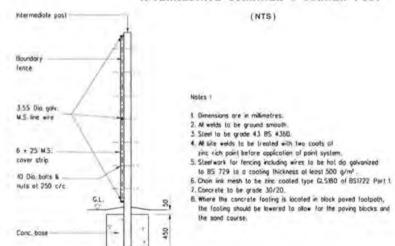
(DIAGRAMMATIC)





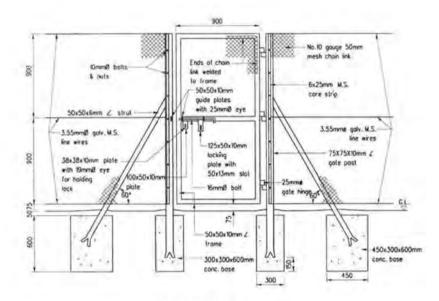


ELEVATION OF INTERMADIATE POST INTERMEDIATE STRAINER & CORNER POST



INTERMEDIATE POST

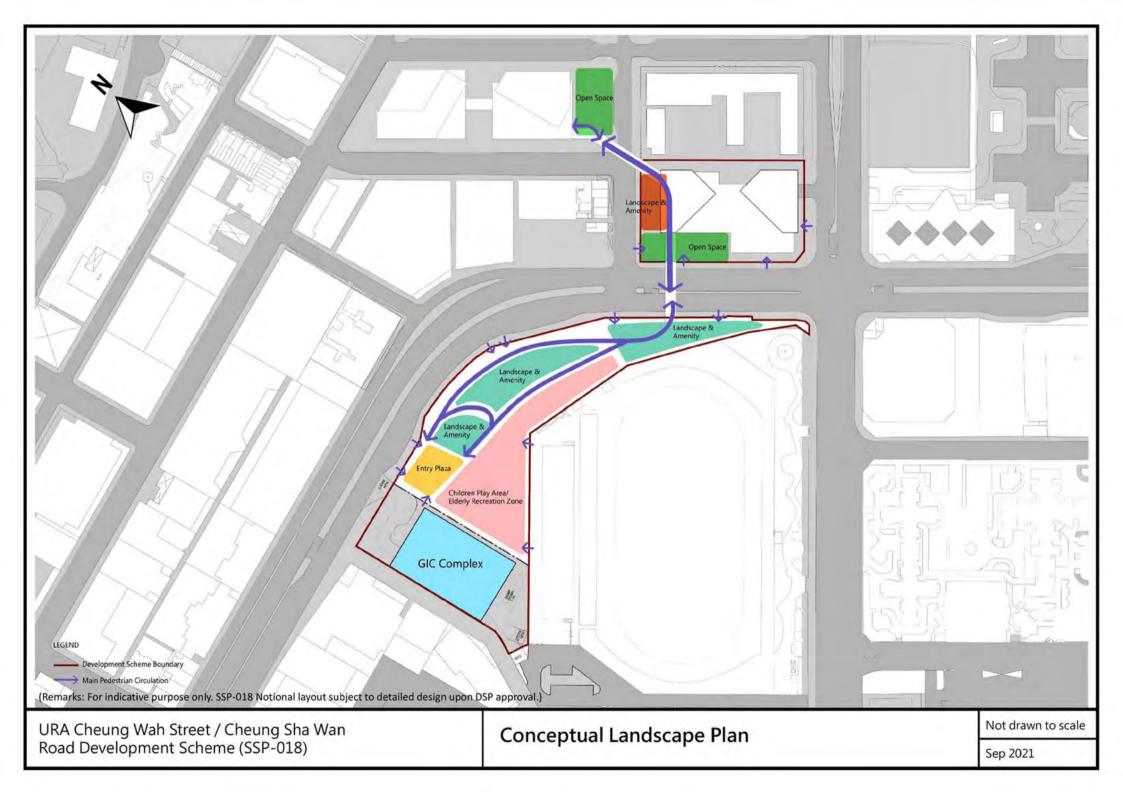
(NTS)



PEDESTRIAN GATE

Note: One pedestrian gate in each enclosure.

Annex VIII Landscape Design Concept



Appendix 3

Visual Impact Assessment (VIA) Report

Urban Renewal Authority Development Scheme

Prepared under Section 25 (3) of the Urban Renewal Authority Ordinance

Cheung Wah Street /
Cheung Sha Wan Road Development Scheme
(SSP-018)

Visual Impact Assessment
September 2021

Photomontages of VP3

Photomontages of VP4 Photomontages of VP5

Photomontages of VP6 Photomontage of VP7

Figure 4.7

Figure 4.8

Figure 4.9 Figure 4.10

Figure 4.11

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Figure 2.	2 Layout Plan of the Baseline Scheme
Figure 4.	1 The Assessment Area and Visual Elements
Figure 4.	2 Locations of Local Viewing Points
Figure 4.	3 Photos of Local Viewing Points
Figure 4.	4 Location of the Strategic Viewing Point (VP7)
Figure 4.	5 Photomontages of VP1
Figure 4.	6 Photomontages of VP2

1 INTRODUCTION

- 1.1 The Urban Renewal Authority (URA) has commenced Cheung Wah Street/ Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under Section 25 of the Urban Renewal Authority Ordinance (URAO). The draft Development Scheme Plan (DSP) No. S/K5/URA3/A is submitted to the Town Planning Board (the Board) for consideration.
- 1.2 The Scheme is located in Sham Shui Po (SSP) District which comprises Sites A and B along Cheung Sha Wan Road. Site A of the Scheme is broadly bounded by Hing Wah Street to the southeast, Cheung Sha Wan Road to the southwest, Cheung Wah Street to the northwest, and Cheung Sha Wan Catholic Secondary School to the northeast. It is currently occupied by the Cheung Sha Wan Sports Centre and a garden under Leisure and Cultural Services Department (LCSD). Site A is currently zoned for "Government, Institution or Community (G/IC)" with maximum building height of 1 storey and "Open Space (O)" on the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37.
- 1.3 Site B of the Scheme broadly bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground to the southeast. It is currently occupied by the Cheung Sha Wan Path Sitting-out Area, part of the Sham Shui Po Sports Ground under LCSD and a temporary maintenance depot of Highways Department. Site B is currently zoned for "Government, Institution or Community (G/IC)" with maximum building height of 1 storey, "Open Space (O)", and shown as "Road" on the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37.

- 1.4 Figure 1.1 shows the draft DSP. Under the draft DSP, the Scheme area in orange colour is proposed to be zoned "R(A)" with an overall plot ratio (PR) of 8.5 which PR of 7.5 is for domestic uses and the remaining PR of 1.0 is for non-domestic uses. About 5,197 sq.m. (PR of 1.0) non-domestic GFA is also proposed for G/IC uses in the Scheme area which is to be exempted from PR calculation under the draft DSP. A maximum height of 140mPD is proposed at Site A under the draft DSP. For Site B, the scheme area in green is proposed to be zoned "O" while the scheme area in blue is proposed to be zoned "G/IC". A maximum building height of 95mPD is proposed for the "G/IC" uses.
- 1.5 This Visual Impact Assessment (VIA) report is prepared to study the potential visual impact with the implementation of the Scheme under the notional design for consideration by the Board.

2 THE PROPOSED SCHEME

- 2.1 As stated in the Planning Report of the DSP submission, a street block at Kim Shin Lane / Fuk Wa Street (namely SSP-017) comprising 90 building blocks of age over 60 with no lifts is identify as a site with imminent redevelopment needs. However, SSP-017 is undesirable for redevelopment because its existing plot ratio is as high as 8.12, hence, the residual plot ratio is 0.88 only. Multiple subdivided units are also identified. Although SSP-017 has all the quality to demand for redevelopment, its redevelopment potential is low. In this respect, a wider area for planning opportunities have to be explored.
- 2.2 Under a "planning-led" approach in urban renewal works in recent years, URA has identified part of Sham Shui Po as Sham Shui Po Action Area 1 (SSPAA1) for holistic planning of urban renewal works. SSP-018 comprises Sites A and B, both Government land opposite each other across Cheung Sha Wan Road is identified for redevelopment to formulate a comprehensive land-use restructuring together with SSP-017 to create more planning gains at district level. The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017.
- 2.3 As SSP-017 and SSP-018 are interrelated and are commenced on the same day, the Proposed Scheme of this VIA report will also consider the cumulative impact of the SSP-017 and SSP-018 redevelopment. It is noted that SSP-017 conforms to the existing planning control, it will be implemented under Section 26 of the Urban Renewal Authority Ordinance (URAO) separately; it does not form part of this DSP.
- 2.4 Figure 2.1 shows the layout plan of the notional design (the Proposed Scheme). Site A of SSP-018 comprises two residential towers (T1 and T2) on top of a commercial/ retail/ G/IC podium, a public open space (POS), and a basement car park for public and ancillary parking spaces. For Site B of SSP-018, it comprises one G/IC complex building and a POS.
- 2.5 A maximum building height of 140mPD is proposed at Site A to enhance flexibility on block size, disposition and layout in building design, enable a slimmer building form and create wider building separations as recommended in the Sustainable Building Design Guidelines. Ground floor setbacks from Cheung Wah Street, Cheung Sha Wan Road and Hing Wah Street are

- proposed to mitigate visual obstruction, create wider pavement and enhance walking environment. A maximum building height of 95mPD is proposed at Site B to utilize the site for G/IC uses. About 750 sq.m. of POS at Site A and 9,600 sq.m. of POS at Site B are also proposed to enhance the visual amenity.
- 2.6 A maximum building height of 120mPD is proposed at SSP-017, which conforms to the existing planning control. SSP-017 comprises two residential towers on top of a commercial/ retail podium. Ground floor setbacks from Cheung Wah Street is also proposed in SSP-017 to mitigate visual obstruction, create wider pavement and enhance walking environment. Under an integrated urban renewal approach, footbridges across Cheung Sha Wan Road and Cheung Wah Street, which do not form part of the Scheme, are suggested to connect up the public open spaces at both URA projects (SSP-017 and SSP-018) to enhance connectivity of the existing built environment.
- 2.7 The notional design is subject to change at the detailed design stage.
- 2.8 **Table 2.1** presents the development parameters of the Proposed Scheme:

Table 2.1 Development Parameters of SSP-018

	Site A	Site B
Scheme Total Area	About 5,197 sq.m.	About 13,857 sq.m.
Net Site (subject to survey and detailed design)	About 5,197 sq.m.	About 4,212 sq.m.
Proposed Zoning	"R(A)"	"G/IC", "O"
Proposed Maximum Domestic GFA	About 38,978 sq.m. (PR=7.5)	1
Proposed Maximum Non-domestic GFA (excluding GFA for G/IC Provision)	About 5,197 sq.m. (PR=1.0)	/
Proposed G/IC GFA G/IC Provision	Not less than 5,197 sq.m. (PR=1.0) (proposed to be exempted from GFA calculation under the DSP)	About 33,696 sq.m. (PR=8.0)
Proposed Public Open Space	About 750 sq.m.	About 9,645 sq.m.
Number of Blocks *	2	1 (G/IC Complex)

	Site A	Site B	
Building Height *	Not more than 140mPD	Not more than 95mPD	
Number of storeys *	About 34 storeys (on top of a 5-storey podium)	About 18 storeys (excluding basements)	

^{*} Remarks: All design parameters are subject to change at the detailed design stage.

- 2.9 To comprehensively compare the visual impact of the Proposed Scheme, a Baseline Scheme is also presented on Figure 2.2. Under the Baseline Scheme, no building will be erected on the scheme area where is zoned either "O" or "Road". Two 1 storey buildings of 12m tall under existing "G/IC" zone within the boundary of SSP-018 Sites A and B are adopted in the Baseline Scheme to reflect the possible redevelopment. For SSP-017, existing buildings are adopted in the Baseline Scheme to reflect the cumulative impact before and after redevelopment.
- 2.10 This VIA will compare the visual changes of both the Proposed Scheme and the Baseline Scheme and thus appraise the visual impact.

3 METHODOLOGY

- 3.1 With reference to the Town Planning Board Guidelines on Submission of Visual Impact Assessment for Planning Application to the Town Planning Board (TPB-PG No.41), this VIA would adopt the following procedures:
- 3.2 1) Define the assessment area (i.e. visual envelope). The assessment area would cover the area of visual influence within which the proposed development is pronouncedly visible from key sensitive viewers. The extent of the assessment area would be determined having regard to the size of the proposed development, the distance of the development, potential visibility from the selected viewing points, and the actual site and the surrounding topographical conditions.
- 3.3 2) Identify Viewing Points (VPs) within the assessment area. The assessment would take into account views from key local and strategic viewing points. Local VPs are determined with reference to the setting of the project and views of local significance. For strategic VP(s), reference would be made to Chapter 11 Urban Design Guidelines in the Hong Kong Planning Standards and Guidelines (HKPSG). VPs should be at human eye level for a realistic presentation of views. For each identified VPs, their sensitivity would be classified as high, medium or low by their activity, public perception and other relevant factors.
- 3.4 3) Appraise visual changes. Visual changes on visual composition, visual obstruction, effect on public views and effect on visual resources would be appraised. Perspectives indicating visual changes will be illustrated by photomontages for each identified VPs.

4 VISUAL IMPACT ANALYSIS

4.1 ASSESSMENT AREA

4.1.1 The assessment area for this VIA is defined by the visual envelope of the indicative Proposed Scheme. This visual envelope covers the fields of views from all sensitive viewers in direct sight of the proposed development. With verification by ground inspection, for Site A, the assessment area is defined by a distance equal to three times of the height (3H) of T1 and T2 in the Proposed Scheme, i.e. 420m, away from Site A. For Site B, since the maximum building height of the G/IC complex is 95mPD, the assessment area is defined by a distance equal to three times of the proposed building height, i.e. 285m, away from Site B. The areas for Sites A and B are combined to form the assessment area of this VIA.

Visual Elements in the Assessment Area

- 4.1.2 Figure 4.1 shows the extent of assessment area. The area broadly extends to Ching Cheung Road to the north, Po On Road to the northeast, Cheung Sha Wan Playground to the southeast, Lai Chi Kok Road to the south and Cheung Lai Street to the west of the Scheme. Figure 4.1 and the following will present the current and future visual elements within the assessment area:
- 4.1.3 The assessment area is densely developed with increasing number of high-rise developments. To the immediate west of the Scheme is the Cheung Sha Wan business area where is mixed with high-rise office towers and mid-rise industrial buildings. Various developments reaching about 120mPD or above are located to the immediate northwest and southwest of the Scheme, including Billion Plaza II (about 130mPD), Billion Plaza (about 120mPD), Clifford Centre (about 125mPD) and Law's Commercial Plaza (about 130mPD). Besides, there are several future high-rise non-domestic developments of about 130mPD to the further northwest of the Scheme, including the proposed developments covered by planning applications nos. A/K5/816 and A/K5/820 approved by the TPB in 2020.

- 4.1.4 The northern and eastern sides of the assessment area is a densely developed residential area with prolonged redevelopment activities. The area comprises high-rise residential developments, mid-rise residential towers and low-rise tenement buildings. To the northeast of the Scheme is a group of residential developments reaching about 120mPD or above, including Beacon Lodge (about 160mPD), Lotus House (about 135mPD), Heya Aqua (about 120mPD), Heya Crystal (about 120mPD), Heya Star (about 120mPD) and Heya Delight (about 120mPD). The building height of the URA-initiated Kim Shin Lane/ Fuk Wa Street Development Project (SSP-017) located to the north of the Scheme is about 120mPD. To the east of the Scheme is Un Chau Estate with towers mainly of about 120mPD.
- 4.1.5 The southern side of the assessment area comprises various low-rise facilities but also buildings with high building heights. To the immediate south of the Scheme is Sham Shui Po Sports Ground, serving as the major public outdoor space in the vicinity. To the further south of the playground is the low-rise Cheung Sha Wan Temporary Wholesale Poultry Market. To the further southwest of the Scheme is a cluster of high-rise residential developments including The Pacifica of about 165 to 185mPD. On the other side of the Poultry Market, there is a future public housing development of about 150mPD planned by the Government at the Wang Cheong Factory Estate site where is adjacent to an existing residential development of about 150mPD named The Sparkle. To the further southeast of the Scheme is Fortune Estate and Hang Chun Court with towers mainly of about 80 to 120mPD.
- 4.1.6 Apart from Sham Shui Po Sportsground, there are also several public outdoor spaces located within the assessment area. To the southeast of Fortune Estate is Cheung Sha Wan Playground serving as a major open space to the neighbourhood. To the immediate east and further northwest of the Scheme are Hing Wah Street Playground and Wing Hong Street Rest Garden respectively.

4.1.7 To conclude, the assessment area is densely developed with increasing number of high-rise developments. Developments reaching 120mPD or above are common around the Scheme while there are several existing or future developments of about 140 to 185mPD, such as The Pacifica and the future public housing development at the Wang Cheong Factory Estate site. Three major public outdoor spaces and open-air facilities are identified, including Sham Shui Po Sportsground, Hing Wah Street Playground and Cheung Sha Wan Playground are identified to the south, east and southeast of the Scheme.

4.2 IDENTIFICATION OF VIEWING POINTS

4.2.1 Based on the assessment area and visual elements identified, six local viewing points (VPs) are identified within the visual envelope as indicated on Figure 4.2. All major public outdoor spaces are included in this assessment. Figure 4.3 then presents the location of the strategic viewing point identified with reference to the HKPSG.

Table 4.1 Viewing Points

VP	Location	Approximate Distance from the Scheme
Local	Viewing Points	
VP1	Hing Wah Street Playground	120m
VP2	Sham Shui Po Sports Ground	150m
VP3	Cheung Sha Wan Playground	400m
VP4	Junction of Cheung Wah Street and Un Chau Street	120m
VP5	Exit B1 of Lai Chi Kok Railway Station	180m
VP6	Wing Hong Street Rest Garden	220m
Strate	egic Viewing Point	
VP7	Sun Yat Sen Memorial Park	5.2km

4.3 APPRAISAL OF VISUAL CHANGES

4.3.1 Photos of the existing condition and photomontages of both the Proposed Scheme and the Baseline Scheme are prepared for full appraisal and comparison of the visual changes before and after the proposed redevelopment at the Scheme together with future developments within its vicinity. The following will describe the visual composition and appraise visual changes of views for each selected VP. Table 4.2 in the later part of this section will summarise the visual changes of all seven viewing points.

VP1 - Hing Wah Street Playground

4.3.2 In accordance with Figures 4.2, VP1 is about 120m to the east of the Scheme. Hing Wah Street Playground is a football pitch without any passive recreational facility. Although VP1 is close to the Scheme, considered that active football activities involve less public viewers who are sensitive to visual concerns and changes, the visual sensitivity of public viewers from this VP is graded as medium.

Visual Composition and Visual Obstruction

- 4.3.3 Figure 4.4 presents the existing visual composition of the view from VP1 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.4 With reference to Figure 4.4, the foreground of the view from VP1 is dominated by Heya Aqua (about 120mPD) and the football pitch of the Playground. Heya Aqua forms a substantial part of the visual composition of the view from VP1. The background of the view is formed by the dense urban development near Cheung Sha Wan Business Area, such as Billion Plaza (about 120mPD), Billion Plaza II (about 130mPD), Charming Garden (about 100mPD) and The Amused (about 100mPD). The local visual context is dense with buildings commonly reaching about 120mPD or above. An open sky view is available at VP1.
- 4.3.5 Under the Proposed Scheme, the proposed development at SSP-017 (about 120mPD) would be visible on the background of the view from VP1. The proposed T1 and T2 within the Scheme area would be visible in front of the dense urban developments near Cheung Sha Wan Business Area. With due regard to the local visual context, the proposed T1 and T2 are of compatible

and similar size and height, as compared to Heya Aqua and the proposed development at SSP-017. Although the Proposed Scheme would obstruct a portion of the open sky view, the obstruction is less substantial than the one caused by Heya Aqua.

- 4.3.6 Various mitigation measures are included in the Proposed Scheme to enhance the visual composition and obstruction. To minimize the blockage of views, the proposed T1 and T2 are disposed in an orientation parallel to the view towards the Scheme from VP1. The proposed maximum building height of 140mPD also enables a slimmer building form which further reduces the visual obstruction to the sky view. Ground floor setbacks from Hing Wah Street and Cheung Sha Wan Road will further reduce the building mass and visual obstruction, in particular at eye level.
- 4.3.7 With the above mitigation measures, despite the proposed development at the Scheme, a substantial portion of the open sky view from VP1 will be preserved. Furthermore, the visual permeability along Fuk Wing Street from VP1 will be preserved under the Proposed Scheme. Thus, a slightly adverse impact to the visual composition and obstruction is considered.

Effect on Public Viewers and Visual Resources

4.3.8 Noted that Hing Wah Street Playground is a football pitch without any passive recreational facility, public viewers involved into active football activities are less sensitive to visual concerns and changes. Thus, the importance and value of the sky view is not of priority. With the aforementioned mitigation measures, the potential negative visual impact caused by the Proposed Scheme can be addressed and minimised. Thus the Proposed Scheme would only cause a slight resultant effect to public viewers. On the contrary, it is more important to consider whether the Proposed Scheme would affect the overall visual context and create visual incompatibility. As compared to the existing visual context, the Proposed Scheme has a similar and compatible building height, mass and scale with the neighbouring developments, such as Heya Aqua (about 120mPD). Therefore, a negligible effect on visual resources caused by the Proposed Scheme is considered.

VP2 - Sham Shui Po Sports Ground

4.3.9 In accordance with Figures 4.2, VP2 is about 150m to the south of the Scheme. Sham Shui Po Sports Ground comprises a sports ground, a football pitch, two basketball courts and a netball court. Together with the provision of passive recreational facilities and sitting-out areas, the Sports Ground is highly utilised by the general public. Thus, the visual sensitivity of public viewers from this VP is graded as high.

- 4.3.10 Figure 4.5 presents the existing visual composition of the view from VP2 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.11 The current foreground of the view from VP2 is mainly the open-air sports facilities and trees inside Sham Shui Po Sports Ground. Although Hang Chun Court (about 110mPD) to the east of VP2 have substantially blocked the sky view, in overall, a wide open sky view can be enjoyed at VP2. The dense high-rise development along Hing Wah Street and Cheung Wah Street, such as Heya Aqua (about 120mPD), CST (about 100mPD) and Charming Garden (about 100mPD) have formulated the background of the view from VP2.
- 4.3.12 In accordance with Figure 4.5, for the Proposed Scheme, the proposed development at SSP-017 (about 120mPD) would be visible although most portion of it would be behind CST and Charming Garden. Although the two residential towers under the Proposed Scheme would appear slightly taller than the developments along Hing Wah Street and Cheung Wah Street, the Proposed Scheme possesses a compatible, appropriate and harmonious scale to integrate with the existing visual context. Negligible impact to the visual composition of the view from VP2 is considered.
- 4.3.13 With regard to visual obstruction, the Proposed Scheme would cause no obstruction to the foreground of the view from VP2. With the mitigation measures of slimmer building form and wider building separation included under the Proposed Scheme, only a minimal portion of the wide open sky view would be obstructed. The overall visual obstruction is considered as negligible.

Effect on Public Viewers and Visual Resources

4.3.14 As the Proposed Scheme integrates with the existing visual context, the Proposed Scheme would not create any sore thumb development and visual incompatibility. While the wide open sky view is an important visual resource and value for public viewers considered the high level of public utilisation of the Sports Ground, with the mitigation measures included, the wide open sky view being enjoyed at VP2 is well preserved under the Proposed Scheme. Thus, negligible effect on public viewers and visual resources is considered.

VP3 - Cheung Sha Wan Playground

4.3.15 In accordance with Figures 4.2, VP3 is about 400m to the southeast of the Scheme. Being surrounded by a group of residential developments, this Playground is highly utilised by the general public for its recreational facilities such as football pitch, basketball court, skating rink, children's playground and sitting out areas. Therefore, the visual sensitivity of public viewers from this VP is graded as high.

- 4.3.16 Figure 4.6 presents the existing visual composition of the view from VP3 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.17 The current foreground of the view from VP3 is mainly the open-air sports facilities and trees inside Cheung Sha Wan Playground. The dense high-rise residential towers of Un Chau Estate (about 120mPD), Heya Aqua (about 120mPD) and Fortune Estate (about 60 120mPD) have composed the background of the view from VP3. A wide open sky view is available on top of these residential towers.
- 4.3.18 With reference to Figure 4.6, the Proposed Scheme is of compatible height with the residential towers of Fortune Estate and Un Chau Estate which demonstrates its full integration and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view being enjoyed at VP3. Thus, a negligible effect to visual composition and obstruction is considered.

Effect on Public Viewers and Visual Resources

4.3.19 The open sky view is an important visual resource for public viewers considered the high level of public utilisation and passive recreational activities at the Playground. Noted that the open sky view being enjoyed at VP3 can be preserved and the Proposed Scheme fully integrates with the existing visual context, a negligible effect on public viewers and visual resources is considered.

VP4 - Junction of Cheung Wah Street and Un Chau Street

4.3.20 In accordance with Figures 4.2, VP4 is about 120m to the northeast of the Scheme. This junction serves as a connector between the Caritas Medical Centre and So Uk Estate towards the transport and community facilities along Cheung Sha Wan Road. Although the duration of sight towards the Scheme of public viewers at VP4 is short, the level of pedestrian and business activities at this junction is high. Thus, the visual sensitivity of public viewers from this VP is graded as high.

- 4.3.21 Figure 4.7 presents the existing visual composition of the view from VP4 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.22 Mid-rise to high-rise residential/ commercial developments, including High One (about 110mPD), Sea Panorama Court (about 85mPD) and The Pacifica (about 165 – 185mPD), have dominated the view from VP4, thus public viewers at VP4 can only access to a narrow sky view.
- 4.3.23 For the Proposed Scheme, the proposed development at SSP-017 would be visible from VP4. Most portions of the residential towers under the Proposed Scheme and the whole G/IC complex would be concealed by the existing buildings along Cheung Wah Street. Although a small portion of the sky view would be obstructed by the Proposed Scheme, it is considered that the Proposed Scheme fully integrates with the existing visual context by its compatible and appropriate building height. The ground floor setbacks from Cheung Wah Street included in both proposed developments at SSP-017 and SSP-018 have further reduced the visual obstruction and enhance the street environment at eye level. Although the footbridge across Cheung Wah Street

connecting SSP-017 and SSP-018 is visible from VP4, it is considered compatible to the local visual context with only minimal visual obstruction at eye level induced. Noted the overall visual compatibility of the Proposed Scheme, a negligible impact to the visual composition and obstruction is considered.

Effect on Public Viewers and Visual Resources

4.3.24 Noted the sky view viewed from VP4 is narrow, it is considered more essential to assess whether the Proposed Scheme would affect the overall visual context and create visual incompatibility. With reference to Figure 4.7 and the above assessment, the Proposed Scheme can fully integrate with the existing visual context, a negligible effect on public viewers and visual resources caused by the Proposed Scheme is considered.

VP5 - Exit B1 of Lai Chi Kok Railway Station

4.3.25 In accordance with Figures 4.2, VP5 is about 180m to the west of the Scheme. Although the duration of sight towards the Scheme of public viewers at VP5 is short, a very high level of pedestrian activity is observed at VP5 as it connects the Lai Chi Kok Railway Station and bus stops along Cheung Sha Wan Road to the commercial developments and the Caritas Medical Centre nearby. Therefore, the visual sensitivity of public viewers from this VP is graded as high.

- 4.3.26 Figure 4.7 presents the existing visual composition of the view from VP5 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.27 With reference to Figure 4.7, both the foreground and background of the view from VP5 are dominated by the mid-rise to high-rise developments along Cheung Sha Wan Road, including Law's Commercial Plaza (about 130mPD), CST (about 100mPD), Charming Garden (about 100mPD), Yan Fook Centre (about 85mPD) and Tin On Industrial Building (about 45mPD). Public viewers at VP5 can only access to a narrow sky view.

4.3.28 The residential towers under the Proposed Scheme are of compatible height with the towers along Cheung Sha Wan Road which demonstrates its full integration and harmony with the existing visual context. Most portions of the residential towers and the G/IC complex are concealed by the existing development. The Proposed Scheme would only induce minimal obstruction to the narrow sky view.

Effect on Public Viewers and Visual Resources

4.3.29 Noted that the duration of sight of public viewers at VP5 towards the Scheme is short, the importance of sky view is not of priority. Instead, it is more important to consider whether the Proposed Scheme would affect the overall visual context and create visual incompatibility. With reference to Figure 4.8 and the above assessment, the Proposed Scheme can fully integrate with the existing visual context, a negligible effect on public viewers and visual resources caused by the Proposed Scheme is considered.

VP6 - Wing Hong Street Rest Garden

4.3.30 In accordance with Figures 4.2, VP6 is about 220m to the north of the Scheme. Situated next to the Caritas Medical Centre, this rest garden mainly comprises passive recreational facilities and sitting-out areas while the level of public utilisation is not high. Therefore, the visual sensitivity of public viewers from this VP is graded as medium.

- 4.3.31 Figure 4.9 presents the existing visual composition of the view from VP6 and potential visual compositions under the Baseline Scheme and the Proposed Scheme respectively.
- 4.3.32 The current foreground of the view from VP6 is mixed with trees inside the rest garden, and the buildings along Fuk Wa Street, including Por Mee Factory Building (about 55mPD) and CST (about 100mPD). An open sky view can be enjoyed at VP6. With reference to Figure 4.9, as the Proposed Scheme will be concealed by the buildings and the proposed development at SSP-017 in the foreground, no visual obstruction will be induced by the Proposed Scheme.

Effect on Public Viewers and Visual Resources

4.3.33 Given that the Proposed Scheme will not be visible from VP6, no effect on public viewers and visual resources is anticipated by the Proposed Scheme.

VP7 - Sun Yat Sen Memorial Park

- 4.3.34 With reference to Figure 4.3, VP7 is one of the key public viewing points stipulated on Chapter 11 in the HKPSG. Viewing from the Sun Yat Sen Memorial Park at the opposite side of the Victoria Harbour, the ridgeline behind Kowloon shall be protected. As shown on Figure 4.3, the Proposed Scheme is in front of the ridgeline between Kam Shan and the Eagle's Nest.
- 4.3.35 By utilizing 3D GIS tools, Figure 4.10 presents the visual impact analysis of the Proposed Scheme to the view from VP7. The 3D GIS skyline analysis shows that Cullinan West (about 160 to 180mPD), The Sparkle (about 150mPD) and Hoi Lok Court (about 120mPD) will conceal most portions of the Proposed Scheme. In addition, the Proposed Scheme is below both the ridgeline and the 20% building free zone. Therefore, negligible visual impact on the view from VP7 is anticipated by the Proposed Scheme.

Table 4.2 Summary of Anticipated Visual Changes

Sensitivity of Public Viewers	Visual Change
et Playground	
Medium Although VP1 is close to the Scheme, public viewers involved active football activities are less sensitive to visual concerns and changes.	Visual Composition and Visual Obstruction: The proposed buildings are of compatible and similar size and height, as compared to Heya Aqua and the proposed development at SSP-017. With various mitigation measures, obstruction of the open sky view caused by the Proposed Scheme is substantially minimised while the visual permeability along Fuk Wing Street from will be preserved. A slightly adverse impact to the visual composition and obstruction is considered. Effect on Public Viewers and Visual Resources: Public viewers involved into active football activities are less sensitive to visual concerns and changes. With various mitigation measures, the potential negative visual impact caused by the Proposed Scheme can be addressed and minimised. As compared to the existing visual context, the Proposed Scheme has a similar and compatible building height, mass and scale with the neighbouring developments. Thus, a negligible effect on visual resources is considered. Overall Visual Impact: Slightly adverse
Sports Ground	
High The Sports Ground is highly utilised by the	Visual Composition and Visual Obstruction: The Proposed Scheme creates a compatible, appropriate and harmonious scale to integrate with the existing visual
	Public Viewers et Playground Medium Although VP1 is close to the Scheme, public viewers involved active football activities are less sensitive to visual concerns and changes. Sports Ground High The Sports Ground is highly

Visual Elements	Sensitivity of Public Viewers	Visual Change		
Background formulated by the dense high-rise development along Hing Wah Street and	recreational facilities.	slimmer building form and wider building separation included under the Proposed Scheme, only a minimal portion of the wide open sky view would be obstructed.		
Cheung Wah Street. In overall, a wide open sky view can be enjoyed at VP2.		Effect on Public Viewers and Visual Resources:		
		The Proposed Scheme would not create any sore thumb development or visual incompatibility. The wide open sky view being enjoyed at VP2 is well preserved under the Proposed Scheme. Thus, negligible effect on public viewers and visual resources is considered.		
		Overall Visual Impact:		
		Negligible		
Foreground mainly occupied by the open-air sports facilities and trees inside the Playground.	High The Playground is highly utilised by the general	Visual Composition and Visual Obstruction: The Proposed Scheme is of compatible height with the residential towers in Fortune Estate and Un Chau Estate,		
Background mainly formed by the dense high-rise residential towers.	public for its recreational facilities.	which demonstrates its full integration, and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view.		
formed by the dense high-rise residential towers. A wide open sky view on top of the	recreational	which demonstrates its full integration, and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view. Effect on Public Viewers and Visual		
formed by the dense high-rise residential towers. A wide open sky view on top of the surrounding residential towers is	recreational	which demonstrates its full integration, and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view. Effect on Public Viewers and Visual Resources:		
formed by the dense high-rise residential towers. A wide open sky view on top of the surrounding	recreational	which demonstrates its full integration, and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view. Effect on Public Viewers and Visual		
formed by the dense high-rise residential towers. A wide open sky view on top of the surrounding residential towers is	recreational	which demonstrates its full integration, and harmony with the existing visual context. Besides, the Proposed Scheme would not induce obstruction to the wide open sky view. Effect on Public Viewers and Visual Resources: The wide open sky view being enjoyed at VP3 can be well preserved and the Proposed Scheme fully integrates with the existing visual context. A negligible effect on public viewers and visual		

Visual Elements	Sensitivity of Public Viewers	Visual Change
VP4 – Junction of C	heung Wah Street	and Un Chau Street
View with a narrow sky view dominated by mid-rise to high-rise residential/ commercial developments along Cheung Wah Street.	High A high level of pedestrian and business activity is observed.	Visual Composition and Visual Obstruction: Most portions of the building blocks of the Proposed Scheme would be concealed by the existing buildings which causes negligible impact. The ground floor setback from Cheung Wah Street included in the Proposed Scheme has further reduced the visual obstruction and enhance the street environment at eye level. Effect on Public Viewers and Visual Resources: As the Proposed Scheme can fully integrate with the existing visual context, a negligible effect on public viewers and visual resources caused by the Proposed Scheme is considered. Overall Visual Impact: Negligible
VP5 – Exit B1 of Lai View dominated by the mid-rise to high- rise developments along Cheung Sha Wan Road with a narrow open sky view.	Chi Kok Railway S High A very high level of pedestrian activity is observed.	Visual Composition and Visual Obstruction: The Proposed Scheme is of compatible height with the towers along Cheung Sha Wan Road, which demonstrates its full integration with the existing visual context. The Proposed Scheme only induces very minimal obstruction to the narrow sky view. Effect on Public Viewers and Visual Resources:
		The Proposed Scheme can fully integrate with the existing visual context, a negligible effect on public viewers and

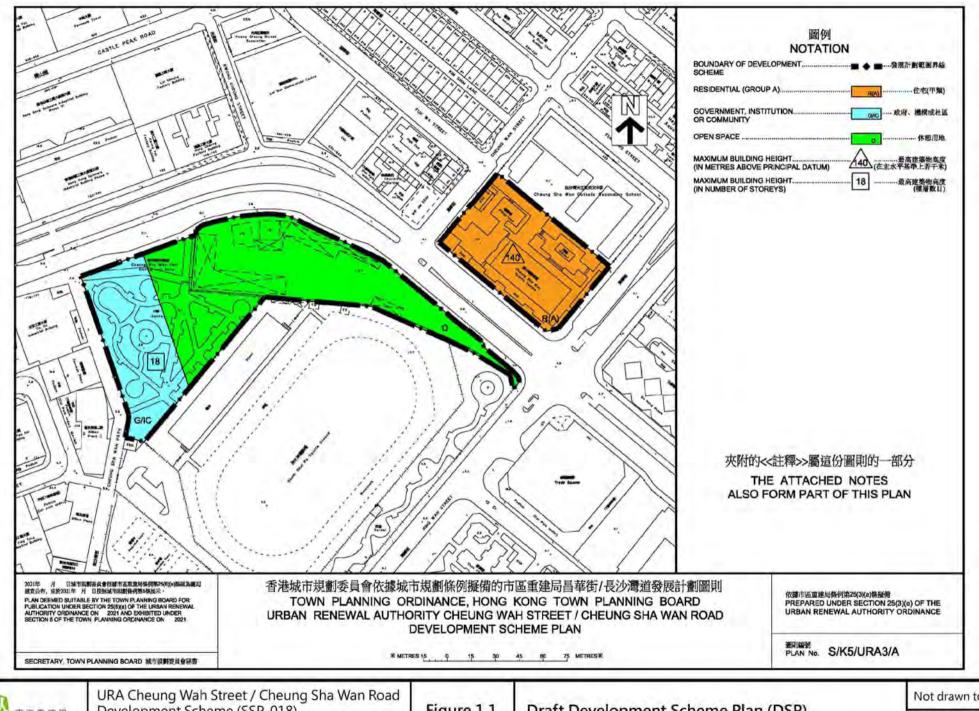
Visual Elements	Sensitivity of Public Viewers	Visual Change	
		visual resources caused by the Proposed Scheme is considered. Overall Visual Impact: Negligible	
VP6 - Wing Hong St	reet Rest Garden		
View mixed with trees inside the rest garden, and the buildings along Fuk Wa Street. Open sky view can be enjoyed.	Medium The level of public utilisation is not high.	Existing buildings in the foreground conceal the Proposed Scheme. No visual change is anticipated. Overall Visual Impact: Negligible	
VP7 - Sun Yat Sen M	lemorial Park		
View mainly formed by the Victoria Harbour, the dense urban development in Kowloon, a wide open sky and the ridgeline from Kam Shan to Tsz Wan Shan.		Existing buildings conceal most portions of the Proposed Scheme. Noted that the Proposed Scheme is below the ridgeline and the 20% building free zone, negligible visual impact is anticipated. Overall Visual Impact: Negligible	

5 EVALUATION OF OVERALL VISUAL IMPACT AND CONCLUSION

- 5.1 The above analysis has compared the visual impact induced by the future redevelopment under both the Baseline Scheme and the Proposed Scheme. Block size, disposition and layout of the Proposed Scheme have been carefully designed with respect to the existing urban design, building height profile and key public viewing points in the vicinity. With the proposed maximum building height, various measures such as slimmer building form, wider building separation, careful building disposition and ground floor setbacks are included in the Proposed Scheme to enhance the visual quality and visual impact.
- 5.2 The Scheme is located in a densely developed residential neighbourhood with an increasing number of high-rise residential developments reaching 120mPD or above. Several existing and future developments of 140mPD or above are found around the Scheme, such as The Pacifica, Beacon Lodge and the public housing development at the Wang Cheong Factory Estate site. Therefore, with full regard to the existing visual context, the proposed maximum building height of 140mPD proposed at Site A, and the proposed maximum building height of 95mPD at scheme area coloured in blue will not result in visual incompatibility.
- 5.3 Referring to the visual impact analysis at VP6, the Proposed Scheme will be entirely concealed by existing developments. For VP4, VP5 and VP7, building blocks under the Proposed Scheme will be mostly concealed by existing developments. Noted the minimal visual change caused by Proposed Scheme, negligible visual impact is anticipated at these VPs.
- 5.4 Referring to VP2 and VP3, with the mitigation measures of slimmer building form and wider building separation being included, only a minimal portion of the wide open sky view would be obstructed by the Proposed Scheme. Since the Proposed Scheme is of compatible height which fully integrates with the existing visual context, a *negligible* overall visual impact is also anticipated at these VPs.

- 5.5 For VP1, although the Proposed Scheme also presents its compatibility with the existing visual context, the Proposed Scheme would obstruct a portion of the open sky view. Various mitigation measures including careful block disposition and slimmer building form are proposed which substantially minimised the visual obstruction. Noted that the public viewers at VP1 are less sensitive to the visual changes of the sky view, the potential negative visual impact caused by the Proposed Scheme can be addressed and minimised. Besides, the visual permeability along Fuk Wing Street is also preserved under the Proposed Scheme. Therefore, only a slightly adverse resultant visual impact is anticipated by the Proposed Scheme.
- 5.6 In conclusion, the Proposed Scheme will induce no significantly adverse visual impact. In overall, the visual impact for most VPs caused by the Proposed Scheme is negligible. The Proposed Scheme has similar building heights with the neighbouring development and is visually compatible to its context. Its induced visual obstruction at VP1 and VP2 could be addressed and minimized by various mitigation measures. Therefore, the result overall visual impact is concluded as negligible.

URBAN RENEWAL AUTHORITY September 2021





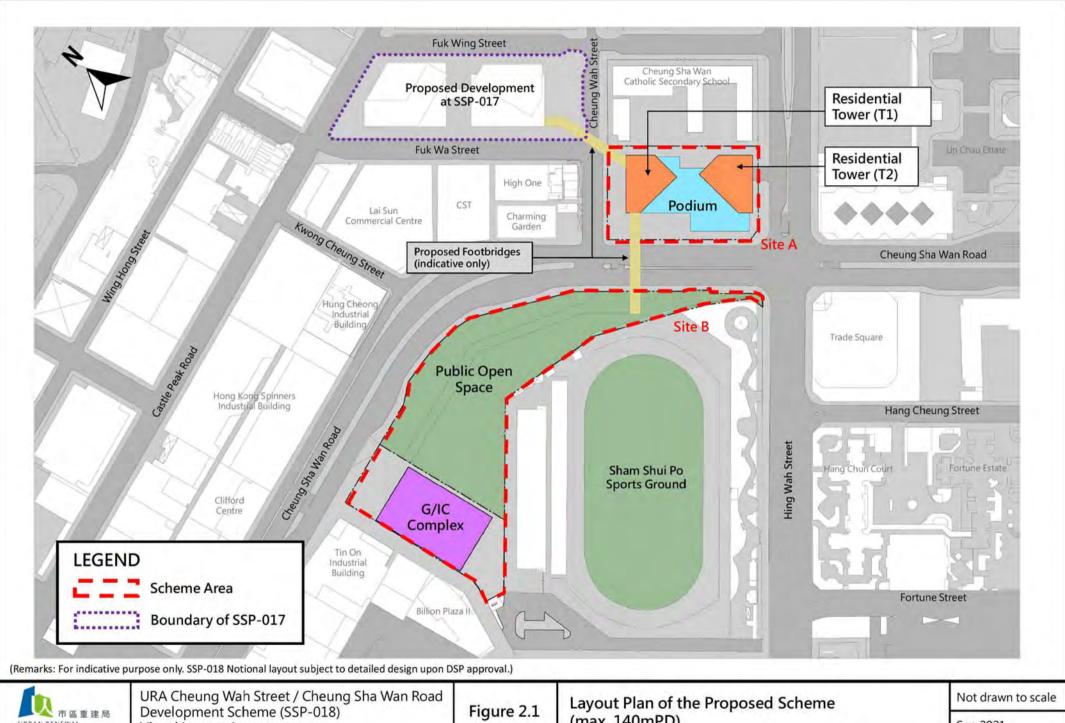
Development Scheme (SSP-018) Visual Impact Assessment

Figure 1.1

Draft Development Scheme Plan (DSP)

Not drawn to scale

Sep 2021

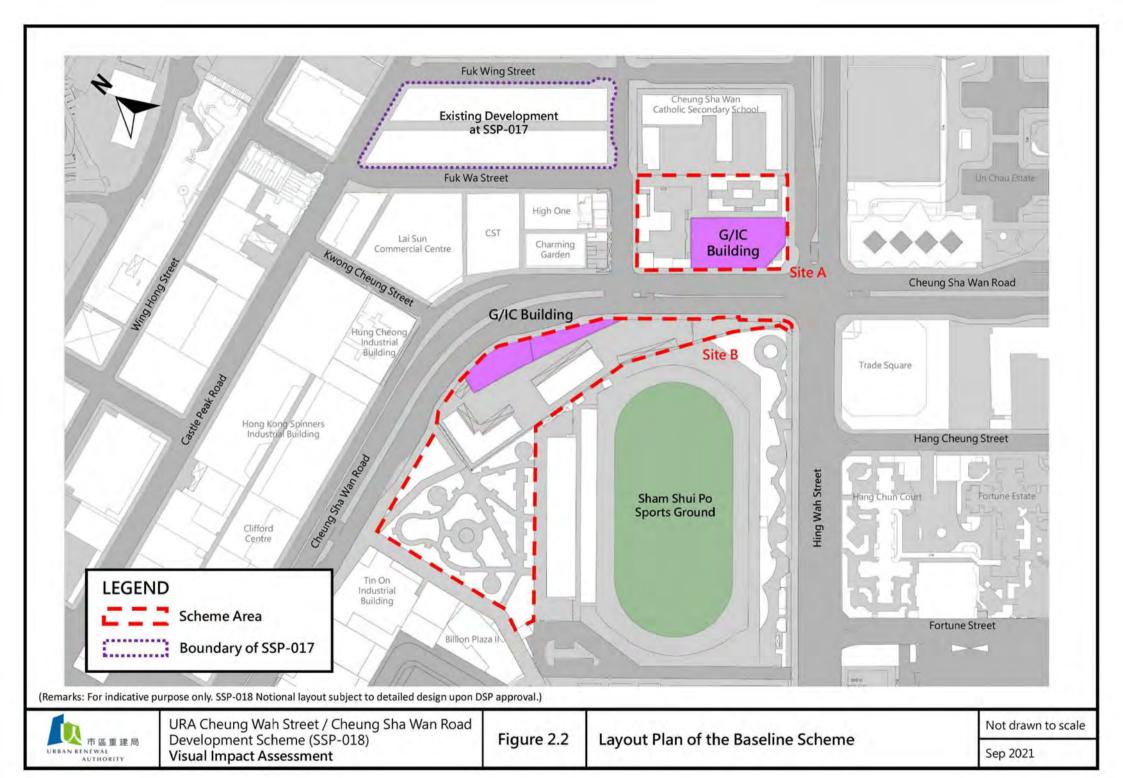


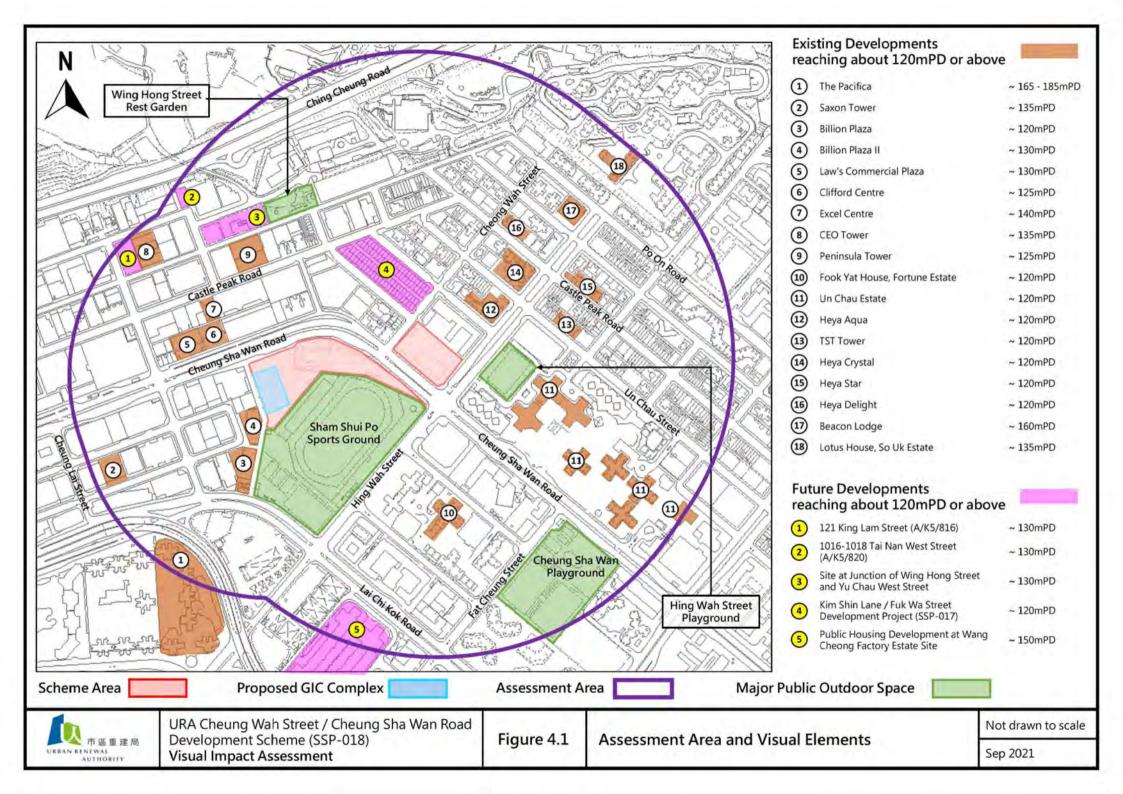
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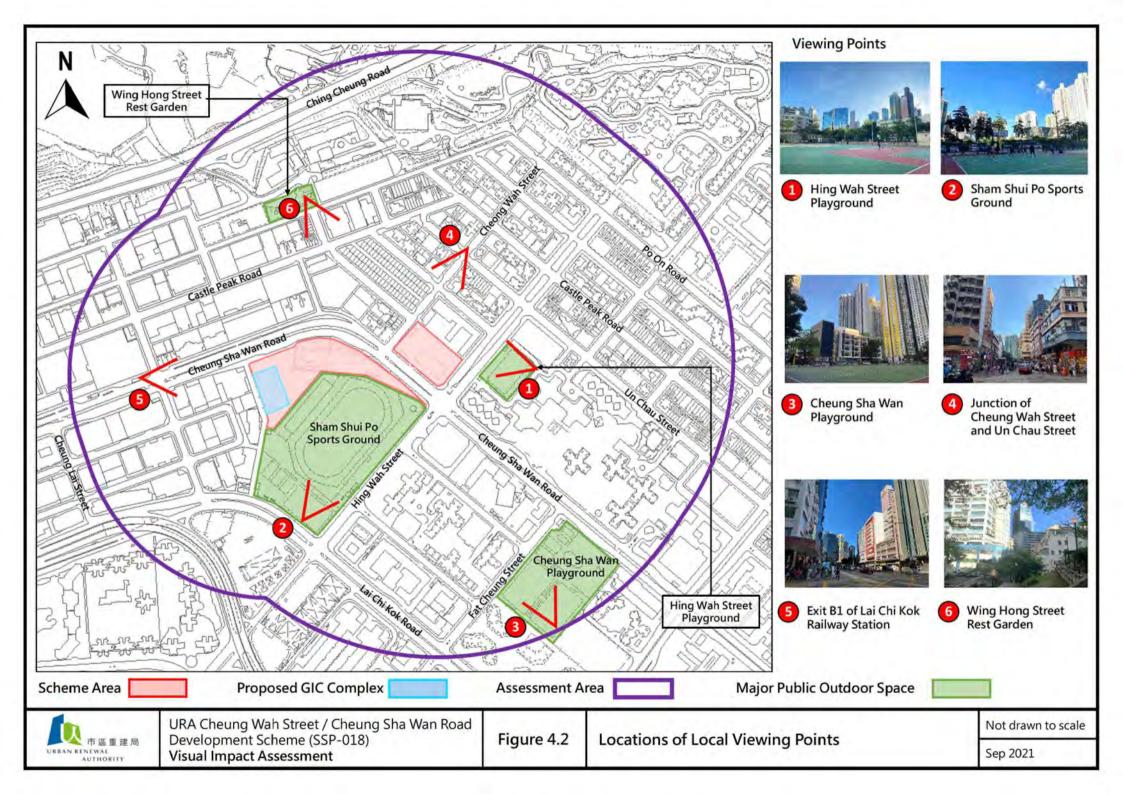
Visual Impact Assessment

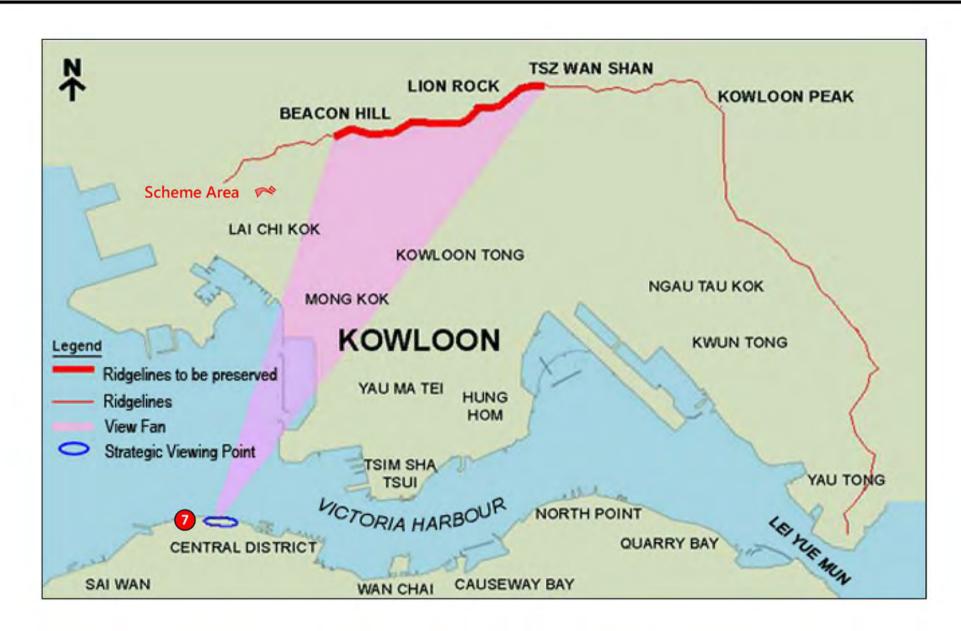
Layout Plan of the Proposed Scheme (max. 140mPD)

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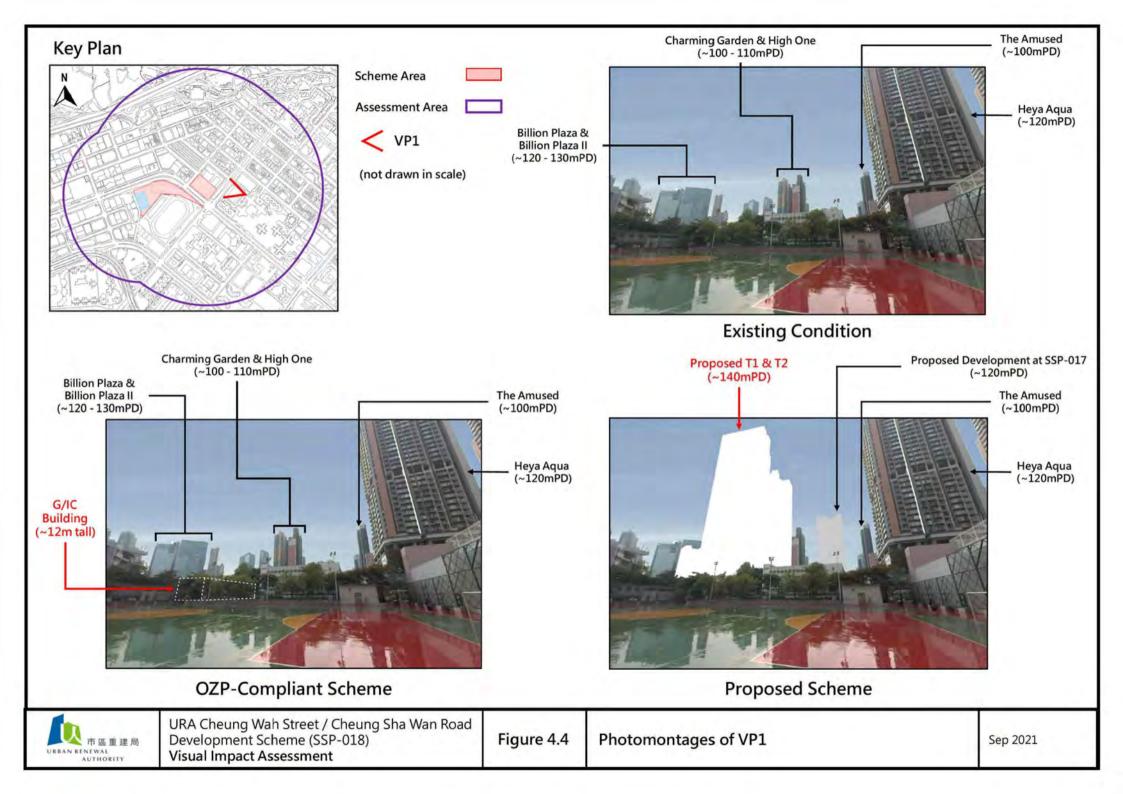


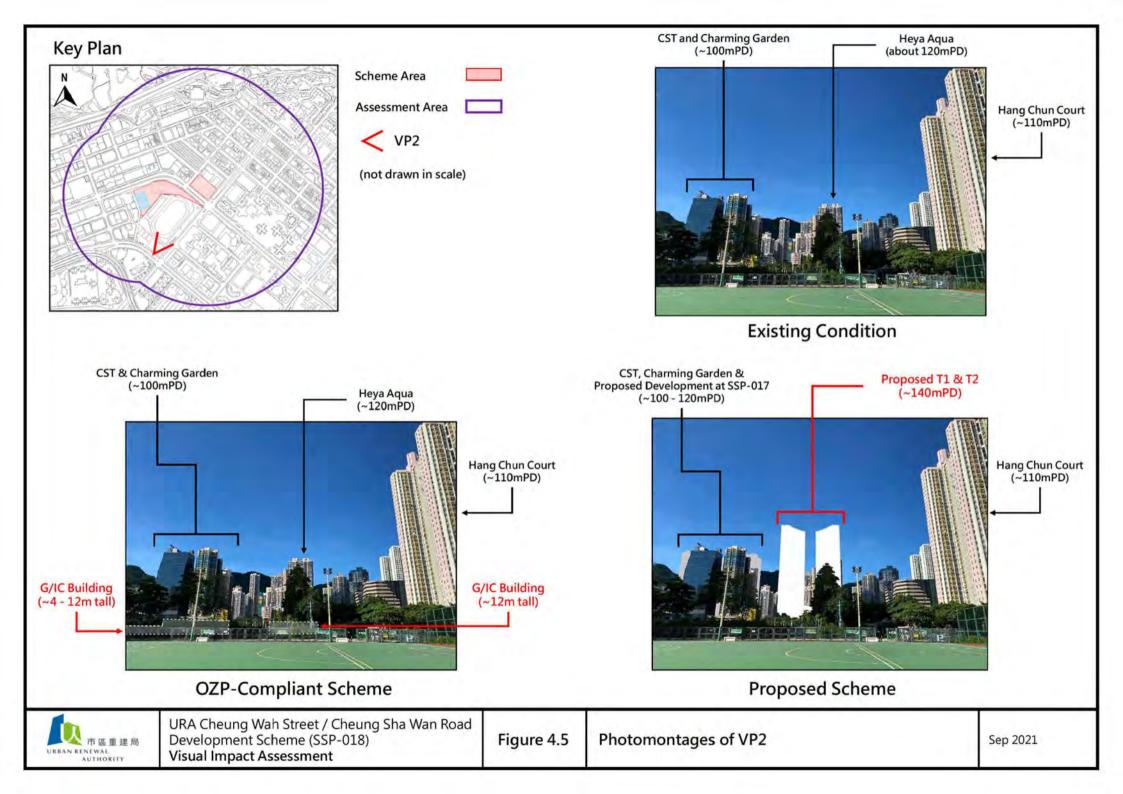


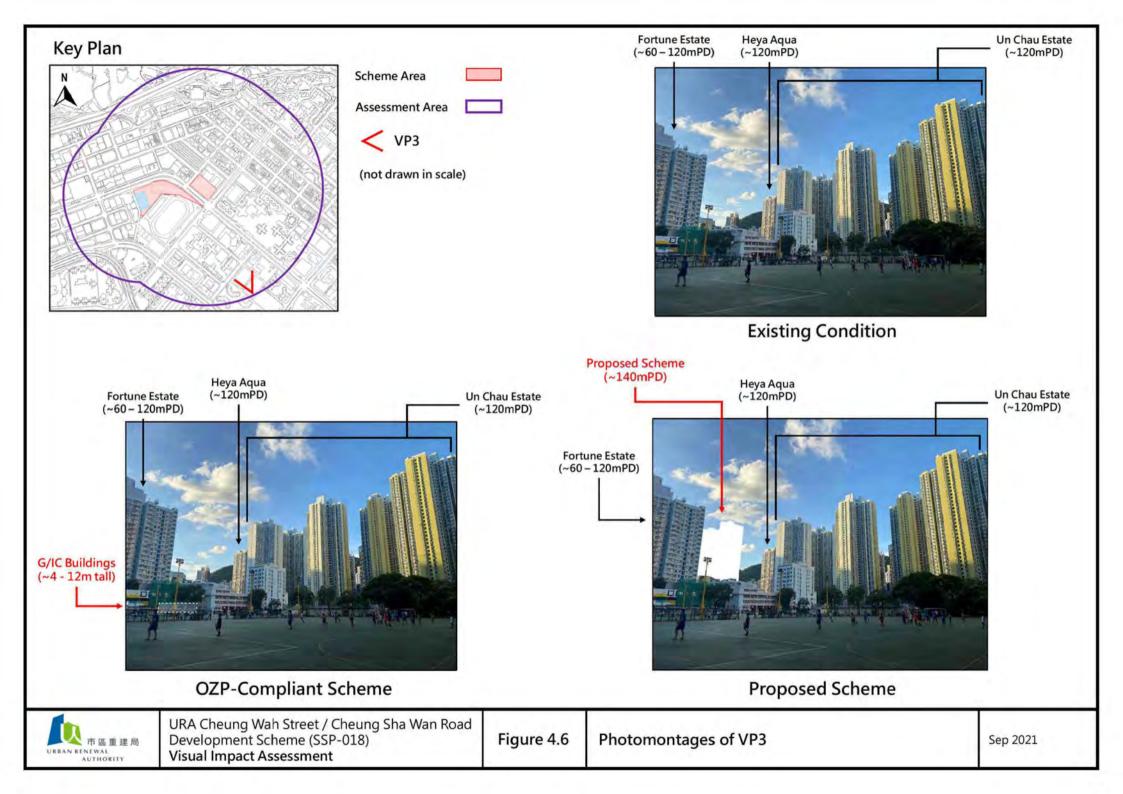
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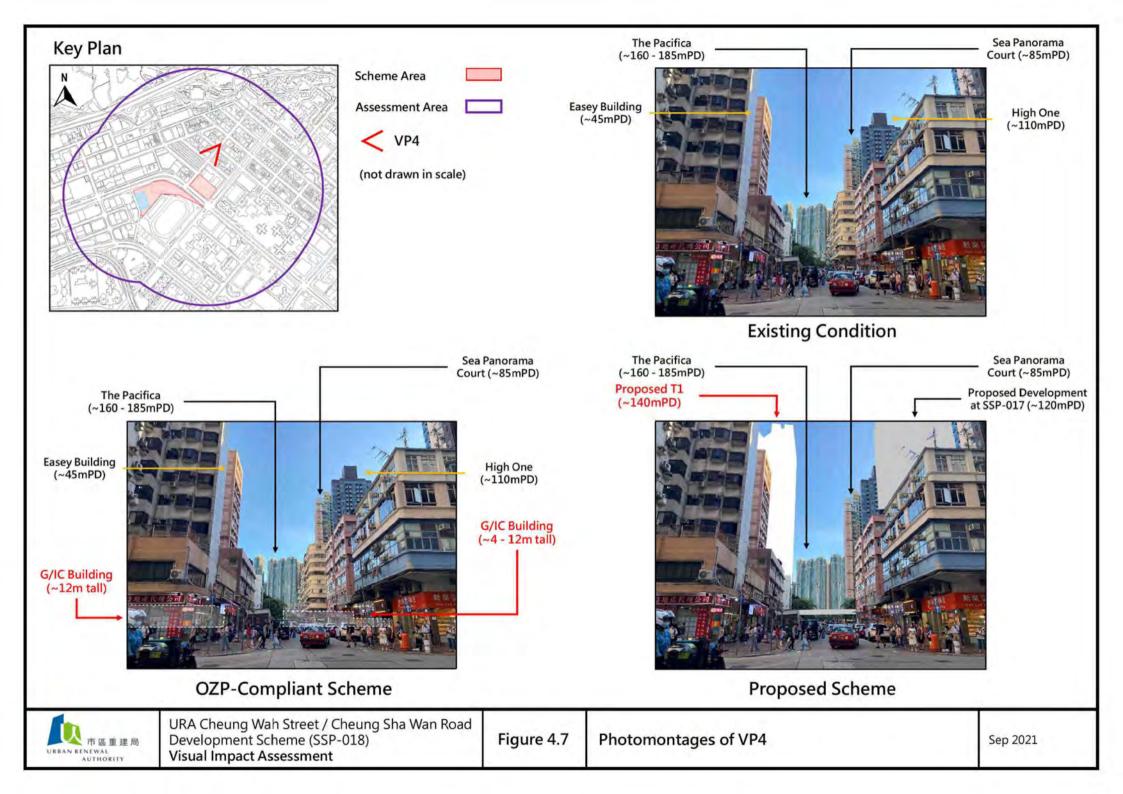
Strategic Viewing Points Webpage of Planning Department for the Town Planning Board Guidelines for Submission of Visual Impact Assessment to the Town Planning Board (TPB PG-No. 41) https://www.pland.gov.hk/pland_en/info_serv/via/web/vp_eng.html

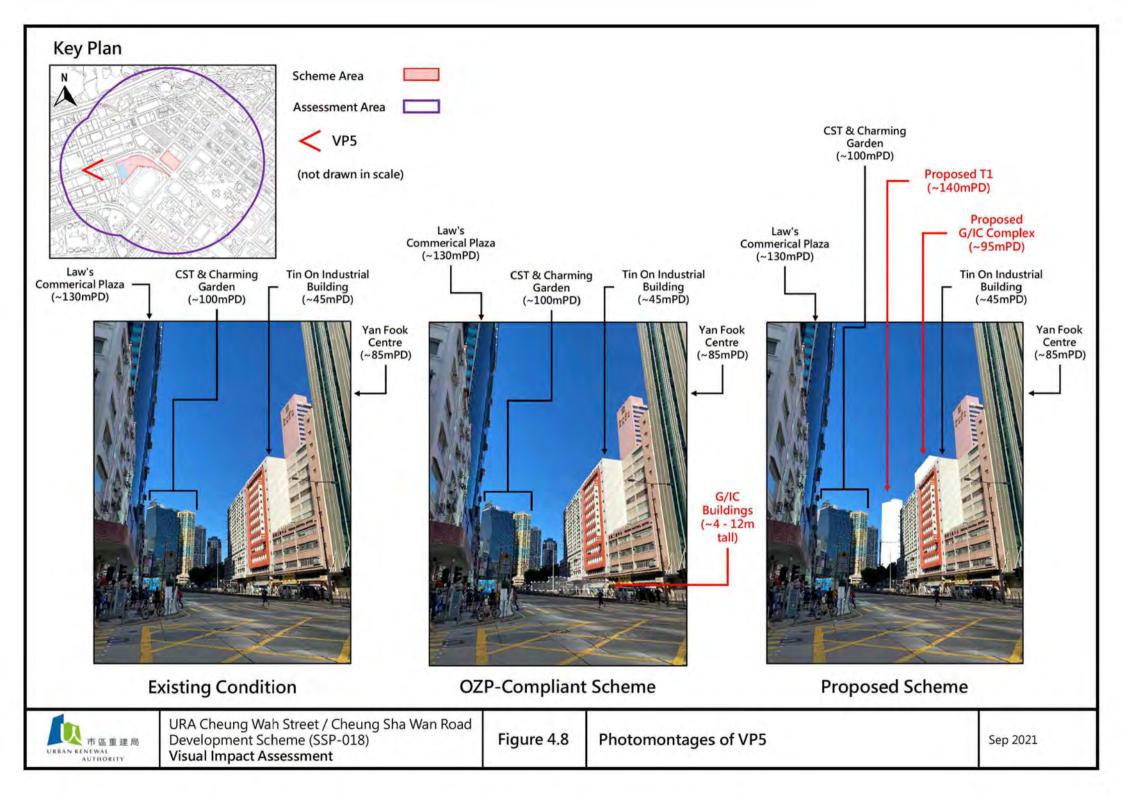


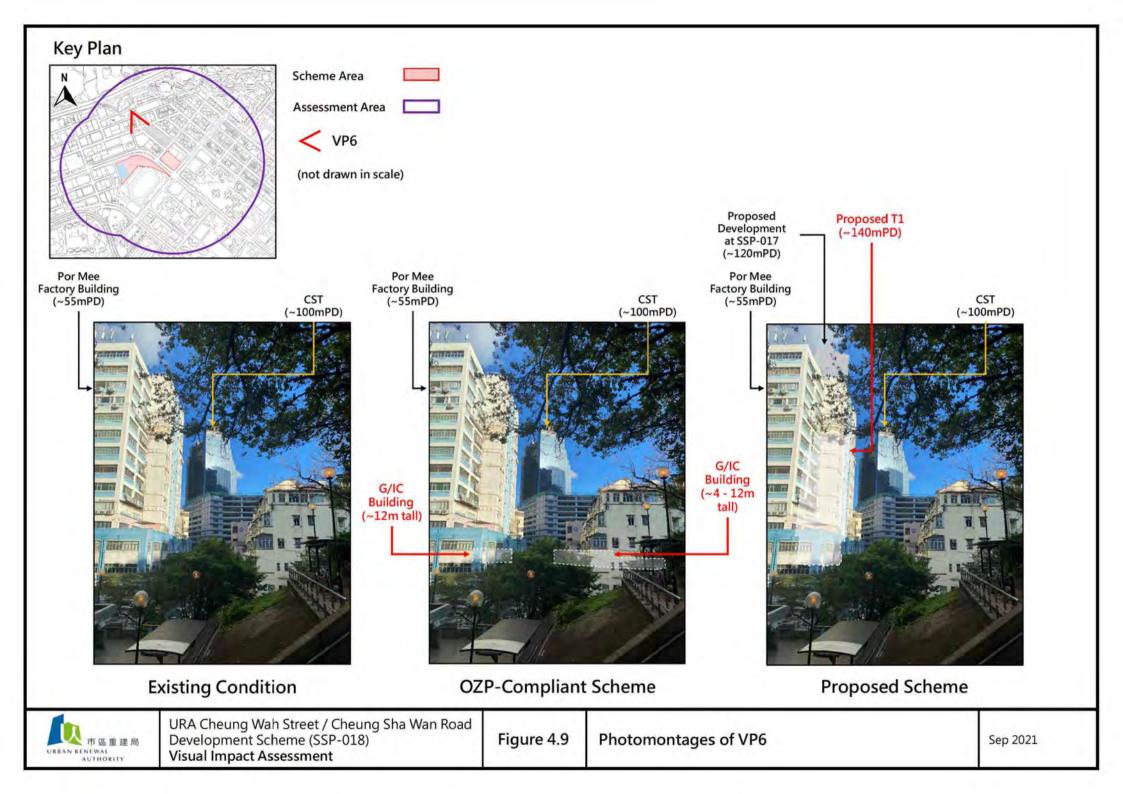


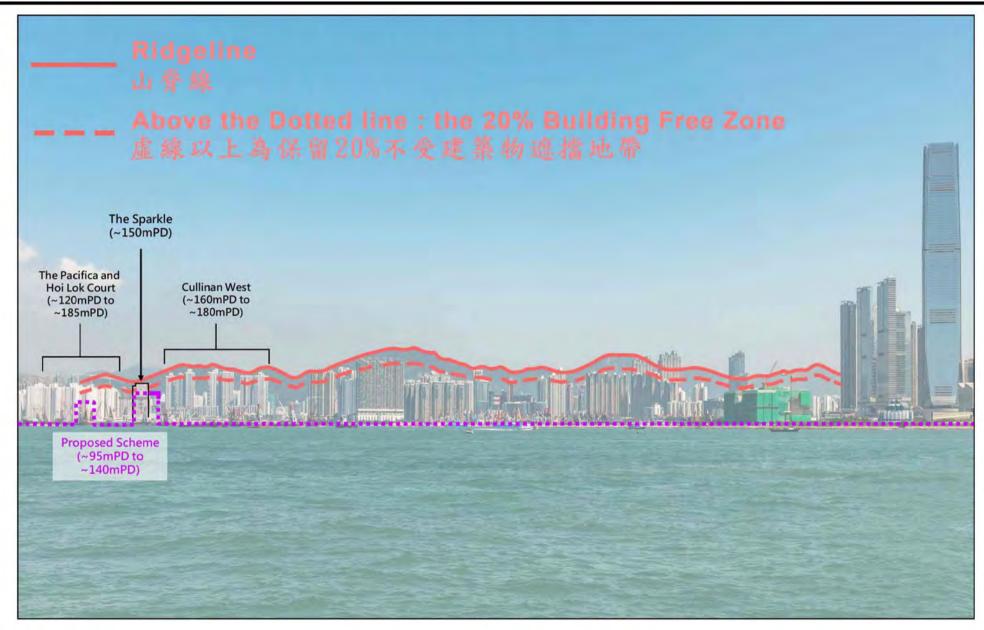












Source:

Strategic Viewing Points Webpage of Planning Department for the Town Planning Board Guidelines for Submission of Visual Impact Assessment to the Town Planning Board (TPB PG-No. 41) https://www.pland.gov.hk/pland_en/info_serv/via/web/vp_eng.html



Appendix 4

Social Impact Assessment (Stage 1) Report



Cheung Wah Street / Cheung Sha Wan Road

Development Scheme (SSP-018)



Stage 1 Social Impact Assessment

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1. INTRODUCTION

- 1.1 According to the Urban Renewal Strategy (URS) issued by the Government in February 2011, the Urban Renewal Authority (URA) will carry out Social Impact Assessment (SIA) studies in the form of "a Stage 1 social impact assessment before the publication of any proposed redevelopment project in the Government Gazette", and "a Stage 2 social impact assessment after the proposed project has been published in the Government Gazette". This Stage 1 SIA is prepared by the URA for the proposed Cheung Wah Street / Cheung Sha Wan Road Development Scheme (the Scheme).
- 1.2 The URS also states "Early social impact assessments will be initiated and conducted by the DURF (District Urban Renewal Forum) before redevelopment is recommended as the preferred option. The URA will update these assessments by DURF before implementing any specific redevelopment project." In the absence of a District Urban Renewal Forum ('DURF') for Sham Shui Po, there is no early SIA conducted by DURF which the URA could update for this Development Scheme.
- 1.3 According to the URS, the main elements of the Stage 1 SIA conducted by the URA before publication of a proposed project should include: -
 - the population characteristics of the proposed project area;
 - the socio-economic characteristics of the area;
 - the housing conditions in the area;
 - the characteristics of local business activities, including small shops and street stalls;
 - the degree of overcrowding in the area;
 - the availability of amenities, community and welfare facilities in the area;
 - the historical background of the area;
 - the cultural and local characteristics of the area;
 - an initial assessment of the potential social impact of the proposed project; and
 - an initial assessment of the mitigation measures required.
- 1.4 The Stage 2 SIA will be conducted after the publication of the project based on the factual information collected in the Freezing Survey (FS) upon project commencement. The URS stipulates the URA should submit both Stage 1 and Stage 2 SIA reports to the Town Planning Board (TPB) under section 25 of the Urban Renewal Authority Ordinance (URAO), and should release the reports for public information.

2. THE PROJECT BACKGROUND

- 2.1 First, a street block at Kim Shin Lane / Fuk Wa Street (namely SSP-017) comprising 90 building blocks of age over 60 with no lifts is identify as a site with imminent redevelopment needs. However, SSP-017 is undesirable for redevelopment because its existing plot ratio is as high as 8.12, hence, the residual plot ratio is 0.88 only. Multiple sub-divided units are also identified. Although SSP-017 has all the quality to demand for redevelopment, its redevelopment potential is low. In this respect, a wider area for planning opportunities have to be explored.
- Under a "planning-led" approach in urban renewal works in recent years, URA has identified part of Sham Shui Po as Sham Shui Po Action Area 1 (SSPAA1) for holistic planning of urban renewal works. The Cheung Wah Street / Cheung Sha Wan Road Development Scheme (the Scheme) (SSP-018) comprises Sites A and B (Figure 2.1), both Government land opposite each other across Cheung Sha Wan Road is identified for redevelopment to formulate a comprehensive land-use restructuring together with SSP-017 to create more planning gains at district level. The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017. As SSP-017 conforms to the existing planning control, it will be implemented under Section 26 of the URAO separately; it does not form part of this Scheme and will be covered by another Stage 1 SIA report.
- 2.3 The Scheme (SSP-018) is located in Sham Shui Po District, comprises Sites A and B along Cheung Sha Wan Road. Site A of the Scheme is bounded by Hing Wah Street on the southeastern boundary, Cheung Sha Wan Road on the southwestern boundary, Cheung Wah Street on the northwestern boundary, and Cheung Sha Wan Catholic Secondary School on the northeastern boundary. It is currently occupied by the Cheung Sha Wan Sports Centre and a garden both under Leisure and Cultural Services Department (LCSD). Subject to site survey and detailed design, the net site area used to calculate the development potential of Site A is about 5,197 sq.m.
- 2.4 Site B of the Scheme is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the southeastern boundary. Subject to site survey and detailed design, it covers a gross site area of about 13,857 sq.m, involving the Cheung Sha Wan Path Sitting-out Area and part of the Sham Shui Po Sports Ground under LCSD, as well as a temporary maintenance depot of Highways Department.

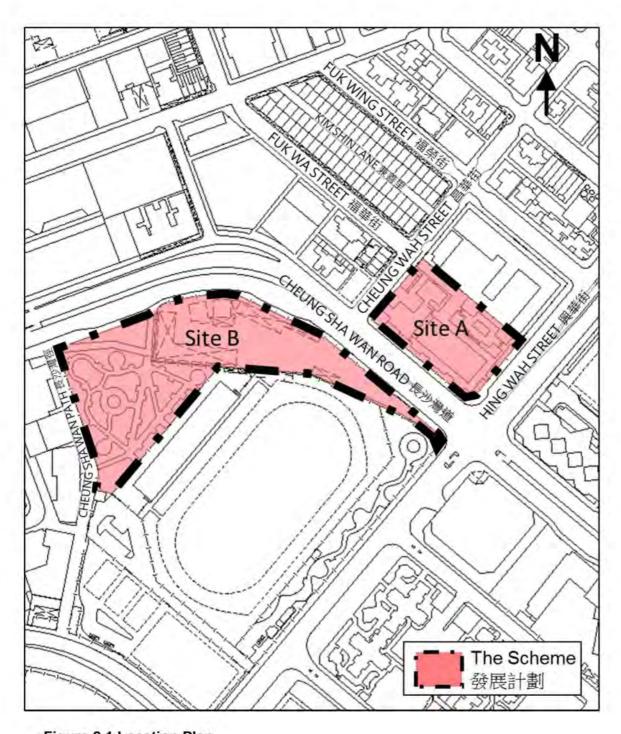


Figure 2.1 Location Plan

Planning Objectives

- 2.5 The URS issued in 2011 promulgates a comprehensive and holistic approach to carry out urban renewal with the following objectives:
 - Restructuring and replanning of concerned urban areas;
 - Designing more effective and environmentally-friendly local transport and road networks within the concerned urban areas;
 - Rationalising land uses within the concerned urban areas;
 - Providing more open space and community/ welfare facilities; and
 - Enhancing the townscape with attractive landscape and urban design.
- 2.6 Under a "planning-led" approach, the Scheme includes the following key planning proposals to achieve the above URS objectives:
 - i. Through re-structuring and re-planning of existing land uses, the Scheme will optimise the land uses to achieve more planning gains for the community. Built in 1976, the existing Cheung Sha Wan Sports Centre at Site A of the Scheme which will be reprovisioned and upgraded at Site B up to present-day standard. Site B of the Scheme will be redeveloped to provide a POS larger than the existing Cheung Sha Wan Path Sitting-out Area and other new Government, institution and community (GIC) facilities to serve the public in a wider district. Under an integrated approach, the new GIC complex and its adjacent proposed public open space (POS) will form a larger leisure and community hub in connection with the Sham Shui Po Sports Ground for public enjoyment.
 - ii. Including the reprovision of the new Cheung Sha Wan Sports Centre, to accommodate the needs of the district on social welfare and health facilities identified by relevant Government departments, not less than 38,000 sq.m. nondomestic GFA is proposed for GIC uses at both sites in the Scheme, which is more than about 33 times of the existing GIC GFA. The provision of floor space for GIC uses is in line with the promotion of the Government's policy on "Single Site, Multiple Uses".
 - iii. Taking this integrated renewal opportunity, footbridges across Cheung Sha Wan Road and Cheung Wah Street are proposed to connect the open space provided in both URA projects (SSP-017 and SSP-018) to enhance connectivity of amenity features for public. The resultant all-weathered at grade and elevated pedestrian network will not only integrate various GIC facilities and POSs, but also enhance overall permeability and connectivity of a wider area of Sham Shui Po in the

vicinity of the Scheme.

iv. Under an integrated urban renewal approach, the Scheme also provides various opportunities for feasible revitalisation initiatives outside the Scheme area. With the provision of underground public vehicle park at Site A, opportunities for the replacement of some on-street parking spaces in the area will be created to make way for possible pavement widening at strategic locations. Those separate revitalisation initiatives will in particular strengthen the connector role of Cheung Wah Street to enhance the connectivity between the medium aged building cluster further north and the future leisure and community hub in the south, thus benefits a wider area. For Site B, there is a possible integration of the new POS with the existing Sham Shui Po Sports Ground in the south subject to further co-ordination with LCSD on the associated revitalisation work separately, upon approval of the DSP and subject to further coordination and acceptancy of relevant Government departments.

URA Projects in the Vicinity

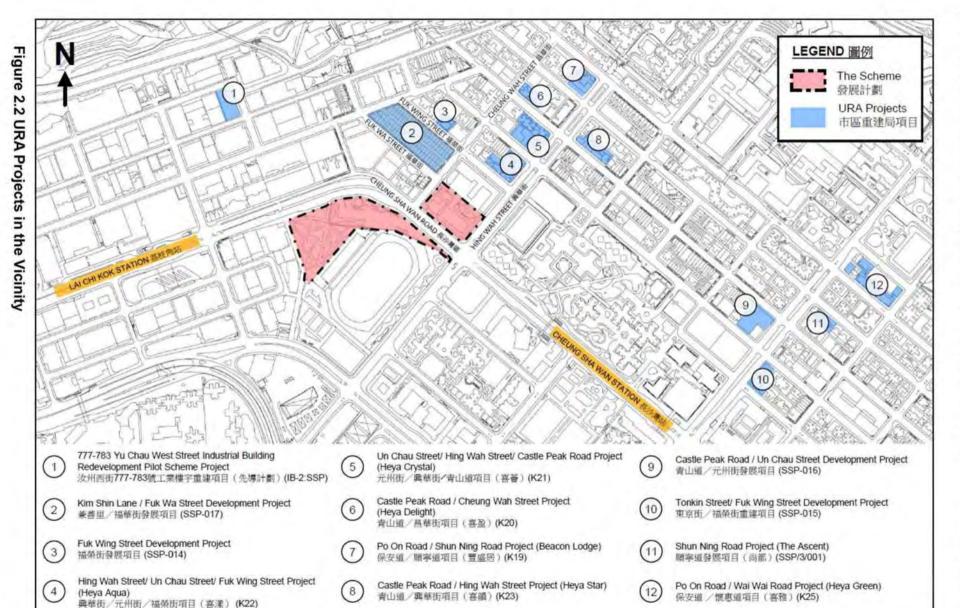
- 2.7 The Scheme is located close to various completed and on-going URA projects nearby (Figure 2.2). To the northeast of the Scheme is a cluster of URA redevelopment projects. Completed URA projects include Fuk Wing Street Development Project (SSP-014), Heya Aqua (K22), Heya Crystal (K21), Heya Delight (K20), Beacon Lodge (K19) and Heya Star (K23), where were completed in 2015 and 2018.
- 2.8 To the east of the Scheme is another cluster of URA redevelopment projects. Tonkin Street/ Fuk Wing Street Development Project (SSP-015) and Castle Peak Road / Un Chau Street Development Project (SSP-016) are currently under construction and are expected to be completed by 2022 and 2023 respectively. There are also two completed URA redevelopment project, Heya Green (K25) and the Ascent (SSP/3/001) which were completed in 2013 and 2018 respectively. To the northwest of the Scheme is the 777-783 Yu Chau West Street Industrial Building Redevelopment Pilot Scheme Project (IB-2:SSP).
- 2.9 The Kim Shin Lane / Fuk Wa Street Development Project (SSP-017) located to the northwest of the Scheme across Cheung Wah Street and was commenced on the same date, allowing broader restructuring and replanning of the neighbourhood. SSP-017 will remove the existing old and dilapidated buildings and develop modern residential developments with commercial/retail uses in the low floors. The Scheme will create synergy with SSP-017 to formulate a comprehensive land-use restructuring together to create more planning gains at district level. As SSP-017 conforms to the existing

planning control, it will be implemented under Section 26 of the URAO separately; it does not form part of this Scheme and will be covered by another Stage 1 SIA report.

Stage

Social Impact Assessment Report

URA Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018)



3. HISTORICAL BACKGROUND AND LOCAL CHARACTERISTICS

3.1 Sham Shui Po was founded as a market town at around 1750-1760s. In the early 19th Century, the town was already well-established and functioned as a service centre for shipping and trade. The town grew rapidly after the establishment of the city of Hong Kong since it was one of the best-located places for the trade in firewood and fresh food for the new city. As a result, the town became a primary market by the 1870s. By the end of 19th Century, certain businesses such as lime-burning, tanning, iron working, boat making and repairing, dyers, joss-stick trades and stone-cutting were well developed in Sham Shui Po. There were also extensive squatter areas settled by duck farmers, pig farmers and market gardeners, such as today's Apliu Street. The following paragraphs summarize some important development in Sham Shui Po since the 20th Century.

Public Housing

3.2 About 40% of housing stock in Sham Shui Po is public rental housing or subsidized home ownership housings (2016 By-Census). Sham Shui Po district also has the first group of public housings in Hong Kong. There are 19 Public Rental Housing (PRH) estates / Tenants Purchase Schemes (TPS) estates, and 9 Home Ownership Scheme/ Private Sector Participation Scheme / Green Form Subsidised Home Ownership Scheme (GSH) estates managed by the Hong Kong Housing Authority ('HA') in the District. A number of these public housing estates built in earlier decades, such as Shek Kip Mei Estate and So Uk Estate, have undergone or are undergoing redevelopment in recent years.

Lei Cheng Uk Han Tomb

3.3 The Lei Cheng Uk tomb, which is located at No. 41 Tonkin Street (see Figure 3.1), is the most important historic feature in Sham Shui Po. It was discovered in 1955 when the Government started construction of resettlement buildings in the area. The tomb was built in the Eastern Han Dynasty (i.e. AD 25-220). Historic items unearthed from the tomb included pottery and bronze objects. The tomb has been declared a gazetted monument for permanent preservation under the Antiquities and Monument Ordinance.

Sham Shui Po Sports Ground

3.4 Sham Shui Po Sports Ground (see Figure 3.1) located in Cheung Sha Wan was first opened on 9 January 1988. It comprises an all-weather, international standard 400metre running track (8 lanes), a grass pitch with flood lights and spectator stand for 2,194 seats. It is a popular sports ground used by the local community in Sham Shui Po as well as hosting major sporting events. It was home to the 2011–12 Hong Kong First Division Football League season and the Fourway Athletics in the 2009–10 season.

Caritas Hospital

- 3.5 Caritas Medical Centre (see **Figure 3.1**) was founded by Caritas Hong Kong and opened by the Hong Kong Governor, David Trench, on 17 December 1964. The centre is now a general hospital with 1,206 beds situated in Sham Shui Po, and is co-managed by the Hospital Authority and Caritas Hong Kong. Caritas Medical Centre is the referral centre of the Kowloon West Cluster of the Hospital Authority in ophthalmology service serving the entire Kowloon west region. Caritas Medical Centre ophthalmology team also provides ophthalmic support to Kwong Wah Hospital (KWH). The Orthopaedic Rehabilitation Service for Kowloon West Cluster is also based at Caritas Medical Centre. The hospital runs the largest Developmental Disabilities Unit (Project Sunshine, Chinese: 陽光之家) for the entire territory of Hong Kong, to provide treatment, training and daily care for severely mentally handicapped patients under the age of 16 in a home-like setting. Despite not being a university hospital, it provides clinical training for medical and nursing students from the local universities.
- 3.6 Places with historical background and local character near the Scheme is shown on Figure 3.1.

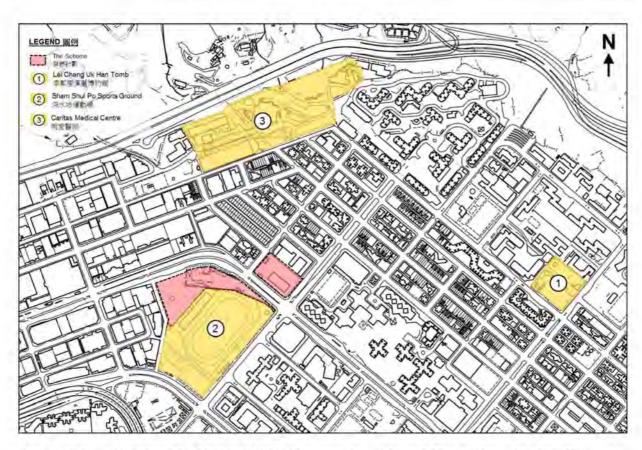


Figure 3.1 Places with Historical Background and Local Character near the Scheme

4. POPULATION & SOCIO-ECONOMIC CHARACTERISTICS

- 4.1 Based on non-obtrusive on-site observation, there is no population and household identified in the Scheme. It will be confirmed at the Stage 2 SIA.
- 4.2 As stated in paragraph 2.3 and 2.4, Site A of the Scheme is currently occupied by the Cheung Sha Wan Sports Centre and a garden under LCSD, while Site B covers the Cheung Sha Wan Path Sitting-out Area and part of Sham Shui Po Sports Ground also under LCSD as well as a temporary maintenance depot of Highways Department. Hence, no household is included in the Scheme.

5. HOUSING & ENVIRONMENTAL CONDITIONS

5.1 No housing is located within the Scheme area. The degree of overcrowding in the Scheme area is not applicable.

Existing Uses

- 5.2 The existing Cheung Sha Wan Sports Centre at Site A is under the LCSD. The sports centre provides some basic recreational facilities for public use during the opening hours and organise recreational activities and training courses regularly for the public. According to the LCSD's website, the sports centre provides 1 multi-purpose arena for 1 volleyball court or converting to 1 basketball court (sub-standard 5-a-side basketball court) or converting to 4 badminton courts, which one of the badminton court can be converted into 2 table-tennis tables on weekdays. The sports centre was built in 1976 which the design and facilities is below current standard.
- 5.3 Site B of the Scheme involves the Cheung Sha Wan Path Sitting-out Area and part of the Sham Shui Po Sports Ground under LCSD as well as a temporary maintenance depot of Highways Department. There is no public access to the temporary maintenance depot of Highways Department, which is a major blockage of the POS at Sites A and B. Local residents in the north of the Scheme has to pass through the Cheung Sha Wan Path Sitting-out Area to reach the Sham Shui Po Sports Ground in the south.
- 5.4 Site B will be first redeveloped to provide more GIC facilities and POS up to present-day standard for the public. After completion, the existing Cheung Sha Wan Sports Centre at Site A will then be reprovisioned at Site B up to present-day standard and continue its operation.

Environmental Condition

- 5.5 The Scheme is located between Lai Chi Kok and Cheung Sha Wan MTR Stations. Cheung Sha Wan Road in between Sites A and B of the Scheme is a primary distributor with high traffic flow. The Scheme is envisaged to be subject to traffic noise generated from the heavy traffic.
- 5.6 Many residents from Un Chau Estate locating at the east of the Scheme and nearby residential developments locating at the north of the Scheme walk to Cheung Sha Wan Road for public transport services. At present, long queuing at the bus stops often appear along the pavement of Cheung Sha Wan Road, resulting in a crowded condition along the pavement. The major pedestrian circulation is therefore concentrated along the pavement of Cheung Sha Wan Road which is often crowded during peak hours.

6. CULTURAL & LOCAL CHARACTERISTICS, AND CHARACTERISTICS OF LOCAL BUSINESS ACTIVITIES

- 6.1 The Scheme is predominately surrounded by residential buildings to the east while there are more industrial and commercial buildings to the west of the Scheme. To the east across Hing Wah Street is predominantly residential, including a public housing estate Un Chau Estate, while private residential buildings are found mainly to the north of the Scheme. Commercial uses such as retail shops, eateries and car repair shops are found on the ground floor of the surrounded residential buildings.
- 6.2 No shop is identified within the Scheme area.

7. RECREATIONAL, AMENITY & COMMUNITY AND WELFARE FACILITIES

- 7.1 Figure 7.1 shows the location of various GIC facilities and public open spaces within the 500m radius of the Scheme area. There are a number of public open spaces near the Scheme area, the closest being Sham Shui Po Sports Ground located to the south and Hing Wah Street Playground to the east of the Scheme.
- 7.2 The major GIC facilities within the 500m radius of the Scheme area include the Cheung Sha Wan Fire Station and Ambulance Depot, and several educational facilities, including primary schools and secondary schools.
- 7.3 For existing social welfare facilities and services (refer to Table 7.1), family and child welfare services, services for the elderly, rehabilitation and medical social services, services for offenders, and services for young people are found in close proximity to the Scheme.
- 7.4 Despite of the existing G/IC facilities in the neighbourhood, the Scheme would take the redevelopment opportunity to provide not less than 38,000 sq.m. non-domestic GFA for G/IC uses at both sites in the Scheme, which is more than 33 times of the existing provision. The existing Cheung Sha Wan Sports Centre at Site A will be reprovisioned at Site B up to present-day standard and continue its operation. The actual use of the new GIC provision will be subject to liaison with relevant government departments as well as views from local stakeholders after the approval of the DSP. The provision of floor space for GIC uses is in line with the promotion of the government's policy on "Single Site, Multiple Uses".
- 7.5 Opportunities for place making and cohesive greening/landscaping to integrate with surrounding landscape will also be explored. Subject to further co-ordination with LCSD, there is a possible integration of the new POS at Site B with the existing Sham Shui Po Sports Ground in the south to improve the pedestrian friendly environment and to enhance the connectivity of the neighbourhood, upon approval of the DSP and subject to further coordination and acceptancy of relevant Government departments.

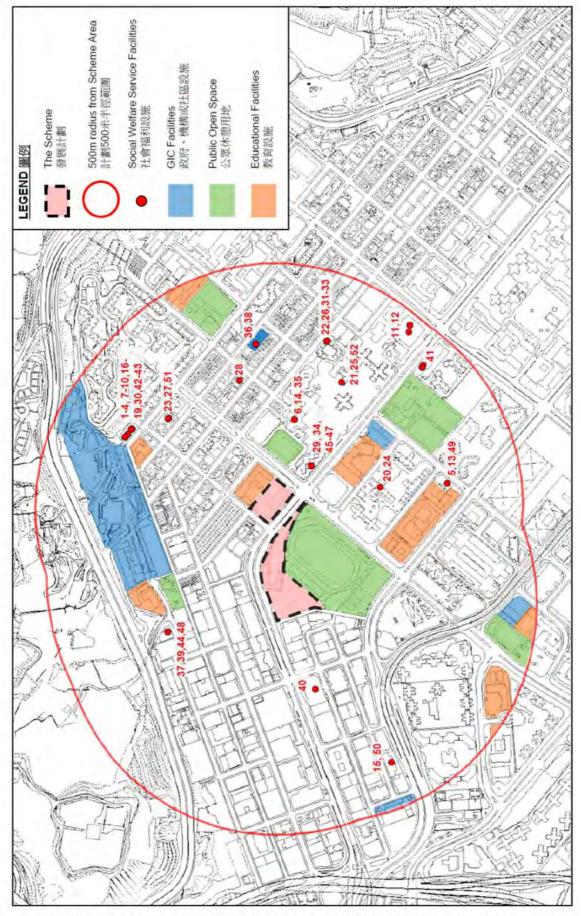


Figure 7.1 G/IC and Amenity Facilities within 500m Radius of the Scheme Area

Table 7.1 Social Welfare Facilities within 500m Radius of the Project Area

Ser	rvice Unit	e Unit Operator Add	
A. I	Family and Child Welfare		
V.J., 1	ency-based Enhancement of Pro	fessional Staff Support	Services in Residential Care
<u>Hoi</u>	<u>mes</u>		ī
1.	Hong Kong Christian Service - So Uk Small Group Home 1	Hong Kong Christian Service	So Uk SGH 1, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
2.	Hong Kong Christian Service - So Uk Small Group Home 2	Hong Kong Christian Service	So Uk SGH 2, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
3.	Hong Kong Christian Service - So Uk Small Group Home 3	Hong Kong Christian Service	So Uk SGH 3, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
4.	Hong Kong Christian Service - So Uk Small Group Home 4	Hong Kong Christian Service	So Uk SGH 4, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
Ext	ended Hours Child Care Service		
5.	Baptist Oi Kwan Social Service - Pui Yan Pre-Primary School (OCCS)	Baptist Oi Kwan Social Service	G/F., 1 Fortune Street, Cheung Sha Wan, Kowloon
6.	Hong Kong Young Women's Christian Association - Chiu Oi Wah Nursery School (OCCS)	The state of the s	Wing B & C, G/F, Un Fung House, Un Chau Estate, Sham Shui Po, Kowloon
Em	ergency/Short-term Care in Sma	III Group Home	
7.	Hong Kong Christian Service - So Uk Small Group Home 1	Hong Kong Christian Service	So Uk SGH 1, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
8.	Hong Kong Christian Service - So Uk Small Group Home 2	Hong Kong Christian Service	So Uk SGH 2, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
9.	Hong Kong Christian Service - So Uk Small Group Home 3	Hong Kong Christian Service	So Uk SGH 3, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
10.	Hong Kong Christian Service - So Uk Small Group Home 4	Hong Kong Christian Service	So Uk SGH 4, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon

Ser	vice Unit	Operator	Address
Fan	nily Aide		
11.	Hong Kong Family Welfare Society - Shamshuipo (West) Integrated Family Service Centre	Hong Kong Family Welfare Society	Unit 204, 2/F, Un Him House, Un Chau Estate, Shamshuipo, Kowloon
Inte	grated Family Service Centre		
12.	Hong Kong Family Welfare Society - Shamshuipo (West) Integrated Family Service Centre	Hong Kong Family Welfare Society	Unit 204, 2/F, Un Him House, Un Chau Estate, Shamshuipo, Kowloon
Occ	casional Child Care Service		
13.	Baptist Oi Kwan Social Service - Pui Yan Pre-Primary School (OCCS)	Baptist Oi Kwan Social Service	G/F., 1 Fortune Street, Cheung Sha Wan, Kowloon
14.	Hong Kong Young Women's Christian Association - Chiu Oi Wah Nursery School (OCCS)	Hong Kong Young Women's Christian Association	Wing B & C, G/F, Un Fung House, Un Chau Estate, Sham Shui Po, Kowloon
Spe	ecialised Co-parenting Support C	<u>Centre</u>	
15.	Hong Kong Family Welfare Society – Parent-child Connect Specialised Co- parenting Support Centre	Hong Kong Family Welfare Society	Unit 302, 3/F, Laford Centre, 838 Lai Chi Kwok Road, Kowloon
Sm	all Group Homes		
16.	Hong Kong Christian Service - So Uk Small Group Home 1	Hong Kong Christian Service	So Uk SGH 1, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
17.	Hong Kong Christian Service - So Uk Small Group Home 2	Hong Kong Christian Service	So Uk SGH 2, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
18.	Hong Kong Christian Service - So Uk Small Group Home 3	Hong Kong Christian Service	So Uk SGH 3, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon
19.	Hong Kong Christian Service - So Uk Small Group Home 4	Hong Kong Christian Service	So Uk SGH 4, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon

Ser	vice Unit	Unit Operator Address	
B. S	Services for the Elderly		
Cor	ntract Home		
20.	Tung Wah Group of Hospitals - Chu Sau Cheung Nursing Home	Tung Wah Group of Hospitals	Unit 302 and 401, 3/F and 4/F, Ancillary Facilities Block, Cheung Sha Wan Estate, 391 Cheung Sha Wan Road, Kowloon
21.	Yan Chai Hospital - Lee Wai Siu Kee Elderly Home	Yan Chai Hospital	G/F (Part) to 2/F, Un Kin House, Un Chau Estate, No. 303 Un Chau Street, Sham Shui Po, Kowloon
Day	Care Centre/Unit for the Elderly	4	
22.	Hong Kong Christian Service - Shamshuipo Day Care Centre for the Elderly		Room 201, 2/F, Un Him House, Un Chau Estate, Sham Shui Po, Kowloon
Dist	trict Elderly Community Centre		
23.	Caritas - Hong Kong - Cheng Shing Fung District Elderly Centre (Sham Shui Po)	Caritas - Hong Kong	UG/F, Lai Bo Garden, 383 Po On Road, Shamshuipo, Kowloon
Nei	ghbourhood Elderly Centre		
24.	Hong Kong Christian Service - Fortune Neighbourhood Elderly Centre	Hong Kong Christian Service	G/F, Fook Yat House, Fortune Estate, Sham Shui Po, Kowloon
25.	Hong Kong Christian Service - Un Chau Neighbourhood Elderly Centre	Hong Kong Christian Service	Wing C, G/F, Un Lok House & Wing C, G/F, Un Nga House, Un Chau Estate, Sham Shui Po, Kowloon
Pilo	t Scheme on Community Care S	Service Voucher for the	<u>Elderly</u>
26.	Yan Chai Hospital - Lee Wai Siu Kee Elderly Home	Yan Chai Hospital	G/F (Part) to 2/F, Un Kin House, Un Chau Estate, No. 303 Un Chau Street, Sham Shui Po, Kowloon
Sup	port Team for the Elderly Based	at District Elderly Com	munity Centres
27.	Caritas - Hong Kong - Cheng Shing Fung District Elderly Centre (Sham Shui Po)	Caritas - Hong Kong	UG/F, Lai Bo Garden, 383 Po On Road, Shamshuipo, Kowloon

Service Unit		Jnit Operator			
Enh	nanced Home and Community C	Care Services			
28.	Tung Wah Group of Hospitals - Enhanced Home and Community Care Service (Sham Shui Po)	Tung Wah Group of Hospitals	Flat C, 3/F, Shun Lee Commercial Building, 338-340 Castle Peak Road, Cheung Sha Wan, Kowloon		
C. F	Rehabilitation and Medical Socia	al Services			
Age	ency-based Occupational Thera	pist Service			
29.	Wai Ji Christian Service - Agency-Based Occupational Therapy Service	Wai Ji Christian Service	1/F, Un Hong House, Un Chau Estate, Sham Shui Po, Kowloon		
Car	re and Attention Home for Sever	rely Disabled Persons v	with Day Care Services for		
Per	sons with Severe Disabilities	1			
30.	Mental Health Association of Hong Kong (The) - So Uk Home	Mental Health Association of Hong Kong (The)	3/F & 4/F, So Uk Amenity and Com. Bldg., So Uk Estate, Sham Shui Po, Kowloon		
Dist	trict Support Centre for Persons	with Disabilities			
31.	Yang Memorial Methodist Social Service - Sham Shui Po District Support Centre	Yang Memorial Methodist Social Service	Unit 201, 2/F, Ancillary Facilities Block, Cheung Sha Wan Estate, Sham Shui Po, Kowloon		
Hor	me-based Rehabilitation Training	g Service			
32.	Yang Memorial Methodist Social Service - Sham Shui Po District Support Centre	Yang Memorial Methodist Social Service	Unit 201, 2/F, Ancillary Facilities Block, Cheung Sha Wan Estate, Sham Shui Po, Kowloon		
Hor	me Care Services for Persons w	vith Severe Disabilities			
33.	Yang Memorial Methodist Social Service - Kowloon (1) Regional Home Care Service	Yang Memorial Methodist Social Service	Unit 201, 2/F, Ancillary Facilities Block, Cheung Sha Wan Estate, Sham Shui Po, Kowloon		
Hos	stel for Moderately Mentally Han	dicapped Persons			
34.	Wai Ji Christian Service - Un Chau Hostel	Wai Ji Christian Service	1/F, Un Hong House, Un Chau Estate, Sham Shui Po, Kowloon		

Ser	vice Unit	Operator	Address	
Inte	grated Programme in Kindergar	ten-cum-Child Care Ce	entre	
35.	Hong Kong Young Women's Christian Association - Chiu Oi Wah Nursery School (OCCS)	Hong Kong Young Women's Christian Association	Wing B & C, G/F, Un Fung House, Un Chau Estate, Sham Shui Po, Kowloon	
On	the Job Training Programme for	People with Disabilitie	<u>s</u>	
36.	Baptist Oi Kwan Social Service - Training & Employment Service (Cheung Sha Wan Centre)	Baptist Oi Kwan Social Service	G/F-2/F, 323 Shun Ning Road, Cheung Sha Wan, Kowloon	
37.	Society of Rehabilitation and Crime Prevention, Hong Kong (The) - Employment Development Service (HQ contact)	Society of Rehabilitation and Crime Prevention, Hong Kong (The)	Flat A, 4/F, Tai Cheong (Liberal) Fty Bldg, 3 Wing Mir Street, Lai Chi Kok, Kowloon	
Sun	nyway - On the Job Training Pro	ogramme for Young Pe	ople with Disabilities	
38.	Baptist Oi Kwan Social Service - Training & Employment Service (Cheung Sha Wan Centre)	Baptist Oi Kwan Social Service	G/F-2/F, 323 Shun Ning Road, Cheung Sha Wan, Kowloon	
39.	Society of Rehabilitation and Crime Prevention, Hong Kong (The) - Employment Development Service (HQ contact)	Society of Rehabilitation and Crime Prevention, Hong Kong (The)	Flat A, 4/F, Tai Cheong (Liberal) Fty Bldg, 3 Wing Ming Street, Lai Chi Kok, Kowloon	
Inte	grated Rehabilitation Services (<u>Centre</u>		
40.	Caritas - Hong Kong - Cheer Home	Caritas - Hong Kong	1/F, Ancillary Facilities Block, Cheung Sha Wan Estate, Sham shui Po, Kowloon	
41.	Po Leung Kuk - So Uk Child Development Centre	Po Leung Kuk	2/F., Amenity and Community Building, So Uk Estate, Sham Shui Po, Kowloon	
Spe	cial Child Care Centres cum Ea	rly Education & Trainin	g Centres	
42.	Po Leung Kuk - So Uk Child Development Centre	Po Leung Kuk	2/F., Amenity and Community Building, So Uk Estate, Sham Shui Po, Kowloon	

Service Unit		Operator	Address
43.	Society of Rehabilitation and Crime Prevention, Hong Kong (The) - Employment Development Service (HQ contact)	Society of Rehabilitation and Crime Prevention, Hong Kong (The)	Flat A, 4/F, Tai Cheong (Liberal) Fty Bldg, 3 Wing Ming Street, Lai Chi Kok, Kowloon
44.	Wai Ji Christian Service - Supported Employment (Sham Shui Po)	Wai Ji Christian Service	1/F, Un Hong House, Un Chau Estate, Sham Shui Po, Kowloon
She	eltered Workshop		
45.	Wai Ji Christian Service - Un Chau Sheltered Workshop	Wai Ji Christian Service	1/F, Un Hong House, Un Chau Estate, Sham Shui Po, Kowloon
Visi	ting Medical Practitioner Schem	<u>e</u>	
46.	Wai Ji Christian Service - Un Chau Hostel	Wai Ji Christian Service	1/F, Un Hong House, Un Chau Estate, Sham Shui Po, Kowloon
D. 8	Services for Offenders		
Ser	vices for Ex-offenders and Disch	narged Prisoners	
47.	Society of Rehabilitation and Crime Prevention, Hong Kong (The) - Employment Development Service (HQ contact)	Society of Rehabilitation and Crime Prevention, Hong Kong (The)	Flat A, 4/F, Tai Cheong (Liberal) Fty Bldg, 3 Wing Ming Street, Lai Chi Kok, Kowloon
E. 5	Services for Young People		
Afte	er School Care Programme		
48.	Baptist Oi Kwan Social Service - [Non-Subvented] Cheung Sha Wan Children Development Education Centre (Formerly known as Cheung Sha Wan After School Care Service)	Baptist Oi Kwan Social Service	1/F., 1 Fortune Street, Cheung Sha Wan, Kowloon

Ser	vice Unit	Operator	Address
49.	Boys' and Girls' Clubs Association of Hong Kong (The) - Nitecat Online - Cyber Youth Support Team	Boys' and Girls' Clubs Association of Hong Kong (The)	Room 202, 2/F, Laford Centre, 838 Lai Chi Kok Road, Cheung Sha Wan, Kowloon
Far	mily Support Networking Team		
50.	Caritas - Hong Kong - Sham Shui Po Family Support Networking Team	Caritas - Hong Kong	UG/F, Lai Po Garden, 383 Po On Road, Sham Shui Po, Kowloon
Dis	trict Youth Outreaching Social W	/ork Teams	
51. Boys' and Girls' Clubs Association of Hong Kong (The) - Sham Shui Po District Youth Outreaching Social Work Team		Boys' and Girls' Clubs Association of Hong Kong (The)	Unit 2, G/F, Un Kin House, Un Chau Estate, Sham Shui Po, Kowloon

Source: Social Welfare Department's website: Local District Service Profile: Welfare Service Units Managed or Funded by Social Welfare Department (Sham Shui Po), as of 10 September 2021.

8. INITIAL ASSESSMENT OF POTENTIAL SOCIAL IMPACT, AND MITIGATION MEASURES

Potential Social Impact

- 8.1 The proposed redevelopment offers an opportunity to optimize land uses through replanning and restructuring, and improve the walkability and connectivity within the Scheme area.
- 8.2 The services and facilities provided in the existing Cheung Sha Wan Path Sitting-out Area at Site B, existing Cheung Sha Wan Sports Centre and garden at Site A will inevitably be interrupted by the proposed redevelopment during construction.

Mitigation Measures

- 8.3 As stated in paragraph 5.2-5.4, Site B of the Scheme will be first redeveloped to provide a public open space (POS) larger than the existing Cheung Sha Wan Path Sitting-out Area and other new GIC facilities to serve the public in a wider area. Under the current planning, it is the intention of URA to relocate the existing Cheung Sha Wan Sports Centre at Site A to Site B after the completion of the new GIC complex. So, the continuous services for public enjoyment can be maintained as far as practicable. Early notification of changes at the sites and careful consideration will be required to minimize the inconvenience caused as far as practicable.
- 8.4 The URA will arrange briefing session(s) and recording video(s) to the stakeholders of the Scheme to explain the planning intentions and procedures of the proposed development.
- 8.5 The Stage 2 SIA to be conducted after the Freezing Survey will further assess the impact of the Scheme in detail on affected persons and propose mitigation measures.

9. CONCLUSION

9.1 This Stage 1 SIA study provides a general profile of the Scheme. The assumptions in this report will be verified by the Stage 2 SIA to be carried out after the Freezing Survey. The needs of the affected persons will be assessed and appropriate arrangements to minimise major adverse social impact, if any, from the Scheme will be proposed in the Stage 2 SIA.

URBAN RENEWAL AUTHORITY September 2021

Appendix 5

Traffic Impact Assessment (TIA) Report



Urban Renewal Authority Development Project in Sham Shui Po (SSP-018)

Traffic Impact Assessment Report

September 2021



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1. Introduction

1.1. Background

- 1.1.1. The Urban Renewal Authority (URA) has proposed a Development Scheme at Cheung Wah Street/ Cheung Sha Wan Road (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). The Scheme is located in Sham Shui Po district, which comprises Sites A and B. Site A of the Scheme is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the southwestern boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B of the Scheme is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary.
- 1.1.2. This Traffic Impact Assessment (TIA) is to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.3. Atkins China Limited (Atkins) was commissioned by URA to conduct a TIA study to assess the traffic impact and the proposal of traffic provisions for the Scheme.

1.2. Scope

- 1.2.1. The scope of this TIA is outlined as follows:
 - conduct surveys to collect the existing traffic flows within the study area;
 - recommend an appropriate and feasible provision and layout of internal transport facilities the proposed development schemes of the Scheme;
 - estimate the vehicular and pedestrian traffic to be generated by the Scheme;
 - forecast the future vehicular and pedestrian traffic demand in the vicinity at the appropriate design year;
 - examine the traffic impact of the Scheme on the surrounding road and pedestrian walkway network; and
 - recommend improvement measures to the problematic roads and junctions, if considered necessary and practicable to the Scheme wherever applicable.

1.3. Report Structure

- 1.3.1. Following this introductory chapter, there are 5 chapters:
 - Chapter 2 presents the Scheme and internal transport facilities;
 - Chapter 3 describes the road network and transport facilities in the vicinity;
 - Chapter 4 describes the methodology for traffic forecasting;
 - Chapter 5 presents the results of the TIA at the adopted design year, and recommends any improvement measures to alleviate the foreseeable traffic problem, if considered necessary; and
 - Chapter 6 summarizes the findings of the study and presents the conclusion.



The Scheme

2.1. Site Location

2.1.1. Site A of the Scheme is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the southwestern boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B of the Scheme is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary. The locations of the subject sites are indicated in Figure 2.1.

2.2. Development Parameters

2.2.1. The subject sites cover a total gross site area of about 19,054 m² and the total net site area for plot ratio calculation is about 9,409 m². The Scheme is anticipated to be completed in two phases and full completion will be by year 2034. The proposed development parameters are tabulated in **Table 2.1**.

Table 2.1 Proposed Development Parameters

C	and a	Development Parameters				
Component		Site A		Site B		
Comple	etion year	2034 Approx. 5,197 m ²		2028 Approx. 13,857 m ²		
Gross	Site Area					
Net S	ite Area	Approx. 5,197 m	n ²	Approx. 4,212 m ²		
Proposed Gross	Residential	Approx. 38,978 m ² GFA	7.5 PR	-	-	
Floor Area (GFA) and Plot	Retail	Approx. 5,197 m ² GFA	1.0 PR	¥	Ψ.	
Ratio (PR)	GIC (1)	Approx. 5,197 m ² GFA	1.0 PR	Approx. 33,696 m ² GFA	8.0 PR	
No. of Bu	ilding Block	2		1		
No. of A $0 \text{ m}^2 \text{ GFA} < \text{Flat}$ Residential Flats Size $\leq 70 \text{ m}^2 \text{ GFA}$		838 Fats		3.		
Average Flat Size		Approx. 47 m ²				
Public O	pen Space	Approx. 750 m ²	2	Approx. 9,645 m	12	

Note: Subject to change at detailed design stage

Remarks: (1) The use of the GIC is not yet confirmed and subject to liaison with government departments upon approval of the Scheme.

2.3. Parking and Servicing Facilities Provision

2.3.1. The required parking and servicing facilities provision are determined in according with the Hong Kong Planning Standards and Guidelines (HKPSG). The requirements and the proposed parking provisions are summarized in **Table 2.2**.



Table 2.2 Required Transport Facilities According to HKPSG

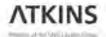
Туре	Parameter	HKPSG Parking Provision Requirement		Required Provision (nos.)	Proposed Provision (nos.)
Site A	1				
Residential					
Private Car Parking Space	838 flats	Global Parking Standard (GPS): 1 car space for 4 - 7 flats Demand Adjustment Ratio (R1): 40 < Flat Size ≤ 70 = 1.2 Accessibility Adjustment Ratio (R2): Within a 500m- radius of rail station = 0.75 Development Intensity Adjustment Ratio (R3): 5.00 < Plot Ratio ≤ 8.00 = 0.90 Parking Requirement = GPS x R1 x R2 x R3	838 units, 40 < Flat Size ≤ 70	97 - 170	97
Visitor Car Parking	2 blocks	5 nos. per residential block with more than 7	75 units	10	10
Motorcycle Parking	838 flats	1 motorcycle parking space per 100-150 flat	ts	6 - 9	9
Loading/ unloading Bay	838 flats/ 2 blocks	1 bay per 800 flats or minimum 1 bay for ea block or as determined by Authority	ch housing	2	2
Retail					
Private Car Parking Space	5,197 m²	Zone 1: Car space per 150 – 300m² GFA		18 – 35	26
Motorcycle Parking	18 – 35	5 – 10% of private car parking space		1-4	3
Loading/ unloading Bay	5,197 m ²	1 bay for GV for every good vehicle for every 800 - 1,200 m ² GFA		5-7	7
GIC Facility (~5,1	97m²) (1)				
Private Car Parking Space		N/A		N/A	9
Loading/ unloading Bay	1	N/A		N/A	1 (2)
Ambulance Lay- by) .	N/A		N/A	1 (3)
Taxi and Private Car Lay-by		N/A		N/A	1 (3)
Motorcycle Parking		N/A		N/A	2 (3)
Underground Pub	olic Carpark				
Private Car Parking Space	- 10-10	£		-	50
		Private Car Parking		125 - 215	192
		Motorcycle Parking		7 – 13	14 (3)
	Site A Total	Loading/ unloading Bay		7-9	9
		Ambulance Lay-by			1 (3)
		Taxi and Private Car Lay-by			1 (3)



Туре	Parameter	HKPSG Parking Provision Requirement	Required Provision (nos.)	Proposed Provision (nos.)	
Accessible Car Parking Space	192	3 spaces for 151-250 total car parking spaces in lot	3	3	
Site B					
GIC Facility (~33,	696 m² GFA) (1)				
Private Car Parking Space	-	N/A	N/A	65 (3)	
Loading/ unloading Bay	1-3-1	N/A	N/A	3 (3)	
Accessible Car Parking Space	65 2 spaces for 51-150 total car parking spaces in lot		2	2 (3)	

Remarks: (1) The intended GIC uses will be subject to further liaison with relevant Government Departments. The proposed transport facilities provision is assumption only.

- (2) Loading/unloading bay to be shared used by the Retail and GIC due to low demand for GIC facilities. However, the provision is assumption only and subject to the GIC operator need in later stage.
- (3) Provision maybe adjusted/ deleted subject to the GIC operator need.
- 2.3.2. As can be seen in the above table, 192 nos. of private car parking space (including 50 nos. of public parking space and 3 nos. of assessable car parking space), 14 nos. of motorcycle parking space, 9 nos. of loading/unloading bay, 1 no. of ambulance lay-by and 1 no. of taxi and private car lay-by are proposed for Site A whist 65 nos. of private car parking space (including 2 nos. of accessible car parking space) and 3 nos. of loading/ unloading bay are proposed for Site B to facilitate the operation of both sites.
- 2.3.3. The proposed parking provision is within the range of the required provision according to the latest HKPSG. Since the subject sites are located within short walking distance to MTR Cheung Sha Wan and Lai Chi Kok Stations, low-end parking provision is adopted for the private car parking space for the residential blocks of Site A.
- 2.3.4. As the type of GIC to be provided at both Sites A and B are not yet identified by relevant government departments, the proposed parking provision for the GIC facilities are assumption only and to be agreed with GIC operator in the detail design stage.
- 2.3.5. Underground public carpark with 50 nos. of private car parking spaces is proposed for Site A to compensate the potential suspension of on-street parking space by the revitalization scheme at the adjacent streets to be proposed by another URA's project. The suspension of on-street parking spaces will make way for pavement widening or partial pedestrianization to enhance walkability in the area under the revitalization scheme.
- 2.3.6. The adjacent street to be affected by the revitalization scheme are including the northern kerb of Fuk Wa Street between Castle Peak Road and Cheung Wah Street and the western kerb of Hing Wah Street between Cheung Sha Wan Road and Fuk Wing Street.



2.3.7. The proposed 50 nos. of public parking spaces are derived based on the existing on-street parking inventory and on-site observation on the parking demand (including illegal parking) at the sections of streets as mentioned in the previous paragraph. The existing parking space inventory and observed parking demand are summarised in Table 2.3.

Table 2.3 Observed Parking Inventory and Demand

Location	Existing Parking Space Revitalization S		Observed Parking Demand (nos.)		
	Private Car	Accessible	Private Car	Accessible	
Fuk Wa Street	20	0	30 (1)	0	
Hing Wah Street	12	2	12	2	
Total	32	2	42	2	

Remarks: (1) Including illegal parking demand.

- 2.3.8. As can be seen in the above table, total numbers of 44 parking spaces (including the accessible parking spaces) are required to accommodate the affected parking spaces by the revitalization scheme and also the additional parking demand and thus 50 numbers of parking spaces are proposed for the underground public carpark at Site A to provide some buffer capacity.
- 2.3.9. Public parking facilities have not been proposed for Site B as the site is above the MTR railway alignment and thus the excavation depth for basement carpark is limited.
- 2.3.10. Besides, 3 and 2 nos. of car parking spaces at Site A and Site B respectively will be reserved for persons with disabilities.
- 2.4. Proposed Layout and Arrangement of Internal Transport Facilities
- 2.4.1. Ancillary car park for the Scheme is mostly provided at the basement levels. Car ramp system is proposed at the two sites to provide vertical connections between the ground and basement levels.

Site A

2.4.2. The ancillary car park for Site A and the proposed public parking spaces are provided in the two basement levels. The loading/unloading area and the Refuse Collection Point are located on Basement Level 1 whilst the private car parking spaces are provided on both parking floors. The required transport facilities to serve the GIC in Site A will also be provided on the Basement Level 1.

Site B

2.4.3. The ancillary car park for Site B is provided on the ground level and the two basement levels. The loading/unloading area is located on the Ground Floor whilst the private car parking spaces are provided on the two parking floors.



- 2.5. Vehicular Access (Run-in/out) Arrangement
- 2.5.1. The proposed run-in/out of Site A of the Scheme would be located at northbound of Hing Wah Street. As the site is abuts Hing Wah Street northbound, Cheung Wah Street southbound and Cheung Sha Wan Road eastbound, Hing Wah Street would be the road with less traffic compare to the others. Moreover, it is also the exit arms of a junction and thus the proposed run-in/out would have less impact to the operation of the adjacent junctions.
- 2.5.2. The schematic layouts of ground level of Site A showing the proposed run-in/out and the typical swept path analysis results are shown in **Figures 2.2** and **2.3**.
- 2.5.3. Three options of run-in/out for Site B have been studied in the early stage of the TIA and detail are descript as below:

Option 1

2.5.4. As the only road abutting Site B is the busy Cheung Sha Wan Road, run-in/out located at westbound of Cheung Sha Wan Road is identified as Option 1 in this study. An existing bus bay at Cheung Sha Wan Road would be affected by the proposed run-in/out and thus relocation of one of the bus stop to the downstream bus bay might be required. This option has been withdrawn from the study due to the impact on existing bus stop.

Option 2

2.5.5. Although Cheung Sha Wan Road is the only public road abutting Site B, alternative has been explored to avoid impact to the busy road. Option 2 is therefore identified at the south-west corner of the site, to make use of the existing driveway for the car park of Sham Shui Po Sports Ground (SSPSG) with run-in/out on Hing Wah Street. This option has also been withdrawn from the study due to it is not preferred administratively.

Option 3

- 2.5.6. In order to provide an access road for the GIC building of Site B, Option 3 is proposed also at the south-west corner of the site but forming a new access road along Cheung Sah Wan Path and connecting Lai Chi Kok Road. The proposed access road in Option 3 would take up some of the area of the adjacent basketball court and thus require additional redevelopment of the area. LCSD suggested URA to explore the feasibility of opening a new access from Lai Chi Kok Road leading to the proposed GIC Complex via the LCSD site with 1 no. of seven-a-side football field and 2 nos. of basketball courts to the immediate southwest of the Sham Shui Po Sports Ground. Hence, Option 3 is proposed which is also feasible from traffic perspective, while the rearrangement of the adjacent ball courts will subject to further liaison with LCSD at detailed design stage.
- 2.5.7. The schematic layout of the run-in/ out, the proposed access road Option 3 and the typical swept path analysis result are illustrated in **Figures 2.4** to **2.6**.



- 2.5.8. As shown in **Figures 2.3**, **2.5** and **2.6**, swept path analysis was assessed at the run-in/out. The result shows that there are sufficient manoeuvring spaces for the ingress and egress movements of a 11m long heavy goods vehicle.
- 2.6. Pedestrian Access Arrangement
- 2.6.1. The anticipated major pedestrian accesses of Site A would be located at both Cheung Wah Street and Hing Wah Street near the boundary of Cheung Sha Wan Catholic Secondary School as an approximate 6.0m walkway connecting the pedestrian entrance of the development is to be provided by building setback.
- 2.6.2. The major pedestrian accesses of Site B would be located at Cheung Sha Wan Road as which is the only frontage to the public road.
- 2.6.3. The building/ podium of Site A will have setback on all four side of the site boundary to provide wider pedestrian walkway and thus enhance the pedestrian walking environment.
- 2.6.4. Moreover, two numbers of footbridges connecting the adjacent URA Project K05/3/002, Site A and Site B of the Scheme will be provided to enhance the connectivity of the redevelopment sites and the public open space at Site B.
- 2.6.5. The footpath along Cheung Sha Wan Road would be the major access route for the east-west direction between the sites and MTR Lai Chi Kok and Cheung Sha Wan Stations. Pedestrian accessing between the sites and the other public transport nodes could via Cheung Sha Wan Road, Hing Wah Street, Lai Chi Kok Road and Cheung Sah Wan Path. The anticipated pedestrian routes are indicated in **Figure 2.7**.



3. Traffic Context

3.1. Road Network

- 3.1.1. The local road network in the vicinity is essentially a grid formed by east-west and north-south running roads.
- 3.1.2. The subject site will be served by the primary distributors of Cheung Sha Wan Road and Lai Chi Kok Road, district distributors of Hing Wah Street, Castle Peak Road, Un Chau Street and Tung Chau Street and the local distributors of Cheung Wah Street. The major vehicular ingress and egress routes to and from the subject sites are shown in **Figure 3.1**.
- 3.1.3. There are four major frontages of the sites abutting Cheung Sha Wan Road, Hing Wah Street and Cheung Wah Street.
- 3.1.4. The section of Cheung Wah Street abutting Site A is a one-way southbound carriageway providing linkage from Castle Peak Road to Cheung Sha Wan Road and also connects the major district/ local distributors such as Un Chau Street, Fuk Wing Street and Fuk Wa Street.
- 3.1.5. Hing Wah Street is a two-way carriageway providing linkage from Po On Road to the north to Tung Chau Street to the south. The section of Hing Wah Street abutting Site A is a dual three-lanes carriage with metered parking space along the kerb.
- 3.1.6. Cheung Sha Wan Road are dual three-lanes carriageway runs in east-west directions providing linkage to Nathan Road to the east and Kwai Chung Road to the west.
- 3.1.7. Castle Peak Road, Un Chau Street, Lai Chi Kok Road and Tung Chau Street runs in east-west direction providing linkage to the adjacent districts.
- 3.1.8. These adjacent roads provide access to/from other areas in the territory. It is anticipated that the subject site will be well served by the existing road network in the vicinity.

3.2. Public Transport Services

3.2.1. Currently, the subject site is serving by several public transport services including MTR, franchised bus, Green Mini-bus (GMB) and Public Light Bus (PLB). The MTR Lai Chi Kok and Cheung Sha Wan Stations are located approximate 300m away from the subject sites. Moreover, there are more than 70 numbers of franchised bus, GMB and PLB routes with servicing points in the vicinity of the subject site. Detail of the services are tabulated in **Table 3.1** and the existing adjacent public transport service points are shown in **Figure 2.7**.



Table 3.1 Existing Public Transport Services

Route No.	Origins & Destinations	Frequency (mins)	
Franchis	ed Bus		
KMB		Q	
6	Star Ferry <-> Lai Chi Kok Bus Terminus	8-10	
37	Olympic Station <-> Kwai Shing (Central)	13-15	
41	Kowloon City Ferry <-> Tsing Yi (Cheung Ching Estate)	25	
42	Shun Lee <-> Tsing Yi (Cheung Hong Estate)	15	
44	Mong Kok East Station <-> Tsing Yi Estate	8-12	
45	Kowloon City Ferry <-> Kwai Chung (Lai Yiu Estate)	20	
46	Jordan (West Kowloon Station) <-> Kwai Chung (Lai Yiu Estate)	25-30	
72	Tai Wo <-> Cheung Sha Wan	15	
86	Wong Nai Tau <-> Mei Foo	15-20	
102	Mei Foo -> Shau Kei Wan	3-6	
102P	Mei Foo -> Shau Kei Wan	7 scheduled service	
171	South Horizons <-> Lai Chi Kok	5-7	
171A	Lei Tung Estate -> Lai Chi Kok	9-15	
171P	South Horizons -> Lai Chi Kok	5-11	
214	Yau Tong <-> Cheung Sha Wan (Kom Tsun Street)	10-13	
904	Kennedy Town (Belcher Bay) <-> Lai Chi Kok	12	
905	Wan Chai North <-> Lai Chi Kok	5-9	
234X	Tsim Sha Tsui East (Mody Road) <-> Tsuen Wan (Bayview Garden)	15	
238X	China Ferry Terminal <-> Tsuen Wan (Riviera Gardens)	12	
265B	Mong Kok (Park Avenue) <-> Tin Heng Estate	5-6	
270B	Olympic Station <-> Sheung Shui	15	
270D	Luen Wo Hui -> Sham Shui Po	1 schedule service	
272E	Sham Shui Po <-> Tai Wo	2 scheduled services	
286C	Shum Shui Po <-> Lee On	6 scheduled services	
286P	Mei Chung Court -> Cheung Sha Wan	5 scheduled services	
286X	Hin Keng <-> Sham Shui Po (Circular)	10	
2A	Lok Wah <-> Mei Foo	8	
2B	Chuk Yuen Estate <-> Cheung Sha Wan	30	
2F	Tsz Wan Shan (North) <-> Cheung Sha Wan	10	
2X	Choi Fook <-> Mei Foo	20	
30X	Whampoa Garden <-> Tsuen Wan (Allway Gardens)	15	
31B	Shek Lei (Tai Loong Street) <-> Olympic Station	12-13	
33A	Mong Kok (Park Avenue) <-> Tsuen Wan (Nina Tower)	15	
35A	Kwai Chung (On Yam Estate) <-> Tsim Sha Tsui East	5-8	
36A	Lei Muk Shue <-> Cheung Sha Wan (Sham Mong Road)	15	
36B	Jordan (West Kowloon Station) <-> Lei Muk Shue	11	
42A	Jordan (West Kowloon Station) <-> Tsing Yi (Cheung Hang Estate)	4-8	
43C	Island Harbourview <-> Tsing Yi (Cheung Hong Estate)	12	



52X	Mong Kok (Park Avenue) <-> Tuen Mun Central	5-9
58X	Mong Kok East Station <-> Leung King Estate	5-8
59X	Mong Kok East Station <-> Tuen Mun Pier Head	3-8
6C	Mei Foo <-> Kowloon City Ferry	9-12
6D	Mei Foo <-> Ngau Tau Kok	12-15
60X	Jordan (West Kowloon Station) <-> Tuen Mun Central	6-8
66X	Olympic Station <-> Tai Hing	8-12
67X	Mong Kok East Station <-> Siu Hong Court	6-11
68X	Mong Kok (Park Avenue) <-> Hung Shui Kiu (Hung Fuk Estate)	10-15
69X	Jordan (West Kowloon Station) <-> Tin Shui	12
86A	Shatin Wai <-> Cheung Sha Wan (Kom Tsun Street)	15
86C	Lee On <-> Cheung Sha Wan	15
98C	Hang Hau (North) (Tseung Kwan O Hospital) <-> Mei Foo	8-10
98S	Lohas Park Station <-> Mei Foo	4 scheduled services
N241	Hung Hom Station <-> Tsing Yi (Cheung Wang Estate)	20
СТВ		A
E21	Tai Kok Tsui (Island Harbourview) <-> AsiaWorld-Expo	10-15
E21A	Ho Man Tin (Oi Man Estate) <-> Tung Chung (Yat Tung Estate)	15
E21C	Tai Kok Tsui (Island Harbourview) <-> Aircraft Maintenance Area	1 scheduled service
N21	Tsim Sha Tsui (Star Ferry) <-> Airport (Ground Transportation Centre)	20
N21A	Tsim Sha Tsui (Star Ferry) <-> Airport (via Yat Tung Estate)	4 scheduled services
KMB/ NV	VFB	
N122	Shau Kei Wan <-> Mei Foo	10
KMB/ CT	В	
N171	Ap Lei Chau Estate <-> Laí Chí Kok	20
Green M		
44S	Hoi Lai Estate < > Castle Peak Road	10-15
45M	Sham Shui Po (Ki Lung Street) < > Wing Hong Street	10
75	Sham Shui Po (Fu Cheong Estate) < > Cheung Sha Wan (Castle Peak Road)	7-9
411	Kwai Chung (Lai Kong Street) < > Sham Shui Po (Un Chau Street)	8-15
97A	Wonderland Villas < > Cheung Sha Wan (Cheung Fat Street)	6-20
Red Min	ibus	
٠.	To Kwa Wan and Hung Hom < > Cheung Sha Wan (Castle Peak Rd)	Depart when fully occupie
-	Wong Tai Sin and Kowloon City < > Cheung Sha Wan (Castle Peak Rd)	Depart when fully occupie
-	Kwun Tong and Wong Tai Sin < > Cheung Sha Wan (Castle Peak Rd)	Depart when fully occupied
-	Ngau Tau Kok Station < > Cheung Sha Wan (HK Spinners Industrial Bldg)	Depart when fully occupied
-	Cheung Sha Wan (HK Spinners Industrial Bldg) < > Kwun Tong (Yee On St)	Depart when fully occupied
	Tsz Wan Shan < > Cheung Sha Wan and Mei Foo	Depart when fully occupie
	To Kwa Wan (Jubilant Place) < > Mei Foo	Depart when fully occupie
	10 KWa Wali (oubliant Flace) ** Well too	Dopart Wholl fully occupie



3.2.2. As shown in the above, the subject site is well served by the existing public transport facilities provided in the vicinity.

3.3. Pedestrian Facilities

3.3.1. The existing pedestrian facilities are well-developed in the vicinity of the subject site. Pedestrians can access the subject sites via the surrounding footpaths and pedestrian crossings to/from nearby taxi, bus and PLB servicing points as well as MTR Lai Chi Kok and Cheung Sha Wan Stations.

3.4. Planned Highway Infrastructure

- 3.4.1. The Central Kowloon Route (CKR) is a dual 3-lane trunk road connecting the West Kowloon reclamation and the proposed Kai Tak Development to relieve traffic congestion on the existing east-west roads across Central Kowloon area and it is anticipated to be commissioned in 2025. In view of the connection point of the CKR, the local traffic pattern near the Scheme would have insignificant impact by the planned road.
- 3.4.2. Except from the widening proposal of Hing Wah Street (which has no programme for implementation at the moment), junction improvement schemes in the area have not been identified and thus the existing road network have been adopted for the assessment.



4. Traffic Forecast

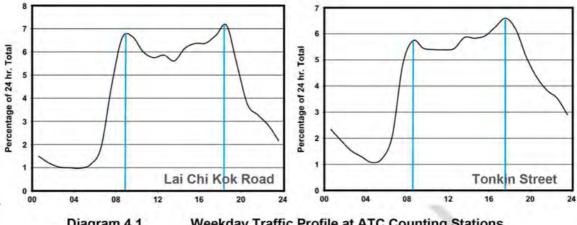
4.1. Methodology

- 4.1.1. According to the current programme, the completion of the Scheme is anticipated to be by phases at year 2028 and 2034 for Site B and A respectively. For the purposes of this study, it has been assumed that full occupation of each site will be occurs in each completion year.
- 4.1.2. Therefore, years 2031 and 2037 (3 years after completion of each site) would be adopted as the design years for assessment purpose.
- 4.1.3. As discussed in the previous Section 3.4, the CKR is planned to be commissioned by year 2025 and the local traffic pattern would have insignificant impact by the new connection bypass the central Kowloon area. Since the road network in design year would be similar to the existing arrangement, the background traffic forecasts for the design years 2031 and 2037 were therefore derived according to the traffic survey results and projected by applying a growth rate. The traffic forecast has been compared with the 2015 Based District Traffic Models (BDTM) K1 published by Transport Department (TD) and found that the set of traffic flows derived by survey results is generally higher.
- 4.1.4. The growth factor used was derived by referring to the past traffic growth trend on the Annual Traffic Census (ATC) Reports published by TD and the latest 2016-based Territory Population and Employment Data Matrices (TPEDM) of Sham Shui Po Area on the website of Planning Department (PlanD).
- 4.1.5. Trip generations by other planned developments in the vicinity were estimated and assigned onto the surrounding road network to produce the reference traffic forecasts at design year.
- 4.1.6. Trip generations of the Scheme was estimated by using appropriate trip generation rates. Traffic generations were then assigned to the surrounding road network and superimposed onto the reference traffic forecasts to create the design year forecasts for assessment at design year.

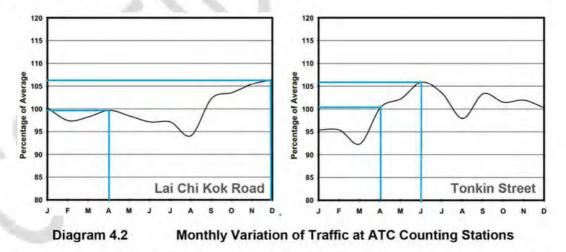
4.2. Traffic Survey

4.2.1. With reference to the weekday daily traffic pattern of the nearest ATC counting stations at Lai Chi Kok Road (from Tonkin Street to Hing Wah Street) and Tonkin Street (from Cheung Sha Wan Road to Un Chau Street) from the subject sites as shown in **Diagram 4.1**. The peak local traffic is occurred around 9:00 and 18:00 during the morning and evening respectively and an afternoon peak is appeared at Tonkin Street around 13:00. As most of the development trips of the Scheme would be generated during the morning and evening peak periods and the local traffic at the evening peak is the peak of the day, manual classified traffic count surveys were conducted to identify the existing traffic flows during the peak hour periods from 07:30 to 09:30 and from 17:00 to 19:00 on a typical weekday in April 2021 to collect the up-to-date traffic data for the assessment use.





- Weekday Traffic Profile at ATC Counting Stations Diagram 4.1
- 4.2.2. As the pandemic situation have been stable, the working arrangement have been resumed to normal and the face-to-face class arrangement have been resumed for most of the school with the upper population limit of two-thirds of the school's maximum capacity during the morning period. The school trips would be very similar to normal situation as the school buses will be operated everyday even with less students on board. Since the afternoon school peak would not be overlapped with the local traffic peak during the evening period, the traffic pattern for the morning and evening peak periods during the survey period is considered under the normal traffic condition.
- 423 The monthly variation of traffic flows at the above mentioned ATC counting stations (as shown in Diagram 4.2) have been referenced to derive the seasonal factor for the local traffic.



- 4.2.4. As can be seen in the above diagram, the peak traffic demand of the year would occur in December and June at Lai Chi Kok Road and Tonkin Street respectively. An average seasonal factor of 1.06 is applied to the observed traffic flows in this study to reflect the peak traffic season scenario of the local area.
- 4.2.5. The locations of the surveyed junctions in the vicinity are listed in Table 4.1 and shown in Figure 2.1.



Table 4.2 Location of Key Junctions

Index (1)	Location	Junction Type	
J1	Castle Peak Road / Hing Wah Street	Signal	
J2	Fuk Wing Street / Cheung Wah Street	Priority	
J3	Un Chau Street / Hing Wah Street	Signal	
J4	Cheung Sha Wan Road / Cheung Lai Street	Signal	
J5	Cheung Sha Wan Road / Tai Nan West Street	Signal	
J6	Cheung Sha Wan Road / Cheung Wah Street	Signal	
J7	Cheung Sha Wan Road / Hing Wah Street	Signal	
J8	Cheung Sha Wan Road / Tonkin Street	Signal	
J9	Lai Chi Kok Road / Cheung Lai Street	Signal	
J10	Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street	Signal	
J11	Lai Chi Kok Road / Hing Wah Street	Signal	
J12	Tung Chau Street / Hing Wah Street West	Signal	
J13	Sham Shing Road / Hing Wah Street West	Signal	

Remarks: (1) Refer to Figure 2.1.

- 4.2.6. The morning and evening peak hours were identified as 08:30 to 09:30 and 17:00 to 18:00 respectively. The year 2021 observed traffic flows are presented in Figure 4.1.
- 4.2.7. Pedestrian head count survey has been conducted at the key section of footpath along the anticipated access routes of the sites during the morning, noon and evening peak periods (07:30 to 09:30, 12:30 to 14:30 and 17:30 to 19:30) on a typical weekday in April 2021 to collect the existing pedestrian demand in the local area.
- 4.2.8. The survey results indicate that the observed peak 15-minute pedestrian demand would be occurs during 08:40 to 08:55, 13:00 to 13:15 and 18:00 to 18:15 in the morning, noon and evening peak periods respectively and the observed pedestrian flows are presented in Figure 4.2.
- 4.2.9. Pedestrian trip generation survey has also been conducted at a similar residential development at 399 Castle Peak Road, Heya Crystal, and the existing Cheung Sha Wan Sport Centre for reference to develop the trip generation rate for the Scheme.
- 4.2.10. In view of the development composition of Heya Crystal with 3 nos. of residential blocks and retail mall in the podium levels, it is located adjacent to the subject sites and completed in the recent years, it is considered as the appropriate site to conduct pedestrian count survey to collect the trip generation data for the study.
- 4.2.11. As Site A of the project would occupy the existing Cheung Sha Wan Sport Centre and to be relocated to the proposed GIC building at Site B, the future sport centre would be serving the same area of local resident and thus the existing pedestrian demand of the sport centre is collected to derive the future demand with reference to the area of both the existing and relocated sport centre.
- 4.2.12. The observed survey results are summarized in Table 4.2.



Table 4.3 Trip Generation Survey Results

.0	No. of	AM Peak		Lunch Peak		PM Peak	
Development	flat/ m ² GFA	GEN (1)	ATT (1)	GEN (1)	ATT (1)	GEN (1)	ATT (1)
		Observ	ed Peak 1	5-minute F m	Pedestrian in)	Demand (ped/15-
Heya Crytal - Residential	350	49	21	24	24	24	47
Heya Crystal - Retail	3,921	57	69	119	141	48	79
Cheung Sha Wan Sports Centre	1,168	14	12	4	10	4	12
		Pedes	strian Trip	Generation 100m ²	n Rate (pe	ed/15-min/	flat or
Heya Crytal - Residential	350	0.1400	0.0600	0.0686	0.0686	0.0686	0.1343
Heya Crystal - Retail	3,921	1.4537	1.7598	3.0349	3.5960	1.2242	2.0148
Cheung Sha Wan Sports Centre	1,168	1.1986	1.0274	0.3425	0.8562	0.3425	1.0274

Remark: (1) "GEN" means "Generation" and "ATT" means Attraction.

4.3. Growth Rate Determination

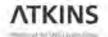
4.3.1. Traffic forecasts for the design years were projected by applying an appropriate growth rate to the observed traffic flows based on the survey results. The growth rates were determined with reference to the ATC reports and the latest 2016-based TPEDM of Sham Shui Po Area on the website of PlanD.

Annual Traffic Census (ATC)

4.3.2. The historical traffic growth trend of the major roads in the vicinity of the subject site was reviewed making reference to the ATC reports. The Annual Average Daily Traffic (AADT) data from year 2013 to year 2019 were extracted and the estimated average annual growth rate is given in **Table 4.3**.

Table 4.4 Traffic Growth Rate Derived from ATC

Station No.	Road Name	AADT							Growth
		2013	2014	2015	2016	2017	2018	2019	Rate (p.a.)
3008	Lai Chi Kok Rd	16,360	16,350	16,280	16,420	16,460	15,530	15,280	
3017	Tonkin St	18,930	18,710	19,580	19,240	18,850	19,320	18,860	1
3225	Cheung Sha Wan Rd	23,350	24,880	24,990	24,770	24,970	25,370	23,670	1
3260	Un Chau St	10,130	10,620	10,970	10,820	10,760	9,000	9,790	1
3261	Castle Peak Rd	16,990	16,600	17,140	16,910	16,800	14,550	12,590	
3263	Hing Wah St	8,650	9,320	9,620	9,490	9,440	13,490	10,870	1
3427	Cheung Sha Wan Rd	30,650	31,990	32,630	35,080	34,850	34,550	37,290	+1.10%
3429	Lai Chi Kok Rd	17,960	16,770	17,850	17,700	17,840	17,960	14,760	
3466	Castle Peak Rd	9,720	9,910	9,160	9,040	8,990	9,110	8,360	1
3468	Hing Wah St	10,470	9,620	9,560	9,430	9,380	9,500	9,580	1
3670	Hing Wah St	9,120	8,850	7,160	7,830	7,780	7,880	7,210	1
3858	Tonkin St	17,430	16,900	17,450	17,320	18,160	18,400	16,840	
3876	Tai Nan W St	7,700	7,460	7,710	7,990	8,120	8,230	7,530	



Station No.	5 - 111	AADT							
	Road Name	2013	2014	2015	2016	2017	2018	2019	Rate (p.a.)
4056	Castle Peak Rd	12,510	12,130	12,530	12,360	11,700	14,380	13,160	
		209,970	210,110	212,630	214,400	214,100	217,270	205,790	

Notes:

The AADT figures with grey colour background are estimated values based on the ATC Reports. Those estimated figures are excluded in calculating the weighted average annual growth rate.

4.3.3. As shown in **Table 4.3**, the weighted average annual growth rate determined from ATC data is about +1.10% per annum (p.a.) from year 2013 to year 2019.

Territory Population and Employment Data Matrices (TPEDM)

4.3.4. Reference was also made to the latest 2016-based TPEDM from year 2016 to year 2026 in Sham Shui Po area published on the PlanD website. The population and employment planning data from year 2016 to 2026 and the estimated annual growth rates are illustrated in **Table 4.4**.

Population Overall Employment District 2016 2021 2026 2016 2021 2026 2016 2021 2026 Sham Shui 438,050 482,700 484,350 235,750 238,900 235,650 673,800 721,600 720,000 Po Growth +1.01% 0.00% +0.67% Rate (p.a.)

Table 4.5 Traffic Growth Rate Derived from TPEDM

4.3.5. As shown in **Table 4.4**, the annual growth rate determined from TPEDM population, employment and the sum of two are about +1.01% p.a., 0% p.a. and +0.67% p.a. respectively from year 2016 to year 2026.

Adopted Growth Rate

4.3.6. Based on the above, the highest growth rate derived from the two sets of data is +1.10% p.a. and thus it is adopted for assessment to produce the years 2031 and 2037 background traffic flows in order to conduct a conservative assessment.

4.4. Other Planned Development Trip Generation

4.4.1. According to the available information, it is noted that there are 22 nos. of planned developments which is under construction or approved in planning application in the vicinity of the subject site and the location are shown in Figure 2.1. These planned developments are assumed to be completed before the design year 2031 in the study and have been considered in the reference traffic flows forecasting. The relevant development parameters are summarised in Table 4.5.

Table 4.6 Design Parameters for Planned Developments

Development Component Parameters



Developments (1)	Development Component	Parameters
217-235 Castle Peak Road & 300-308A	Residential	About 337 Flats
Un Chau Street (SSP-016)	Retail	About 2,474 m ²
24-38 Tonkin Street & 240-244 Fuk Wing	Residential	About 175 Flats
Street (SSP-015)	Retail	About 1,070 m ²
Public Housing Development Projects		
	Residential	About 2,591 Flats
	Retail	About 4,204 m ²
North West Kowloon Reclamation (NWKR) Site 1	Office	About 9,454 m ²
(INVVR) Site I	Kindergarten	6 Classrooms
	Social Welfare Services	About 2,990 m ²
-	Residential	About 2,483 Flats
	Market	About 80 Stalls
	Indoor Sport Centre	About 2,809 m ²
North West Kowloon Reclamation Site 6	District Library	About 2,885 m ²
(Phase 2 & 3 and GIC)	Reserved Stack for Hong Kong Central Library	About 7,263 m ²
	Kindergarten	6 Classrooms
	Social Welfare Services	About 6,600 m ²
	Residential	About 1,200 Flats
Wang Cheong Factory Estate	Retail	About 347 m ²
Private Development Projects		
91 King Lam Street	Office	About 92,736 m ²
121 King Lam Street	Industrial	About 7,320 m ²
1016-1018 Tai Nan West Street	Industrial	About 16,488 m ²
NKIL 6572 Junction of Wing Hong Street, Yu Chau West Street and Wing Ming Street	Office	About 34,473 m ²
550-556 Castle Peak Road	Office	About 21,186 m ²
42A Wing Hong Street	Hotel	132 Rooms
	Residential	About 92 Flats
320-328 Shun Ning Road	Retail	About 349 m ²
	Residential	About 414 Flats
27-29 Tonkin Street	Retail	About 3,605 m ²
7.74.0000	Residential	About 42 Flats
7, 7A, 9 & 9A Cheung Wah Street	Retail	About 451 m ²
916-922 Cheung Sha Wan Road	Office	About 12,000 m ²
924-926 Cheung Sha Wan Road	Office	About 16,000 m ²
	Office	About 49,995 m ²
NKIL 6582 Cheung Shun Street	Public Vehicle Park	85 spaces
822 Lai Chi Kok Road	Office	About 20,279 m ²
CDA Site bounded by Lai Hong Street,	Residential	About 3,647 Flats
Fat Tseung Street West, Sham Mong	Retail	About 11,000 m ²
Road and West Kowloon Corridor	Kindergarten	12 Classrooms



Developments (1)	Development Component	Parameters
	Social Welfare Services	About 3,830 m ²
	Public Vehicle Park	97 spaces
NKIL 6549 Off Hing Wah Street	Residential	About 1,347 Flats
NKIL 6550 Off Hing Wah Street	Hotel	975 Rooms

Remarks: (1) Refer to Figure 2.1 for location of the planned development.

4.4.2. Development trips generated by the above planned developments were estimated making reference to the Transport Planning and Design Manual (TPDM) published by TD, the trip rate adopted in the BDTM and the in-house survey data. Mean value of the trip rate provided in TPDM have been adopted in the study to in line with the forecasting methodology of BDTM. The adopted trip rates and traffic generation of the planned/ committed developments are summarized in Table 4.6.

Table 4.7 Traffic Generation by Planned Developments

Developments (1)	Parameters		00m ² GF	es (pcu/hr A or pcu/h		Trij	o Genera	tion (pcu	/hr)
Shin Lane (SSP-017) 217-235 Castle Peak Road & 300-308A Un Chau Street 24-38 Tonkin Street & 240-244 Fuk Wing Street	Turumeters	AM		PM		AM		PM	
		GEN (3)	ATT (3)	GEN (3)	ATT (3)	GEN (3)	ATT (3)	GEN (3)	ATT (3
Development at Kim	995 Flats	0.0718	0.0425	0.0286	0.0370	71	42	28	37
Shin Lane (SSP-017)	9,249 m ² Retail	0.2296	0.2434	0.3100	0.3563	21	23	29	33
217-235 Castle Peak	337 Flats	0.0718	0.0425	0.0286	0.0370	24	14	10	12
Road & 300-308A Un Chau Street	2,474 m² Retail	0.2296	0.2434	0.3100	0.3563	6	6	8	9
24-38 Tonkin Street &	175 Flats	0.0718	0.0425	0.0286	0.0370	13	7	5	6
240-244 Fuk Wing Street	1,070 m² Retail	0.2296	0.2434	0.3100	0.3563	2	3	3	4
North West Kowloon Reclamation Site 1	2,591 Flats	0.0432	0.0326	0.0237	0.0301	112	84	61	78
	4,204 m ² Retail	0.2296	0.2434	0.3100	0.3563	10	10	13	15
	9,454 m ² Office	0.1703	0.2452	0.1573	0.1175	16	23	15	11
	6 Classrooms	2.3056	2.3056	0.0286	0.0286	14	14	0	0
	2,990 m ² GIC	0.1703	0.2452	0.1573	0.1175	5	7	5	4
$\mathcal{A} = \mathcal{A}$	2,483 Flats	0.0432	0.0326	0.0237	0.0301	107	81	59	75
- / /	80 Stalls	0.1340	0.0860	0.0590	0.0350	11	7	5	3
\sim	Indoor Sport Centre	-	6	1-1		10	10	10	10
North West Kowloon Reclamation Area Site	District Library	-	1.4	16	.9.	10	10	10	10
6	Reserved Stack for Hong Kong Central Library	÷	٥		ē	5	5	5	5
- 1	6 Classrooms	2.3056	2.3056	0.0286	0.0286	14	14	0	0
	6,600 m ² GIC	0.1703	0.2452	0.1573	0.1175	11	16	10	8
Wang Cheong Factory	1,200 Flats	0.0432	0.0326	0.0237	0.0301	52	39	28	36
Estate	347 m² Retail	0.2296	0.2434	0.3100	0.3563	1	1	1	1
91 King Lam Street	92,736 m ² Office	0.1703	0.2452	0.1573	0.1175	158	227	146	109
121 King Lam Street	7,320 m ² Industrial	0.0926	0.1386	0.1350	0.1049	7	10	10	8



Developments (1)	Davanatan			es (pcu/hi A or pcu/h		Trij	p Genera	tion (pcu	/hr)
Developments (1)	Parameters	A	M	PM		AM		PM	
		GEN (3)	ATT (3)	GEN (3)	ATT (3)	GEN (3)	ATT (3)	GEN (3)	ATT (3
1016-1018 Tai Nan West Street	16,488 m ² Industrial	0.0926	0.1386	0.1350	0.1049	15	23	22	17
NKIL 6572 at Wing Hong Street	34,473 m ² Office	0.1703	0.2452	0.1573	0.1175	59	85	54	41
550-556 Castle Peak Road	21,186 m ² Office	0.1703	0.2452	0.1573	0.1175	36	52	33	25
42A Wing Hong Street	132 Hotel Rooms	0.1329	0.1457	0.1290	0.1546	18	19	17	20
320-328 Shun Ning	92 Flats	0.0718	0.0425	0.0286	0.0370	7	4	3	3
Road	349 m² Retail	0.2296	0.2434	0.3100	0.3563	1	1	1	1
27 20 Tankin Street	414 Flats	0.0718	0.0425	0.0286	0.0370	30	18	12	15
27-29 Tonkin Street	3,605 m ² Retail	0.2296	0.2434	0.3100	0.3563	8	9	11	13
7, 7A, 9 & 9A Cheung	42 Flats	0.0718	0.0425	0.0286	0.0370	3	2	1	2
Wah Street	451 m ² Retail	0.2296	0.2434	0.3100	0.3563	1	1	1	2
916-922 Cheung Sha Wan Road	12,000 m ² Office	0.1703	0.2452	0.1573	0.1175	20	29	19	14
924-926 Cheung Sha Wan Road	16,000 m ² Office	0.1703	0.2452	0.1573	0.1175	27	39	25	19
NIKIL CEOO OL	49,995 m ² Office	0.1703	0.2452	0.1573	0.1175	85	123	79	59
NKIL 6582 Cheung Shun Street	85 Public Parking Spaces	0.1000	0.0949	0.1154	0.0846	9	8	10	7
822 Lai Chi Kok Road	20,279 m ² Office	0.1703	0.2452	0.1573	0.1175	35	50	32	24
	3,647 Flats	0.0718	0.0425	0.0286	0.0370	262	155	104	135
	11,000 m ² Retail	0.2296	0.2434	0.3100	0.3563	25	27	34	39
CDA Site at Fat	12 Classrooms	6.9375	6.9375	5.4375	5.4375	83	83	65	65
Tseung Street West	3,830 m ² GIC	0.1703	0.2452	0.1573	0.1175	7	9	6	5
	97 Public Parking Spaces	0.1000	0.0949	0.1154	0.0846	10	9	11	8
NKIL 6549 Off Hing Wah Street	1,347 Flats	0.0888	0.0515	0.0356	0.0480	120	69	48	65
NKIL 6550 Off Hing Wah Street	975 Hotel Rooms	0.1329	0.1457	0.1290	0.1546	130	142	126	151
N 1					Total	1,671	1,610	1,175	1,204

Remarks: (1) Refer to Figure 2.1 for location of the planned development.

(3) "GEN" means "Generation" and "ATT" means Attraction.

* Trip Generation is rounded to the nearest digit.

Note:

4.4.3. As shown in **Table 4.6**, the planned developments will generate overall 2-way trips of 2,541 pcu/hr and 1,806 pcu/hr during the morning and evening peak hour respectively.

⁽²⁾ Refer to TPDM Vol. 1, Ch. 3, Appendix, Table 1 and Table 2, BDTM Urban Final Report, Appendix Q or inhouse survey results for public wet market and public car park;



4.4.4. In order to produce a comprehensive assessment results, the pedestrian trips to be generated by the adjacent planned development at Kim Shin Lane and 7, 7A, 9 & 9A Cheung Wah Street have also been considered in the TIA study and it is summarised in Table 4.7.

Table 4.8 Pedestrian Trip Generation by Planned Development

Development	No. of flat/	AM I	Peak	Lunch	Peak	PM Peak	
Use	m ² GFA	GEN (1)	ATT (1)	GEN (1)	ATT (1)	GEN (1)	ATT (1)
		Pedestr	ian Trip Ger	eration Rate	(ped/15-mi	n/flat or 100	m² GFA)
Residential		0.1400	0.0600	0.0686	0.0686	0.0686	0.1343
Retail		1.4537	1.7598	3.0349	3.5960	1.2242	2.0148
			Pedestr	ian Trip Gen	eration (ped	/15-min)	
Residential Develo	pment at Kin Sh	in Lane		- 6	-12		
Residential	995	139	60	68	68	68	134
Retail	9,249	134	163	281	333	113	186
Residential Develo	pment at 7, 7A,	9 & 9A Che	ung Wah Str	eet		-	
Residential	42	6	3	3	3	3	6
Retail	451	7	8	14	16	6	9
	Total	286	234	366	420	190	335

Remarks:

(1) "GEN" means "Generation" and "ATT" means Attraction.

* Trip Generation is rounded to the nearest digit.

4.5. Reference Traffic Flows

4.5.1. The traffic and pedestrian demand to be generated/ attracted by the planned/ committed developments will be assigned on the surrounding road network and superimposed onto the years 2031 and 2037 background traffic flows to produce the reference traffic and pedestrian flows. The years 2031 and 2037 reference traffic and pedestrian flows are shown in Figures 4.3 to 4.5.

4.6. Development Traffic Generation

4.6.1. Trip generation of the Scheme is estimated using the appropriate trip rates given in TPDM and in-house survey data. The estimation of traffic trips to be generated by the Scheme is summarized in **Table 4.8**.

Table 4.9 Traffic Generation by the Scheme

Component		(pcu/hr	Adopted Trip Rates u/hr/flat or pcu/hr/100 m² GFA) (1)			T	r)		
	Parameter	AM		PM		AM		PM	
		GEN (2)	ATT (2)	GEN (2)	ATT (2)	GEN (2)	ATT (2)	GEN (2)	ATT (2)
Site A									
Residential	838 flats	0.0718	0.0425	0.0286	0.0370	60	36	24	31
Retail	5,197 m ²	0.2296	0.2434	0.310	0.3563	12	13	16	19
GIC (3)	5,197 m ²	0.1703	0.2452	0.1573	0.1175	9	13	8	6



					Total	142	143	107	102
GIC (3)	27,116 m ²	0.1703	0.2452	0.1573	0.1175	46	66	43	32
Indoor Recreation Centre (4)	6,580 m²	4	i e		19,	10	10	10	10
Site B									
Underground Public Carpark	50 space	0.1000	0.0949	0.1154	0.0846	5	5	6	4

Remarks: (1) Refer to TPDM Vol. 1, Ch. 3, Appendix, Table 1 and Table 2 or in-house survey results for TD managed public car park;

(2) "GEN" means "Generation" and "ATT" means Attraction;

(3) Trip rate for GIC referenced to Office rate in TPDM Vol. 1, Ch. 3, Appendix, Table 2

Note:

* Trip Generation is rounded to the nearest digit.

- 4.6.2. As presented in the above table, the Scheme will produce 2-way trips of 285 pcu/hr and 209 pcu/hr during the morning and evening peak hours respectively.
- 4.6.3. Nominal traffic trip for the Indoor Recreation Centre at Site B is proposed due to it is serving the local area and thus most of the user will make their trips to the centre onfoot. Besides, public parking will not be provided at Site B, it will also encourage the user to the public transport instead.
- 4.6.4. The forecast of pedestrian trip generation for the Scheme was derived with reference to the development schedule and the observed pedestrian trip generation rates in Table 4.2. The estimated pedestrian trips of the Scheme during the peak hour periods are tabulated in Table 4.9.

Table 4.10 Pedestrian Trip Generation by the Scheme

Development	No. of flat/ m ²	AMI	Peak	Lunch	Peak	PM Peak		
Use	GFA	GEN (1)	ATT (1)	GEN (1)	ATT (1)	GEN (1)	ATT (1)	
	11	Pedestri	an Trip Gen	eration Rate	(ped/15-mi	n/flat or 100	m² GFA)	
Residential	-3/	0.1400	0.0600	0.0686	0.0686	0.0686	0.1343	
Retail	100	1.4537	1.7598	3.0349	3.5960	1.2242	2.0148	
Sport Centre		1.1986	1.0274	0.3425	0.8562	0.3425	1.0274	
7 /	1		Pedestri	an Trip Gen	eration (ped	1/15-min)		
Site A	1							
Residential	838	117	50	57	57	57	113	
Retail	5,197	76	91	158	187	64	105	
GIC (2)	5,197	10	10	10	10	10	10	
	Sub-total	203	151	225	254	131	228	
Site B								
Indoor Recreation Centre	6,580	79	68	23	56	23	68	
GIC (2)	27,116	50	50	50	50	50	50	
	Sub-total	129	118	73	106	73	118	
	Total	332	269	298	360	204	346	



Remarks: (1) "GEN" means "Generation" and "ATT" means Attraction.

(2) Pedestrian trips are assumed value. The type of G/IC facilities is to be confirmed with government

departments.

Note: * Trip Generation is rounded to the nearest digit.

4.6.5. As can be seen in the above table, the peak demand of 2-way pedestrian trips would be 658 ped/15-minute during the noon peak. The estimated pedestrian trip to be generated by the Scheme will be assigned onto the surrounding pedestrian walkway network based on the trip distribution to/from the major transport node with reference to the model split of the 2016 population by-census results of the adjacent residential buildings as shown in **Table 4.10**.

Table 4.11 Modal Split Adopted for the Subject Development

Providence	Type of	Population	Population Census Model Split (1)							
Development	Population		MTR	BUS	PLB	Walk	Other	Total		
473 & 473A Castle Peak Road, odd number of 535 –	Working	982	60.4%	11.3%	7.3%	21.0%	0%	100%		
573 Fuk Wing Street & 1 – 41 Kim Shin Lane	Student	256	26.7%	15.4%	(2)	38.6%	19.3%	100%		
475 & 475A Castle Peak Road, even number of 544 –	Working	979	42.6%	20.9%	16.5%	18.5%	1.5%	100%		
588 Fuk Wa Street & 2 – 44 Kim Shin Lane	Student	265	24.2%	21.2%	_ (2)	38.0%	16.6%	100%		
	Overall	2,482	45.9%	16.6%	9.4%	23.7%	4.4%	100%		

Remarks:

(1) Year 2016 population by-census results:

(2) PLB trips are classified as "Other" for the model split of student's trips.

4.6.6. The estimated development pedestrian trips for each transport mode are then distributed onto the pedestrian network and superimposed onto the 2031 and 2037 reference pedestrian flows to produce the 2031 and 2037 design pedestrian flows (with the Scheme). The 2031 and 2037 design pedestrian forecasts are shown in Figure 4.6.

4.7. Design Traffic Flows

- 4.7.1. The estimated development vehicular flows of the Scheme were assigned on the surrounding road network according to the vehicle access route of each site and superimposed onto the years 2031 and 2037 reference traffic flows to produce the design traffic flows.
- 4.7.2. The years 2031 and 2037 design traffic flows during the peak hours are shown in Figures 4.7 and 4.8.



Traffic Impact Assessment

5.1. Methodology

- 5.1.1. Junction capacity analysis was conducted for the base year 2021 and design years 2031 and 2037 (three years after completion of each site) for the junctions which are likely to be affected by the Scheme.
- 5.1.2. Capacity analysis was carried out in accordance with the procedures outlined in the Transport Planning and Design Manual (TPDM). The capacity analysis was based on the observed traffic flows at year 2021 and traffic forecasts at design years 2031 and 2037 for Reference Scenarios (without the Scheme) and Design Scenarios (with the Scheme).

5.2. Junction Analysis

5.2.1. The results of the capacity analysis for existing year 2021 Observed Scenario, design years 2031 and 2037 Reference and Design Scenarios are summarized in Tables 5.1, 5.2 and 5.3 respectively. The calculation sheets are attached in Appendix B.

Table 5.1 Junction Performance for Year 2021 Observed Scenario

Index	1	Junction	RC%/	DFC (2)
(1)	Location	Туре	AM	PM
J1	Castle Peak Road / Hing Wah Street	Signal	>50%	>50%
J2	Fuk Wing Street / Cheung Wah Street	Priority	0.68	0.55
J3	Un Chau Street / Hing Wah Street	Signal	>50%	>50%
J4	Cheung Sha Wan Road / Cheung Lai Street	Signal	>50%	>50%
J5	Cheung Sha Wan Road / Tai Nan West Street	Signal	32%	46%
J6	Cheung Sha Wan Road / Cheung Wah Street	Signal	>50%	>50%
J7	Cheung Sha Wan Road / Hing Wah Street	Signal	35%	26%
J8	Cheung Sha Wan Road / Tonkin Street	Signal	>50%	50%
J9	Lai Chi Kok Road / Cheung Lai Street	Signal	32%	47%
J10	Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street	Signal	>50%	>50%
J11	Lai Chi Kok Road / Hing Wah Street	Signal	12%	14%
J12	Tung Chau Street / Hing Wah Street West	Signal	16%	21%
J13	Sham Shing Road / Hing Wah Street West	Signal	>50%	>50%

Remarks: (1) Refer to Figure 2.1.

5.2.2. As can be seen in Table 5.1, most of the assessed key junctions are operating satisfactorily in the existing year 2021 (RC ≥ 15% or DFC ≤ 0.85). Besides, the junction of Lai Chi Kok Road / Hing Wah Street (J11) would be operated below the marginal capacity (RC <15%) especially during the morning peak period.</p>

^{(2) &}quot;RC%" means reserved capacity and "DFC" means design flow capacity.



Table 5.2 Junction Performance for Year 2031

		RC%/ DFC (2)						
Index	Location	Refe	rence	Design				
,,,		AM	PM	AM	PM			
J1	Castle Peak Road / Hing Wah Street	>50%	>50%	>50%	>50%			
J2	Fuk Wing Street / Cheung Wah Street	0.86	0.69	0.86	0.69			
J3	Un Chau Street / Hing Wah Street	>50%	>50%	>50%	>50%			
J4	Cheung Sha Wan Road / Cheung Lai Street	45%	41%	42%	39%			
J5	Cheung Sha Wan Road / Tai Nan West Street	-12%	11%	-12%	11%			
J6	Cheung Sha Wan Road / Cheung Wah Street	37%	32%	37%	32%			
J7	Cheung Sha Wan Road / Hing Wah Street	12%	8%	9%	6%			
J8	Cheung Sha Wan Road / Tonkin Street	29%	29%	29%	28%			
J9	Lai Chí Kok Road / Cheung Lai Street	-1%	13%	-3%	11%			
J10	Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street	22%	31%	22%	31%			
J11	Lai Chi Kok Road / Hing Wah Street	-8%	-5%	-8%	-5%			
J12	Tung Chau Street / Hing Wah Street West	-5%	2%	-5%	2%			
J13	Sham Shing Road / Hing Wah Street West	>50%	>50%	>50%	>50%			

Remarks:

(1) Refer to Figure 2.1.

5.2.3. As shown in **Tables 5.2**, the junctions of Cheung Sha Wan Road / Hing Wah Street (J7) would be operating below the marginal capacity limit (i.e. RC ≤ 15%) in design year 2031 even without the operational of Site B of the Scheme. Moreover, the junctions of Cheung Sha Wan Road / Tai Nan West Street (J5), Lai Chi Kok Road / Cheung Lai Street (J9), Lai Chi Kok Road / Hing Wah Street (J11) and Tung Chau Street / Hing Wah Street West (J12) would be operating over capacity (i.e. RC ≤ 0) during the peak hours under the Reference Scenario in 2031.

Table 5.3 Junction Performance for Year 2037

		RC%/ DFC (2)					
Index	Location	Refe	rence	Design			
**		AM	PM	AM	PM		
J1	Castle Peak Road / Hing Wah Street	>50%	>50%	>50%	>50%		
J2	Fuk Wing Street / Cheung Wah Street	0.92	0.73	1.04	0.80		
J3	Un Chau Street / Hing Wah Street	>50%	>50%	45%	>50%		
J4	Cheung Sha Wan Road / Cheung Lai Street	37%	32%	33%	31%		
J5	Cheung Sha Wan Road / Tai Nan West Street	-16%	5%	-16%	5%		
J6	Cheung Sha Wan Road / Cheung Wah Street	28%	23%	25%	22%		
J7	Cheung Sha Wan Road / Hing Wah Street	5%	2%	2%	-1%		
J8	Cheung Sha Wan Road / Tonkin Street	21%	21%	21%	21%		
J9	Lai Chi Kok Road / Cheung Lai Street	-6%	6%	-8%	5%		
J10	Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street	15%	24%	15%	24%		
J11	Lai Chi Kok Road / Hing Wah Street	-14%	-10%	-14%	-11%		
J12	Tung Chau Street / Hing Wah Street West	-10%	-4%	-11%	-5%		
J13	Sham Shing Road / Hing Wah Street West	>50%	>50%	>50%	>50%		

^{(2) &}quot;RC%" means reserved capacity and "DFC" means design flow capacity.



Remarks: (1) Refer to Figure 2.1.

(2) "RC%" means reserved capacity and "DFC" means design flow capacity.

- 5.2.4. As shown in **Tables 5.3**, the junctions of Fuk Wing Street/ Cheung Wah Street (J2) and Cheung Sha Wan Road / Hing Wah Street (J7) would be operating below the marginal capacity limit (i.e. RC ≤ 15%) in design year 2037 even without the Scheme.
- 5.2.5. The junctions of Cheung Sha Wan Road / Tai Nan West Street (J5), Lai Chi Kok Road / Cheung Lai Street (J9), Lai Chi Kok Road / Hing Wah Street (J11) and Lai Chi Kok Road / Hing Wah Street West (J12) would be overloaded in year 2037 under the Reference Scenario.
- 5.2.6. Owing to the foreseeable adverse traffic conditional to be induced by the traffic growth of the district in the Reference Scenarios and the minor traffic impact (0 to 3%) to be induced by the Scheme to the Junctions J5, J7, J9, J11 and J12, junction improvement schemes are suggested for TD consideration to enhance the operational performance of the critical junctions.
- 5.2.7. Besides, junction improvement scheme is proposed for Junction J2 to mitigate the traffic impact to be induced by the Scheme.
- 5.3. Junction Improvement Schemes
- 5.3.1. Junction improvement schemes are proposed for the junction to be affected by the development traffic of the Scheme and suggested for the five junctions to be below marginal capacity or overloaded in the design year even without the operation of the Scheme.
 - <u>Proposed Improvement for Junction of Fuk Wing Street / Cheung Wah Street (J2) Figure 5.1</u>
- 5.3.2. The existing operational performance is restricted by the visibility from the give-way arm of the junction at southbound of Cheung Wah Street. In order to enhance the operation, it is proposed to re-arrange the give-way arm to Fuk Wing Street. As the traffic flow from Cheung Wah Street is higher than Fuk Wing Street, the proposed give-way arrangement at Fuk Wing Street would benefit the traffic flow on Cheung Wah Street.
- 5.3.3. Moreover, it is noted that building setback at Cheung Wah Street will be proposed by the adjacent planned development and thus the visibility from Fuk Wing Street to the right side of Cheung Wah Street southbound will be improved.
 - <u>Suggested Improvement for Junction of Cheung Sha Wan Road / Tai Nan West Street (J5) Figure 5.2</u>
- 5.3.4. The operational performance of the junction of Cheung Sha Wan Road / Tai Nan West Street during the critical morning peak hour is dictated by the heavy traffic flows at the left-turn of Cheung Sha Wan Road eastbound and northbound of Tai Nan West Street.



- 5.3.5. In order to provide more capacity for the critical traffic movement, it is suggested to modify the road marking at eastbound of Cheung Sha Wan Road to provide exclusive left-turn lane and shared straight ahead and left-turn traffic lanes for the near side two lanes and maintain the existing signal phasing sequence. The proposed junction arrangement as shown in **Figure 5.2**.
 - <u>Suggested Improvement for Junction of Cheung Sha Wan Road / Hing Wah Street</u> (J7) Figure 5.3
- 5.3.6. The operational performance of the junction of Cheung Sha Wan Road / Hing Wah Street is dictated by the heavy traffic flows along both directions of Cheung Sha Wan Road. As widening to Cheung Sha Wan Road is not feasible due to site constraint and the east-west traffic already running concurrently in the traffic signal phase, enhancement could only be proposed at both arms of Hing Wah Street.
- 5.3.7. In order to enhance the operation, it is proposed to provide one additional traffic lane at both directions of Hing Wah Street and maintain the existing signal phasing sequence. The proposed junction arrangement as shown in **Figure 5.3**.
 - <u>Suggested Improvement for Junction of Lai Chi Kok Road / Cheung Lai Street (J9)</u>
 Figure 5.4
- 5.3.8. The junction of Lai Chi Kok Road / Cheung Lai Street is overloaded due to the heavy traffic along eastbound of Lai Chi Kok Road. An additional traffic lane is suggested at Lai Chi Kok Road near the junction to increase the capacity of the critical carriageway.
- 5.3.9. The existing traffic signal phasing sequence will be maintained and the proposed junction arrangement as shown in **Figure 5.4**.
 - <u>Suggested Improvement for Junction of Lai Chi Kok Road / Hing Wah Street (J11)</u> <u>- Figure 5.5</u>
- 5.3.10. Similar to Junction J7, the operational performance of the junction of Lai Chi Kok Road / Hing Wah Street is dictated by the heavy traffic flows along both directions of Lai Chi Kok Road, however widening of the road is not feasible due to site constraint.
- 5.3.11. In order to enhance the operation, it is suggested to ban the right-turn movement of Hing Wah Street northbound, provide split phase for the right-turn of Hong Wah Street southbound and modify the vehicle phasing for the north-south directions along Hing Wah Street to runs concurrently.
- 5.3.12. It is anticipated that the affect right-turn from Hing Wah Street northbound would has 70 pcu/hr and 95 pcu/hr traffic during the morning and evening peak periods in the design year 2037. The affect traffic may choose the turn earlier at the junction with Tung Chau Street or turn later at the junction with Cheung Sha Wan Road. However, the diverted traffic may affect the already critical Junction J7.
- 5.3.13. The suggested junction arrangement and signal phasing are as shown in **Figure 5.5**.

 <u>Suggested Improvement for Junction of Tung Chau Street / Hing Wah Street (J12)</u>

 <u>- Figure 5.6</u>



- 5.3.14. The junction of Tung Chau Street / Hing Wah Street would have the similar situation with Junctions J11 and thus junction improvement with ban turn, split phase and north-south traffic running concurrently at the traffic sign phasing are suggested. The affected ban turn for this junction would have only 5 pcu/hr at both peak period in the design year of 2037. Therefore, the diverted traffic would have neglectable impact to the surrounding road network. The suggested junction arrangement and signal phasing are as shown in Figure 5.6.
- 5.3.15. The operational performance of the proposed and suggested junction improvement schemes are summerised in **Table 5.4**.

Table 5.4 Junction Performance in Design Years with Improvement Measure

		RC%/ DFC (2)								
Index	Location	2031 Reference		2031 Design		2037 Reference		2037 Design		
.,,		AM	PM	AM	PM	AM	PM	AM	PM	
J2	Fuk Wing Street / Cheung Wah Street	0.75	0.72	0.75	0.72	0.80	0.76	0.82	0.77	
J5	Cheung Sha Wan Road / Tai Nan West Street	29%	34%	26%	32%	21%	26%	18%	24%	
J7	Cheung Sha Wan Road / Hing Wah Street	15%	11%	12%	10%	8%	4%	6%	3%	
J9	Lai Chi Kok Road / Cheung Lai Street	20%	37%	17%	34%	14%	29%	11%	27%	
J11	Lai Chi Kok Road / Hing Wah Street	31%	34%	31%	34%	23%	26%	23%	26%	
J12	Tung Chau Street / Hing Wah Street West	15%	22%	15%	22%	8%	15%	8%	14%	

Remarks:

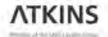
(1) Refer to Figure 2.1.

- 5.3.16. As can be seen in the assessment results, three of the concerned junctions would be operated within the marginal capacity in the design year 2037 with the implementation of improvement scheme whilst the junction of Cheung Sah Wan Road / Hing Wah Street (J7), Lai Chi Kok Road / Cheung Lai Street (J9) and Tung Chau Street / Hing Wah Street (J12) would be operated below the marginal capacity (i.e. RC ≤ 15%).
- 5.3.17. As the critical vehicle phase for Junctions J7, J9 and J12 are on the mainstream Cheung Sha Wan Road, Lai Chi Kok Road and Tung Chau Street respectively and the capacity of those road could not be enhanced due to site constraint. Potential improvement to the three junctions is limited.
- 5.3.18. As indicated by the assessment results in **Tables 5.2** and **5.3**, the proposed/ suggested junction improvement scheme is proposed to be implemented by phases according to the schedule in **Table 5.5** to mitigate the foreseeable adverse traffic conditions.

Table 5.5 Junction Improvement Scheme Implementation Proposal

Index (1)	Location	Implementation Year
J2	Fuk Wing Street / Cheung Wah Street	By 2037
J5	Cheung Sha Wan Road / Tai Nan West Street	By 2031
J7	Cheung Sha Wan Road / Hing Wah Street	By 2031
J9	Lai Chi Kok Road / Cheung Lai Street	By 2031
J11	Lai Chi Kok Road / Hing Wah Street	By 2031

^{(2) &}quot;RC%" means reserved capacity and "DFC" means design flow capacity.



Index (1)	Location	Implementation Year
J12	Tung Chau Street / Hing Wah Street West	By 2031

Remarks: (1) Refer to Figure 2.1.

5.4. Pedestrian Walkway Assessment

- 5.4.1. Existing performance of the key footpath and pedestrian crossing facilities likely to be affected by the Scheme are assessed with the observed pedestrian traffic flows.
- 5.4.2. Current performance of the key pedestrian links is summarized in **Table 5.6** below in terms of Level-of-Service (LOS). The key footpath sections are currently operating desirably during the morning, noon and evening peak periods with all of those having LOS A. The evening peak was found to have higher pedestrian demand than the morning and noon peaks in most of these key pedestrian linkages. For details of the LOS, please refer to **Section 5.4.3** and **Table 5.7** below.

Table 5.6 Existing Key Pedestrain Link Performance

Ref	Footp ath Width (m)	Effective	Observed Pedestrian Demand (pph)			Flow	Rate (p)	om/m)	LOS		
		Width (m) (2)	AM Peak	Noon Peak	PM Peak	AM Peak	Noon Peak	PM Peak	AM Peak	Noon Peak	PM Peak
P1	2.5	1.5	210	235	260	9.3	10.4	11.6	Α	Α	Α
P2	3	1	60	105	130	4.0	7.0	8.7	Α	Α	Α
P3	3.5	2.5	70	105	230	1.9	2.8	6.1	Α	Α	Α
P4	3.5	2.5	150	45	140	4.0	1.2	3.7	Α	Α	Α
P5	4.5	3.5	75	115	135	1.4	2.2	2.6	Α	Α	Α
P6	4.7	3.7	75	120	145	1.4	2.2	2.6	Α	Α	Α
P7	3.5	2	300	170	365	10.0	5.7	12.2	Α	A	Α

Remarks: (1) Refer to Figure 4.2.

5.4.3. Performance of walkway is measured by LOS based on Highway Capacity Manual (HCM) 2000 (Exhibit 11-8). It illustrates the degree of congestion in pedestrian facilities. The definition of LOS is illustrated in Table 5.7. The TPDM states that the "LOS C is desirable for most design at streets with dominant 'living' pedestrian facilities".

⁽²⁾ Effective Width = Footpath Width - Dead Width (0.5m for kerb/ wall/ fence, 0.7m for shop frontage and 1.0m for tree pits along the eastern footpath of Cheung Wah Street).



Table 5.7 Pedestrian Walkway LOS

LOS	S Flow Rate (ppm) Description						
Α	≤ 16	Pedestrians move in desired paths without altering their movements in response to other pedestrians. Walking speeds are freely selected, and conflicts between pedestrians are unlikely.					
В	16 – 23	There is sufficient area for pedestrians to select walking speeds freely, to bypass other pedestrians, and to avoid crossing conflicts. At this level, pedestrians begin to be aware of other pedestrians, and to respond to their presence when selecting a walking path.					
С	23 – 33	Space is sufficient for normal walking speeds, and for bypassing other pedestrians in primarily unidirectional streams. Reverse-direction or crossing movements can cause minor conflicts, and speeds and flow rate are somewhat lower.					
D	33 – 49	Freedom to select individual walkway speeds and to bypass other pedestrians is restricted. Crossing or reserve-flow movements face a high probability of conflict, requiring frequent changes in speed and position. The LOS provides reasonably fluid flow, but friction and interaction between pedestrians is likely.					
E	49 – 75	Virtually all pedestrians restrict their normal walking speed, frequently adjusting their gait. At the lower range, forward movement is possible only by shuffling. Space is not sufficient for passing slower pedestrians. Cross- or reverse-flow movements are possible only with extreme difficulties. Design volumes approach the limit of walkway capacity, with stoppages and interruptions to flow.					
F	> 75	All walking speeds are severely restricted, and forward progress is made only by shuffling. There is frequent, unavoidable contact with other pedestrians. Cross- and reverse-flow movements are virtually impossible. Flow is sporadic and unstable. Space is more characteristic of queued pedestrians than of moving pedestrian streams.					

5.4.4. The performance of the key pedestrian links in the design years 2031 and 2037 reference (without the Scheme) and design (with the Scheme) scenarios are summarized in Table 5.8 below in terms of LOS. The pedestrian walkway along the boundary of Site A will be widened in year 2037 due to the proposed building set back.



Table 5.8 Design Years Key Pedestrain Link Performance

Ref (1)	Effective Width (m) (2)	Casassia	Pede	strian De (pph)	mand	Flow Rate (ppm/m)			LOS		
		Maria Contraction And Contraction Contract	AM Peak	Noon Peak	PM Peak	AM Peak	Noon Peak	PM Peak	AM Peak	Noon Peak	PM Peak
		2031 Reference	240	275	300	10.7	12.2	13.3	Α	Α	Α
D4	4.5	2031 Design	260	290	315	11.6	12.9	14	Α	Α	Α
P1	1.5	2037 Reference	260	290	320	11.6	12.9	14.2	Α	Α	Α
		2037 Design	310	345	365	13.8	15.3	16.2	Α	Α	В
		2031 Reference	115	185	190	7.7	12.3	12.7	Α	Α	Α
DO	1	2031 Design	125	195	200	8.3	13	13.3	Α	Α	Α
P2		2037 Reference	120	195	200	8	13	13.3	Α	Α	Α
	6 (3)	2037 Design	190	285	270	2.1	3.2	3	Α	Α	Α
	2.5	2031 Reference	120	185	300	3.2	4.9	8	Α	Α	Α
D2		2031 Design	205	245	365	5.5	6.5	9.7	Α	Α	Α
P3		2037 Reference	125	190	320	3.3	5.1	8.5	Α	Α	Α
		2037 Design	240	290	415	6.4	7.7	11.1	Α	Α	Α
	2.5	2031 Reference	180	70	170	4.8	1.9	4.5	Α	Α	Α
D4		2031 Design	235	110	210	6.3	2.9	5.6	Α	Α	Α
P4		2037 Reference	190	75	180	5.1	2	4.8	Α	Α	Α
	6.3 (3)	2037 Design	245	115	220	2.6	1.2	2.3	Α	Α	Α
		2031 Reference	200	305	270	3.8	5.8	5.1	Α	Α	Α
DE	3.5	2031 Design	255	345	310	4.9	6.6	5.9	Α	Α	Α
P5	2	2037 Reference	205	315	280	3.9	6	5.3	Α	Α	Α
	8.8 (3)	2037 Design	455	620	520	3.4	4.7	3.9	Α	Α	Α
		2031 Reference	180	280	260	3.2	5	4.7	Α	Α	Α
DC	0.7	2031 Design	235	320	300	4.2	5.8	5.4	Α	Α	Α
P6	3.7	2037 Reference	185	290	270	3.3	5.2	4.9	Α	Α	Α
	- V	2037 Design	305	420	375	5.5	7.6	6.8	Α	A	Α
		2031 Reference	460	375	530	15.3	12.5	17.7	Α	Α	В
D7		2031 Design	490	395	555	16.3	13.2	18.5	В	Α	В
P7	2	2037 Reference	480	390	560	16	13	18.7	Α	Α	В
	- 19	2037 Design	705	675	780	23.5	22.5	26	С	В	С

Remarks: (1) Refer to Figures 4.5 and 4.6.

5.4.5. As can be seen in the above assessment results, all of the key sections of footpath are still operating desirably during the morning, noon and evening peak periods with the additional pedestrian trip to be generated by the Scheme.

⁽²⁾ Effective Width = Footpath Width – Dead Width (0.5m for kerb/ wall/ fence, 0.7m for shop frontage and 1.0m for tree pits along the eastern footpath of Cheung Wah Street).

⁽³⁾ Footpath widened due to proposed building set back of Site A.



6. Summary and Conclusion

6.1. Summary

- 6.1.1. A Traffic Impact Assessment (TIA) Study was carried out to investigate the traffic impact induced by Site A and Site B of the Scheme in Sham Shui Po. Site A consist of residential blocks, retail, GIC facilities and underground public car park while Site B consist of public open space and a GIC building with the relocated indoor sport centre.
- 6.1.2. The proposed development parameters for Site A will meet the high-end of the HKPSG parking requirement for the proposed residential and retail development. The transport facilities would be provided at the ancillary basement car park at Site A and the ground floor loading/unloading area and ancillary basement carpark at Site B. Besides, car ramps are proposed for the two sites to facilitate vehicle manoeuvring and entering to the basement car park.
- 6.1.3. To facilitate the future operation needs of the GIC provision, the parking provision is proposed with reference to the same facilities at other development projects. The actual provision for GIC uses will be subject to liaison with the relevant government departments and services providers upon the Development Scheme Plan (DSP) approval.
- 6.1.4. Provision of public car park is proposed at Site A to accommodate some of the parking demand in the local area. The provision of underground public carpark at Site A may create opportunity for the replacement of some on-street parking spaces in the area. It makes way for pavement widening or partial pedestrianization to enhance walkability in the area under separated revitalization scheme.
- 6.1.5. Swept path analysis is conducted based on the notional layout. The notional layout for the development run-in/out and access road is technically feasible from traffic engineering point of view.
- 6.1.6. Building setback on all four side of Site A is proposed to provide wider pedestrian walkway and thus enhance the pedestrian walking environment.
- 6.1.7. Pedestrians can access the subject site via the surrounding footpaths and pedestrian crossings to/ from nearby bus, GMB and PLB servicing points as well as to/ from MTR Lai Chi Kok and Cheung Sha Wan Stations.
- 6.1.8. The key junctions within the study area were assessed with respect to traffic generation of the Scheme in design years 2031 and 2037 (three years after completion of each site), taking into account the traffic generation by the major planned/approved developments in the vicinity of the subject site.
- 6.1.9. Based on the assessment results, it was found that some of identified junctions would be operating under the marginal capacity (i.e. $RC \le 15\%$) or even over capacity (i.e. $RC \le 0\%$) in design years 2031 and 2037 for the scenarios without the Scheme.

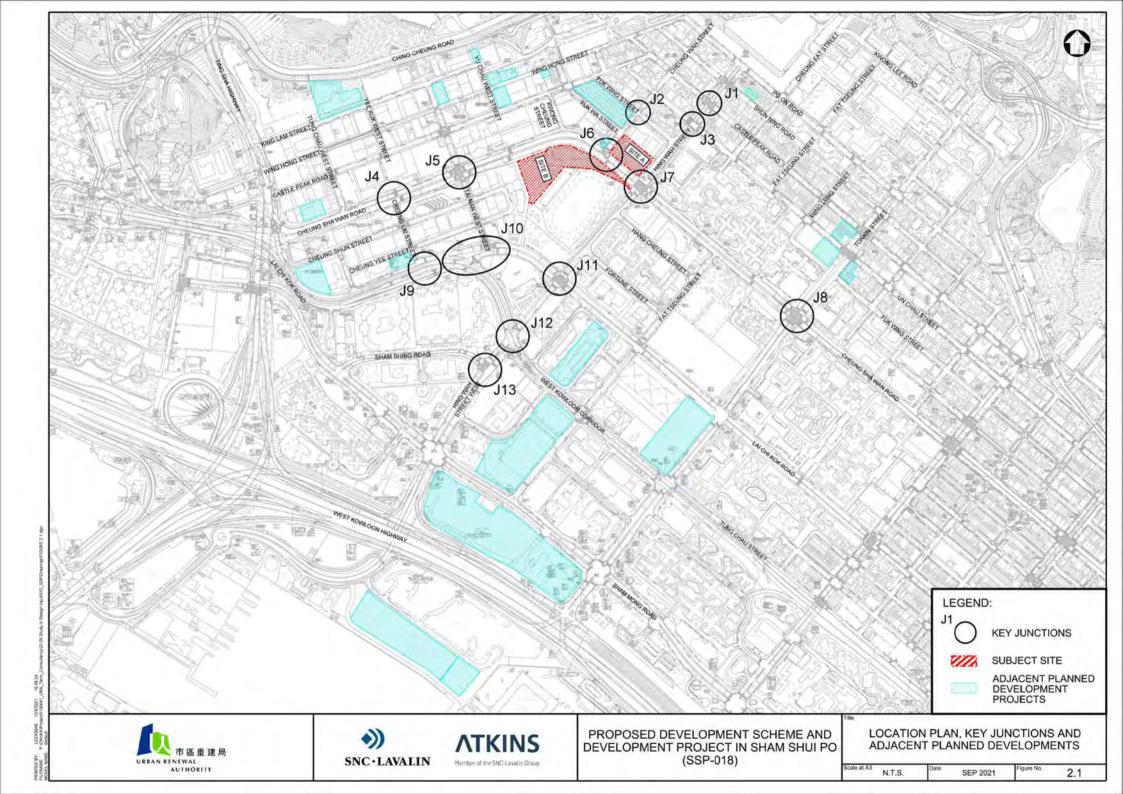


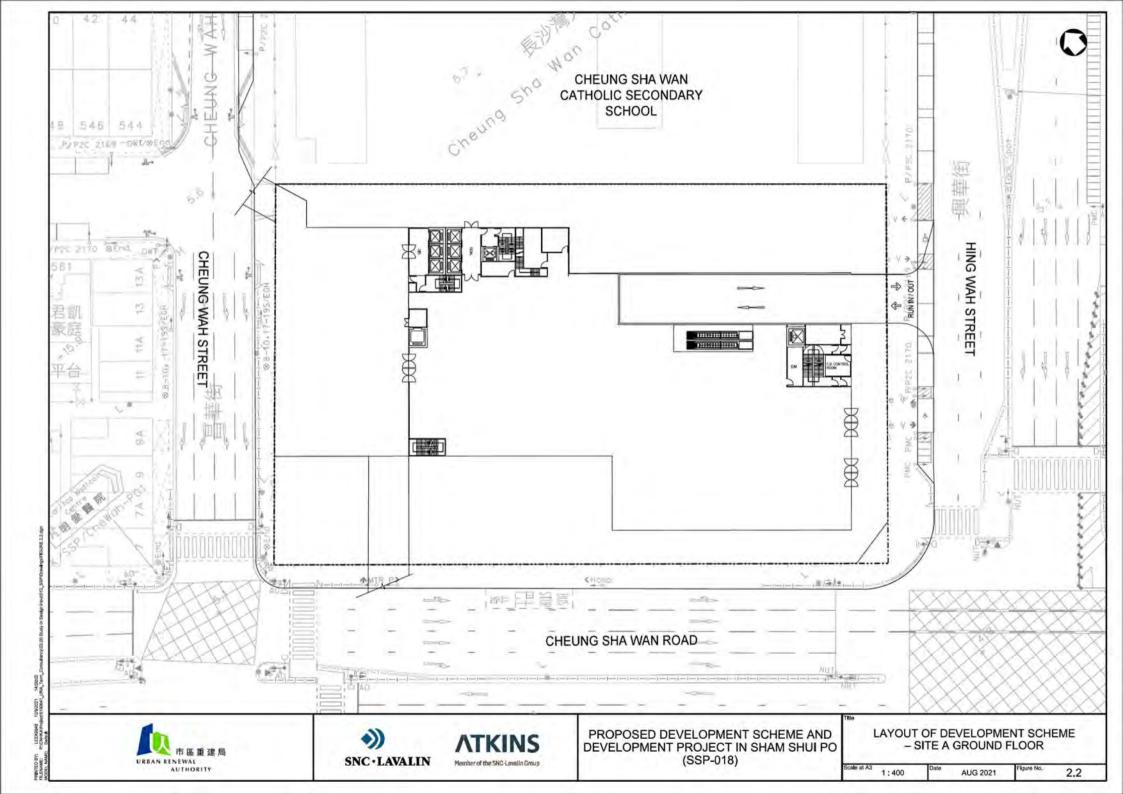
6.1.10. Traffic enhancement measure is proposed for one junction that would be overloaded by the development trips of the Scheme and suggested for five junctions that are expected to be overloaded in the design years by the local traffic growth even without the operation of the Scheme for TD consideration to enhance the traffic condition in the local area.

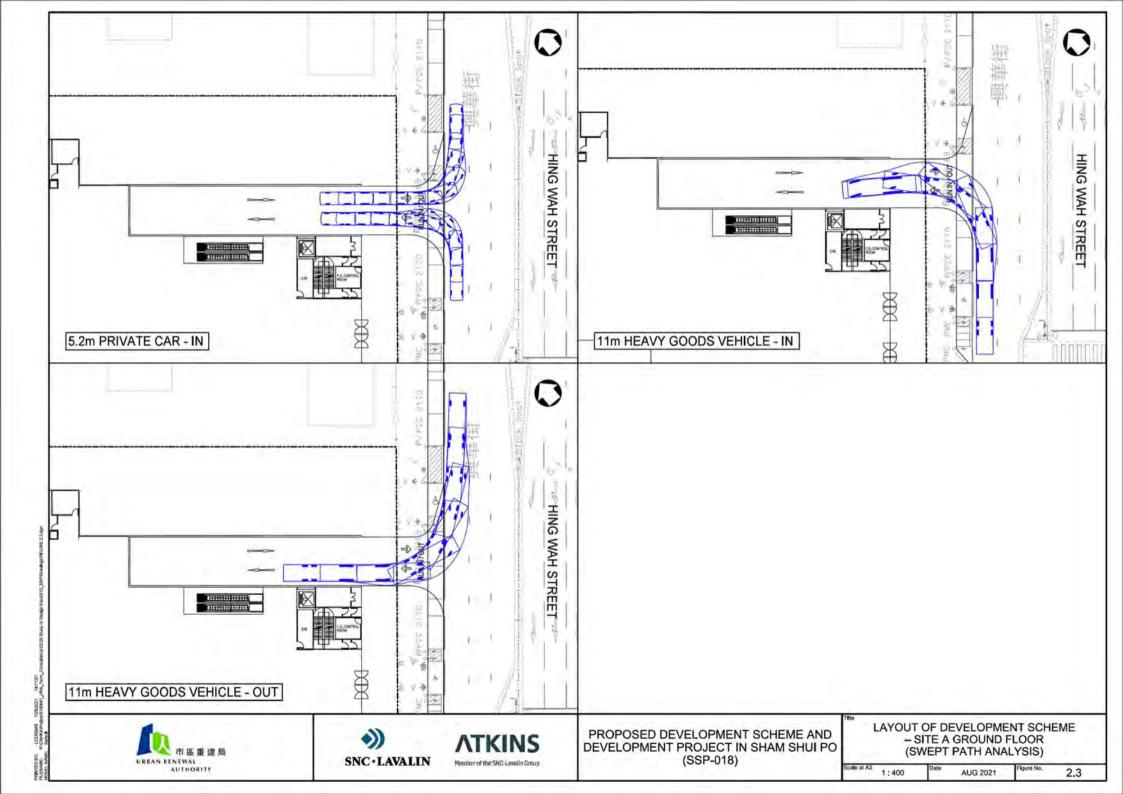
6.2. Conclusion

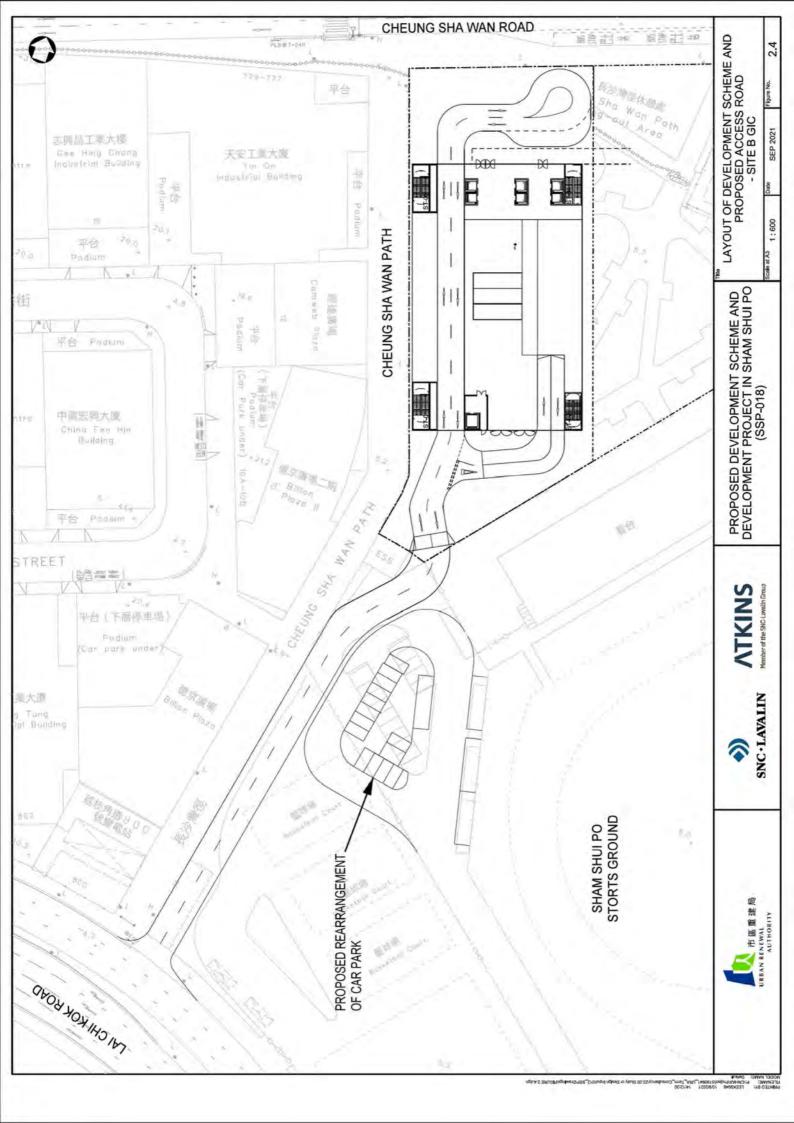
- 6.2.1. It is concluded that with the proposed and suggested junction improvement measures, the Scheme would not induce adverse traffic impact on the surrounding road network and would enhance the pedestrian walking environment of the adjacent local streets.
- 6.2.2. The proposed traffic provision to the Scheme, with reference to the notional layout, is considered technically feasible and acceptable.

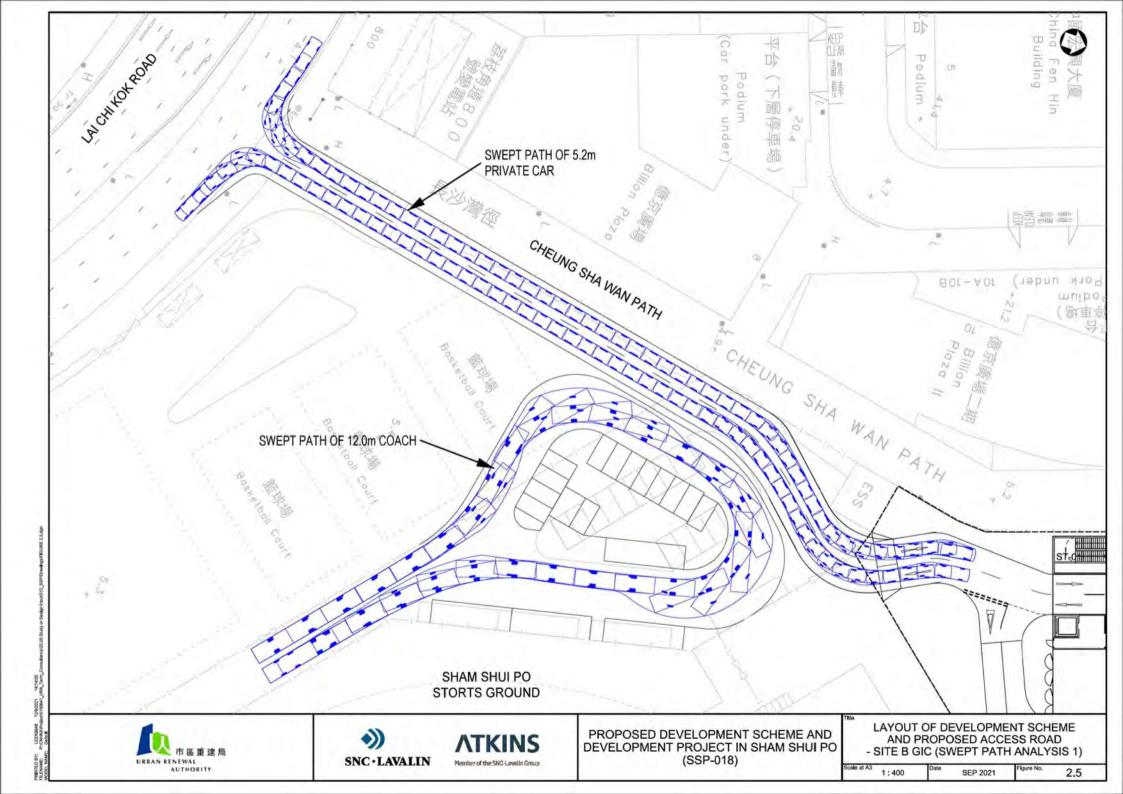
Figures

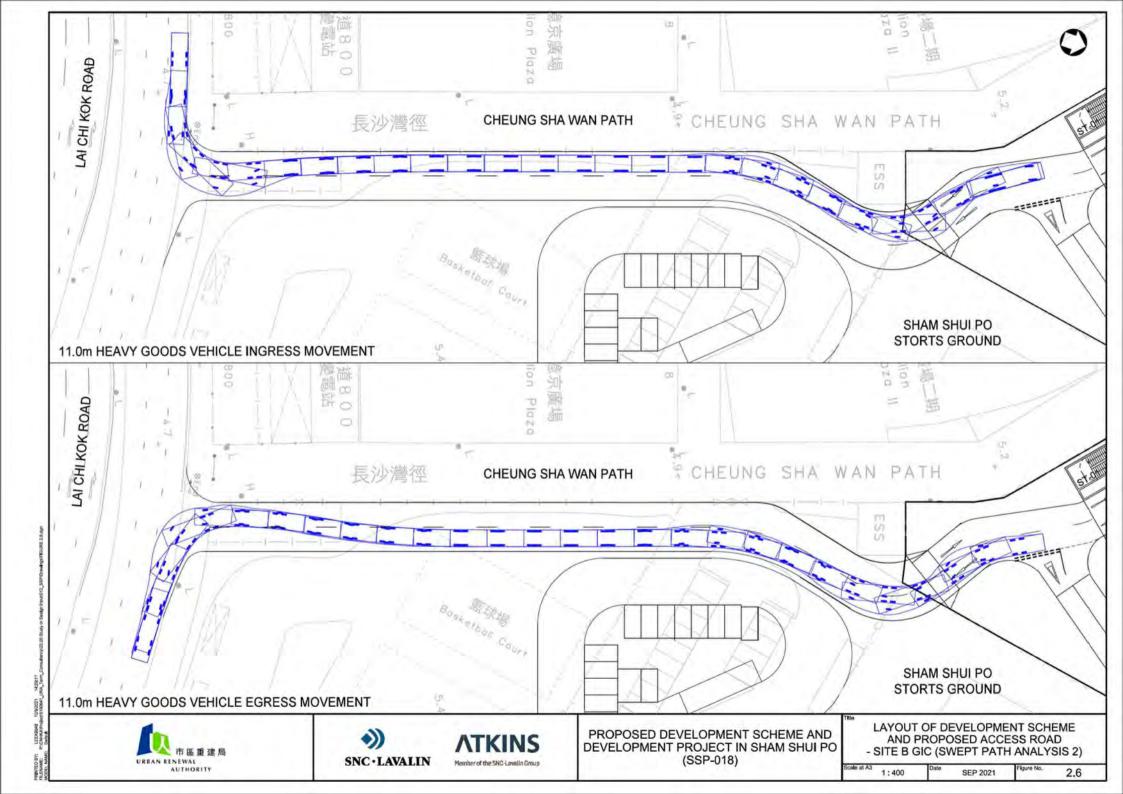


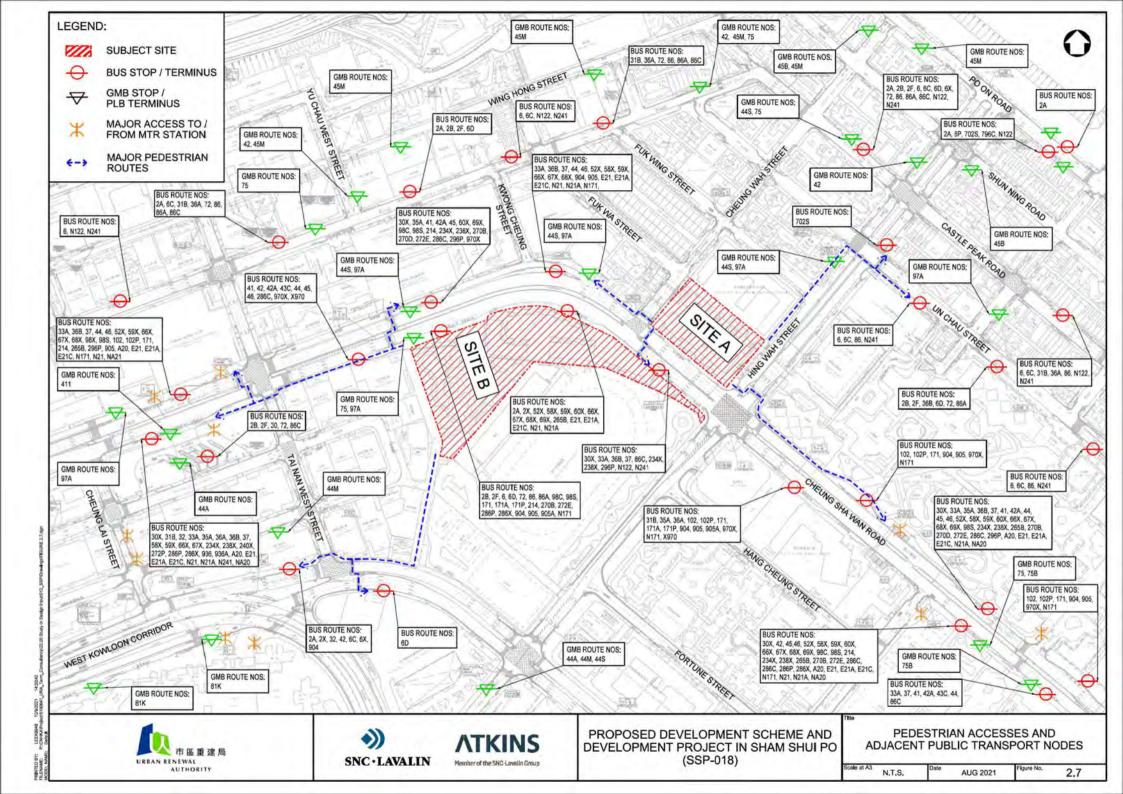


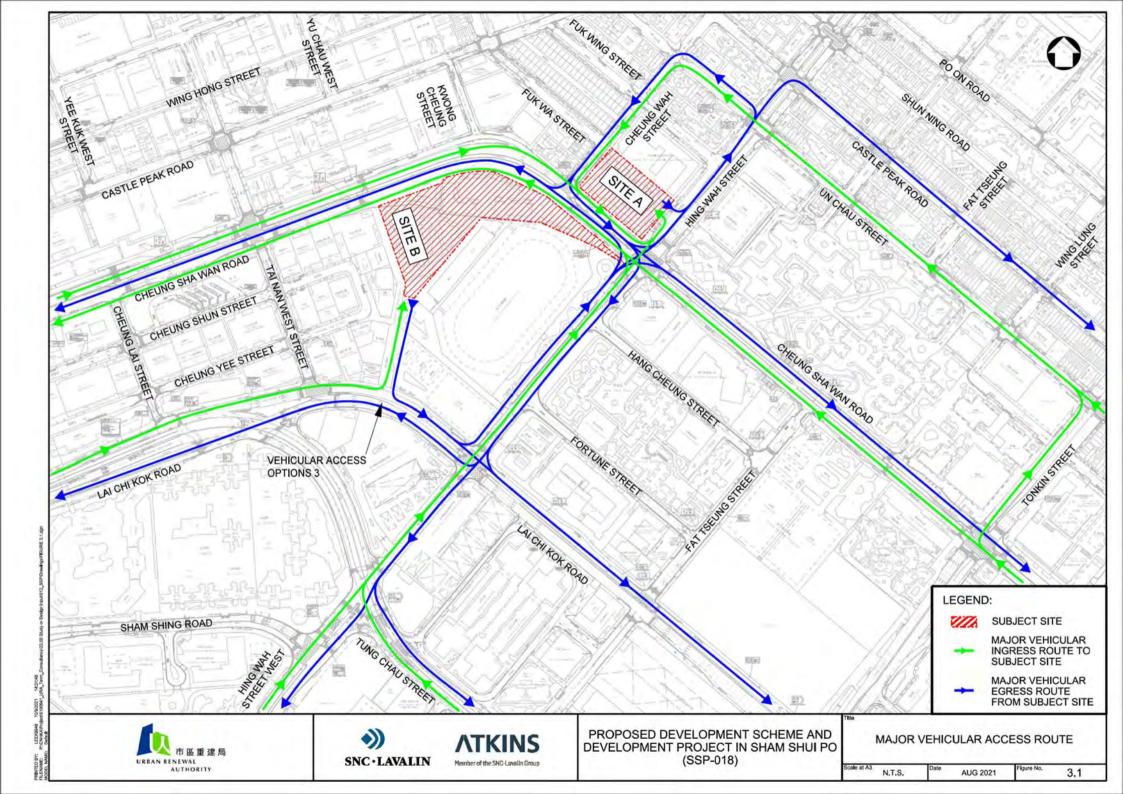


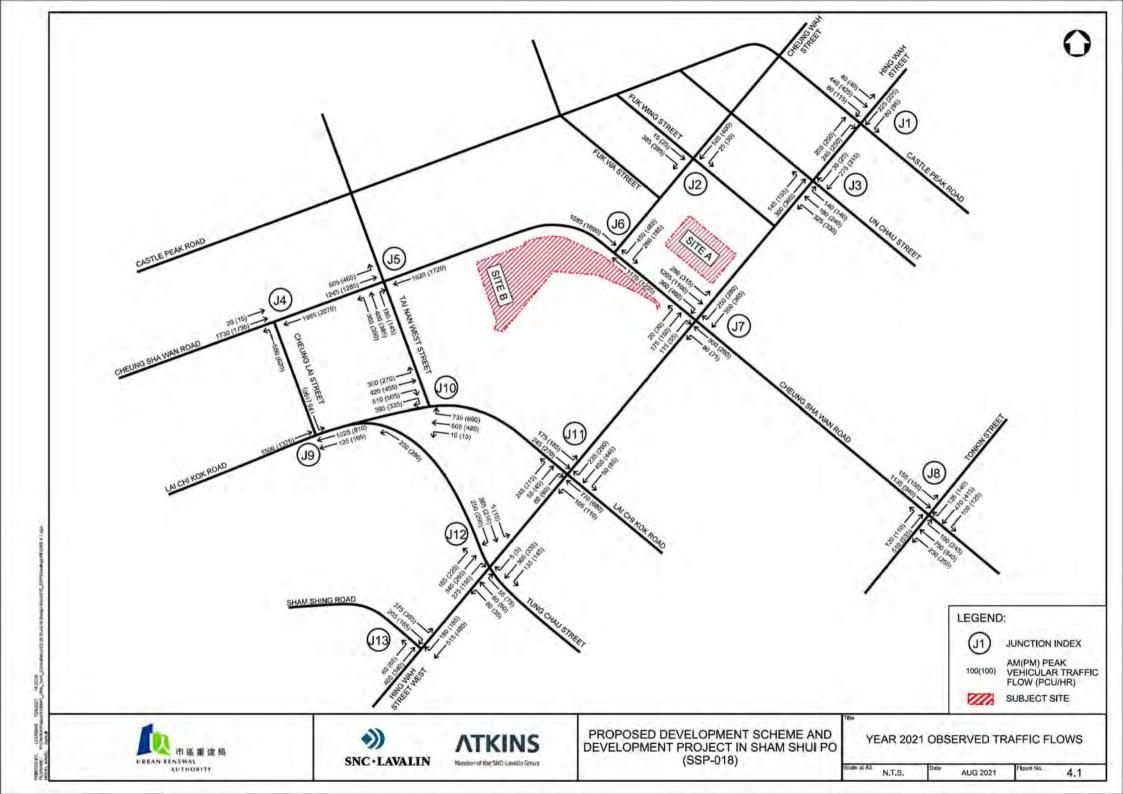


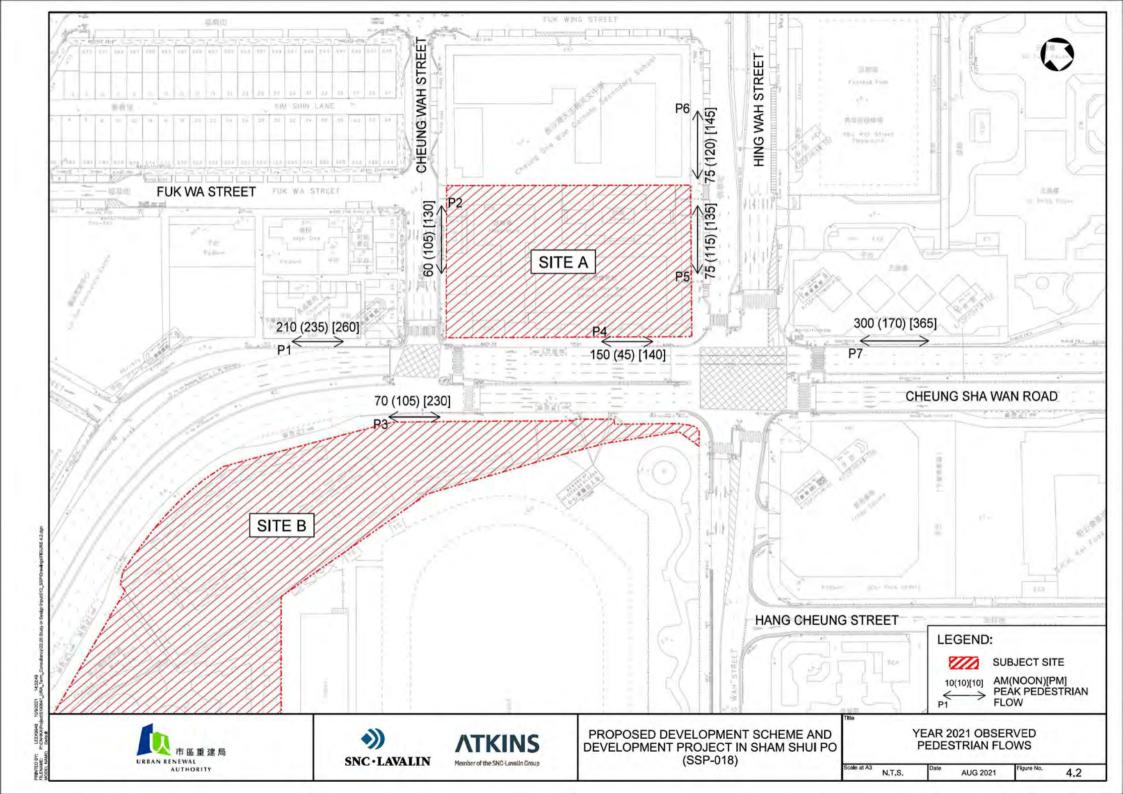


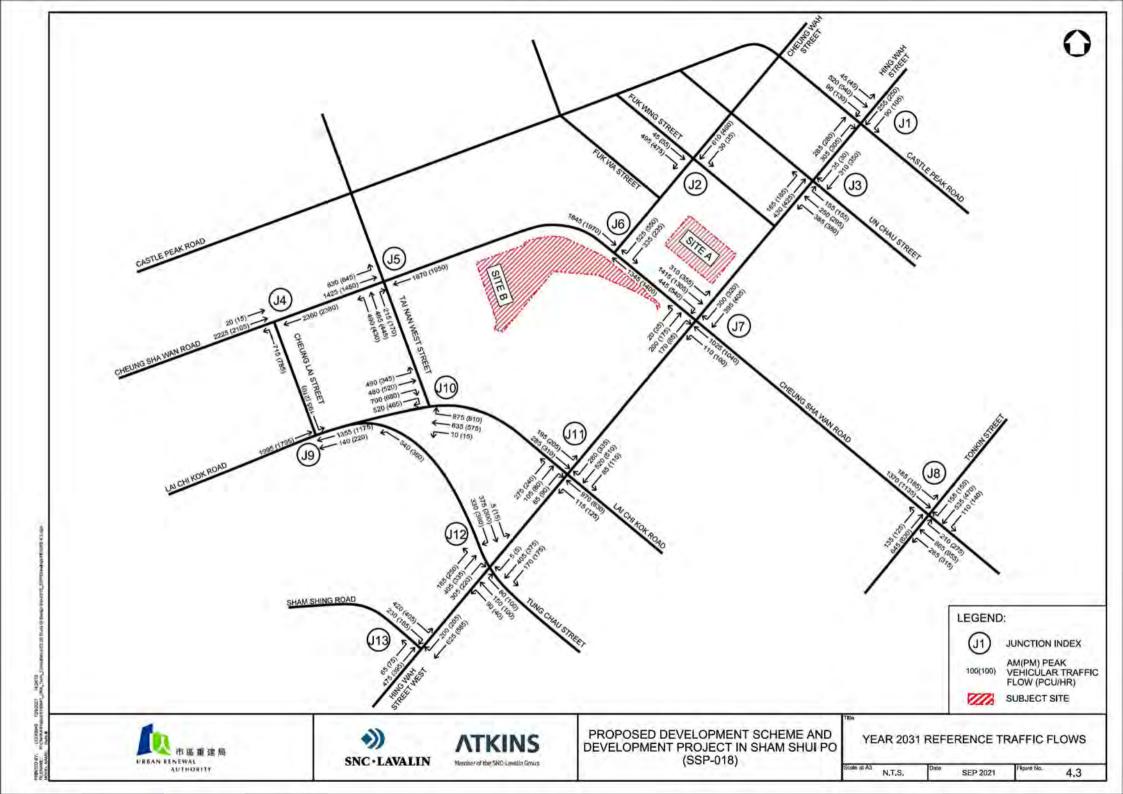


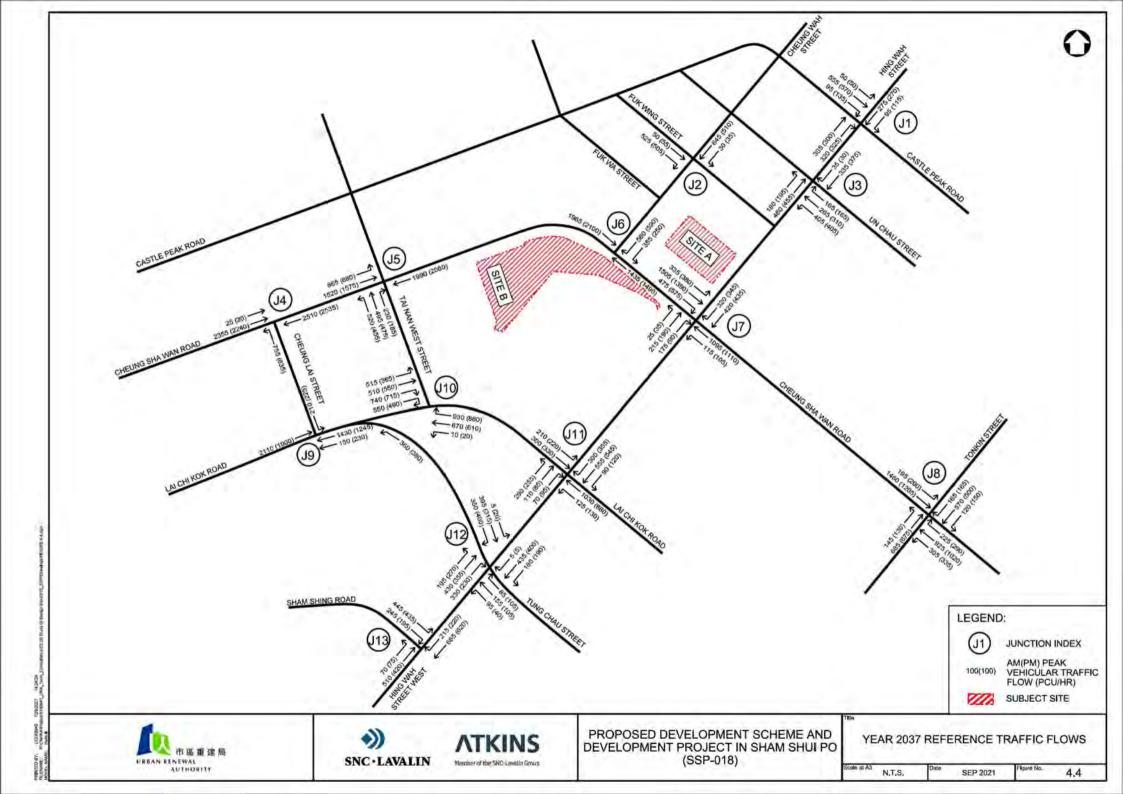


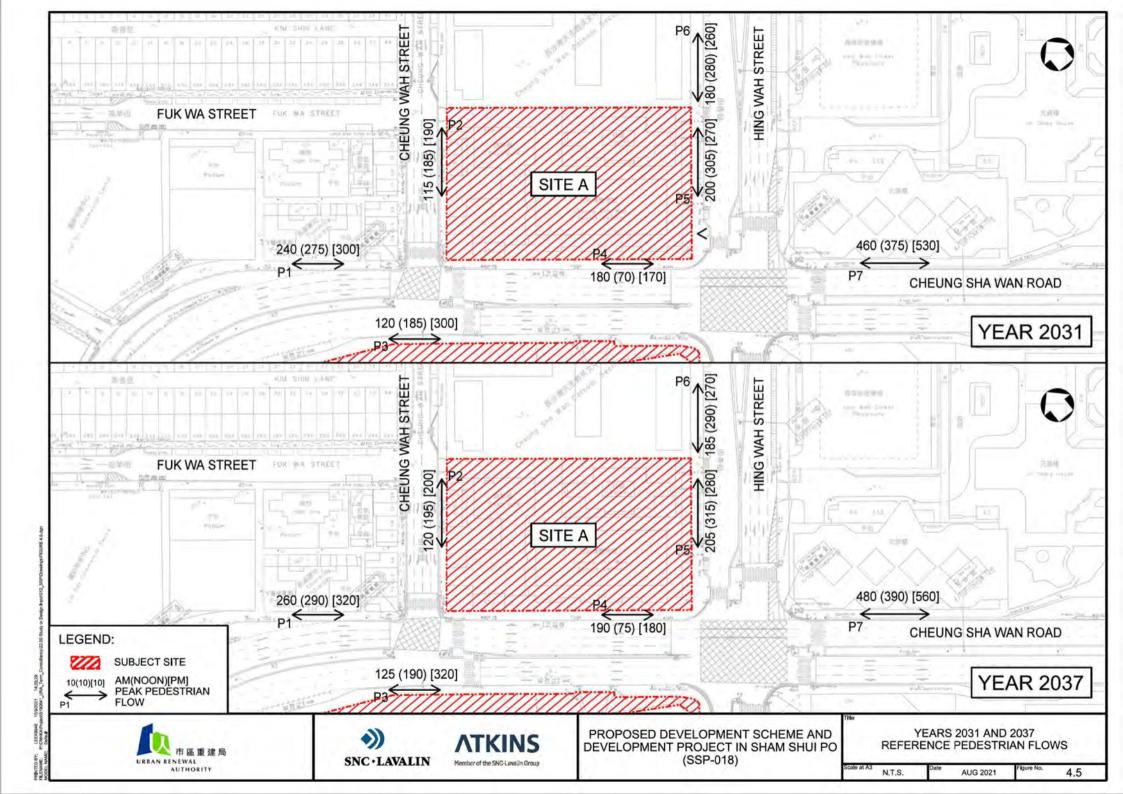


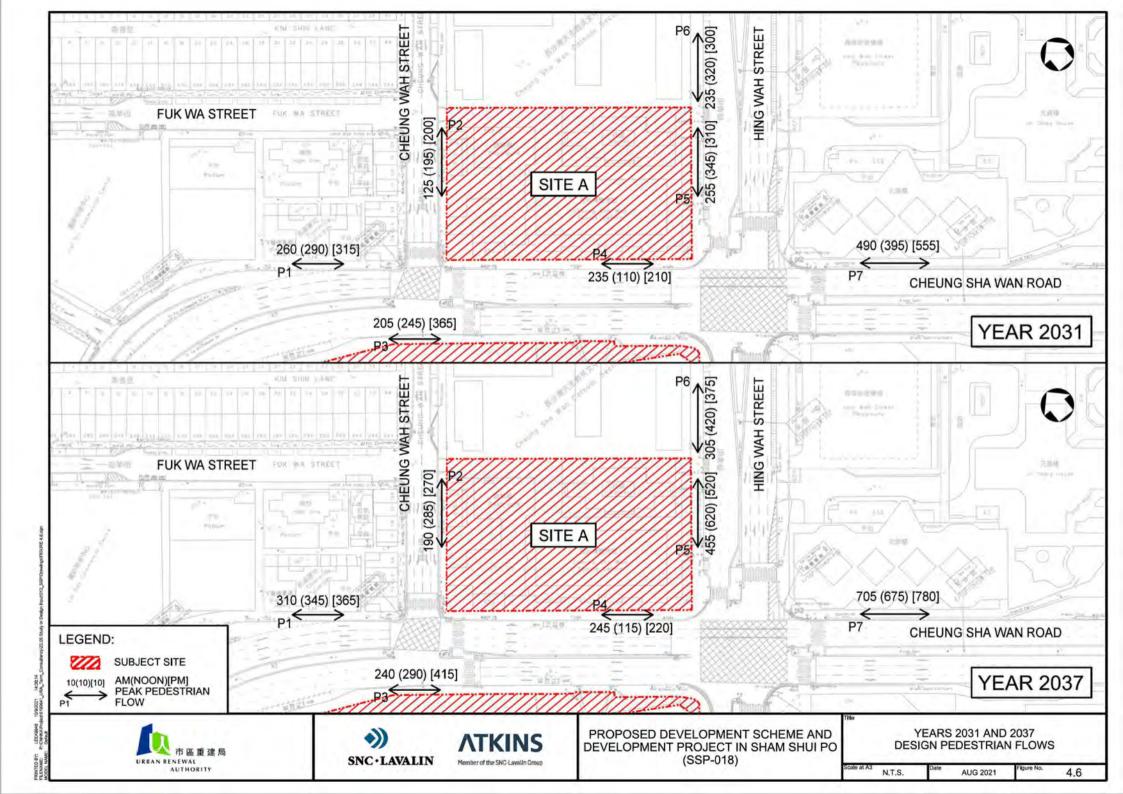


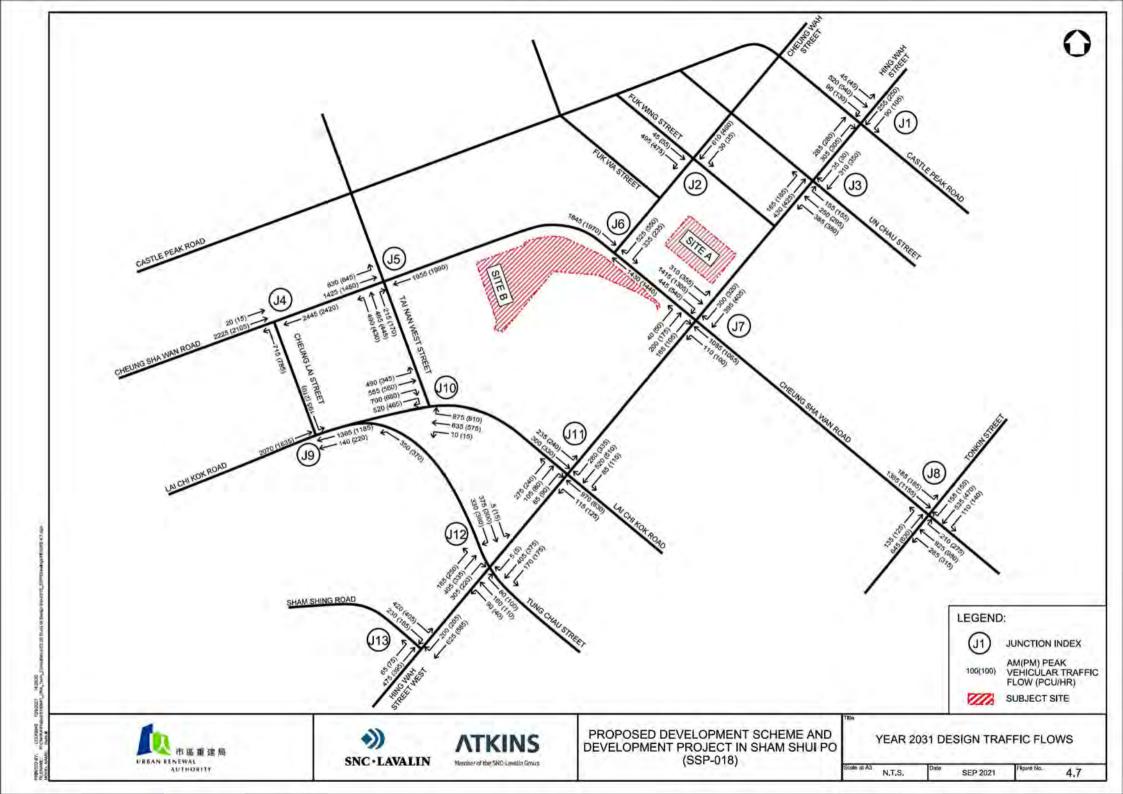


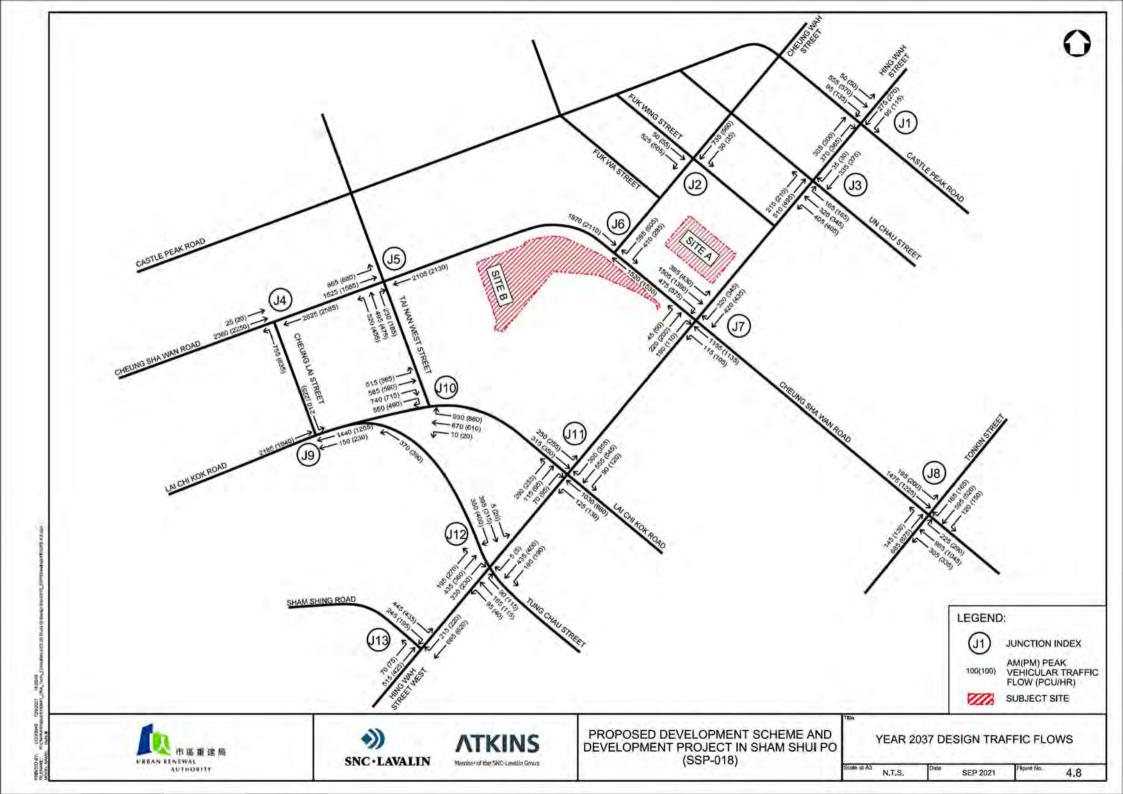


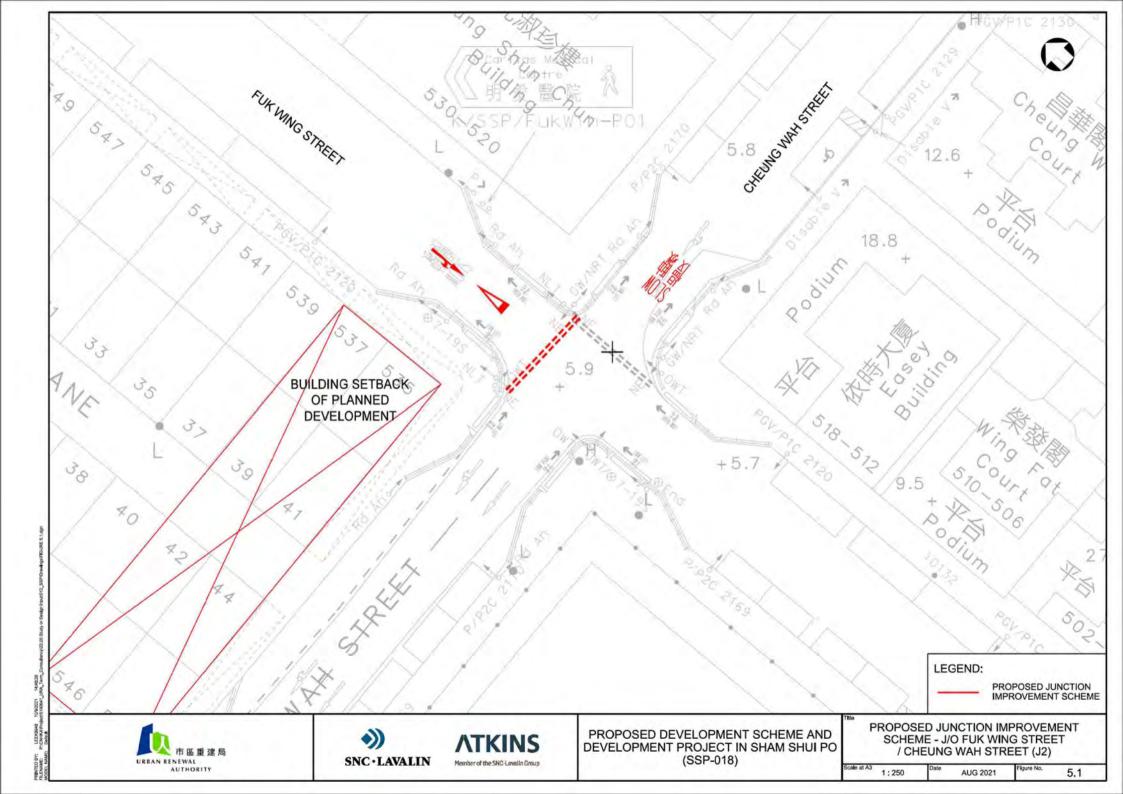


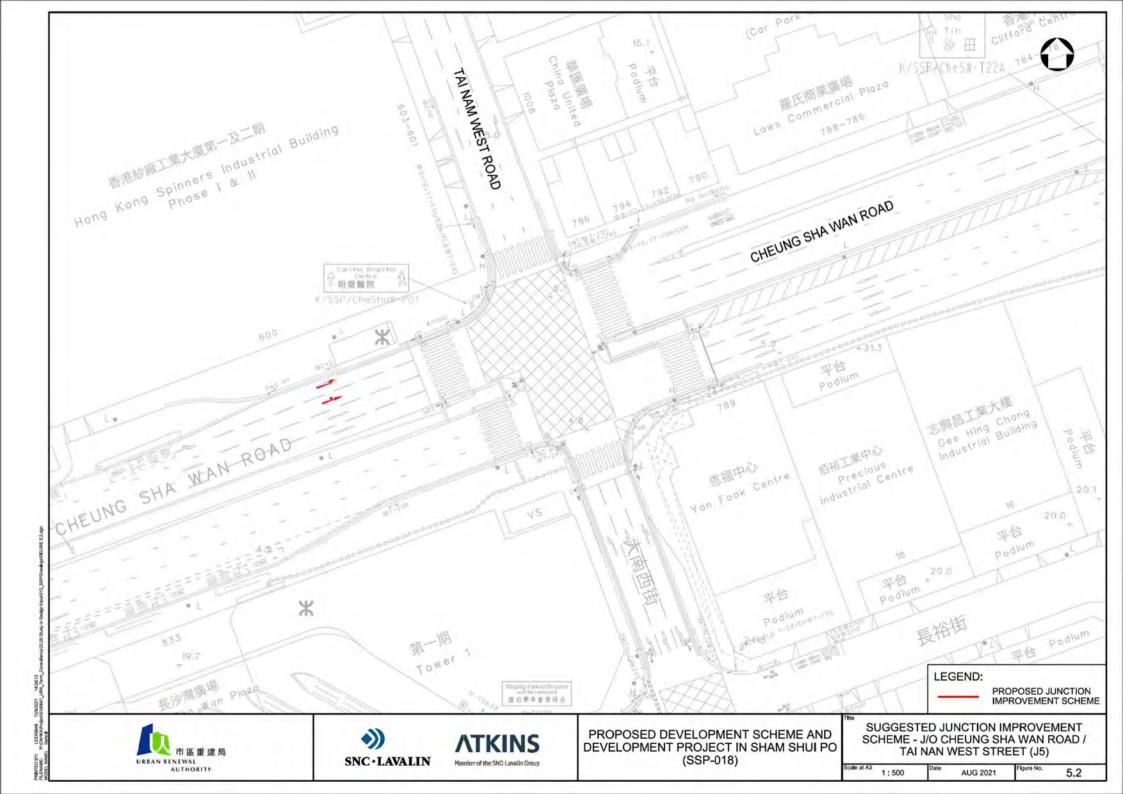


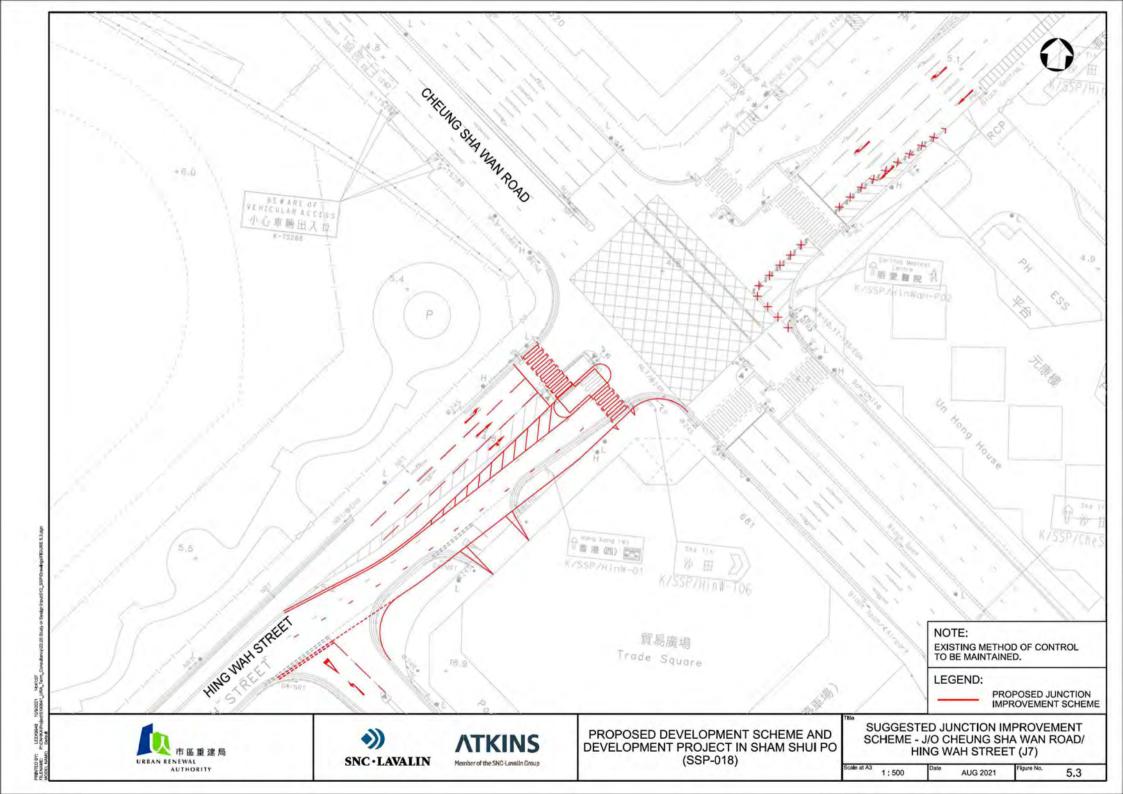


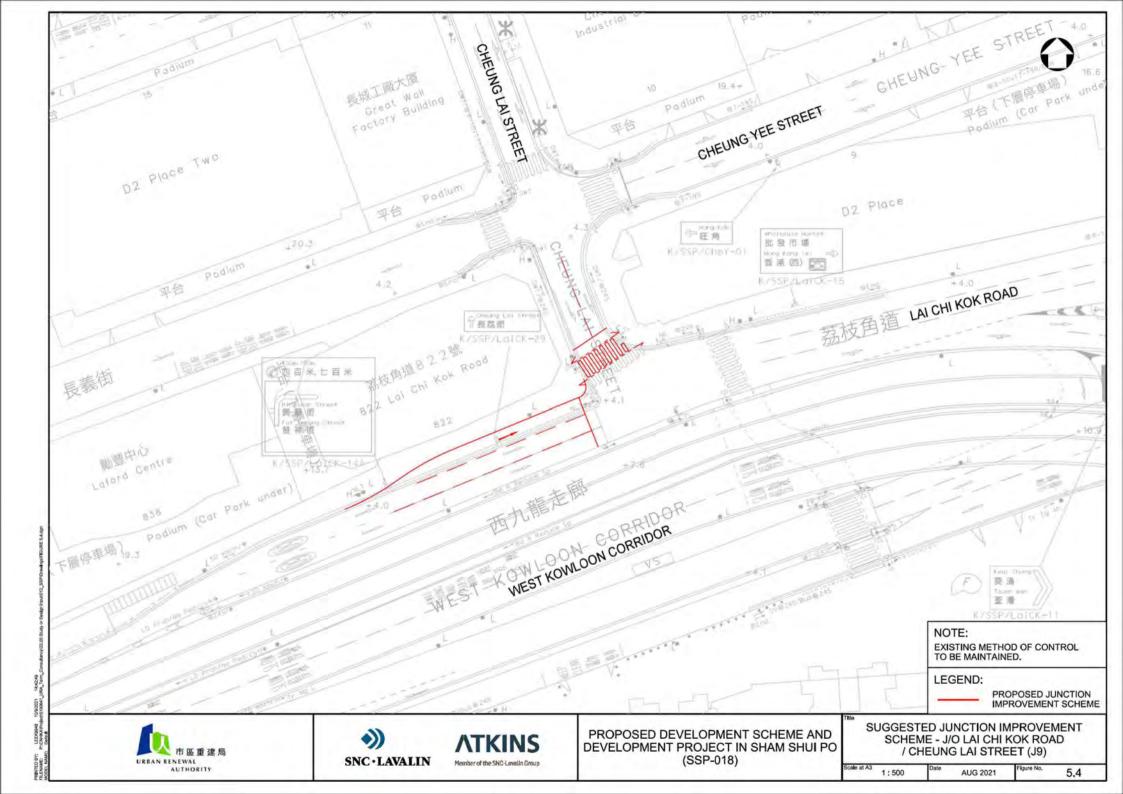


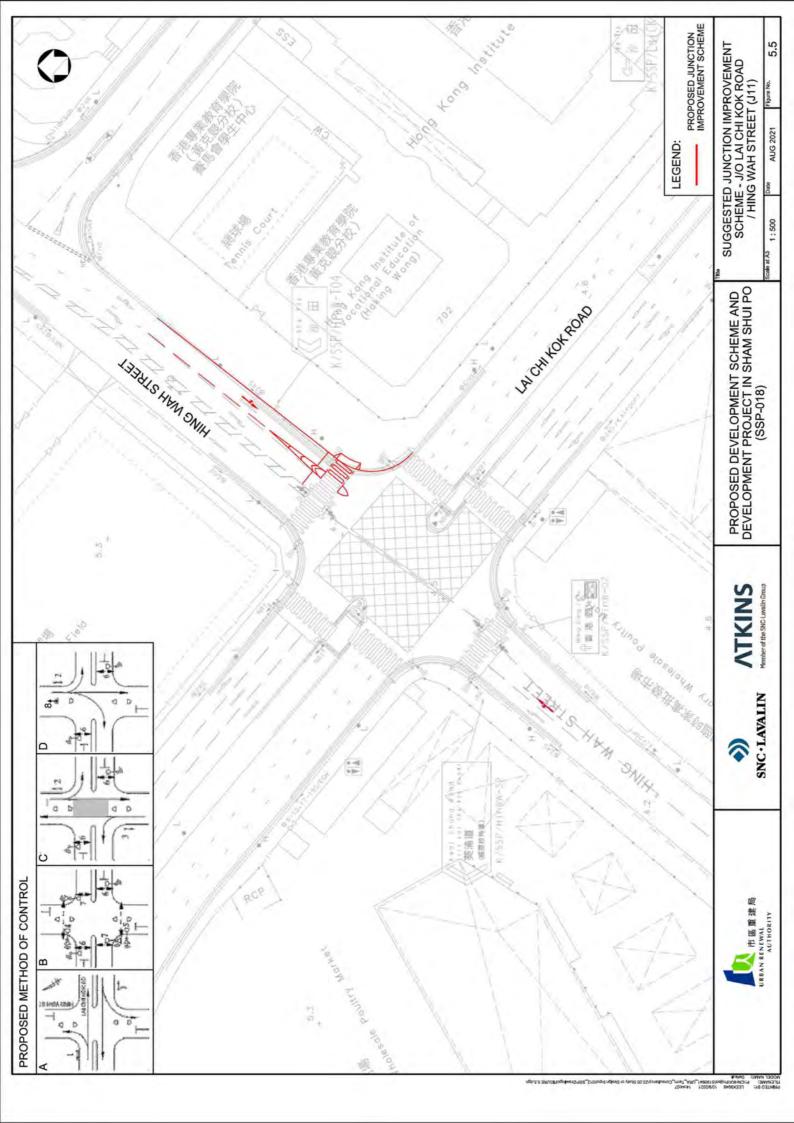


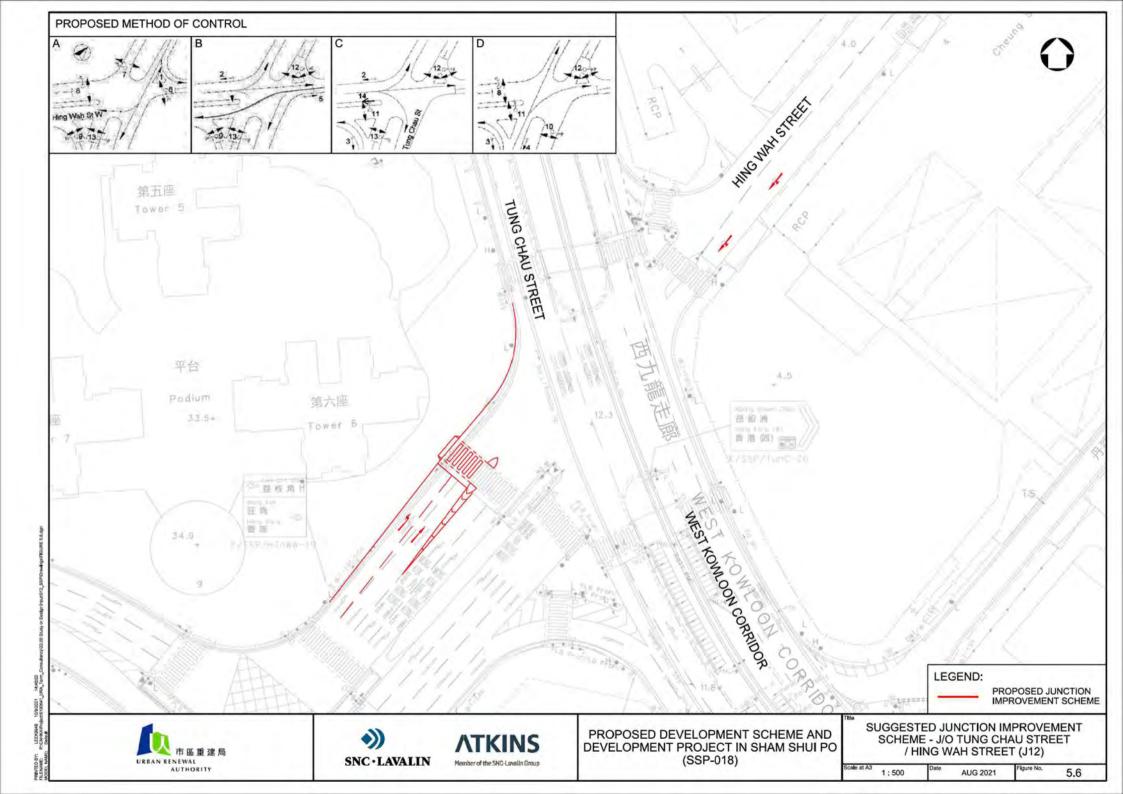












Appendix A – Junction Calculation Sheets

IG=8

1+2+3

ATKINS

G=

IG=

JOB NO. : _____ 5190641 J1 - Castle Peak Road / Hing Wah Street 2021 Scheme : Existing Designed by. Checked by:_ ↑N Traffic Flow (pcu/hr) X 225(225) B0(95) 40(40) _ CASTLE PEAK ROAD 440(425) -80(115) 255(250) 245(250) STAGE / PHASE DIAGRAM

G=

Capacity	Calculat	ions				-		AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Castle Peal	Road EB		1											
1A	A	4.00	Y	N	10		169	24%	1750	0.097	177	23%	1755	0.101
1B	A	4.00	N	N			208		2155	0.097	217		2155	0.101
10	Α	4.00	Y	N	10		183	44%	1890	0.097	186	62%	1845	0.101
Hing Wah S	Stroot SR													
2A	B	3.60	Y	N	10		141	57%	1820	0.077	147	65%	1800	0.082
2B	В	3.60	N	N	,,,		164	5176	2115	0.078	173	0570	2115	0.082
Hing Wah S	Street NB													
3A	С	3.60	Y	N			255		1975	0.129	250		1975	0.127
3B	C	3.60	N	N	13		245	100%	1890	0.130	250	100%	1890	0.132
4p	B,C		8GM +	10FG =	18	sec								
5p	A,B		6GM+	7FG =	13	sec								
6р	A,C		6GM +	7FG=	13	sec								
7p	В		8GM +	7FG =	15	sec								
8p	C		5GM +	10FG =	15	sec								

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.304	Sum of Critical y Y	0.315
	Lost Time L (sec)	15	Lost Time L (sec)	15
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.782	Practical Y Ypr	0.791
	Reserve Capacity RC	157%	Reserve Capacity RC	151%

ATKINS

G=

IG=

IG=

JOB NO. : _____ 5190641 J1 - Castle Peak Road / Hing Wah Street 2031 Design Year: Scheme : 2031 Reference Designed by. Checked by:_ ↑N Traffic Flow (pcu/hr) HING 255(250) 90(105) 45(45) __ 520(540) __ 90(130) CASTLE PEAK ROAD 305(305) 285(280) STAGE / PHASE DIAGRAM

G=

G=

IG=8

1+2+3

1+2+3

Capacity	y Calculat	ions						AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
astle Pea	k Road EB							1					" '	
1A	A	4.00	Y	N	10		198	23%	1755	0.113	218	21%	1760	0.124
1B	A	4.00	N	N			243		2155	0.113	267		2155	0.124
10	A	4.00	Y	N	10		214	42%	1895	0.113	230	57%	1860	0.124
ling Wah	Street SB													
2A	В	3.60	Y	N	10		160	56%	1820	0.088	163	64%	1800	0.091
2B	В	3.60	N	N			185		2115	0.087	192		2115	0.091
Hing Wah	Street NB													
3A	C	3.60	Y	N			285		1975	0.144	280		1975	0.142
3B	C	3.60	N	N	13		305	100%	1890	0.161	305	100%	1890	0.161
4р	B,C		8GM+	10FG =	18	sec								
5p	A,B		6GM+	7FG =	13	sec								
6р	A,C		6GM +	7FG =	13	sec								
7p	В		8GM +	7FG =	15	sec								
8p	С		5GM +	10FG =	15	sec								
	,													
									1			-		

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.362	Sum of Critical y Y	0.376
	Lost Time L (sec)	15	Lost Time L (sec)	15
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.782	Practical Y Ypr	0.791
	Reserve Capacity RC	116%	Reserve Capacity RC	110%

ATKINS

G=

IG=

IG=

JOB NO. : _____ 5190641 J1 - Castle Peak Road / Hing Wah Street 2031 Scheme : 2031 Design Designed by. Checked by:_ ↑N Traffic Flow (pcu/hr) W HING 255(250) 90(105) 45(45) ____ 520(540) ___ 90(130) CASTLE PEAK ROAD 305(305) 285(280) STAGE / PHASE DIAGRAM

G=

G=

IG=8

1+2+3

1+2+3

Capacity	Calculat	ions				-		AM	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Castle Peal	Road EB												-	
1A	A	4.00	Y	N	10		198	23%	1755	0.113	218	21%	1760	0.124
1B	A	4.00	N	N			243		2155	0.113	267		2155	0.124
10	Α	4.00	Y	N	10		214	42%	1895	0.113	230	57%	1860	0.124
Hing Wah S	Stroot SR													
2A	B	3.60	Y	N	10		160	56%	1820	0.088	163	64%	1800	0.091
2B	В	3.60	N	N	,,,		185	3070	2115	0.087	192	0476	2115	0.091
Hing Wah S	Street NR													
3A	C	3.60	Y	N			285		1975	0.144	280		1975	0.142
3B	Č	3.60	N	N	13		305	100%	1890	0.161	305	100%	1890	0.161
4p	B.C		8GM +	10FG =	18	sec								
5p	A,B		6GM+	7FG =	13	sec								
6р	A,C		6GM +	7FG =	13	sec								
7p	В		8GM +	7FG =	15	sec								
8p	С		5GM +	10FG =	15	sec								
						= 4								
	ļ													

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.362	Sum of Critical y Y	0.376
	Lost Time L (sec)	15	Lost Time L (sec)	15
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.782	Practical Y Ypr	0,791
	Reserve Capacity RC	116%	Reserve Capacity RC	110%

IG=8

1+2+3

ATKINS

G=

IG=

IG=

JOB NO. : _____ 5190641 J1 - Castle Peak Road / Hing Wah Street 2037 Scheme : 2037 Reference Designed by. Checked by:_ ↑N Traffic Flow (pcu/hr) HING 275(270) 95(115) 50(50) _ CASTLE PEAK ROAD 555(570) 95(135) 320(325) 305(300) STAGE / PHASE DIAGRAM

G=

Capacity	Calculat	ions						AMI	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Castle Pea	k Road EB		- ()					1		-	-			-
1A	A	4.00	Y	N	10		211	24%	1750	0.121	230	22%	1755	0.131
1B	A	4.00	N	N			260		2155	0.121	282		2155	0.131
10	A	4.00	Y	N	10		229	41%	1895	0.121	243	56%	1860	0.131
Hing Wah	Street SR													
2A	В	3.60	Y	N	10		171	56%	1825	0.094	177	65%	1800	0.098
2B	В	3.60	N	N			199		2115	0.094	208	-	2115	0.098
Hing Wah	Street NB													
3A	С	3.60	Y	N			305		1975	0.154	300		1975	0.152
3B	C	3.60	N	N	13		320	100%	1890	0.169	325	100%	1890	0.172
4p	B,C		8GM +	10FG =	18	sec								
5p	A,B		6GM+	7FG =	13	sec								
6р	A,C		6GM +	7FG=	13	sec								
7p	В		8GM +	7FG =	15	sec								
8p	С		5GM +	10FG =	15	sec								
												-		

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.384	Sum of Critical y Y	0.401
	Lost Time L (sec)	15	Lost Time L (sec)	15
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.782	Practical Y Ypr	0.791
	Reserve Capacity RC	103%	Reserve Capacity RC	97%

IG=8

1+2+3

ATKINS

G=

IG=

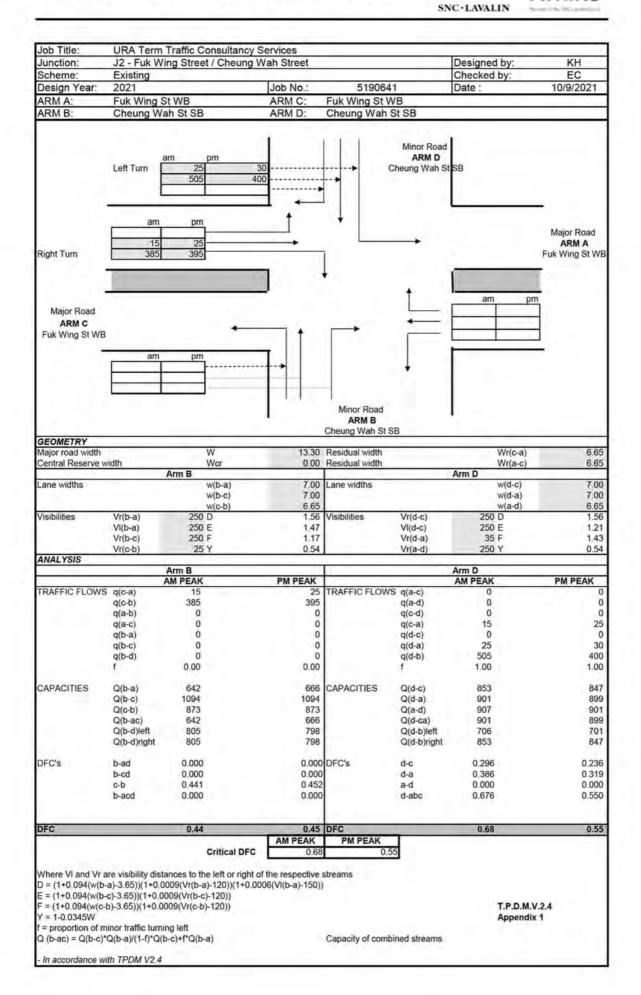
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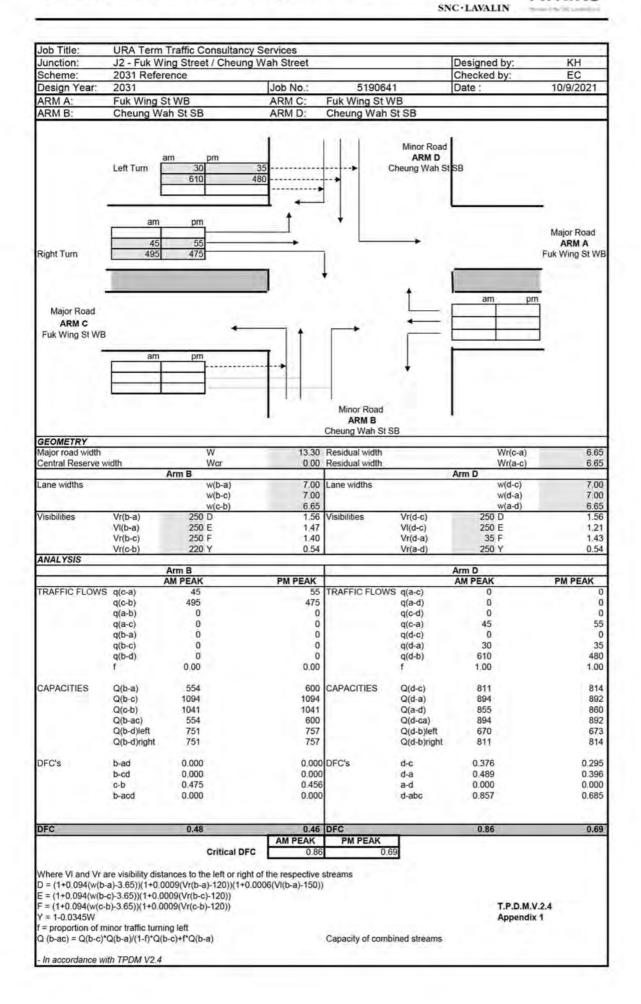
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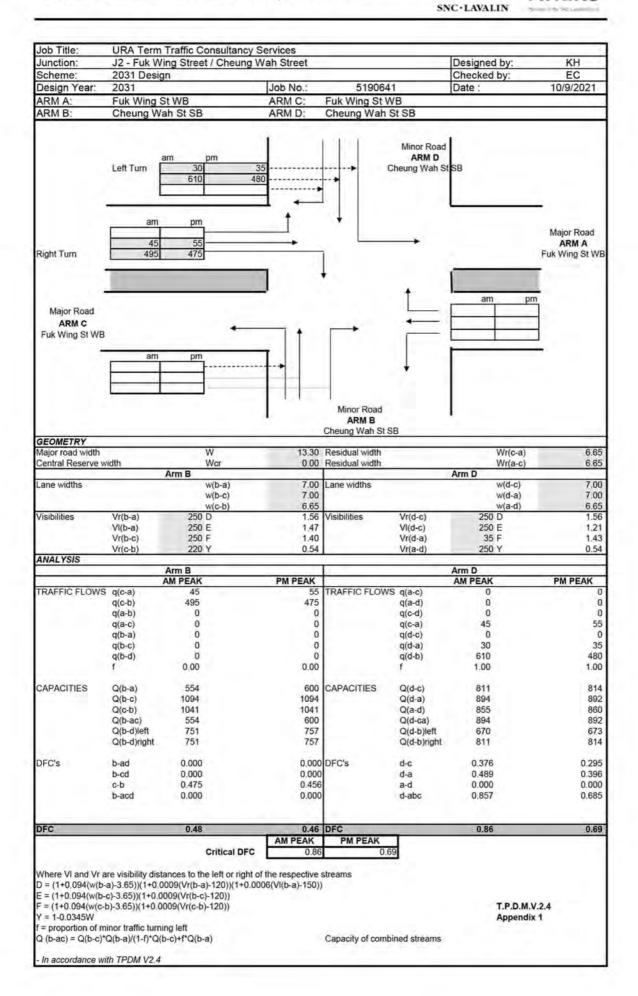
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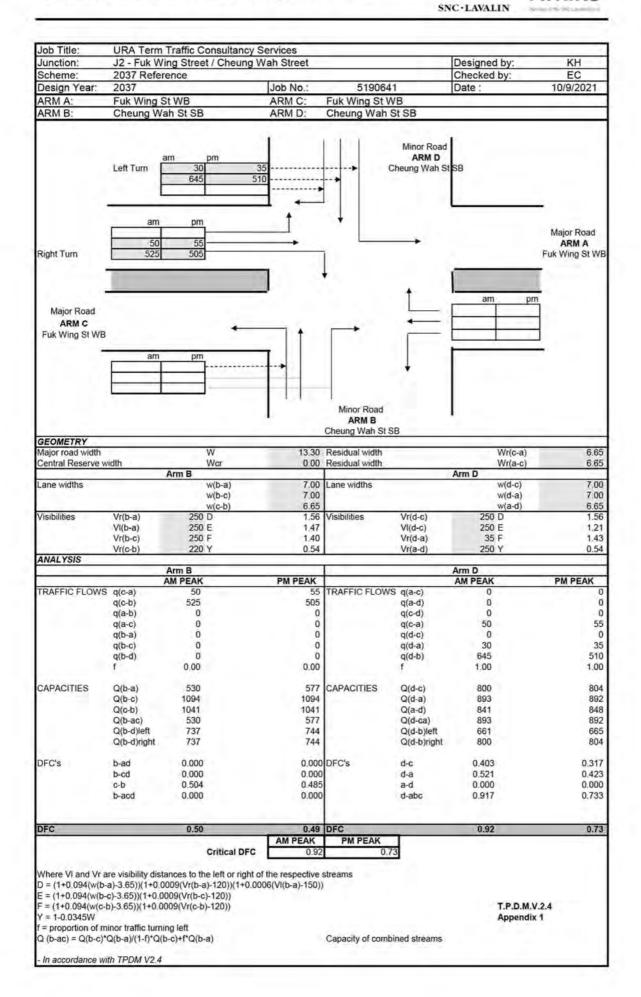
Capacity	Calculat	ions				-		AM	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Castle Peal	Road EB		- ()								-		-	-
1A	A	4.00	Y	N	10		211	24%	1750	0.121	230	22%	1755	0.131
1B	A	4.00	N	N			260		2155	0.121	282		2155	0.131
10	Α	4.00	Y	N	10		229	41%	1895	0.121	243	56%	1860	0.131
Hing Wah S	Street SR													
2A	В	3.60	Y	N	10		171	56%	1825	0.094	177	65%	1800	0.098
2B	В	3.60	N	N	.,,		199	- Sura	2115	0.094	208	0070	2115	0.098
Hing Wah S	Street NB													
3A	С	3.60	Y	N			305		1975	0.154	300		1975	0.152
3B	С	3.60	N	N	13		370	100%	1890	0.196	365	100%	1890	0.193
4p	B.C		8GM +	10FG =	18	sec								
5p	A,B		6GM+	7FG =	13	sec								
6р	A,C		6GM +	7FG=	13	sec								
7p	В		8GM +	7FG =	15	sec								
8p	С		5GM +	10FG =	15	sec								
	-													
						= 4								
									1.5			-		

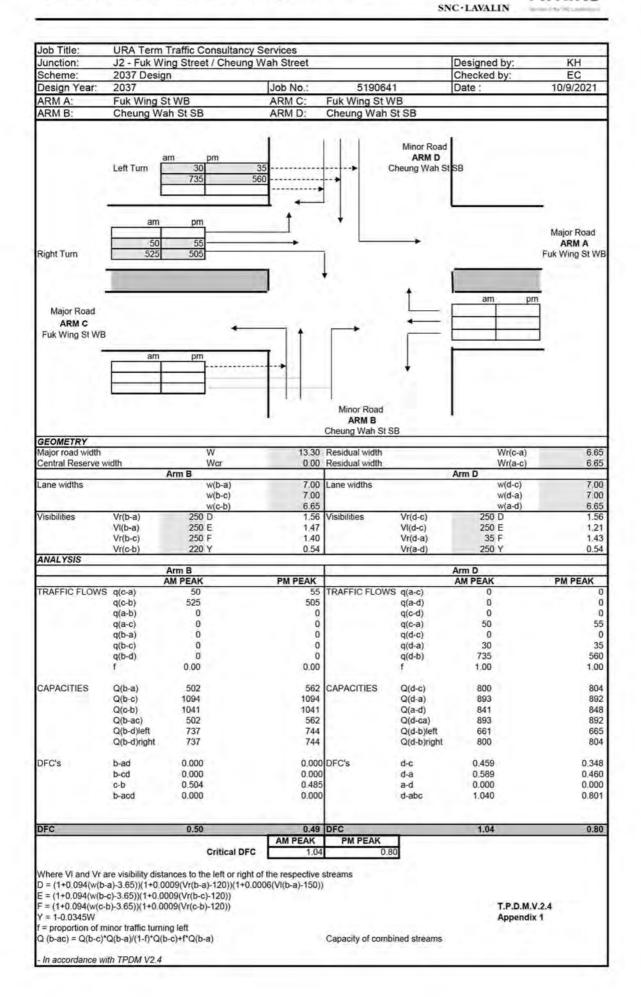
Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.411	Sum of Critical y Y	0.423
	Lost Time L (sec)	15	Lost Time L (sec)	15
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.782	Practical Y Ypr	0.791
	Reserve Capacity RC	90%	Reserve Capacity RC	87%

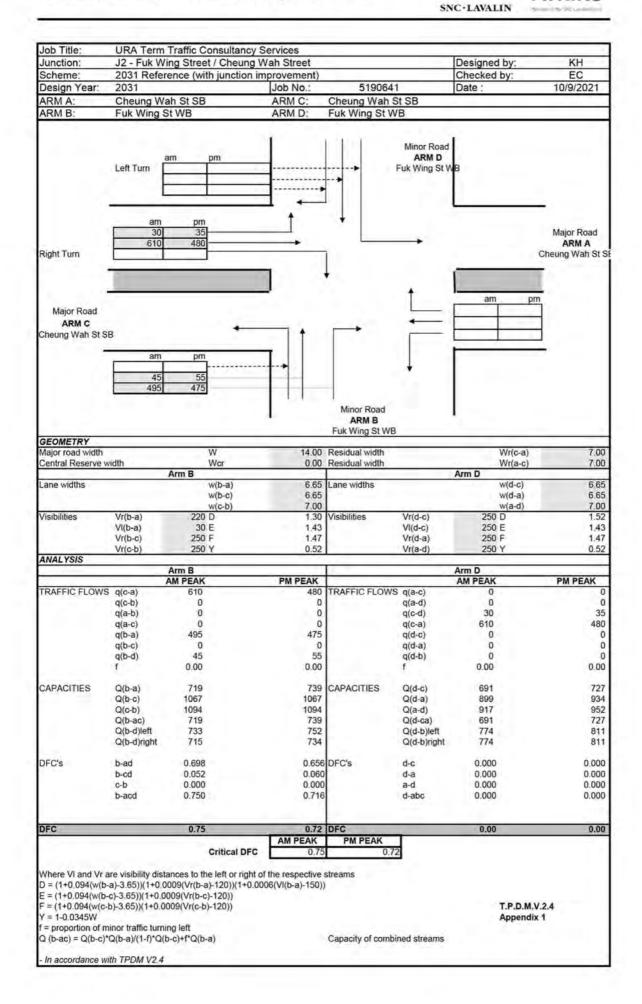


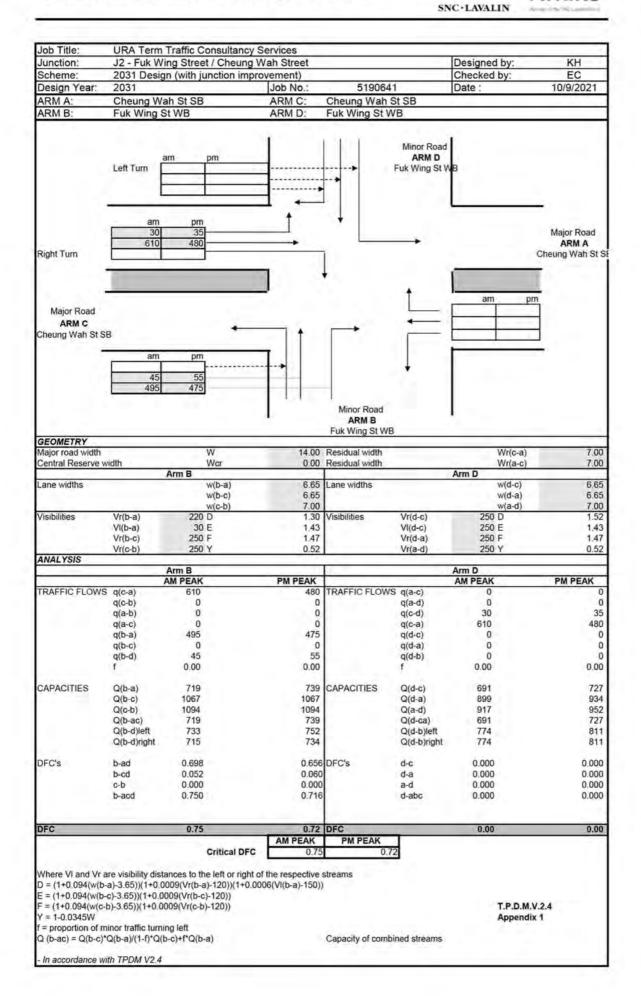


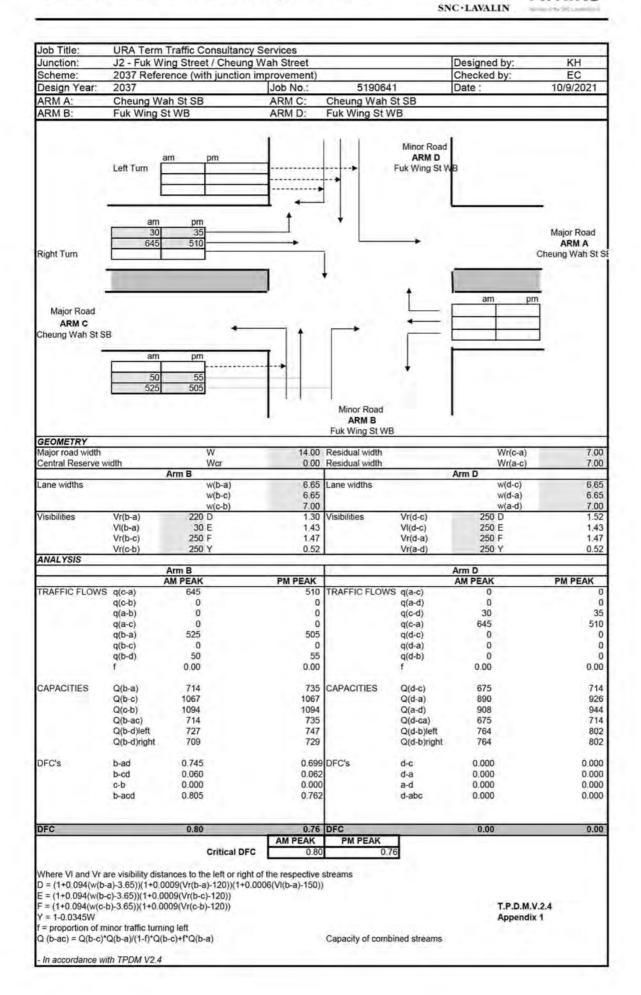


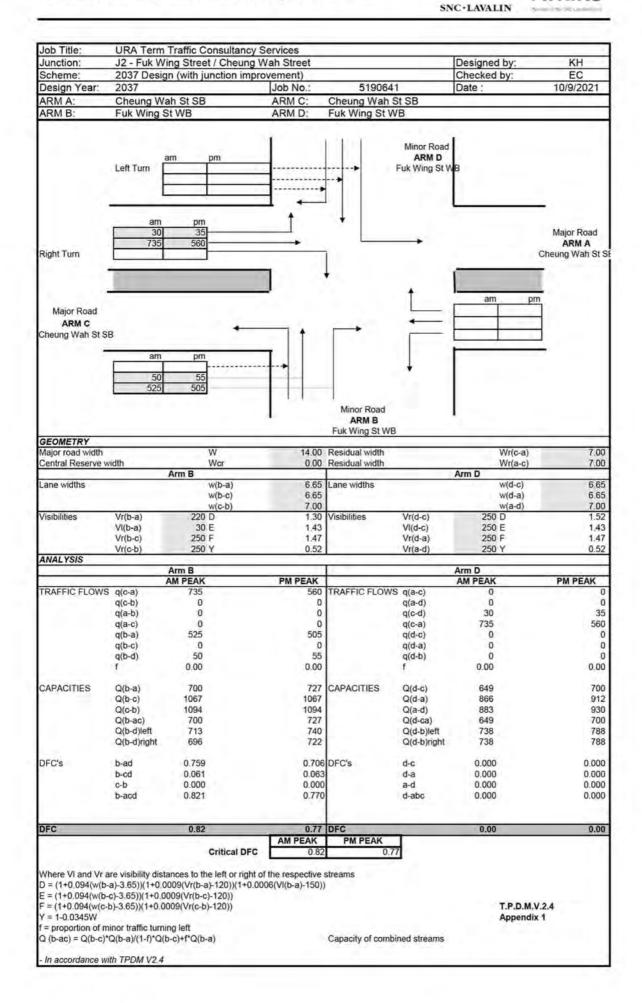












G=

IG=7

IG=7

1+2+8p

ATKINS

G=

IG=

Capacity	Calcula	tions						AM	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Jn Chau St	reet WB					- 1								
1A	A	4.00	Y	N	10		325	100%	1750	0.186	330	100%	1750	0.189
1B	A	4.00	N	N			181		2155	0.084	207		2155	0.096
10	Α	4.00	Y	N	10		149	94%	1765	0.084	173	81%	1795	0.096
Hing Wah S	Street NR													
2A	В	3.60	Y	N	10		203	71%	1425	0.142	207	75%	1420	0.146
2B	В	3.60	N	N	,,,		302	7170	2115	0.143	308	1970	2115	0.146
Un Chau St	reet SB													
3A	С	3.60	Y	N			149		1975	0.075	166		1975	0.084
3B	C	3.60	N	N	10		156	19%	2055	0.076	174	14%	2070	0.084
4p	B,C		7GM+	11FG =	18	sec								
5p	A,B		6GM+	9FG =	15	sec								
6р	A,C		7GM+	12FG =	19	sec								
7p	В		7GM+	13FG =	20	sec								
8p	С		6GM +	11FG =	17	sec								
	,													
	1													

Notes:	AM Peak	1+2+8p	PM Peak	1+2+3
	Sum of Critical y Y	0.329	Sum of Critical y Y	0.418
	Lost Time L (sec)	34	Lost Time L (sec)	14
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.632	Practical Y Ypr	0.798
	Reserve Capacity RC	92%	Reserve Capacity RC	91%

G=

IG=7

IG=7

1+2+8p

ATKINS

G=

IG=

Capacity	Calcula	tions				-		AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Un Chau St	reet WB												-	-
1A	A	4.00	Y	N	10		385	100%	1750	0.220	380	100%	1750	0.217
1B	Α	4.00	N	N			221		2155	0.103	245		2155	0.114
10	Α	4.00	Y	N	10		184	84%	1790	0.103	205	76%	1810	0.113
Hing Wah S	Street NR													
2A	В	3.60	Y	N	10		240	69%	1430	0.168	245	76%	1420	0.173
2B	В	3.60	N	N			355	0010	2115	0.168	365	1	2115	0.173
Un Chau St	reet SB													
3A	С	3.60	Y	N			169		1975	0.086	186		1975	0.094
3B	C	3.60	N	N	10		176	20%	2055	0.086	194	15%	2065	0.094
4p	B,C		7GM+	11FG =	18	sec								
5p	A,B		6GM+	9FG =	15	sec								
6р	A,C		7GM +	12FG =	19	sec								
7p	В		7GM +	13FG =	20	sec								
8p	С		6GM +	11FG =	17	sec								

Notes:	AM Peak	1+2+8p	PM Peak	1+2+3
	Sum of Critical y Y	0.388	Sum of Critical y Y	0.484
	Lost Time L (sec)	34	Lost Time L (sec)	14
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.632	Practical Y Ypr	0.798
	Reserve Capacity RC	63%	Reserve Capacity RC	65%

G=

IG=7

IG=7

1+2+8p

ATKINS

G=

IG=

Capacity	Calcula	tions				-		AMI	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
In Chau St	reet WB		- (:)							11 11 11			-	-
1A	A	4.00	Y	N	10		385	100%	1750	0.220	380	100%	1750	0.217
1B	Α	4.00	N	N			221		2155	0.103	245		2155	0.114
1C	Α	4.00	Y	N	10		184	84%	1790	0.103	205	76%	1810	0.113
Hing Wah S	Street NR													
2A	В	3.60	Y	N	10		240	69%	1430	0.168	245	76%	1420	0.173
2B	В	3.60	N	N			355		2115	0.168	365		2115	0.173
Jn Chau St	reet SB													
3A	С	3.60	Y	N			169		1975	0.086	186		1975	0.094
3B	C	3.60	N	N	10		176	20%	2055	0.086	194	15%	2065	0.094
4p	B,C		7GM+	11FG =	18	sec								
5p	A,B		6GM +	9FG =	15	sec								
6р	A,C		7GM +	12FG =	19	sec								
7p	В		7GM +	13FG =	20	sec								
8p	С		6GM +	11FG =	17	sec				-				

Notes:	AM Peak	1+2+8p	PM Peak	1+2+3
	Sum of Critical y Y	0.388	Sum of Critical y Y	0.484
	Lost Time L (sec)	34	Lost Time L (sec)	14
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.632	Practical Y Ypr	0.798
	Reserve Capacity RC	63%	Reserve Capacity RC	65%

IG=7

1+2+8p

ATKINS

G=

IG=

IG=7

Capacity	Calcula	tions				-		AM	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Un Chau St	reet WB						-						-	-
1A	A	4.00	Y	N	10		405	100%	1750	0.231	405	100%	1750	0.231
1B	Α	4.00	N	N			235		2155	0.109	258		2155	0.120
1C	Α	4.00	Y	N	10		195	85%	1790	0.109	217	76%	1810	0.120
Hing Wah S	Street NR													
2A	В	3.60	Y	N	10		258	70%	1430	0.180	261	75%	1420	0.184
2B	В	3.60	N	N			382		2115	0.181	389		2115	0.184
Un Chau St	reet SB													
3A	С	3.60	Y	N			181		1975	0.092	198		1975	0.100
3B	C	3.60	N	N	10		189	19%	2060	0.092	207	14%	2070	0.100
4p	B,C		7GM+	11FG =	18	sec								
5p	A,B		6GM +	9FG =	15	sec								
6р	A,C		7GM+	12FG =	19	sec								
7p	В		7GM +	13FG =	20	sec								
8p	С		6GM +	11FG =	17	sec								

Notes:	AM Peak	1+2+8p	PM Peak	1+2+3
	Sum of Critical y Y	0.412	Sum of Critical y Y	0.516
	Lost Time L (sec)	34	Lost Time L (sec)	14
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.632	Practical Y Ypr	0.798
	Reserve Capacity RC	53%	Reserve Capacity RC	55%

G=

IG=7

1+2+8p

ATKINS

G=

IG=

Capacity	Calcula	tions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
In Chau S	treet WB						-						"	-
1A	A	4.00	Y	N	10		405	100%	1750	0.231	405	100%	1750	0.231
1B	A	4.00	N	N			263		2155	0.122	276		2155	0.128
10	Α	4.00	Y	N	10		222	74%	1815	0.122	234	71%	1820	0.129
ling Wah S	Street NB													
2A	В	3.60	Y	N	10		292	74%	1425	0.205	283	74%	1420	0.199
2B	В	3.60	N	N			433		2115	0.205	422		2115	0.200
Jn Chau S	treet SB													
3A	С	3.60	Y	N			181		1975	0.092	198		1975	0.100
3B	C	3.60	N	N	10		189	19%	2060	0.092	207	14%	2070	0.100
4p	B,C		7GM+	11FG =	18	sec		_						
5p	A,B		6GM+	9FG =	15	sec								
6р	A,C		7GM +	12FG =	19	sec								
7p	В		7GM+	13FG =	20	sec								
8p	С		6GM +	11FG =	17	sec								
	1													

Notes:	AM Peak	1+2+8p	PM Peak	1+2+3
	Sum of Critical y Y	0.436	Sum of Critical y Y	0.531
	Lost Time L (sec)	34	Lost Time L (sec)	14
	Cycle Time c (sec)	114	Cycle Time c (sec)	124
	Practical Y Ypr	0.632	Practical Y Ypr	0.798
	Reserve Capacity RC	45%	Reserve Capacity RC	50%

ATKINS

G=

Capacity	Calcula	tions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
heung Sh	a Wan Roa	d EB												
1A	A,D	5.30	Y	N			20		2145	0.009	15		2145	0.007
1B	A,D	3.30	N	N			577		2085	0.277	578		2085	0.277
1C	A,D	3.30	N	N			576		2085	0.276	579		2085	0.278
1D	A,D	3.30	N	N			577		2085	0.277	578		2085	0.277
Cheung La	Street NB													
2A	C,D	3.50	Y	N	13	-	176	100%	1405	0.125	199	100%	1405	0.142
2B	C,D	3.50	N	N	15		192	100%	1530	0.125	216	100%	1530	0.141
2C	C,D	3.50	Y	N	18		182	100%	1450	0.126	205	100%	1450	0.141
Cheung Sh	a Wan Roa	d WB												
3A	A,B	3.60	Y	N			540		1580	0.342	563		1580	0.356
3B	A,B	3.60	N	N			722		2115	0.341	753	-	2115	0.356
3C	A,B	3.60	N	N			723		2115	0.342	754		2115	0.357
4р	C,D		6GM +	9FG =	15	sec								
5p	B,C		6GM +	9FG =	15	sec								
6р	A,B		6GM +	18FG =	24	sec								
									-					

Notes:	AM Peak	3+2	PM Peak	3+2
	Sum of Critical y Y	0.467	Sum of Critical y Y	0.498
	Lost Time L (sec)	10	Lost Time L (sec)	10
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.827	Practical Y Ypr	0.831
	Reserve Capacity RC	77%	Reserve Capacity RC	67%

ATKINS

G=

Capacity	Calcula	tions				-		AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	d EB				- 1		1						
1A	A,D	5.30	Y	N			20		2145	0.009	15		2145	0.007
1B	A,D	3.30	N	N			742		2085	0.356	702		2085	0.337
1C	A,D	3.30	N	N			741		2085	0.355	701		2085	0.336
1D	A,D	3.30	N	N			742		2085	0.356	702		2085	0.337
Cheung Lai	Street NB													
2A	C,D	3.50	Y	N	13	-	229	100%	1405	0.163	252	100%	1405	0.179
2B	C,D	3.50	N	N	15		250	100%	1530	0.163	273	100%	1530	0.178
2C	C,D	3.50	Y	N	18		236	100%	1450	0.163	260	100%	1450	0.179
Cheung Sh	a Wan Roa	d WB								-				
3A	A,B	3.60	Y	N			642		1580	0.406	647		1580	0.409
3B	A,B	3.60	N	N			859		2115	0,406	867		2115	0.410
3C	A,B	3.60	N	N			859		2115	0.406	866		2115	0.409
4p	C,D		6GM +	9FG =	15	sec								
5p	B,C		6GM +	9FG =	15	sec								
6р	A,B		6GM +	18FG =	24	sec								
	-													

Notes:	AM Peak	3+2	PM Peak	3+2
	Sum of Critical y Y	0.570	Sum of Critical y Y	0.589
	Lost Time L (sec)	10	Lost Time L (sec)	10
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.827	Practical Y Ypr	0.831
	Reserve Capacity RC	45%	Reserve Capacity RC	41%

ATKINS

G=

Capacity	Calcula	tions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
heung Sh	a Wan Roa	d EB	- (-
1A	A,D	5.30	Y	N			20		2145	0.009	15		2145	0.007
1B	A,D	3.30	N	N			742		2085	0.356	702		2085	0.337
1C	A,D	3.30	N	N			741		2085	0.355	701		2085	0.336
1D	A,D	3.30	N	N			742		2085	0.356	702		2085	0.337
Cheung Lai	Street NB													
2A	C,D	3.50	Y	N	13		229	100%	1405	0.163	252	100%	1405	0.179
2B	C,D	3.50	N	N	15		250	100%	1530	0.163	273	100%	1530	0.178
2C	C,D	3.50	Y	N	18		236	100%	1450	0.163	260	100%	1450	0.179
Cheung Sh	a Wan Roa	d WB												
3A	A,B	3.60	Y	N			665		1580	0.421	658		1580	0.416
3B	A,B	3.60	N	N			890		2115	0.421	881	-	2115	0.417
3C	A,B	3.60	N	N			890		2115	0.421	881		2115	0.417
4р	C,D		6GM+	9FG =	15	sec								
5p	B,C		6GM +	9FG =	15	sec								
6р	A,B		6GM +	18FG =	24	sec								
	1													
									-					

Notes:	AM Peak	3+2	PM Peak	3+2
	Sum of Critical y Y	0.584	Sum of Critical y Y	0.596
	Lost Time L (sec)	10	Lost Time L (sec)	10
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.827	Practical Y Ypr	0.831
	Reserve Capacity RC	42%	Reserve Capacity RC	39%

ATKINS

G=

Capacity	Calcula	tions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
heung Sh	a Wan Roa	d EB												
1A	A,D	5.30	Y	N			20		2145	0.009	15		2145	0.007
1B	A,D	3.30	N	N			785		2085	0.376	747		2085	0.358
1C	A,D	3.30	N	N			785		2085	0.376	746		2085	0.358
1D	A,D	3.30	N	N			785		2085	0.376	747		2085	0.358
Cheung Lai	Street NB													
2A	C,D	3.50	Y	N	13	-	242	100%	1405	0.172	268	100%	1405	0.191
2B	C,D	3.50	N	N	15		263	100%	1530	0.172	291	100%	1530	0.190
2C	C,D	3.50	Y	N	18		250	100%	1450	0.172	276	100%	1450	0.190
Cheung Sh	a Wan Roa	d WB												
3A	A,B	3.60	Y	N			683		1580	0.432	689		1580	0.436
3B	A,B	3.60	N	N			913		2115	0.432	923	-	2115	0.436
3C	A,B	3.60	N	N			914		2115	0.432	923		2115	0.436
4р	C,D		6GM +	9FG =	15	sec								
5p	B,C		6GM +	9FG =	15	sec								
6р	A,B		6GM +	18FG =	24	sec								

Notes:	AM Peak	3+2	PM Peak	3+2
	Sum of Critical y Y	0.605	Sum of Critical y Y	0.627
	Lost Time L (sec)	10	Lost Time L (sec)	10
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.827	Practical Y Ypr	0.831
	Reserve Capacity RC	37%	Reserve Capacity RC	32%

ATKINS

G=

Capacity	Calcula	tions				-		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	d EB	- ()										-	
1A	A,D	5.30	Y	N			20		2145	0.009	15		2145	0.007
1B	A,D	3.30	N	N			787		2085	0.377	750		2085	0.360
1C	A,D	3.30	N	N			786		2085	0.377	750		2085	0.360
1D	A,D	3.30	N	N			787		2085	0.377	750		2085	0.360
Cheung Lai	Street NB													
2A	C,D	3.50	Y	N	13		242	100%	1405	0.172	268	100%	1405	0.191
2B	C,D	3.50	N	N	15		263	100%	1530	0.172	291	100%	1530	0.190
2C	C,D	3.50	Y	N	18		250	100%	1450	0.172	276	100%	1450	0.190
Cheung Sh	a Wan Roa	d WB												
3A	A,B	3.60	Y	N			714		1580	0.452	703		1580	0.445
3B	A,B	3.60	N	N			955		2115	0.452	941	1	2115	0.445
3C	A,B	3.60	N	N			956	-	2115	0.452	941		2115	0.445
4р	C,D		6GM+	9FG =	15	sec								
5p	B,C		6GM +	9FG =	15	sec								
6р	A,B		6GM +	18FG =	24	sec								
			-											

Notes:	AM Peak	3+2	PM Peak	3+2
	Sum of Critical y Y	0.624	Sum of Critical y Y	0.636
	Lost Time L (sec)	10	Lost Time L (sec)	10
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.827	Practical Y Ypr	0.831
	Reserve Capacity RC	33%	Reserve Capacity RC	31%

1+6p+3

1+6p+3

ATKINS

G=

IG=

G=

Capacity	Calcula	tions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sha	a Wan Roa	id EB				- 17							-	
1A	A	3.00	Y	N	15		505	100%	1565	0.323	465	100%	1565	0.297
1B	Α	3.00	N	N			415		2055	0.202	428		2055	0.208
1C	A	3.00	N	N			415		2055	0.202	428		2055	0.208
1D	Α	3.00	N	N			415		2055	0.202	429		2055	0.209
Cheung Sha	a Wan Roa	d WB												
2A	Α	3.40	Y	N			515		1955	0.263	547		1955	0.280
2B	Α	3.40	N	N			553		2095	0.264	587		2095	0.280
2C	A	3.40	N	N			552		2095	0.263	586		2095	0.280
Tai Nan We	st Street N	IB												
3A	C	3.30	Y	N	10		289	100%	1690	0.171	267	100%	1690	0.158
3B	C	3.30	N	N	13		347	22%	2030	0.171	320	26%	2020	0.158
3C	С	3.30	Y	N	15		314	59%	1835	0.171	293	49%	1855	0.158
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6р	В		5GM +	12FG =	17	sec								
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM +	11FG =	16	sec								

Notes:	AM Peak	1+6p+3	PM Peak	1+6p+3
	Sum of Critical y Y	0.494	Sum of Critical y Y	0.456
	Lost Time L (sec)	34	Lost Time L (sec)	34
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0.665
	Reserve Capacity RC	32%	Reserve Capacity RC	46%

1+6p+3

1+6p+3

ATKINS

G=

IG=

G=

Capacity	Calcula	tions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	id EB	- (-			- 1			-	-
1A	A	3.00	Y	N	15		830	100%	1565	0.530	645	100%	1565	0.412
1B	A	3.00	N	N			475		2055	0.231	493		2055	0.240
1C	A	3.00	N	N			475		2055	0.231	493		2055	0.240
1D	Α	3.00	N	N			475		2055	0.231	494		2055	0.240
Cheung Sh	a Wan Roa	d WB												
2A	A	3.40	Y	N			595		1955	0.304	620		1955	0.317
2B	Α	3.40	N	N			637		2095	0.304	665		2095	0.317
2C	A	3.40	N	N			638		2095	0.305	665		2095	0.317
Tai Nan We	st Street N	IB												
3A	С	3.30	Y	N	10		357	100%	1690	0.211	318	100%	1690	0.188
3B	С	3.30	N	N	13		424	31%	2010	0.211	378	30%	2015	0.188
3C	С	3.30	Y	N	15		389	55%	1845	0.211	349	49%	1855	0.188
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6p	В		5GM +	12FG =	17	sec								
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM +	11FG =	16	sec								
	.7													
					-									

Notes:	AM Peak	1+6p+3	PM Peak	1+6p+3
	Sum of Critical y Y	0.742	Sum of Critical y Y	0.600
	Lost Time L (sec)	34	Lost Time L (sec)	34
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0.665
	Reserve Capacity RC	-12%	Reserve Capacity RC	11%

1+6p+3

1+6p+3

ATKINS

G=

IG=

G=

Capacity	Calcula	tions						AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa		- (,							- 1			"	-
1A	A	3.00	Y	N	15		830	100%	1565	0.530	645	100%	1565	0.412
1B	A	3.00	N	N			475		2055	0.231	493		2055	0.240
1C	A	3.00	N	N			475		2055	0.231	493		2055	0.240
1D	Α	3.00	N	N			475		2055	0.231	494		2055	0.240
Cheung Sh	a Wan Roa	ad WB												
2A	A	3.40	Y	N		-	622		1955	0.318	633		1955	0.324
2B	Α	3.40	N	N			666		2095	0.318	679		2095	0.324
2C	A	3.40	N	N			667		2095	0.318	678		2095	0.324
Tai Nan We	st Street N	IB												
3A	С	3.30	Y	N	10		357	100%	1690	0.211	318	100%	1690	0.188
3B	С	3.30	N	N	13		424	31%	2010	0.211	378	30%	2015	0.188
3C	C	3.30	Y	N	15		389	55%	1845	0.211	349	49%	1855	0.188
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6р	В		5GM +	12FG =	17	sec								
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM+	11FG =	16	sec								
									1					

Notes:	AM Peak	1+6p+3	PM Peak	1+6p+3
	Sum of Critical y Y	0.742	Sum of Critical y Y	0.600
	Lost Time L (sec)	34	Lost Time L (sec)	34
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0.665
	Reserve Capacity RC	-12%	Reserve Capacity RC	11%

1+6p+3

1+6p+3

ATKINS

G=

G=

Proportion Saturation Flow surning (%) flow S factor (peu/hr) y 100% 1565 0.553 2055 0.247 2055 0.247 2055 0.246	Design Froportion Flow q turning (9 (pcu/hr) f 680 100% 525 525 525	
100% 1565 0.553 2055 0.247 2055 0.247	525 525	1565 0. 2055 0.
2055 0.247 2055 0.247	525 525	2055 0.
2055 0.247	525	
2055 0.246	525	2000 0.
		2055 0.
1955 0.324	662	1955 0.
2095 0.324	709	2095 0.
2095 0.324	709	2095 0.
100% 1690 0.225	339 100%	1690 0.
31% 2010 0.224	404 29%	2015 0.
56% 1845 0.224	372 50%	1855 0.
	2095 0.324 2095 0.324 100% 1690 0.225 31% 2010 0.224	100% 1690 0.225 339 100% 31% 2010 0.224 404 29%

Notes:	AM Peak	1+6p+3	PM Peak	1+6p+3
	Sum of Critical y Y	0.778	Sum of Critical y Y	0.635
	Lost Time L (sec)	34	Lost Time L (sec)	34
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0,665
	Reserve Capacity RC	-16%	Reserve Capacity RC	5%

1+6p+3

1+6p+3

ATKINS

G=

G=

Capacity Calculations					AM Peak				PM Peak					
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	ad EB			1	- 17							-	
1A	A	3.00	Y	N	15		865	100%	1565	0.553	680	100%	1565	0.435
1B	A	3.00	N	N			508		2055	0.247	528		2055	0.257
1C	A	3.00	N	N			508		2055	0.247	528		2055	0.257
1D	Α	3.00	N	N			509		2055	0.248	529		2055	0.257
Cheung Sh	a Wan Roa	ad WB												
2A	A	3.40	Y	N			670		1955	0.343	678		1955	0.347
2B	Α	3.40	N	N			717		2095	0.342	726		2095	0.347
2C	A	3.40	N	N			718		2095	0.343	726		2095	0.347
Tai Nan We	st Street N	IB												
3A	C	3.30	Y	N	10		380	100%	1690	0.225	339	100%	1690	0.201
3B	C	3.30	N	N	13		451	31%	2010	0.224	404	29%	2015	0.200
3C	С	3.30	Y	N	15		414	56%	1845	0.224	372	50%	1855	0.201
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6р	В		5GM +	12FG =	17	sec			111					
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM+	11FG =	16	sec								
	1													
					-				-					

Notes:	AM Peak	1+6p+3	PM Peak	1+6p+3
	Sum of Critical y Y	0.778	Sum of Critical y Y	0.635
	Lost Time L (sec)	34	Lost Time L (sec)	34
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0,665
	Reserve Capacity RC	-16%	Reserve Capacity RC	5%

1+6p+3

2+6p+3

ATKINS

G=

IG=

G=

Capacity Calculations					AM Peak				PM Peak					
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa		(inst	(may			4		4		- 17		4.55.07	
1A	A	3.00	Y	N	15		463	100%	1565	0.296	434	100%	1565	0.277
1B	A	3.00	N	N	18		576	64%	1950	0.295	551	38%	1990	0.277
1C	A	3.00	N	N			608		2055	0.296	570		2055	0.277
1D	Α	3.00	N	N			608		2055	0.296	570		2055	0.277
Cheung Sh	a Wan Roa	d WB												
2A	A	3.40	Υ	N		-	595		1955	0.304	620	1	1955	0.317
2B	Α	3.40	N	N			637		2095	0.304	665		2095	0.317
2C	A	3.40	N	N			638		2095	0.305	665		2095	0.317
Tai Nan We	st Street N	IB												
3A	С	3.30	Y	N	10		357	100%	1690	0.211	318	100%	1690	0.188
3B	C	3.30	N	N	13		424	31%	2010	0.211	378	30%	2015	0.188
3C	С	3.30	Y	N	15		389	55%	1845	0.211	349	49%	1855	0.188
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6p	В		5GM +	12FG =	17	sec								
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM+	11FG =	16	sec								

Notes:	AM Peak	1+6p+3	PM Peak	2+6p+3
	Sum of Critical y Y	0.507	Sum of Critical y Y	0.506
	Lost Time L (sec)	34	Lost Time L (sec)	32
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0.678
	Reserve Capacity RC	29%	Reserve Capacity RC	34%

2+6p+3

2+6p+3

ATKINS

G=

IG=

G=

Capacity Calculations							AM I	Peak		PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	d EB	- ()							1	-		"	
1A	A	3.00	Y	N	15		463	100%	1565	0.296	434	100%	1565	0.277
1B	A	3.00	N	N	18		576	64%	1950	0.295	551	38%	1990	0.277
1C	A	3.00	N	N			608	1	2055	0.296	570		2055	0.277
1D	Α	3.00	N	N			608		2055	0.296	570		2055	0.277
Cheung Sh	a Wan Roa	d WB												
2A	Α	3.40	Y	N			622		1955	0.318	633		1955	0.324
2B	Α	3.40	N	N			666		2095	0.318	679		2095	0.324
2C	Α	3.40	N	N			667		2095	0.318	678		2095	0.324
Tai Nan We	est Street N	IB												
3A	C	3.30	Y	N	10		357	100%	1690	0.211	318	100%	1690	0.188
3B	C	3.30	N	N	13		424	31%	2010	0.211	378	30%	2015	0.188
3C	С	3.30	Y	N	15	- 14	389	55%	1845	0.211	349	49%	1855	0.188
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec		1						
6p	В		5GM +	12FG =	17	sec			1 11					
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM +	11FG =	16	sec								
	1													
	U				1					-				

Notes:	AM Peak	2+6p+3	PM Peak	2+6p+3
	Sum of Critical y Y	0.530	Sum of Critical y Y	0.512
	Lost Time L (sec)	32	Lost Time L (sec)	32
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.668	Practical Y Ypr	0.678
	Reserve Capacity RC	26%	Reserve Capacity RC	32%

1+6p+3

2+6p+3

ATKINS

G=

G=

Capacity	Calcula	tions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Cheung Sh	a Wan Roa	d EB	(1.1.1)	(may		-3-	4						4.55.07	
1A	A	3.00	Y	N	15		489	100%	1565	0.312	460	100%	1565	0.294
1B	A	3.00	N	N	18		610	62%	1950	0.313	586	38%	1990	0.294
1C	A	3.00	N	N			643		2055	0.313	605		2055	0.294
1D	Α	3.00	N	N			643		2055	0.313	604		2055	0.294
Cheung Sh	a Wan Roa	ad WB												
2A	A	3.40	Y	N			633		1955	0.324	662		1955	0.339
2B	Α	3.40	N	N			679		2095	0.324	709		2095	0.338
2C	Α	3.40	N	N			678		2095	0.324	709		2095	0.338
Tai Nan We	st Street N	IB												
3A	С	3.30	Y	N	10		380	100%	1690	0.225	339	100%	1690	0.201
3B	C	3.30	N	N	13		451	31%	2010	0.224	404	29%	2015	0,200
3C	С	3.30	Y	N	15		414	56%	1845	0.224	372	50%	1855	0.201
4р	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec			1					
6p	В		5GM +	12FG =	17	sec								
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM +	11FG =	16	sec								
	J								- 1					

Notes:	AM Peak	1+6p+3	PM Peak	2+6p+3
	Sum of Critical y Y	0.538	Sum of Critical y Y	0.539
	Lost Time L (sec)	34	Lost Time L (sec)	32
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.653	Practical Y Ypr	0.678
	Reserve Capacity RC	21%	Reserve Capacity RC	26%

2+6p+3

2+6p+3

ATKINS

G=

IG=

G=

Capacity	Calcula	tions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	d EB												
1A	A	3.00	Y	N	15		490	100%	1565	0.313	462	100%	1565	0.295
1B	A	3.00	N	N	18		612	61%	1950	0.314	589	37%	1990	0.296
1C	A	3.00	N	N			644		2055	0.313	607		2055	0.295
1D	Α	3.00	N	N			644		2055	0.313	607		2055	0.295
Cheung Sh	a Wan Roa	ad WB												
2A	Α	3.40	Y	N			670		1955	0.343	678		1955	0.347
2B	Α	3.40	N	N			717		2095	0.342	726		2095	0.347
2C	A	3.40	N	N			718		2095	0.343	726		2095	0.347
Tai Nan We	st Street N	IB												
3A	С	3.30	Y	N	10		380	100%	1690	0.225	339	100%	1690	0.201
3B	C	3.30	N	N	13		451	31%	2010	0.224	404	29%	2015	0,200
3C	С	3.30	Y	N	15		414	56%	1845	0.224	372	50%	1855	0.201
4p	B,C		5GM +	12FG =	17	sec								
5p	В		5GM +	11FG =	16	sec								
6p	В		5GM +	12FG =	17	sec			111					
7p	A,B		5GM +	11FG =	16	sec								
8p	В		5GM +	12FG =	17	sec								
9p	B,C		5GM +	11FG =	16	sec								
	.1													

Notes:	AM Peak	2+6p+3	PM Peak	2+6p+3
	Sum of Critical y Y	0.568	Sum of Critical y Y	0.547
	Lost Time L (sec)	32	Lost Time L (sec)	32
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.668	Practical Y Ypr	0.678
	Reserve Capacity RC	18%	Reserve Capacity RC	24%

G=14

IG=8

IG=14

1+5p+3 1+5p+3 **ATKINS**

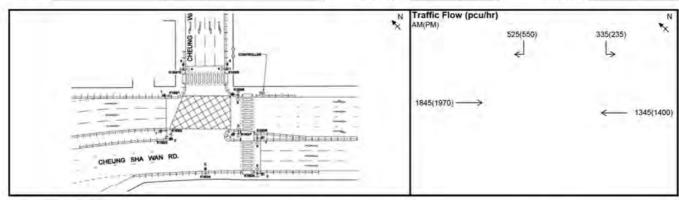
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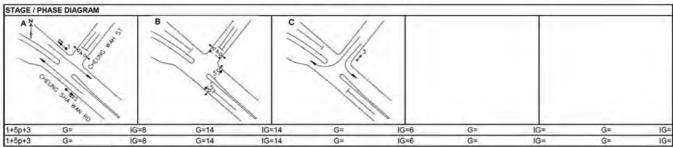
JOB NO. : _____ 5190641 J6 - Cheung Sha Wan Road / Cheung Wah Street 2021 Scheme : Designed by: _ Checked by: N Traffic Flow (pcu/hr) 450(485) 260(185) Action to the second 1585(1690) ----- 1170(1235) Hilliannen CHEUNG SHA WAN RD. STAGE / PHASE DIAGRAM

Capacity	Calcula	tions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
heung Sh	a Wan Roa	id EB				- 1	-							-
1A	A	3.30	Y	N			504		1945	0.259	538		1945	0.277
1B	A	3.30	N	N			541		2085	0.259	576		2085	0.276
1C	Α	3.30	N	N			540		2085	0.259	576		2085	0.276
Cheung Sh	a Wan Roa	ed WB												
2A	A	3.30	Y	N			222		975	0.228	234		975	0.240
2B	A	3.30	N	N			474		2085	0.227	500		2085	0.240
2C	Α	3.30	N	N			474		2085	0.227	501		2085	0.240
Cheung Wa	h Street S	В												
3A	C	3.00	Y	N	10		124	100%	1665	0.074	88	100%	1665	0.053
3B	C	3.00	N	N	13		136	100%	1835	0.074	97	100%	1835	0.053
3C	C	3.00	N	N	18		235	100%	1895	0.124	253	100%	1895	0.134
3D	С	3.00	Y	N	15		215	100%	1740	0.124	232	100%	1740	0.133
4р	A,B		11GM+	11FG =	22	sec								
5р	В		14GM +	12FG =	26	sec								
	-													
	Ŭ.				1				- 17			-		

Notes:	AM Peak	1+5p+3	PM Peak	1+5p+3
	Sum of Critical y Y	0.383	Sum of Critical y Y	0.410
	Lost Time L (sec)	40	Lost Time L (sec)	40
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.610	Practical Y Ypr	0.623
	Reserve Capacity RC	59%	Reserve Capacity RC	52%

ATKINS





Capacity	Calcula	tions						AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
heung Sh	a Wan Roa	d EB												
1A	A	3.30	Y	N			587		1945	0.302	627		1945	0.322
1B	A	3.30	N	N			629		2085	0.302	671		2085	0.322
1C	A	3.30	N	N			629		2085	0.302	672		2085	0.322
Cheung Sh	a Wan Roa	d WB												
2A	A	3.30	Y	N			255		975	0.262	265		975	0.272
2B	A	3.30	N	N			545		2085	0.261	567		2085	0.272
2C	A	3.30	N	N			545		2085	0.261	568		2085	0.272
Cheung Wa	h Street S	В												
3A	C	3.00	Y	N	10		159	100%	1665	0.095	112	100%	1665	0.067
3B	C	3.00	N	N	13		176	100%	1835	0.096	123	100%	1835	0.067
3C	С	3.00	N	N	18		274	100%	1895	0.145	287	100%	1895	0.151
3D	С	3.00	Y	N	15		251	100%	1740	0.144	263	100%	1740	0.151
4p	A,B		11GM+	11FG =	22	sec								
5р	В		14GM +	12FG =	26	sec								

Notes:	AM Peak	1+5p+3	PM Peak	1+5p+3
	Sum of Critical y Y	0.446	Sum of Critical y Y	0.474
	Lost Time L (sec)	40	Lost Time L (sec)	40
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.610	Practical Y Ypr	0.623
	Reserve Capacity RC	37%	Reserve Capacity RC	32%

CHEUNG SHA WAN RD.

ATKINS

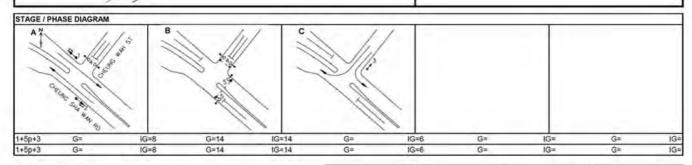
 JOB NO.:
 5190641

 Junction:
 J6 - Cheung Sha Wan Road / Cheung Wah Street
 Design Year:
 2031

 Scheme:
 2031 Design
 Designed by:
 KH
 Checked by:
 EC

 NAM(PM)
 AM(PM)
 525(550)
 335(235)
 N

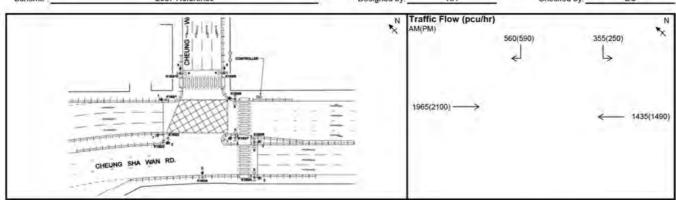
 1845(1970)
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 1430(1440)

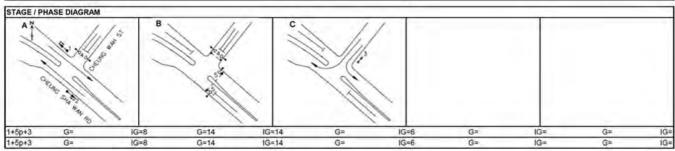


Capacity	Calcula	tions						AMI	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	d EB												
1A	A	3.30	Y	N			587		1945	0.302	627		1945	0.322
1B	A	3.30	N	N			629		2085	0.302	671		2085	0.322
1C	A	3.30	N	N			629		2085	0.302	672		2085	0.322
Cheung Sh	a Wan Pos	d WR												
2A	A	3.30	Y	N			271		975	0.278	273		975	0.280
2B	A	3.30	N	N		-	579	_	2085	0.278	583		2085	0.280
2C	A	3.30	N	N			580		2085	0.278	584		2085	0.280
Cheung Wa	h Street S													
3A	C	3.00	Y	N	10		159	100%	1665	0.095	112	100%	1665	0.067
3B	C	3.00	N	N	13		176	100%	1835	0.096	123	100%	1835	0.067
3C	C	3.00	N	N	18		274	100%	1895	0.145	287	100%	1895	0.151
3D	С	3.00	Y	N	15		251	100%	1740	0.144	263	100%	1740	0.151
4p	A,B		11GM+	11FG =	22	sec								
5р	В		14GM +	12FG =	26	sec								

Notes:	AM Peak	1+5p+3	PM Peak	1+5p+3
	Sum of Critical y Y	0.446	Sum of Critical y Y	0.474
	Lost Time L (sec)	40	Lost Time L (sec)	40
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.610	Practical Y Ypr	0.623
	Reserve Capacity RC	37%	Reserve Capacity RC	32%

ATKINS

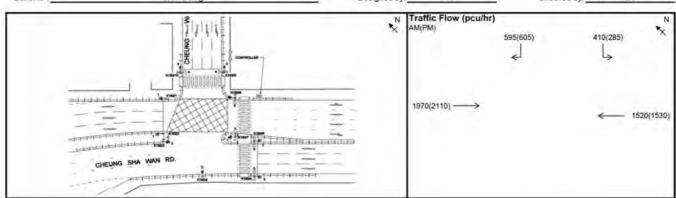


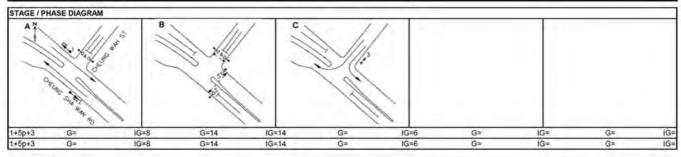


Capacity	Calcula	tions						AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Roa	ad EB												
1A	A	3.30	Y	N			625		1945	0.321	668		1945	0.343
1B	A	3.30	N	N			670		2085	0.321	716		2085	0.343
10	A	3.30	N	N			670		2085	0.321	716		2085	0.343
Cheung Sh	a Wan Roa	ad WR												
2A	A	3.30	Y	N			272		975	0.279	282		975	0.289
2B	A	3.30	N	N		-	581		2085	0.279	604		2085	0.290
2C	A	3.30	N	N			582		2085	0.279	604		2085	0.290
Cheung Wa	h Street S													
3A	C	3.00	Y	N	10		169	100%	1665	0.102	119	100%	1665	0.071
3B	C	3.00	N	N	13		186	100%	1835	0.101	131	100%	1835	0.071
3C	C	3.00	N	N	18		292	100%	1895	0.154	308	100%	1895	0.163
3D	С	3.00	Y	N	15		268	100%	1740	0.154	282	100%	1740	0.162
4p	A.B		11GM+	11FG =	22	sec								
5р	В		14GM +	12FG =	26	sec								

Notes:	AM Peak	1+5p+3	PM Peak	1+5p+3
	Sum of Critical y Y	0.475	Sum of Critical y Y	0.506
	Lost Time L (sec)	40	Lost Time L (sec)	40
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.610	Practical Y Ypr	0.623
	Reserve Capacity RC	28%	Reserve Capacity RC	23%

ATKINS





eak	PM P				Peak	AM F						tions	Calcula	Capacity
Saturation Flow flow S facto (pcu/hr) y	9 (%)	Propor turning f	Design Flow q (pcu/hr)	Flow factor y	Saturation flow S (pcu/hr)	Proportion turning (%)	Design Flow q (pcu/hr)	Gradient in %	Radius for turning (m)	Opposed turn? (Y/N)	Nearside lane? (Y/N)	Lane Width (m)	Stage	Phase
									1	-		d EB	Wan Roa	Cheung Sha
1945 0.34			671	0.322	1945		627			N	Y	3.30	A	1A
2085 0.34			720	0.322	2085		671			N	N	3.30	A	1B
2085 0.34			719	0.322	2085		672			N	N	3.30	A	1C
												d WR	Wan Poa	Cheung Sha
975 0.29		1	290	0.295	975		288			N	Y	3.30	A	2A
2085 0.29		+	620	0.295	2085		616	-		N	N	3.30	A	2B
2085 0.29			620	0.295	2085		616			N	N	3.30	A	2C
												В	h Street S	Cheung Wa
1665 0.08	1%	1009	136	0.117	1665	100%	195		10	N	Y	3.00	C	3A
1835 0.08	1%	1009	149	0.117	1835	100%	215		13	N	N	3.00	C	3B
1895 0.16)%	1009	315	0.164	1895	100%	310		18	N	N	3.00	C	3C
1740 0.16)%	1009	290	0.164	1740	100%	285	14	15	N	Y	3.00	С	3D
	-							sec	22	11FG =	11GM+		A,B	4p
	-	-						sec	26	12FG =	14GM +		В	5р

Notes:	AM Peak	1+5p+3	PM Peak	1+5p+3
	Sum of Critical y Y	0.486	Sum of Critical y Y	0.512
	Lost Time L (sec)	40	Lost Time L (sec)	40
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.610	Practical Y Ypr	0.623
	Reserve Capacity RC	25%	Reserve Capacity RC	22%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2021 Scheme: Existing Designed by: Checked by:_ Traffic Flow (pcu/hr) 250(280) 350(365) 280(315)___ 1205(1100) -360(460) 900(925) 80(75) 20(30) 175(150) 115(55) STAGE / PHASE DIAGRAM 10 105 13

Capacity	Calculat	ions						AM I	Peak			PM I	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road	WB												
1A	A,E	3.50	Y	N	13		305	26%	1905	0.160	312	24%	1910	0.163
18	A,E	3.50	N	N			338		2105	0.161	344		2105	0.163
1C	A,E	3.50	N	N			337		2105	0.160	344		2105	0.163
Chauna Sh	a Wan Roa	450												
2A	A,B	3.20	Y	N	13		449	62%	1800	0.249	424	74%	1775	0.239
2B	A,B	3.20	N	N	10		518	0270	2075	0.249	496	7470	2075	0.239
2C	A,B	3.20	N	N		-	518		2075	0.250	495		2075	0.239
3A	B B	3.20	N	N	23		360	100%	1945	0.250	495	100%	1945	0.237
Hing Wah S	Street SB	1 1 2 1												
4A	С	3.30	γ	N			195		1945	0.100	210		1945	0.108
48	С	3.30	N	N	30		207	25%	2060	0.100	222	30%	2055	0.108
4C	С	3.30	N	N	28		198	100%	1975	0,100	213	100%	1975	0.108
Hing Wah S	Street NB													
5A	D	3.50	Y	N	15		160	13%	1940	0.082	120	25%	1915	0.063
5B	D	3.50	N	N	30		150	77%	1825	0.082	115	48%	1850	0.062
6р	A,B,C,E		7GM+	7FG =	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM +	11FG =	22	sec								
11p	С		7GM +	7FG =	14	sec								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.529	Sum of Critical y Y	0.571
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	35%	Reserve Capacity RC	26%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2031 Scheme: 2031 Reference Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(320) 395(405) 1415(1305) · 445(540) 1025(1040) 110(100) 20(35) 200(175) 170(85) STAGE / PHASE DIAGRAM 10 105 13

Capacity	/ Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road						-							
1A	A,E	3.50	Y	N	13		352	31%	1895	0.186	355	28%	1900	0.187
18	A,E	3.50	N	N			392		2105	0.186	393		2105	0.187
1C	A,E	3.50	N	N			391		2105	0.186	392		2105	0.186
Chauna Sh	na Wan Roa	d EB												
2A	A,B	3.20	Y	N	13		523	59%	1805	0.290	499	71%	1785	0.280
2B	A,B	3.20	N	N	10		601	3070	2075	0.290	581	1170	2075	0.280
2C	A,B	3.20	N	N			601		2075	0.290	580		2075	0.280
3A	В	3.20	N	N	23		445	100%	1945	0.229	540	100%	1945	0.278
Hing Wah	Careet SB													
4A	C	3.30	Y	N			226	1	1945	0.116	236		1945	0.121
4B	C	3.30	N	N	30		239	29%	2055	0.116	249	32%	2050	0.121
4C	c	3.30	N	N	28		230	100%	1975	0.116	240	100%	1975	0.122
Hing Wah	Street NB													
5A	D	3.50	Υ	N	15		202	10%	1945	0.104	151	23%	1920	0.079
5B	D	3.50	N	N	30		188	90%	1815	0.104	144	59%	1840	0.078
6р	A,B,C,E		7GM+	7FG =	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM+	11FG =	22	sec								
11p	C		7GM +	7FG =	14	sec								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.635	Sum of Critical y Y	0.665
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	12%	Reserve Capacity RC	8%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2031 Scheme: 2031 Design Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(320) 395(405) 310(355)__ 1415(1305) · 445(540) 1085(1065) 110(100) 40(50) 200(175) 185(105) STAGE / PHASE DIAGRAM 10 105 13

Capacit	y Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow facto
Cheung SI	ha Wan Road	WB	1	1			· de-const		10				9	
1A	A,E	3.50	Y	N	13		371	30%	1895	0.196	363	28%	1900	0.19
18	A,E	3.50	N	N			412		2105	0.196	401		2105	0.19
1C	A,E	3.50	N	N			412		2105	0.196	401		2105	0.19
Cheung SI	ha Wan Roa	d EB												
2A	A,B	3.20	Y	N	13		523	59%	1805	0.290	499	71%	1785	0.28
28	A,B	3.20	N	N			601		2075	0.290	581		2075	0.28
2C	A,B	3.20	N	N			601		2075	0.290	580		2075	0.28
3A	В	3.20	N	N	23		445	100%	1945	0.229	540	100%	1945	0.27
Hing Wah	Street SB													
4A	C	3.30	Y	N			226		1945	0.116	236		1945	0.12
4B	С	3.30	N	N	30		239	29%	2055	0.116	249	32%	2050	0.12
4C	С	3.30	N	N	28		230	100%	1975	0.116	240	100%	1975	0.12
Hing Wah	Street NB													
5A	D	3.50	Y	N	15		219	18%	1930	0.113	168	30%	1910	0.08
5B	D	3.50	N	N	30		206	90%	1815	0.113	162	65%	1835	0.08
6р	A,B,C,E		7GM+	7FG =	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM +	11FG =	22	sec								
11p	С		7GM +	7FG =	14	sec								
						1								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.655	Sum of Critical y Y	0.678
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	9%	Reserve Capacity RC	6%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2037 Scheme: 2037 Reference Designed by: Checked by:_ EC Traffic Flow (pcu/hr) 320(345) 420(435) 1095(1110) 115(105) 25(35) 215(190) 175(90) STAGE / PHASE DIAGRAM 10 105 13

Capacity	/ Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung St	na Wan Road	WB												
1A	A,E	3.50	Y	N	13		376	31%	1895	0.198	378	28%	1900	0.199
18	A,E	3.50	N	N			417		2105	0.198	419		2105	0.199
1C	A,E	3.50	N	N			417		2105	0.198	418		2105	0.199
Chauna Sh	na Wan Roa	d EB												
2A	A,B	3.20	Y	N	13		558	60%	1805	0.309	532	71%	1780	0.299
2B	A,B	3.20	N	N	19		641	0070	2075	0.309	619	7.170	2075	0.298
2C	A,B	3.20	N	N		-	641	1	2075	0.309	619		2075	0.298
3A	В	3.20	N	N	23		475	100%	1945	0.244	575	100%	1945	0.296
Hing Wah	Cleant CD													
4A	C	3.30	Υ	N			241	-	1945	0.124	254		1945	0.131
4B	c	3.30	N	N	30		254	30%	2055	0.124	268	32%	2050	0.131
4C	C	3.30	N	N	28		245	100%	1975	0.124	258	100%	1975	0.131
40		3,30	14	- 14	20		243	100%	1973	0.124	230	100%	1973	0.131
Hing Wah	Street NB													
5A	D	3.50	Υ	N	15		215	12%	1940	0.111	161	22%	1925	0.084
5B	D	3.50	N	N	30		200	88%	1815	0.110	154	58%	1840	0.084
6р	A,B,C,E		7GM+	7FG=	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM+	11FG =	22	sec								
11p	C		7GM +	7FG =	14	sec								
	11													

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.678	Sum of Critical y Y	0.709
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	5%	Reserve Capacity RC	2%

ATKINS

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2037 Scheme: 2037 Design Designed by: Checked by:_ Traffic Flow (pcu/hr) 320(345) 420(435) 1505(1390) · 475(575) 1155(1135) 115(105) 45(50) 220(200) 190(110) STAGE / PHASE DIAGRAM 10 105 13 G=

Capacity	/ Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Cheung St	a Wan Road	WB												
1A	A,E	3.50	Y	N	13	-	395	29%	1900	0.208	386	27%	1905	0.203
18	A,E	3.50	N	N			438		2105	0.208	427		2105	0.203
1C	A,E	3.50	N	N			437		2105	0.208	427	-	2105	0.203
Cheuna St	na Wan Roa	dFR												
2A	A,B	3.20	Y	N	13		572	69%	1785	0.320	544	79%	1765	0.308
2B	A,B	3.20	N	N	10		664	0070	2075	0.320	638	1079	2075	0.307
2C	A,B	3.20	N	N			664		2075	0.320	638		2075	0.307
3A	В	3.20	N	N	23		475	100%	1945	0.244	575	100%	1945	0.296
Hing Wah	Street SB													
4A	С	3.30	Y	N			241		1945	0.124	254		1945	0.131
4B	С	3.30	N	N	30		254	30%	2055	0.124	268	32%	2050	0.131
4C	С	3.30	N	N	28		245	100%	1975	0.124	258	100%	1975	0.131
Hing Wah	Street NB													
5A	D	3.50	Υ	N	15		234	19%	1930	0.121	184	27%	1915	0.096
5B	D	3.50	N	N	30		221	86%	1815	0.122	176	63%	1835	0.096
6р	A,B,C,E		7GM +	7FG=	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM+	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM+	11FG =	22	sec								
11p	С		7GM +	7FG =	14	sec								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.698	Sum of Critical y Y	0.725
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	2%	Reserve Capacity RC	-1%

ATKINS

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2031 2031 Reference (with junction improvement) Designed by: Checked by:_ Scheme: Traffic Flow (pcu/hr) 300(320) 395(405) 1415(1305) · 445(540) 1025(1040) 110(100) 20(35) 200(175) 170(85) STAGE / PHASE DIAGRAM 10 105 13

Capacity	/ Calculat	ions						AM I	Peak		PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
Cheung St	a Wan Road	WB													
1A	A,E	3.50	Y	N	13		352	31%	1895	0.186	355	28%	1900	0.187	
18	A,E	3.50	N	N			392		2105	0.186	393		2105	0.187	
1C	A,E	3.50	N	N			391		2105	0.186	392		2105	0.186	
Chauna St	na Wan Roa	dER													
2A	A,B	3.20	Y	N	13		523	59%	1805	0.290	499	71%	1785	0.280	
2B	A,B	3.20	N	N	19		601	5070	2075	0.290	581		2075	0.280	
2C	A,B	3.20	N	N			601		2075	0.290	580		2075	0.280	
3A	В	3.20	N	N	23		445	100%	1945	0.229	540	100%	1945	0.278	
Hing Wah	Street SB														
4A	С	3.30	Y	N			156	1	1360	0.115	160		1360	0.118	
4B	C	3.30	N	N			239		2085	0.115	245		2085	0.118	
4C	С	3.30	N	N	30		150	100%	1985	0.076	160	100%	1985	0.081	
4D	С	3.30	N	N	28		150	100%	1975	0.076	160	100%	1975	0.081	
Hing Wah	Street NB														
5A	D	3.50	Y	N	15		20	100%	1785	0.011	35	100%	1785	0.020	
5B	D	3.50	N	N			189		2105	0.090	132		2105	0.063	
5C	D	3.50	N	N	30		181	94%	2010	0.090	128	66%	2035	0.063	
6р	A,B,C,E		7GM+	7FG =	14	sec									
7p	D		8GM +	8FG =	16	sec									
8p	B,C,D		9GM+	9FG =	18	sec									
9p	C,E		9GM +	9FG =	18	sec									
10p	A,B,D,E		11GM+	11FG =	22	sec									
11p	С		7GM +	7FG =	14	sec									

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+7p
	Sum of Critical y Y	0.620	Sum of Critical y Y	0.582
	Lost Time L (sec)	26	Lost Time L (sec)	37
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.644
	Reserve Capacity RC	15%	Reserve Capacity RC	11%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2031 2031 Design (with junction improvement) Designed by: Checked by:_ Scheme: Traffic Flow (pcu/hr) 395(405) 300(320) 310(355)__ 1415(1305) 1085(1065) 110(100) 40(50) 200(175) 185(105) STAGE / PHASE DIAGRAM 10 105 13

Capacity	y Calculat	ions						AM I	Peak			Flow q turning (%) flow S (pcu/hr) f (pcu/hr			
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	turning (%)	flow S	Flow facto	
Cheuna St	na Wan Road		1	1			- George				- Granner				
1A	A,E	3.50	Y	N	13		371	30%	1895	0.196	363	28%	1900	0.19	
18	A,E	3.50	N	N			412		2105	0.196			2105	0.190	
1C	A,E	3.50	N	N			412		2105	0.196	401	-	2105	0.190	
Cheung St	na Wan Roa	d EB													
2A	A,B	3.20	Y	N	13		523	59%	1805	0.290	499	71%	1785	0.280	
28	A,B	3.20	N	N			601		2075	0.290				0.280	
2C	A,B	3.20	N	N			601		2075	0.290				0.28	
3A	В	3.20	N	N	23		445	100%	1945	0.229	540	100%	1945	0.278	
Hing Wah	Street SB														
4A	С	3.30	Υ	N			156		1360	0.115	160		1360	0.118	
4B	С	3.30	N	N			239		2085	0.115	245		2085	0.118	
4C	С	3.30	N	N	30		150	100%	1985	0.076	160	100%	1985	0.08	
4D	С	3.30	N	N	28		150	100%	1975	0.076	160	100%	1975	0.08	
Hing Wah	Street NB														
5A	D	3.50	Υ	N	15		40	100%	1785	0.022	50	100%	1785	0.028	
5B	D	3.50	N	N			197		2105	0.094	143		2105	0.068	
5C	D	3.50	N	N	30		188	98%	2005	0.094	137	77%	2025	0.068	
6р	A,B,C,E		7GM+	7FG =	14	sec									
7p	D		8GM +	8FG =	16	sec									
8p	B,C,D		9GM +	9FG =	18	sec									
9p	C,E		9GM +	9FG =	18	sec									
10p	A,B,D,E		11GM+	11FG =	22	sec									
11p	С		7GM +	7FG =	14	sec									

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+7p
	Sum of Critical y Y	0.633	Sum of Critical y Y	0.586
	Lost Time L (sec)	26	Lost Time L (sec)	37
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.644
	Reserve Capacity RC	12%	Reserve Capacity RC	10%

1 3 G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2037 2037 Reference (with junction improvement) Designed by: Checked by:_ EC Scheme: Traffic Flow (pcu/hr) 320(345) 420(435) 1095(1110) 115(105) 25(35) 215(190) 175(90) STAGE / PHASE DIAGRAM 10 10%

Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Cheung Sh	a Wan Road	WB												
1A	A,E	3.50	Y	N	13		376	31%	1895	0.198	378	28%	1900	0.199
18	A,E	3.50	N	N			417		2105	0.198	419		2105	0.199
1C	A,E	3.50	N	N			417		2105	0.198	418		2105	0.199
Chauna Sh	a Wan Roa	dER												
2A	A,B	3.20	Y	N	13		558	60%	1805	0.309	532	71%	1780	0.299
2B	A,B	3.20	N	N	19		641	90,0	2075	0.309	619	1.130	2075	0.298
2C	A,B	3.20	N	N			641		2075	0.309	619		2075	0.298
3A	В	3.20	N	N	23		475	100%	1945	0.244	575	100%	1945	0.296
Hing Wah S	Street SB													
4A	С	3.30	Y	N			166	1	1360	0.122	172		1360	0.126
4B	С	3.30	N	N			254		2085	0.122	263		2085	0.126
4C	С	3.30	N	N	30		160	100%	1985	0.081	173	100%	1985	0.087
4D	С	3.30	N	N	28		160	100%	1975	0.081	172	100%	1975	0.087
Hing Wah S	Street NB						_							
5A	D	3.50	Y	N	15		25	100%	1785	0.014	35	100%	1785	0.020
5B	D	3.50	N	N			199		2105	0.095	142		2105	0.067
5C	D	3.50	N	N	30		191	92%	2015	0.095	138	65%	2040	0.068
6р	A,B,C,E		7GM+	7FG =	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM +	11FG =	22	sec								
11p	С		7GM +	7FG =	14	sec								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+7p
	Sum of Critical y Y	0.659	Sum of Critical y Y	0.621
	Lost Time L (sec)	26	Lost Time L (sec)	37
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.644
	Reserve Capacity RC	8%	Reserve Capacity RC	4%

G=

IG=10

JOB NO. : 5190641 J7 - Cheung Sha Wan Road / Hing Wah Street 2037 2037 Design (with junction improvement) Designed by: Checked by:_ Scheme: Traffic Flow (pcu/hr) 320(345) 420(435) 1505(1390) · 475(575) 1155(1135) 115(105) 45(50) 190(110) 220(200) STAGE / PHASE DIAGRAM 10 105 13

Capacity	/ Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung St	a Wan Road	WB												
1A	A,E	3.50	Y	N	13	-	395	29%	1900	0.208	386	27%	1905	0.203
18	A,E	3.50	N	N			438		2105	0.208	427		2105	0.203
1C	A,E	3.50	N	N			437		2105	0.208	427		2105	0.203
Cheuna St	na Wan Roa	dFR												
2A	A,B	3.20	Y	N	13		572	69%	1785	0.320	544	79%	1765	0.308
2B	A,B	3.20	N	N	10		664	0070	2075	0.320	638	1079	2075	0.307
2C	A,B	3.20	N	N			664		2075	0.320	638		2075	0.307
3A	В	3.20	N	N	23		475	100%	1945	0.244	575	100%	1945	0.296
Hing Wah	Street SB													
4A	С	3.30	Y	N			166		1360	0.122	172		1360	0.126
4B	С	3.30	N	N			254		2085	0.122	263		2085	0.126
4C	С	3.30	N	N	30		160	100%	1985	0.081	173	100%	1985	0.087
4D	С	3.30	N	N	28		160	100%	1975	0.081	172	100%	1975	0.087
Hing Wah	Street NB													
5A	D	3.50	Υ	N	15		45	100%	1785	0.025	50	100%	1785	0.028
5B	D	3.50	N	N			210		2105	0.100	158		2105	0.075
5C	D	3.50	N	N	30		200	95%	2010	0,100	152	72%	2030	0.075
6р	A,B,C,E		7GM+	7FG =	14	sec								
7p	D		8GM +	8FG =	16	sec								
8p	B,C,D		9GM +	9FG =	18	sec								
9p	C,E		9GM +	9FG =	18	sec								
10p	A,B,D,E		11GM+	11FG =	22	sec								
11p	С		7GM +	7FG =	14	sec								

Notes:	AM Peak	1+3+4+5	PM Peak	1+3+4+5
	Sum of Critical y Y	0.674	Sum of Critical y Y	0.700
	Lost Time L (sec)	26	Lost Time L (sec)	26
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.711	Practical Y Ypr	0.720
	Reserve Capacity RC	6%	Reserve Capacity RC	3%

			JOI	B NO. ;	5190641
Junction :	J8 -Cheung Sha Wan Road / Tonkin	Street	Design Year;_		2021
Scheme:	Existing	Designed by:	КН	Checke	ed by: EC
, s	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	‡ N Tr	raffic Flow (pcu/hr) M(PM)	135(140) 470(415) 100(125) X
1			155(150)^ 1135(940)>		↑ 190(245) < 750(840) √ 230(255)
			120(110)	↑ 510(535)	
STAGE / PHASE DIAGRAM A Change of the control of	(2)	10 9 6	11/1	E .	1 8

Capacity	Calculat	tions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road													
1A	D,E	3.50	Y	N	13		398	39%	1875	0.212	335	45%	1865	0.180
18	D,E	3.50	N	N			446		2105	0.212	378		2105	0.180
1C	D,E	3.50	N	N			446		2105	0.212	377		2105	0.179
Chauna Sh	a Wan Road	- WP												
2A	A,E	3.00	Y	N	18	-	298	77%	1795	0.166	333	77%	1795	0.186
2B	A,E	3.00	N	N	10		341	1170	2055	0.166	381	1770	2055	0.185
2B 2C		3.00		N			341		2055	0.166	381		2055	0.185
3A	A,E A	3.00	N	N N	28		190	100%	1560	0.100	245	100%	1560	0.157
Tonkin Str	eet NB													
4A	В	3.00	Y	N	13		120	100%	1370	0.088	110	100%	1370	0.080
4B	В	3.00	N	N			170		2055	0.083	178		2055	0.087
4C	В	3.00	N	N			170		2055	0.083	179		2055	0.087
4D	В	3.00	N	N			170		2055	0.083	178		2055	0.087
Tonkin Str	eet SB													
5A	B,C	3.50	Y	N	15		83	100%	715	0.116	79	100%	715	0.110
5B	B,C	3.50	N	N	18		243	7%	2090	0.116	229	20%	2070	0.111
5C	B,C	3.50	N	N			244		2105	0.116	232		2105	0.110
6A	C	3.50	N	N	25	-	135	100%	1985	0.068	140	100%	1985	0.071
7p	A		5GM+	9FG =	14	sec								
8p	A,D,E		7GM +	13FG =	20	sec								
9p	C	1	5GM +	9FG =	14	sec		+						
10p	A,B,C		5GM +	10FG =	15	sec								
11p	D D		5GM +	9FG =	14	sec		-						
12p	D	_	6GM +	11FG =	17	sec		1						
13p	B,C,D		6GM+	11FG =	17	sec		1						
Top	0,0,0		OOW 7	1110=	.,,	360	_	1						

Notes:	AM Peak	3+4+6+1	PM Peak	3+4+6+1
	Sum of Critical y Y	0.490	Sum of Critical y Y	0.494
	Lost Time L (sec)	24	Lost Time L (sec)	24
	Cycle Time c (sec)	136	Cycle Time c (sec)	136
	Practical Y Ypr	0.741	Practical Y Ypr	0.741
	Reserve Capacity RC	51%	Reserve Capacity RC	50%

3+4+6+1

JOB NO. : 5190641 J8 -Cheung Sha Wan Road / Tonkin Street 2031 Scheme: 2031 Reference Designed by Checked by:_ Traffic Flow (pcu/hr) 155(155) 535(470) 110(140) 210(275) 865(955) 285(315) 1370(1135) 135(125) 645(630) STAGE / PHASE DIAGRAM 10 9 6 one she han Ro 10, 8 8 . 8 3 25 25 4 13 13 13

Capacity	Calculat	ions					AM Peak				PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
Cheung Sh	a Wan Road	EB													
1A	D,E	3.50	Y	N	13		480	39%	1880	0.255	405	46%	1865	0.217	
18	D,E	3.50	N	N			538		2105	0.256	458	7 7	2105	0.218	
1C	D,E	3.50	N	N			537		2105	0.255	457		2105	0.217	
Chauna Sh	a Wan Road	WP													
2A	A,E	3.00	Y	N	18		349	82%	1790	0.195	385	82%	1790	0.215	
2B	A,E	3.00	N	N	10		401	0270	2055	0.195	443	02.70	2055	0.216	
2C	A,E	3.00	N	N			400		2055	0.195	442		2055	0.215	
3A	A	3.00	N	N	28		210	100%	1560	0.135	275	100%	1560	0.176	
Faultin Otto															
Tonkin Stre	-	3.00	Y	41	13		135	100%	1370	0.000	125	100%	4070	0.091	
4A 4B	B B	3.00	N	N N	13		215	100%	2055	0.099	210	100%	1370 2055	0.091	
46 4C		3.00	N	N			215	-	2055	0.105	210		2055	0.102	
4C 4D	В	3.00						_							
40	В	3.00	N	N			215		2055	0.105	210		2055	0.102	
Tonkin Stre	et SB														
5A	B,C	3.50	Y	N	15		.94	100%	715	0.131	89	100%	715	0.124	
5B	B,C	3.50	N	N	18		275	6%	2095	0.131	258	20%	2070	0.125	
5C	B,C	3.50	N	N			276		2105	0.131	263		2105	0.125	
6A	С	3.50	N	N	25	-	155	100%	1985	0.078	155	100%	1985	0.078	
7p	A		5GM +	9FG =	14	sec									
8p	A,D,E		7GM +	13FG =	20	sec									
9p	C		5GM +	9FG =	14	sec									
10p	A,B,C		5GM +	10FG =	15	sec									
11p	D		5GM +	9FG =	14	sec									
12p	D	- 7	6GM +	11FG =	17	sec									
13p	B,C,D		6GM +	11FG =	17	sec									

Notes:	AM Peak	3+4+6+1	PM Peak	3+4+6+1
	Sum of Critical y Y	0.573	Sum of Critical y Y	0.574
	Lost Time L (sec)	24	Lost Time L (sec)	24
	Cycle Time c (sec)	136	Cycle Time c (sec)	136
	Practical Y Ypr	0.741	Practical Y Ypr	0.741
	Reserve Capacity RC	29%	Reserve Capacity RC	29%

3+4+6+1

JOB NO. : 5190641 J8 -Cheung Sha Wan Road / Tonkin Street 2031 Scheme: 2031 Design Designed by Checked by:_ Traffic Flow (pcu/hr) 155(155) 535(470) 110(140) 210(275) 925(980) 285(315) 1385(1155) 135(125) 645(630) STAGE / PHASE DIAGRAM 10 9 6 one she han Ro 10, 8 8 . 8 3 25 25 4 13 13 13

Capacity Calculations Phase Stage Lane Nearside Opposed Radius for Gradient							AM I	Peak			PM	Peak		
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road						-							-
1A	D,E	3.50	Y	N	13	-	484	38%	1880	0.257	411	45%	1865	0.220
18	D,E	3.50	N	N			543	1	2105	0.258	465		2105	0.221
1C	D,E	3.50	N	N			543		2105	0.258	464		2105	0.220
Chauna Sh	a Wan Road	- WP												
2A	A,E	3.00	Y	N	18		368	77%	1795	0.205	393	80%	1790	0.220
2B	A,E	3.00	N	N	10		421	1170	2055	0.205	451	0076	2055	0.220
2B 2C		3.00		N		-	421		2055	0.205	451		2055	0.219
3A	A,E A	3.00	N	N N	28		210	100%	1560	0.205	275	100%	1560	0.218
									1000			13634		
Tonkin Str	eet NB													
4A	В	3.00	Y	N	13		135	100%	1370	0.099	125	100%	1370	0.091
4B	В	3.00	N	N	-		215		2055	0.105	210		2055	0.102
4C	В	3.00	N	N			215		2055	0.105	210		2055	0.102
4D	В	3.00	N	N			215		2055	0.105	210		2055	0.102
Tonkin Str	et SB													
5A	B,C	3.50	Y	N	15		94	100%	715	0.131	89	100%	715	0.124
5B	B,C	3.50	N	N	18		275	6%	2095	0.131	258	20%	2070	0.125
5C	B,C	3.50	N	N	10		276	570	2105	0.131	263	2370	2105	0.125
6A	C	3.50	N	N	25	-	155	100%	1985	0.078	155	100%	1985	0.078
7p	A		5GM +	9FG =	14	sec								
8p	A,D,E		7GM +	13FG =	20	sec								
9p	C	_	5GM +	9FG =	14	sec		1						
10p	A,B,C		5GM +	10FG =	15	sec								
11p	D D		5GM +	9FG =	14	sec								
12p	D		6GM +	11FG =	17	sec		1						
13p	B,C,D		BGM +	11FG =	17	sec		1						
Top	5,0,0		OGWI +	TIFG -	111	260		+						

Notes:	AM Peak	3+4+6+1	PM Peak	3+4+6+1
	Sum of Critical y Y	0.575	Sum of Critical y Y	0.577
	Lost Time L (sec)	24	Lost Time L (sec)	24
	Cycle Time c (sec)	136	Cycle Time c (sec)	136
	Practical Y Ypr	0.741	Practical Y Ypr	0.741
	Reserve Capacity RC	29%	Reserve Capacity RC	28%

3+4+6+1

JOB NO. : 5190641 J8 -Cheung Sha Wan Road / Tonkin Street 2037 Scheme: 2037 Reference Designed by Checked by:_ Traffic Flow (pcu/hr) 165(165) 570(500) 120(150) 225(290) 925(1020) 305(335) 1460(1205) 145(130) 685(675) STAGE / PHASE DIAGRAM 30 9 M one she han Ro 10, 8 8 . 8 3 25 25 4 13 13 13

Capacity Calculations Phase Stape Lane Nearside Opposed Radius for Gradient							AM I	Peak			PM	Peak		
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road	EB												
1A	D,E	3.50	Y	N	13	-	511	38%	1880	0.272	431	46%	1860	0.232
18	D,E	3.50	N	N			572		2105	0.272	487		2105	0.231
1C	D,E	3.50	N	N			572		2105	0.272	487		2105	0.231
Chauna Sh	a Wan Road	I WR												
2A	A,E	3.00	Y	N	18		373	82%	1790	0.208	411	82%	1790	0.230
2B	A,E	3.00	N	N	10		429	0270	2055	0.209	472	02.70	2055	0.230
2C	A,E	3.00	N	N		-	428	1	2055	0.208	472		2055	0.230
3A	A,E	3.00	N	N	28		225	100%	1560	0.144	290	100%	1560	0.186
VA.		3.00	14		20		220	100%	1300	0.144	250	100%	1500	0.100
Tonkin Str	eet NB													
4A	В	3.00	Υ	N	13		145	100%	1370	0.106	130	100%	1370	0.095
48	В	3.00	N	N	-		228		2055	0.111	225		2055	0.109
4C	В	3.00	N	N			229		2055	0.111	225		2055	0.109
4D	В	3.00	N	N			228		2055	0.111	225		2055	0.109
Tonkin Str	et SB													
5A	B,C	3.50	Y	N	15		100	100%	715	0.140	95	100%	715	0.133
5B	B,C	3.50	N	N	18		294	7%	2095	0.140	275	20%	2070	0.133
5C	B,C	3.50	N	N			296	1.00	2105	0.141	280	2070	2105	0.133
6A	C	3.50	N	N	25	-	165	100%	1985	0.083	165	100%	1985	0.083
7p	A		5GM +	9FG =	14	sec								
8p	A,D,E		7GM +	13FG =	20	sec		+						
9p	C		5GM +	9FG =	14	sec		+						
10p	A,B,C		5GM +	10FG =	15	sec								
11p	D		5GM +	9FG =	14	sec		1						
12p	D		6GM+	11FG =	17	sec								
13p	B,C,D		6GM+	11FG =	17	sec		1						
iop	0,0,0		OOM 2	1110=		960								

Notes:	AM Peak	3+4+6+1	PM Peak	3+4+6+1
	Sum of Critical y Y	0.611	Sum of Critical y Y	0.610
	Lost Time L (sec)	24	Lost Time L (sec)	24
	Cycle Time c (sec)	136	Cycle Time c (sec)	136
	Practical Y Ypr	0.741	Practical Y Ypr	0.741
	Reserve Capacity RC	21%	Reserve Capacity RC	21%

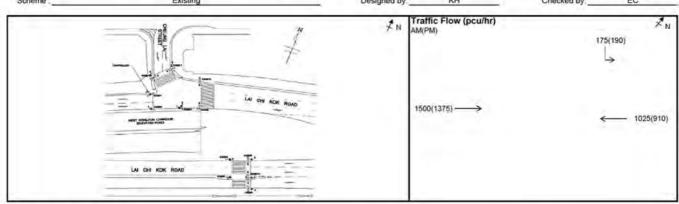
3+4+6+1

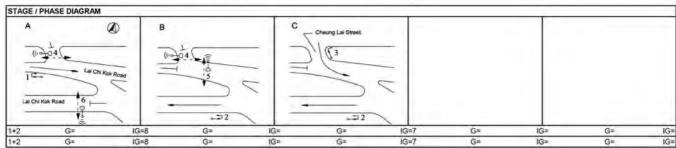
JOB NO. : 5190641 J8 -Cheung Sha Wan Road / Tonkin Street 2037 Scheme: 2037 Design Designed by Checked by:_ Traffic Flow (pcu/hr) 165(165) 595(520) 120(150) 225(290) 985(1045) 305(335) 1475(1225) 145(130) 685(675) STAGE / PHASE DIAGRAM 30 9 M one she han Ro 10, 8 8 . 8 3 25 25 4 13 13 13

Capacity Calculations Phase Stage Lane Nearside Opposed Radius for Gradient							AM I	Peak			PM	Peak		
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Cheung Sh	a Wan Road	EB												-
1A	D,E	3.50	Y	N	13	-	515	38%	1880	0.274	437	46%	1865	0.234
18	D,E	3.50	N	N			578		2105	0.275	494	7 %	2105	0.235
1C	D,E	3.50	N	N			577		2105	0.274	494		2105	0.235
Chauna Sh	a Wan Road	WP												
2A	A,E	3.00	Y	N	18		392	78%	1795	0.218	419	80%	1790	0.234
2B	A,E	3.00	N	N	10		449	1070	2055	0.218	481	0070	2055	0.234
2C	A,E	3.00	N	N		-	449	1	2055	0.218	480		2055	0.234
3A	A	3.00	N	N	28		225	100%	1560	0.144	290	100%	1560	0.186
- CORRES AND														
Tonkin Stre		0.00	Y		- 10		445	10001	1070	0.400	400	40004	4070	0.000
4A	В	3.00		N	13		145	100%	1370	0.106	130	100%	1370	0.095
4B	В	3.00	N	N			228	-	2055	0.111	225		2055	0.109
4C	В	3.00	N	N			229	_	2055	0.111	225	_	2055	0.109
4D	В	3.00	N	N			228		2055	0.111	225		2055	0.109
Tonkin Stre	et SB													
5A	B,C	3.50	Y	N	15	-	104	100%	715	0.145	98	100%	715	0.137
5B	B,C	3.50	N	N	18		305	5%	2095	0.146	284	18%	2070	0.137
5C	B,C	3.50	N	N			306		2105	0.145	288		2105	0.137
6A	С	3.50	N	N	25	-	165	100%	1985	0.083	165	100%	1985	0.083
7p	A		5GM +	9FG =	14	sec								
8p	A,D,E		7GM +	13FG =	20	sec								
9p	C		5GM +	9FG =	14	sec								
10p	A,B,C		5GM +	10FG =	15	sec								
11p	D		5GM +	9FG=	14	sec								
12p	D	- 7	6GM +	11FG =	17	sec								
13p	B,C,D		6GM +	11FG =	17	sec								

Notes:	AM Peak	3+4+6+1	PM Peak	3+4+6+1
	Sum of Critical y Y	0.613	Sum of Critical y Y	0.613
	Lost Time L (sec)	24	Lost Time L (sec)	24
	Cycle Time c (sec)	136	Cycle Time c (sec)	136
	Practical Y Ypr	0.741	Practical Y Ypr	0.741
	Reserve Capacity RC	21%	Reserve Capacity RC	21%

			JOB N	10.:519	90641
Junction :	J9 - Lai Chi Kok Road / Cheung Lai Street		Design Year:	2021	
Scheme	Existing	Designed by:	КН	Checked by:	EC
	W 38	₹N Tra	affic Flow (pcu/hr)		₹N

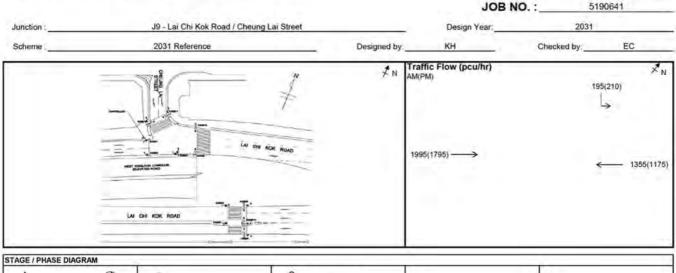




Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB		3.55	1		-	42		AP					-
1A	Α	3.60	Y	N			724		1975	0.367	664		1975	0.336
18	А	3.60	N	N			776		2115	0.367	711		2115	0.336
ai Chi Kok	Post WP							1						
2A	B,C	4.50	Y	N			125	+	2065	0.061	195		2065	0.094
2B	B,C	3.50	N	N			513	1 -	2105	0.244	455	_	2105	0.216
2C	B,C	3.50	N	N			512		2105	0.243	455		2105	0.216
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		87	100%	1070	0.081	94	100%	1070	880.0
3B	С	3.50	Y	N	18		88	100%	1085	0.081	96	100%	1085	0.088
4p	A,B		10GM +	11FG =	21	sec								
5p	В		11GM +	12FG =	23	sec		1						
6р	A		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.611	Sum of Critical y Y	0.552
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	32%	Reserve Capacity RC	47%

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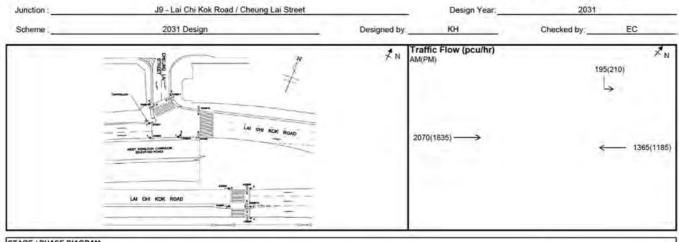


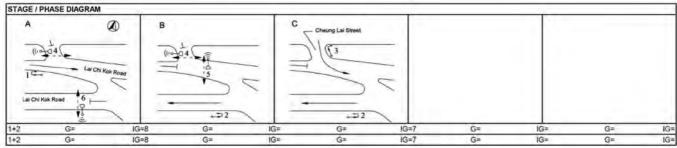
((in)	Lai Chi Kok	Road	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		122					
1+2	G=	IG=8	G=	IG=	G=	IG=7	G=	IG=	G=	IG:
1+2	G=	IG=8	G=	IG=	G=	IG=7	G=	IG=	G=	IĞ:
Capacit	y Calculations					AM Peak		Р	M Peak	
Phase	Stage t	ane Nearsid	e Opposed Ra	adius for Gradier	nt Design F	Proportion Saturation	n Flow	Design Proporti	on Saturation	Flow

Capacity	Calculati	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in % g	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
ai Chi Kok	Road EB											-		
1A	Α	3.60	Y	N			963		1975	0.488	867		1975	0.439
18	A	3.60	N	N			1032		2115	0.488	928		2115	0.439
ai Chi Kok	Road WB												-	
2A	B,C	4.50	Y	N			140		2065	0.068	220		2065	0.107
2B	B,C	3.50	N	N			678		2105	0.322	588		2105	0.279
2C	B,C	3.50	N	N			677		2105	0,322	587		2105	0.279
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		97	100%	1070	0.091	104	100%	1070	0.097
3B	С	3.50	Y	N	18		98	100%	1085	0.090	106	100%	1085	0.098
4p	A,B		10GM +	11FG=	21	sec								
5p	В		11GM+	12FG =	23	sec						-		
6р	А		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.810	Sum of Critical y Y	0.718
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	-1%	Reserve Capacity RC	13%

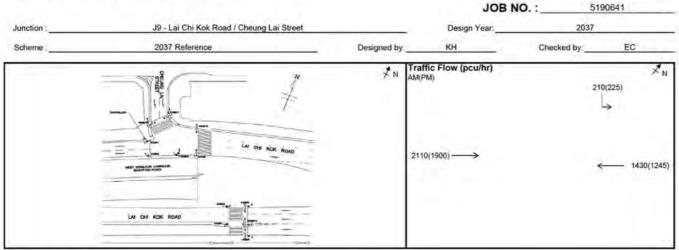
JOB NO. : 5190641

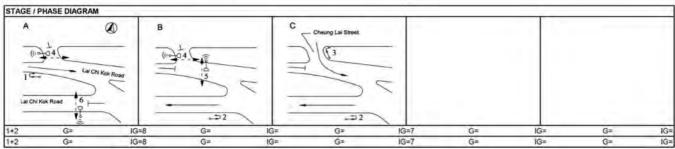




Capacity	Calculat	ions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB											-		
1A	Α	3.60	Y	N			1000		1975	0,506	886		1975	0.449
18	А	3.60	N	N			1070		2115	0.506	949		2115	0.449
ai Chi Kok	Road WB											-	4	
2A	B,C	4.50	Y	N			140		2065	0.068	220		2065	0.107
2B	B,C	3.50	N	N			683		2105	0.324	593		2105	0.282
2C	B,C	3.50	N	N			682		2105	0.324	592		2105	0.281
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		97	100%	1070	0.091	104	100%	1070	0.097
3B	C	3.50	Y	N	18		98	100%	1085	0.090	106	100%	1085	0.098
4p	A,B		10GM +	11FG =	21	sec								
5p	В		11GM+	12FG =	23	sec								
6р	A		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.831	Sum of Critical y Y	0.730
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	-3%	Reserve Capacity RC	11%





Capacity	Calculat	ions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in % g	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
ai Chi Kok	Road EB											-		
1A	Α	3.60	Y	N			1019		1975	0.516	917		1975	0.464
18	A	3.60	N	N			1091		2115	0.516	983		2115	0.465
ai Chi Kok	Road WB													
2A	B,C	4.50	Y	N			150		2065	0.073	230		2065	0.111
2B	B,C	3.50	N	N			715		2105	0.340	623		2105	0.296
2C	B,C	3.50	N	N			715		2105	0.340	622		2105	0.295
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		104	100%	1070	0.097	112	100%	1070	0.105
3B	С	3.50	Y	N	18		106	100%	1085	0.098	113	100%	1085	0.104
4p	A,B		10GM +	11FG=	21	sec								
5p	В		11GM+	12FG =	23	sec						-		
6р	A		11GM +	13FG =	24	sec								
						-								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.856	Sum of Critical y Y	0.761
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	-6%	Reserve Capacity RC	6%

Lai Chi Kek Road

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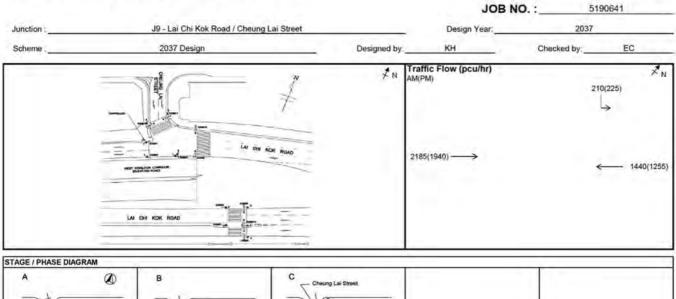
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Lai Chi Kok Road

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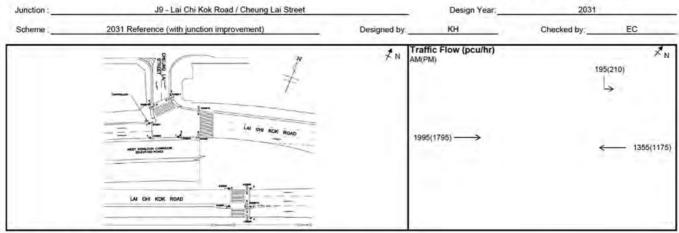
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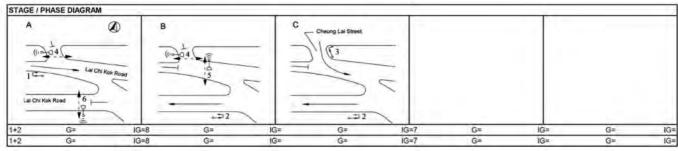
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Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kok	Road EB		1	1			4		100		- U			
1A	Α	3.60	Y	N			1055		1975	0.534	937		1975	0.474
18	A	3.60	N	N			1130		2115	0.534	1003		2115	0.474
Lai Chi Kok	Road WB											-		
2A	B,C	4.50	Y	N			150		2065	0.073	230		2065	0.111
2B	B,C	3.50	N	N			720		2105	0.342	628		2105	0.298
2C	B,C	3.50	N	N			720		2105	0.342	627		2105	0.298
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		104	100%	1070	0.097	112	100%	1070	0.105
3B	С	3.50	Y	N	18		106	100%	1085	0.098	113	100%	1085	0.104
4p	A,B		10GM +	11FG =	21	sec								
5p	В		11GM+	12FG =	23	sec								
6р	A		11GM+	13FG =	24	sec								
						1								
						1								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.876	Sum of Critical y Y	0.773
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	-8%	Reserve Capacity RC	5%

JOB NO. : 5190641





Capacity	Calculati	ons				-		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB											-		
1A	Α	3.30	Y	N			542		1555	0.349	487		1555	0.313
18	A	3.30	N	N			727		2085	0.349	654		2085	0.314
1C	Α	3.30	N	N			726		2085	0.348	654		2085	0.314
ai Chi Kok	Road WB													
2A	B,C	4.50	Y	N			150		2065	0.073	230		2065	0.111
2B	B,C	3.50	N	N			678		2105	0.322	588		2105	0.279
2C	B,C	3.50	N	N			677		2105	0.322	587		2105	0.279
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		97	100%	895	0.108	104	100%	895	0.116
3B	С	3.50	Y	N	18		98	100%	905	0.108	106	100%	905	0.117
	4.0		10GM +	11FG =	24									
4p	A,B	_			21	sec	_	-				-		
5p	В		11GM+	12FG =	23	sec	_	-				_		
6р	A		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.671	Sum of Critical y Y	0.593
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	20%	Reserve Capacity RC	37%

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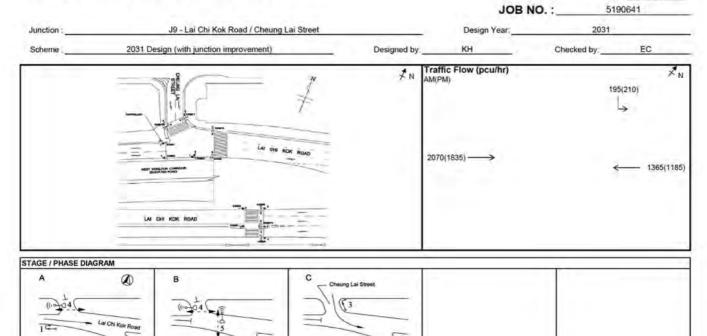
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Lai Chi Kok Road

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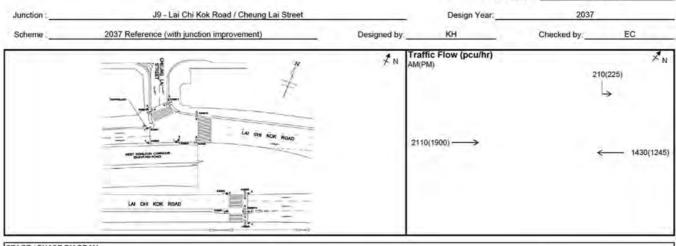
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Capacity	Calculat	ions						AM	Peak		PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
Lai Chi Kok	Road EB		44	49		- 3	(Breeze, m)		April 107		(pace) = 1		(peering)	-	
1A	A	3.30	Y	N			562		1555	0.361	498		1555	0.320	
18	A	3.30	N	N			754	1	2085	0.362	669		2085	0.321	
1C	Α	3.30	N	N			754		2085	0.362	668		2085	0.320	
ai Chi Kok	Road WB							-							
2A	B,C	4.50	Y	N			150	1	2065	0.073	230		2065	0.111	
2B	B,C	3.50	N	N			683		2105	0.324	593		2105	0.282	
2C	B,C	3.50	N	N			682		2105	0.324	592		2105	0.281	
Cheung La	Street SB														
3A	C	3.50	Y	N	15		97	100%	895	0.108	104	100%	895	0.116	
3B	C	3.50	Y	N	18	-	98	100%	905	0.108	106	100%	905	0.117	
		0.50		,-				10070		0.130		10010	945	3.17	
4p	A,B		10GM +	11FG =	21	sec									
5p	В		11GM+	12FG =	23	sec						-			
6р	A		11GM+	13FG =	24	sec									

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.686	Sum of Critical y Y	0.603
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	17%	Reserve Capacity RC	34%

JOB NO. : 5190641



((co	Lai Cru j	(i) (ii) Road	201		Cheung Lai Street					
	=			1						
+2	G=	IG=8	G=	IG=	G=	IG=7	G=	IG=	G=	IG=

Capacity	Calculati	ions				- 4		AM I	Peak			PM	/ Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB											-		
1A	A	3.30	Y	N		-	573		1555	0.368	516	-	1555	0.332
18	A	3.30	N	N			769		2085	0.369	692		2085	0.332
1C	Α	3.30	N	N			768		2085	0.368	692		2085	0.332
ai Chi Kok	Road WB													
2A	B,C	4.50	Y	N			150		2065	0.073	230		2065	0.111
2B	B,C	3.50	N	N			715		2105	0.340	623		2105	0.296
2C	B,C	3.50	N	N			715		2105	0.340	622		2105	0.295
Cheung Lai	Street SB													
3A	С	3.50	Y	N	15		104	100%	895	0.116	112	100%	895	0.125
3B	С	3.50	Y	N	18		106	100%	905	0.117	113	100%	905	0.125
	4.0		40011	11FG =	24									
4p	A,B B		10GM + 11GM +	11FG =	21	sec	_	-				-		
5p					23	sec	_	1		_		-		
6р	A		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.708	Sum of Critical y Y	0.628
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	14%	Reserve Capacity RC	29%

₩2

IG=

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IG=8

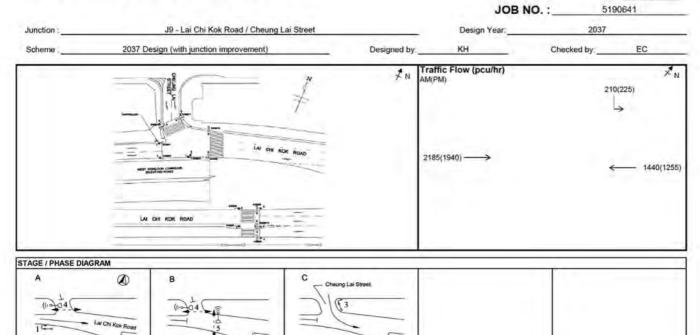
Lai Chi Kok Road

G=

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IG=



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IG=7

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Capacity	Calculati	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB													
1A	Α	3.30	Y	N			593		1555	0.381	527		1555	0.339
18	A	3.30	N	N			796		2085	0.382	707		2085	0.339
1C	A	3.30	N	N			796		2085	0.382	706		2085	0.339
ai Chi Kok	Road WB							-				1		
2A	B,C	4.50	Y	N			150		2065	0.073	230		2065	0.111
2B	B,C	3.50	N	N			720		2105	0.342	628		2105	0.298
2C	B,C	3.50	N	N			720		2105	0.342	627		2105	0.298
Cheung Lai	Street SB													
3A	C	3.50	Y	N	15		104	100%	895	0.116	112	100%	895	0.125
3B	С	3.50	Y	N	18		106	100%	905	0.117	113	100%	905	0.125
4p	A,B		10GM +	11FG =	21	sec						_		
5p	В		11GM+	12FG =	23	sec		1			_			
6р	A		11GM+	13FG =	24	sec								

Notes:	AM Peak	1+2	PM Peak	1+2
	Sum of Critical y Y	0.724	Sum of Critical y Y	0.637
	Lost Time L (sec)	13	Lost Time L (sec)	13
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.806	Practical Y Ypr	0.810
	Reserve Capacity RC	11%	Reserve Capacity RC	27%

1+11p+3

1+4+3

IG=

G=

IG=12

IG=12

G=

Capacity	Calculati	ions						AM I	Peak		PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
ai Chi Kok	Road EB		44	Ling		- 3	Ap. sec. my		Apriletoy	-	(pac)		4	-	
1A	A	3.60	N	N			482		2115	0.228	445		2115	0.210	
18	A	3,60	N	N	10		423	93%	1855	0.228	395	85%	1875	0.21	
ai Chi Kok	Road EB														
2A	Α	3.30	Y	N	10		168	100%	1690	0.099	157	100%	1690	0.093	
28	Α	3.30	N	N	13		186	98%	1865	0.100	180	63%	1940	0.093	
2C	Α	3.30	N	N			208		2085	0.100	194		2085	0.09	
2D	Α	3.30	N	N			208		2085	0.100	194		2085	0.093	
ai Chi Kok	Road WB														
3A	С	3.40	Y	N			249		1955	0.127	239		1955	0.12	
38	С	3.40	N	N			266		2095	0.127	256		2095	0.12	
3C	C	3.40	N	N	23		369	100%	1965	0.188	346	100%	1965	0.17	
3D	С	3.40	N	N	20		366	100%	1950	0.188	344	100%	1950	0.17	
3E	С	3.50	Y	N	18		182	5%	1955	0.093	175	9%	1950	0.09	
3F	С	3.50	N	N			196		2105	0.093	188		2105	0.08	
3G	С	3.50	N	N			137		1475	0.093	132		1475	0.08	
ung Chau		17.													
4A	В	3.80	Y	N	30		120	100%	1900	0.063	140	100%	1900	0.074	
4B	В	3.80	N	N	35		130	100%	2045	0.064	150	100%	2045	0.073	
5p	B,C		6GM +	12FG =	18	sec				- 5					
6р	A,B		5GM +	9FG =	14	sec									
7p	B,C		5GM +	8FG =	13	sec									
8p	A,C		5GM +	9FG =	14	sec									
9p	A,B		6GM +	11FG =	17	sec									
10p	B,C		5GM +	9FG =	14	sec									
11p	В		5GM +	10FG =	15	sec									
12p	A,B		5GM +	6FG =	- 11	sec									

Notes:	AM Peak	1+11p+3	PM Peak	1+4+3
	Sum of Critical y Y	0.416	Sum of Critical y Y	0.461
	Lost Time L (sec)	35	Lost Time L (sec)	19
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.646	Practical Y Ypr	0.768
	Reserve Capacity RC	55%	Reserve Capacity RC	67%

1+11p+3

1+4+3

IG=

G=

JOB NO. : 5190641 J10 - Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street 2031 Scheme . 2031 Reference Designed by: Checked by:___ Traffic Flow (pcu/hr) AM(PM) ×_N 490(345) 875(810) 635(575) 10(15) 480(520) 700(680) ¥ 520(465) ← 340(360) STAGE / PHASE DIAGRAM 20) 7 (T3

IG=12

IG=12

G=

apacity Calculations						AM Peak				PM Peak				
Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
Road EB		3	17			- de-		in the second		- de-				
Α	3.60	N	N			649		2115	0.307	607		2115	0.287	
A	3,60	N	N	10		571	91%	1860	0.307	538	86%	1870	0.288	
Road EB														
A	3.30	Y	N	10		233	100%	1690	0.138	188	100%	1690	0.111	
Α	3.30	N	N	13		257	100%	1860	0.138	213	74%	1915	0.111	
Α	3.30	N	N			240		2085	0.115	232		2085	0.11	
Α	3.30	N	N			240		2085	0.115	232		2085	0.11	
Road WB														
С	3.40	Y	N			311	1	1955	0.159	285		1955	0.146	
С	3.40	N	N			334		2095	0.159	305		2095	0.14	
С	3.40	N	N	23		439	100%	1965	0.223	407	100%	1965	0.20	
С	3.40	N	N	20		436	100%	1950	0.224	403	100%	1950	0.20	
С	3.50	Y	N	18		228	4%	1960	0.116	208	7%	1955	0.10	
С	3.50	N	N			245		2105	0.116	225		2105	0.10	
С	3.50	N	N			172		1475	0.117	157		1475	0.10	
	100													
													0.09	
В	3.80	N	N	35		176	100%	2045	0.086	187	100%	2045	0.091	
B,C		6GM +	12FG =	18	sec				- 3					
A,B		5GM +	9FG =	14	sec									
B,C		5GM +	8FG =	13	sec									
A,C		5GM +	9FG =	14	sec									
A,B		6GM +	11FG =	17	sec									
B,C		5GM +	9FG =	14	sec									
В		5GM +	10FG =	15	sec									
A,B		5GM +	6FG =	11	sec									
	Road EB A A A A A A A A A A B C C C C C C C C	Road EB A 3.60 A 3.60 A 3.60 Road EB A 3.30 A 3.30 A 3.30 A 3.30 A 3.30 C 3.40 C 3.40 C 3.40 C 3.50 C 3.60 B 3.80 B 3.80 B,C A,B B,C A,B B,C A,B B,C B,C B	Width (m) tane? (Y/N) Road EB A 3.60 N A 3.60 N A 3.30 N C 3.40 N C 3.40 N C 3.40 N C 3.40 N C 3.50 N C 3.50 N C 3.50 N C 3.50 N Street NB B 3.80 N B B 3.80 N B G G G G G G G G	Width (m) tane? (Y/N)	Width (m) lane? turn? turning (m) r	Width (m) tane? turn? turning (m) in % g	Width (m) tane? turn? turning (m) in % Flow q (pcu/hr) r g r r r r r r r r	Width (m) lane? turn? turning (m) n % Flow q (pcu/hr) f	Width (m) lane?	Width (m) tane? (Y/N) turning (m) in % flow q (pcu/hr) f flow S (pcu/hr) y	Nidth (m) lane? tum? tuming (m) n % Flow g (pcu/hr) f flow S factor flow g (pcu/hr) f flow g flow S factor flow g flow S factor flow g flow S factor flow g flow S flow S factor flow g flow S flow S flow S flow S flow S flow S flow G flow S flow S flow S flow G flow S flow S flow S flow G flow S flow S flow S flow S flow S flow S flow G flow S flow S flow S flow S flow S flow S flow G flow S flow S flow S flow S flow S flow S flow G flow S flow S flow S flow S flow S flow S flow G flow S flow S	Width (m) lane? turn? turning (m) r g (pculhr) f f (pculhr) f (pculhr)	Width (m) lane? turn? turning (m) n % Flow q (pculhr) f (pculhr	

Notes:	AM Peak	1+11p+3	PM Peak	1+4+3
	Sum of Critical y Y	0.531	Sum of Critical y Y	0.586
	Lost Time L (sec)	35	Lost Time L (sec)	19
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.646	Practical Y Ypr	0.768
	Reserve Capacity RC	22%	Reserve Capacity RC	31%

1+11p+3

1+4+3

IG=

G=

JOB NO. : 5190641 J10 - Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street 2031 Scheme 2031 Design Designed by: Checked by: Traffic Flow (pcu/hr) AM(PM) × N 490(345) 555(560) 700(680) 520(465) 875(810) 635(575) 10(15) 350(370) STAGE / PHASE DIAGRAM 20) (0 70 (53

IG=12

IG=12

G=

Capacity	Calculat	ions				-		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB													
1A	Α	3.60	N	N			649		2115	0.307	607		2115	0.287
18	Α	3.60	N	N	10		571	91%	1860	0.307	538	86%	1870	0.288
ai Chi Kok	Road EB													=
2A	A	3.30	Y	N	10		233	100%	1690	0.138	196	100%	1690	0.116
2B	Α	3.30	N	N	13		257	100%	1860	0.138	225	66%	1930	0.117
2C	Α	3.30	N	N			277		2085	0.133	242		2085	0.116
2D	A	3.30	N	N		-	278		2085	0.133	242		2085	0.116
Lai Chi Kok	Road WB													
3A	C	3.40	Y	N			311		1955	0.159	285		1955	0.146
3B	С	3.40	N	N			334		2095	0.159	305		2095	0.146
3C	C	3.40	N	N	23		439	100%	1965	0.223	407	100%	1965	0.207
3D	С	3.40	N	N	20		436	100%	1950	0.224	403	100%	1950	0.207
3E	C	3.50	Y	N	18		228	4%	1960	0.116	208	7%	1955	0.106
3F	С	3.50	N	N			245		2105	0.116	225		2105	0.107
3G	С	3.50	N	N			172		1475	0.117	157		1475	0.106
Tung Chau	Street NB					-		1 -						
4A	В	3.80	Y	N	30		169	100%	1900	0.089	178	100%	1900	0.094
4B	В	3.80	N	N	35		181	100%	2045	0.089	192	100%	2045	0.094
5p	B,C		6GM +	12FG =	18	sec								
6р-	A,B		5GM +	9FG =	14	sec								
7p	B,C		5GM +	8FG =	13	sec								
8p	A,C		5GM +	9FG =	14	sec								
9p	A,B		6GM +	11FG =	17	sec								
10p	B,C		5GM +	9FG =	14	sec								
11p	В		5GM +	10FG =	15	sec								
12p	A,B		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+11p+3	PM Peak	1+4+3
	Sum of Critical y Y	0.531	Sum of Critical y Y	0.589
	Lost Time L (sec)	35	Lost Time L (sec)	19
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.646	Practical Y Ypr	0.768
	Reserve Capacity RC	22%	Reserve Capacity RC	31%

1+11p+3

1+4+3

IG=

G=

JOB NO. : 5190641 J10 - Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street 2037 Scheme . 2037 Reference Designed by: Checked by:___ Traffic Flow (pcu/hr) AM(PM) ₹_N 515(365)_ 930(860) 670(610) 10(20) 510(550) 740(715) ¥ 550(490) ← 360(380) STAGE / PHASE DIAGRAM 20) (0 70 (53

IG=12

IG=12

G=

Capacity	Calculat	ions						AM I	Peak		PM Peak			
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB						-							
1A	Α	3.60	N	N		-	686		2115	0.324	639		2115	0.302
18	A	3,60	N	N	10		604	91%	1860	0.325	566	87%	1870	0.303
ai Chi Kok	Road EB										_			
2A	A	3.30	Y	N	10		245	100%	1690	0.145	199	100%	1690	0.118
2B	A	3.30	N	N	13		270	100%	1860	0.145	226	73%	1915	0.118
2C	A	3.30	N	N			255		2085	0.122	245		2085	0.118
2D	A	3.30	N	N			255		2085	0.122	245		2085	0.118
ai Chi Kok	Road WB													
3A	C	3.40	Y	N			328		1955	0.168	304		1955	0.155
38	C	3.40	N	N			352		2095	0.168	326		2095	0.156
3C	C	3.40	N	N	23		467	100%	1965	0.238	432	100%	1965	0.220
3D	С	3.40	N	N	20		463	100%	1950	0.237	428	100%	1950	0.219
3E	C	3.50	Y	N	18		240	4%	1960	0.122	222	9%	1950	0.114
3F	С	3.50	N	N			259		2105	0.123	240		2105	0.114
3G	С	3.50	N	N			181		1475	0.123	168		1475	0.114
Tung Chau	Street NB					-								
4A	В	3.80	Y	N	30		173	100%	1900	0.091	183	100%	1900	0.096
48	В	3.80	N	N	35		187	100%	2045	0.091	197	100%	2045	0.096
5p	B,C		6GM +	12FG =	18	sec								
6р	A,B		5GM +	9FG =	14	sec								
7p	B,C		5GM +	8FG =	13	sec								
8p	A,C		5GM +	9FG =	14	sec								
9р	A,B		6GM +	11FG =	17	sec								
10p	B,C		5GM +	9FG =	14	sec								
11p	В		5GM +	10FG =	15	sec								
12p	A,B		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+11p+3	PM Peak	1+4+3
	Sum of Critical y Y	0.562	Sum of Critical y Y	0.619
	Lost Time L (sec)	35	Lost Time L (sec)	19
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.646	Practical Y Ypr	0.768
	Reserve Capacity RC	15%	Reserve Capacity RC	24%

1+11p+3

1+4+3

IG=

G=

JOB NO. : 5190641 J10 - Lai Chi Kok Road / Tung Chau Street / Tai Nan West Street 2037 Scheme 2037 Design Designed by: Checked by:___ Traffic Flow (pcu/hr) AM(PM) × N 585(590) 740(715) 550(490) 930(860) 670(610) 10(20) 370(390) STAGE / PHASE DIAGRAM 20) (0 70 (53

IG=12

IG=12

G=

Capacity	Calculat	ions				- 4		AM I	Peak		PM Peak			
Phase	Stage	Lane Width (m)	Nearside tane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
ai Chi Kok	Road EB													
1A	A	3.60	N	N			686		2115	0.324	639		2115	0.302
18	A	3.60	N	N	10		604	91%	1860	0.325	566	87%	1870	0.303
ai Chi Kok	Road ER												-	
2A	A	3.30	Y	N	10		245	100%	1690	0.145	207	100%	1690	0.122
2B	A	3.30	N	N	13		270	100%	1860	0.145	237	67%	1930	0.123
2C	A	3.30	N	N			292	100,0	2085	0.140	255	51.14	2085	0.122
2D	Α	3.30	N	N			293		2085	0.141	256		2085	0.123
ai Chi Kok	Road WB													
3A	С	3.40	Y	N	1		328	1	1955	0.168	304		1955	0.155
38	С	3.40	N	N			352	1	2095	0.168	326		2095	0.156
3C	С	3.40	N	N	23		467	100%	1965	0.238	432	100%	1965	0.220
3D	С	3.40	N	N	20		463	100%	1950	0.237	428	100%	1950	0.219
3E	С	3.50	Y	N	18		240	4%	1960	0.122	222	9%	1950	0.114
3F	С	3.50	N	N			259		2105	0.123	240		2105	0.114
3G	С	3.50	N	N			181		1475	0.123	168		1475	0.114
ung Chau	Street NB													
4A	В	3.80	Y	N	30		178	100%	1900	0.094	188	100%	1900	0.099
4B	В	3.80	N	N	35		192	100%	2045	0.094	202	100%	2045	0.099
5p	B,C		6GM +	12FG =	18	sec								
6р	A,B		5GM +	9FG =	14	sec								
7p	B,C		5GM +	8FG =	13	sec								
8p	A,C		5GM +	9FG =	14	sec								
9p	A,B		6GM +	11FG =	17	sec								
10p	B,C		5GM +	9FG =	14	sec								
11p	В		5GM +	10FG =	15	sec								
12p	A,B		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+11p+3	PM Peak	1+4+3
rs:	Sum of Critical y Y	0.562	Sum of Critical y Y	0.621
	Lost Time L (sec)	35	Lost Time L (sec)	19
	Cycle Time c (sec)	124	Cycle Time c (sec)	130
	Practical Y Ypr	0.646	Practical Y Ypr	0.768
	Reserve Capacity RC	15%	Reserve Capacity RC	24%

ATKINS

							JO	B NO. :		5190641	
Junction :		J11 - La	i Chi Kok Road / H	ling Wah Street		-	Design Year;		202	1	
Scheme		Exi	sting		Designed	oy:	КН		Checked by:_		EC
	4.41	94 ROG 2	† 		1,	N Tra	ffic Flow (pcu/hr) PM)	235(290)	450(445)	50(85)	×
	/						175(185)			←	770(680) 105(110)
17	1	A sept of the sept					245(215)	↑ 55(45)	60(80)		
A 1	ASE DIAGRAM	B - 1 0 1	07 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	dy dy	0 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3 0 0	pt-			
1+7p+2+3	G=	IG=9	G=10	IG=12	G=	IG=8	G=	10	S=7	G=	IG
1+7p+2+3	G=	IG=9	G=10	IG=12	G=	IG=8	G=	10	3=7	G=	1G

Capacity	Calculat	ions				- 4	AM Peak				PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
Lai Chi Kol	Road EB						-								
1A	A	3.30	Y	N	10	-	175	100%	1690	0.104	185	100%	1690	0.109	
18	A	3.30	N	N			123		2085	0.059	135		2085	0.065	
1C	Α	3.30	N	N			122		2085	0.059	135		2085	0.065	
Lai Chi Kol	Road WB														
1D	A	3.40	Y	N	15		271	39%	1880	0.144	244	45%	1870	0.130	
1E	A	3.40	N	N	1,5		302	50,0	2095	0.144	273	10,0	2095	0.130	
1F	Α	3.40	N	N			302		2095	0.144	273		2095	0.130	
Hing Wah S	Street SB														
2A	С	3.30	Y	N	15		500	10%	1925	0.260	530	16%	1915	0.277	
28	C	3.30	N	N	28		235	100%	1975	0.119	290	100%	1975	0.147	
Hing Wah S	Street NB														
3A	D	3.20	Υ	N	10		108	100%	840	0.129	102	100%	840	0.121	
3B	D	3.20	N	N	17.5/22.5		252	54% / 24%	1955	0.129	238	47% / 34%	1950	0.122	
4p	В		8GM+	7FG =	15	sec									
5p	В		7GM +	7FG =	14	sec		1							
6p	B,C,D		9GM +	9FG =	18	sec									
7p	В.		10GM +	10FG =	20	sec									

lotes:	AM Peak	1+7p+2+3	PM Peak	1+7p+2+3
	Sum of Critical y Y	0.533	Sum of Critical y Y	0.529
	Lost Time L (sec)	43	Lost Time L (sec)	43
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.598	Practical Y Ypr	0.602
	Reserve Capacity RC	12%	Reserve Capacity RC	14%

1+7p+2+3

1+7p+2+3

G=

IG=9

G=10

IG=12

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2031 Scheme . 2031 Reference Designed by: Checked by:_ Traffic Flow (pcu/hr) 280(335) 520(510) 85(115) 195(205) ______^ 970(830) 115(125) 275(240) 105(80) 65(90) STAGE / PHASE DIAGRAM IG=

G=

IG=8

Capacity	Calculat	ions				-		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kol	Road EB													
1A	A	3.30	Y	N	10	-	195	100%	1690	0.115	205	100%	1690	0.121
18	Α	3.30	N	N			143		2085	0.069	155		2085	0.074
1C	A	3.30	N	N			142		2085	0.068	155		2085	0.074
Lai Chi Kol	Road WB													
1D	A	3.40	Y	N	15		337	34%	1890	0.178	295	42%	1875	0.157
1E	A	3.40	N	N	19		374	54,0	2095	0.179	330	72.70	2095	0.158
1F	A	3.40	N	N			374		2095	0.179	330		2095	0.158
Hing Wah S	Street SB													
2A	С	3.30	Y	N	15		605	14%	1920	0.315	625	18%	1910	0.327
2B	C	3.30	N	N	28		280	100%	1975	0.142	335	100%	1975	0.170
Hing Wah S	Street NB													
3A	D	3.20	Υ	N	10		133	100%	840	0.158	123	100%	840	0.146
3B	D	3.20	N	N	17.5/22.5		312	46% / 21%	1970	0.158	287	41% / 31%	1965	0.146
4p	В		8GM+	7FG=	15	sec								
5p	В		7GM +	7FG =	14	sec								
6p	B,C,D		9GM +	9FG =	18	sec								
7p	В.		10GM +	10FG =	20	sec								
				10.0										

lotes:	AM Peak	1+7p+2+3	PM Peak	1+7p+2+3
	Sum of Critical y Y	0.652	Sum of Critical y Y	0.631
	Lost Time L (sec)	43	Lost Time L (sec)	43
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.598	Practical Y Ypr	0.602
	Reserve Capacity RC	-8%	Reserve Capacity RC	-5%

G=

IG=7

G=

1+7p+2+3

1+7p+2+3

G=

IG=9

G=10

IG=12

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2031 Scheme . 2031 Design Designed by: Checked by:_ Traffic Flow (pcu/hr) 280(335) 520(510) 85(115) 235(240) ______^ 970(830) 115(125) 275(240) 105(80) 65(90) STAGE / PHASE DIAGRAM

G=

IG=8

Capacity	Calculat	ions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kol	Road EB													
1A	A	3.30	Y	N	10		235	100%	1690	0.139	240	100%	1690	0.142
18	Α	3.30	N	N			150		2085	0.072	165		2085	0.079
1C	A	3.30	N	N			150		2085	0.072	165		2085	0.079
Lai Chi Kol	Road WB													
1D	A	3.40	Y	N	15		337	34%	1890	0.178	295	42%	1875	0.157
1E	A	3.40	N	N	1.5		374		2095	0.179	330		2095	0.158
1F	Α	3.40	N	N		-	374		2095	0.179	330		2095	0.158
Hing Wah S	Street SB													
2A	С	3.30	Y	N	15		605	14%	1920	0.315	625	18%	1910	0.327
2B	С	3.30	N	N	28		280	100%	1975	0.142	335	100%	1975	0.170
Hing Wah S	Street NB													
3A	D	3.20	Υ	N	10		133	100%	840	0.158	123	100%	840	0.146
3B	D	3.20	N	N	17.5/22.5		312	46% / 21%	1970	0.158	287	41% / 31%	1965	0.146
4p	В		8GM+	7FG =	15	sec								
5p	В		7GM +	7FG =	14	sec								
6р	B,C,D		9GM +	9FG =	18	sec								
7p	В.		10GM +	10FG =	20	sec								

lotes:	AM Peak	1+7p+2+3	PM Peak	1+7p+2+3
	Sum of Critical y Y	0.652	Sum of Critical y Y	0.631
	Lost Time L (sec)	43	Lost Time L (sec)	43
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.598	Practical Y Ypr	0.602
	Reserve Capacity RC	-8%	Reserve Capacity RC	-5%

G=

1+7p+2+3

1+7p+2+3

G=

IG=9

G=10

IG=12

ATKINS

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2037 Scheme . 2037 Reference Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(355) 555(545) 90(120) 210(220) ______^ 1030(880) 125(130) 290(255) 110(85) 70(95) STAGE / PHASE DIAGRAM

G=

IG=8

Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kol	Road EB													
1A	A	3.30	Y	N	10	-	210	100%	1690	0.124	220	100%	1690	0.130
18	A	3.30	N	N			150		2085	0.072	165		2085	0.079
1C	Α	3.30	N	N			150		2085	0.072	165		2085	0.079
l ai Chi Kol	Road WB													
1D	A	3.40	Y	N	15		359	35%	1890	0.190	312	42%	1875	0.166
1E	A	3.40	N	N	1,5		398	55.5	2095	0.190	349	72.7	2095	0.167
1F	Α	3.40	N	N			398		2095	0.190	349		2095	0.167
Hing Wah S	Street SB													
2A	С	3.30	Y	N	15		645	14%	1920	0.336	665	18%	1910	0.348
2B	C	3.30	N	N	28		300	100%	1975	0.152	355	100%	1975	0.180
Hing Wah S	Street NB													
3A	D	3.20	Υ	N	10		140	100%	840	0.167	130	100%	840	0.155
3B	D	3.20	N	N	17.5/22.5		330	45% / 21%	1970	0.168	305	41% / 31%	1965	0.155
4p	В		8GM+	7FG =	15	sec								
5p	В		7GM +	7FG =	14	sec		1						
6p	B,C,D		9GM +	9FG =	18	sec								
7p	В.		10GM +	10FG =	20	sec								

lotes:	AM Peak	1+7p+2+3	PM Peak	1+7p+2+3
	Sum of Critical y Y	0.693	Sum of Critical y Y	0.670
	Lost Time L (sec)	43	Lost Time L (sec)	43
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.598	Practical Y Ypr	0.602
	Reserve Capacity RC	-14%	Reserve Capacity RC	-10%

G=

1+7p+2+3

1+7p+2+3

G=

IG=9

G=10

IG=12

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2037 Scheme . 2037 Design Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(355) 555(545) 90(120) 250(255) _____^ 1030(880) 125(130) 290(255) 115(95) 70(95) STAGE / PHASE DIAGRAM IG=

G=

IG=8

Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kol	Road EB						-							
1A	A	3.30	Y	N	10		250	100%	1690	0.148	255	100%	1690	0.151
18	Α	3.30	N	N			158		2085	0.076	175		2085	0.084
1C	A	3.30	N	N			157		2085	0.075	175		2085	0.084
Lai Chi Kol	Road WB													
1D	A	3.40	Y	N	15		359	35%	1890	0.190	312	42%	1875	0.166
1E	A	3.40	N	N	10		398	5070	2095	0.190	349	4270	2095	0.167
1F	A	3.40	N	N			398		2095	0.190	349		2095	0.167
Hing Wah S	Street SB													
2A	С	3.30	Y	N	15		645	14%	1920	0.336	665	18%	1910	0.348
28	C	3.30	N	N	28		300	100%	1975	0.152	355	100%	1975	0.180
Hing Wah S	Street NB													
3A	D	3.20	Υ	N	10		142	100%	840	0.169	133	100%	840	0.158
3B	D	3.20	N	N	17.5/22.5		333	44% / 21%	1970	0.169	312	39% / 30%	1970	0.158
4p	В		8GM+	7FG =	15	sec								
5p	В		7GM +	7FG =	14	sec								
6p	B,C,D		9GM +	9FG =	18	sec		1						
7p	В.С.О		10GM +	10FG =	20	sec		1						
			TOOM	101 0	20	300								

lotes:	AM Peak	1+7p+2+3	PM Peak	1+7p+2+3
	Sum of Critical y Y	0.695	Sum of Critical y Y	0.673
	Lost Time L (sec)	43	Lost Time L (sec)	43
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.598	Practical Y Ypr	0.602
	Reserve Capacity RC	-14%	Reserve Capacity RC	-11%

G=

IG=7

G=

1+7p+2

1+7p+2

G=

IG=9

G=10

G=10

IG=12

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2031 Scheme . 2031 Reference (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) 280(335) 520(510) 85(115) 195(205) ______^ 970(830) 115(125) 275(240) 105(80) 65(90) STAGE / PHASE DIAGRAM

G=

IG=

Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kol	Road EB													
1A	A	3.30	Y	N	10		195	100%	1690	0.115	205	100%	1690	0.121
18	Α	3.30	N	N			143		2085	0.069	155		2085	0.074
1C	A	3.30	N	N			142		2085	0.068	155		2085	0.074
Lai Chi Kol	Road WB													
1D	A	3.40	Y	N	15		337	34%	1890	0.178	295	42%	1875	0.157
1E	A	3.40	N	N	19		374		2095	0.179	330	12.14	2095	0.158
1F	A	3.40	N	N			374		2095	0.179	330		2095	0.158
Hing Wah S	Street SB													
2A	C,D	3.30	Y	N	15		605	14%	1920	0.315	625	18%	1910	0.327
8A	D	3.30	N	N	28		280	100%	1975	0.142	335	100%	1975	0.170
Hing Wah S	Street NB													
3A	C	3.20	Υ	N	10		203	100%	1685	0.120	187	100%	1685	0.111
3B	С	3.20	N	N	13		242	30%	2005	0.121	223	24%	2015	0.111
40	В		8GM+	7FG =	15	en è								
4p 5p	В		7GM +	7FG =	14	sec								
6p	B,C,D		9GM +	9FG =	18	sec								
7p	В.С.О		10GM +	10FG =	20	sec		1						
			TOOM	101 0	20	300								

lotes:	AM Peak	1+7p+2	PM Peak	1+7p+2
	Sum of Critical y Y	0.494	Sum of Critical y Y	0.485
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	31%	Reserve Capacity RC	34%

G=

1+7p+2

1+7p+2

G=

IG=9

G=10

G=10

IG=12

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2031 Scheme . 2031 Design (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) 280(335) 520(510) 85(115) 235(240) ______^ 970(830) 115(125) 275(240) 105(80) 65(90) STAGE / PHASE DIAGRAM

G=

IG=

Calculat	ions						AM	Peak			PM	Peak	
Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Road EB	-	1	1,9		- 3	(p.cc., o)		Apricay	-	(pac)		g-22.55	-
	3.30	Y	N	10		235	100%	1690	0.139	240	100%	1690	0.142
				- 10							13,617		0.079
Α	3.30	N	N			150		2085	0.072	165		2085	0.079
Road WB													
Α	3.40	Y	N	15		337	34%	1890	0.178	295	42%	1875	0.157
A	3.40	N	N			374		2095	0.179	330		2095	0.158
Α	3.40	N	N			374		2095	0.179	330		2095	0.158
treet SB													
C,D	3.30	Y	N	15		605	14%	1920	0.315	625	18%	1910	0.327
D	3.30	N	N	28		280	100%	1975	0.142	335	100%	1975	0.170
Street NB													
C	3.20	Y	N	10		203	100%	1685	0.120	187	100%	1685	0.111
С	3.20	N	N	13		242	30%	2005	0.121	223	24%	2015	0.111
R		8GM +	7FG =	15	SAC								
		1 1 2 2 3 3 1 1 1 1							_				
	Road EB A A A Road WB A A Ctreet SB C,D D	Width (m) w	Width (m) lane? (Y/N)	Width (m) lane? (Y/N) (Y/N)	Width (m) lane? tum? tuming (m) r	Width (m) lane? turn? turning (m) in % g	Width (m) tane? tum? tuming (m) in % Flow q (pcu/hr)	Width (m) lane? turm? turming (m) in % Flow q (pcu/hr) f	Width (m) lane? turning (m) in % Flow q (pcu/hr) flow S (pcu/hr) r g (pcu/hr) f f f (pcu/hr) f f f (pcu/hr) f f f (pcu/hr) f f f f f f f f f	Width (m) lane? turn? turning (m) r g Flow q (pcu/hr) f flow S factor y	Width (m) lane? turn? turning (m) in % Flow q (pcu/hr) f (pcu/hr) y (pcu/hr) y (pcu/hr) x (pcu/h	Width (m) tane? turning (m) in % Flow q (pculhr) f (pculhr) f	Width (m) lane? tum? tuming (m) r g (pculhr) f (

Notes:	AM Peak	1+7p+2	PM Peak	1+7p+2
	Sum of Critical y Y	0.494	Sum of Critical y Y	0.485
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	31%	Reserve Capacity RC	34%

G=

1+7p+2

1+7p+2

G=

IG=9

G=10

IG=12

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2037 Scheme . 2037 Reference (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(355) 555(545) 90(120) 210(220) ______^ 1030(880) 125(130) 290(255) 110(85) 70(95) STAGE / PHASE DIAGRAM

G=

IG=

Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Kok	Road EB													-
1A	A	3.30	Y	N	10		210	100%	1690	0.124	220	100%	1690	0.130
18	Α	3.30	N	N			150		2085	0.072	165		2085	0.079
1C	Α	3.30	N	N			150		2085	0.072	165		2085	0.079
Lai Chi Kok	Pood WR													
1D	A	3.40	Y	N	15		359	35%	1890	0.190	312	42%	1875	0.166
1E	A	3.40	N	N	10		398	3070	2095	0.190	349	4270	2095	0.167
1F	A	3.40	N	N			398		2095	0.190	349		2095	0.167
Hing Wah S	treet SB													
2A	C,D	3.30	Y	N	15		645	14%	1920	0.336	665	18%	1910	0.348
8A	D	3.30	N	N	28		300	100%	1975	0.152	355	100%	1975	0.180
Hing Wah S	Street NB													
3A	C	3.20	Υ	N	10		215	100%	1685	0.128	198	100%	1685	0.118
3B	С	3.20	N	N	13		255	29%	2005	0.127	237	24%	2015	0.118
			2011	750	46									
4p 5p	B B		8GM + 7GM +	7FG =	15	sec	_							
6p	B,C,D		9GM +	9FG =	18	sec								
7р	B,C,D		10GM +	10FG =	20	sec	-							
γp.			TOGNIT	101-01-	20	Sec								

Notes:	AM Peak	1+7p+2	PM Peak	1+7p+2
	Sum of Critical y Y	0.526	Sum of Critical y Y	0.515
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	23%	Reserve Capacity RC	26%

G=

1+7p+2

1+7p+2

G=

IG=9

G=10

G=10

IG=12

IG=

G=

JOB NO. : 5190641 J11 - Lai Chi Kok Road / Hing Wah Street 2037 Scheme . 2037 Design (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) 300(355) 555(545) 90(120) 250(255) _____^ 1030(880) 125(130) 290(255) 115(95) 70(95) STAGE / PHASE DIAGRAM

G=

IG=

Capacity	/ Calculat	ions				- 4		AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Lai Chi Ko	k Road EB	-	44	49		- 3	(2.00.10)		April 107		(panyay		(Fee.in)	
1A	A	3.30	Y	N	10		250	100%	1690	0.148	255	100%	1690	0.151
18	A	3.30	N	N	- 7.0		158		2085	0.076	175	12.0.1	2085	0.084
1C	A	3.30	N	N			157		2085	0.075	175		2085	0.084
Lai Chi Ko	k Road WB													
1D	A	3.40	Y	N	15		359	35%	1890	0.190	312	42%	1875	0.166
1E	A	3.40	N	N			398		2095	0.190	349		2095	0.167
1F	Α	3.40	N	N			398		2095	0.190	349		2095	0.167
Hing Wah	Street SB													
2A	C,D	3.30	Y	N	15		645	14%	1920	0.336	665	18%	1910	0.348
8A	D	3.30	N	N	28		300	100%	1975	0.152	355	100%	1975	0.180
Hing Wah	Street NB													
3A	C	3.20	Y	N	10		217	100%	1685	0.129	202	100%	1685	0.120
3B	С	3.20	N	N	13		258	28%	2005	0.129	243	22%	2020	0.120
4p	В		8GM+	7FG =	15	sec								
5p	В		7GM +	7FG =	14	sec								
6p	B,C,D		9GM +	9FG =	18	sec								
7p	B,0,0		10GM +	10FG =	20	sec				_				
.,-			100.0	10.0										

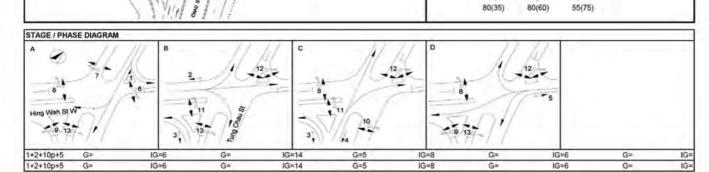
Notes:	AM Peak	1+7p+2	PM Peak	1+7p+2
	Sum of Critical y Y	0.526	Sum of Critical y Y	0.515
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	23%	Reserve Capacity RC	26%

G=

5(5) 365(335) 135(145)

> 165(225) ___ 340(285) —

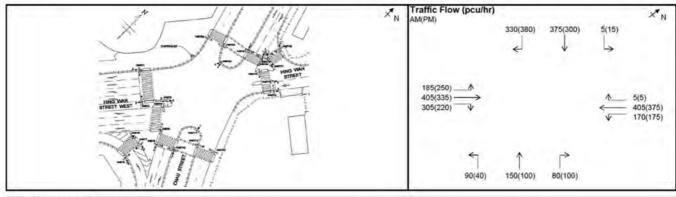
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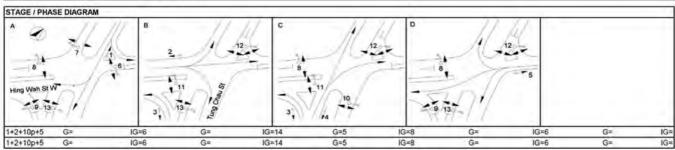


Capacity	Calculat	ions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Tung Chau	Street SB							-						
1A	A	3.30	Y	N	15		255	2%	1940	0.131	225	7%	1930	0.117
18	A	3.30	N	N	40		265	94%	2015	0.132	295	100%	2010	0.147
Hang Wah	Street West	EB						1						
2A	В	3.50	Y	N	25		165	100%	1760	0.094	225	100%	1760	0.128
2B	В	3.50	N	N			340		2000	0.170	285		2000	0.143
2C	В	3.50	N	N	20		138	100%	1860	0.074	98	100%	1860	0.053
2D	В	3.50	N	N	18		137	100%	1840	0.074	97	100%	1840	0.053
Tung Chau	Street NB													
3A	B,C	3.60	Y	N	20		80	100%	1835	0.044	35	100%	1835	0.019
4A	С	3.60	N	N			69		2115	0.033	60		2115	0.028
48	С	3.60	N	N	40		66	83%	2050	0.032	75	100%	2040	0.037
Hang Wah	Street WB													
5A	D	3.90	Y	N	20/20		505	27% / 1%	1965	0.257	485	30% / 1%	1960	0.247
6р	Α		5GM +	6FG =	11	sec								
7p	A		5GM +	7FG =	12	sec								
8p	A,C,D		5GM +	12FG =	17	sec		1						
9p	A,D		5GM +	8FG =	13	sec		-			_			
10p	C		5GM +	BFG =	11	sec	_	-			_			
11p	B,C		5GM +	9FG =	14	sec	_	-						
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,D		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+2+10p+5	PM Peak	1+2+10p+5
	Sum of Critical y Y	0.559	Sum of Critical y Y	0.537
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	16%	Reserve Capacity RC	21%

Scheme .

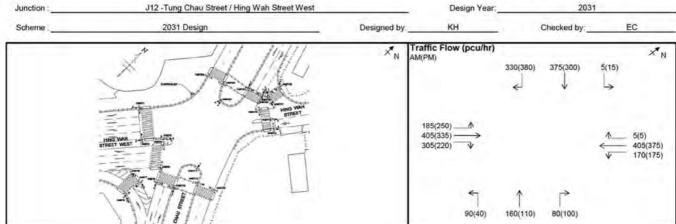


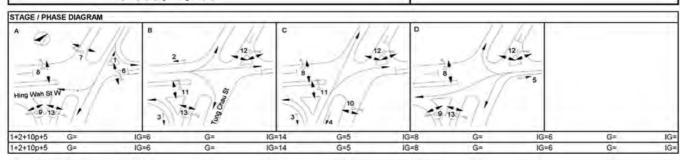


Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	A	3.30	Y	N	15		348	1%	1940	0.179	315	5%	1935	0.163
18	A	3.30	N	N	40		362	91%	2015	0.180	380	100%	2010	0.189
Hang Wah	Street West	EB												
2A	В	3.50	Y	N	25		185	100%	1760	0.105	250	100%	1760	0.142
2B	В	3.50	N	N			405		2000	0.203	335		2000	0.168
2C	В	3.50	N	N	20		153	100%	1860	0.082	111	100%	1860	0.060
2D	В	3.50	N	N	18		152	100%	1840	0.083	109	100%	1840	0.059
Tung Chau	Street NB													
3A	B,C	3.60	Y	N	20		90	100%	1835	0.049	40	100%	1835	0.022
4A	C	3.60	N	N			116		2115	0.055	100		2115	0.047
48	С	3.60	N	N	40		114	70%	2060	0.055	100	100%	2040	0.049
Hang Wah	Street WB													
5A	D	3.90	Y	N	20/20		580	29% / 1%	1960	0.296	555	32% / 1%	1955	0.284
6р	A		5GM +	6FG =	11	sec		-			_			
7p	A		5GM +	7FG =	12	sec	_							
8p	A,C,D		5GM +	12FG =	17	sec	_							
9p	A,D		5GM +	8FG =	13	sec	_							
10p	C		5GM +	6FG =	11	sec	_	-						
11p	B,C		5GM +	9FG =	14	sec	_							
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,D		5GM +	6FG =	- 13	sec								

Notes:	AM Peak	1+2+10p+5	PM Peak	1+2+10p+5
	Sum of Critical y Y	0.678	Sum of Critical y Y	0.640
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	-5%	Reserve Capacity RC	2%

JOB NO. : 5190641 sign Year: 2031

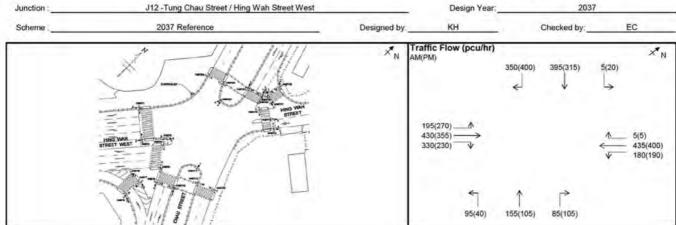


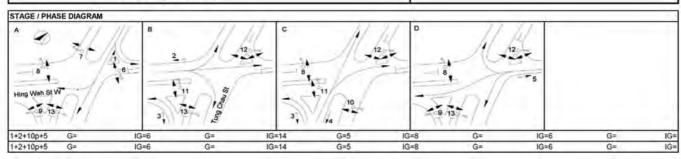


Capacity	Calculat	ions				-		AM	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in % g	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	Α	3.30	Y	N	15	-	348	1%	1940	0.179	315	5%	1935	0.163
18	A	3.30	N	N	40		362	91%	2015	0.180	380	100%	2010	0.189
Hang Wah	Street West	EB												
2A	В	3.50	Y	N	25		185	100%	1760	0.105	250	100%	1760	0.142
2B	В	3.50	N	N			405		2000	0.203	335		2000	0.168
2C	В	3.50	N	N	20		153	100%	1860	0.082	111	100%	1860	0.060
2D	В	3.50	N	N	18		152	100%	1840	0.083	109	100%	1840	0.059
Tung Chau	Street NB													
3A	B,C	3.60	Y	N	20		90	100%	1835	0.049	40	100%	1835	0.022
4A	С	3.60	N	N			121		2115	0.057	107	1 1 2	2115	0.051
48	С	3.60	N	N	40		119	67%	2065	0.058	103	97%	2040	0.050
Hang Wah	Street WB													
5A	D	3.90	Y	N	20/20		580	29% / 1%	1960	0.296	555	32% / 1%	1955	0.284
6p	A		5GM +	6FG = 7FG =	11	sec	_	+			_			
7p	A,C,D		5GM +	12FG =	12	sec		-						
8p 9p	A,C,D A,D		5GM +	12FG = 8FG =	13	sec	_	-						
10p	C		5GM +	6FG =	11	sec	-	-						
11p	B,C		5GM +	9FG =	14	sec	_	1						
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,D		5GM +	6FG =	13	sec								

Notes:	AM Peak	1+2+10p+5	PM Peak	1+2+10p+5
	Sum of Critical y Y	0.678	Sum of Critical y Y	0.640
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	-5%	Reserve Capacity RC	2%

JOB NO. : 5190641 2037

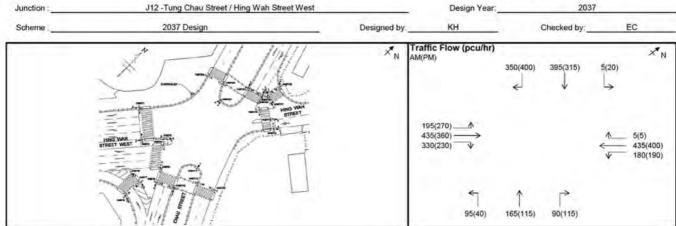


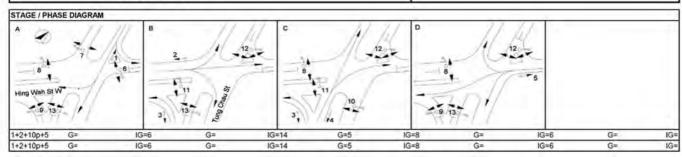


Capacity	Calculat	ions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	A	3.30	Y	N	15		368	1%	1940	0.190	335	6%	1935	0.173
18	A	3.30	N	N	40		382	92%	2015	0,190	400	100%	2010	0.199
Hang Wah	Street West	EB												
2A	В	3.50	Y	N	25		195	100%	1760	0.111	270	100%	1760	0.153
2B	В	3.50	N	N			430		2000	0.215	355		2000	0.178
2C	В	3.50	N	N	20		166	100%	1860	0.089	116	100%	1860	0.062
2D	В	3.50	N	N	18		164	100%	1840	0.089	114	100%	1840	0.062
Tung Chau	Street NB													
3A	B,C	3.60	Y	N	20		95	100%	1835	0.052	40	100%	1835	0.022
4A	C	3.60	N	N			122		2115	0.058	105		2115	0.050
48	С	3.60	N	N	40		118	72%	2060	0.057	105	100%	2040	0.051
Hang Wah	Street WB													
5A	D	3.90	Y	N	20/20		620	29% / 1%	1960	0.316	595	32% / 1%	1955	0.304
6р	A		5GM +	6FG =	11	sec		-						
7p	A		5GM +	7FG =	12	sec	_							
8p	A,C,D		5GM +	12FG =	17	sec	_							
9p	A,D		5GM +	8FG =	13	sec	_							
10p	C		5GM +	6FG =	11	sec	_	-						
11p	B,C		5GM +	9FG =	14	sec	_							
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,D		5GM +	BFG =	- 13	sec								

Notes:	AM Peak	1+2+10p+5	PM Peak	1+2+10p+5
	Sum of Critical y Y	0.721	Sum of Critical y Y	0.681
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	-10%	Reserve Capacity RC	-4%

JOB NO. : 5190641 2037





Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	A	3.30	Y	N	15		368	1%	1940	0.190	335	6%	1935	0.173
18	A	3.30	N	N	40		382	92%	2015	0,190	400	100%	2010	0.199
Hang Wah	Street West	EB												
2A	В	3.50	Y	N	25		195	100%	1760	0.111	270	100%	1760	0.153
2B	В	3.50	N	N			435		2000	0.218	360		2000	0.180
2C	В	3.50	N	N	20		166	100%	1860	0.089	116	100%	1860	0.062
2D	В	3.50	N	N	18		164	100%	1840	0.089	114	100%	1840	0.062
Tung Chau	Street NB													
3A	B,C	3.60	Y	N	20		95	100%	1835	0.052	40	100%	1835	0.022
4A	C	3.60	N	N			129		2115	0.061	115		2115	0.054
48	С	3.60	N	N	40		126	71%	2060	0.061	115	100%	2040	0.056
Hang Wah	Street WB													
5A	D	3.90	Y	N	20/20		620	29% / 1%	1960	0.316	595	32% / 1%	1955	0.304
6р	Α		5GM +	6FG =	11	sec						_		
7p	A		5GM +	7FG =	12	sec	_							
8p	A,C,D		5GM +	12FG =	17	sec	_							
9p	A,D		5GM +	8FG =	13	sec	_	-						
10p	C		5GM +	6FG =	11	sec	_	-			_			
11p	B,C		5GM +	9FG =	14	sec	_	-						
12p	B,C,D		5GM+	6FG =	11	sec	_							
13p	A,B,D		5GM +	6FG =	- 13	sec								

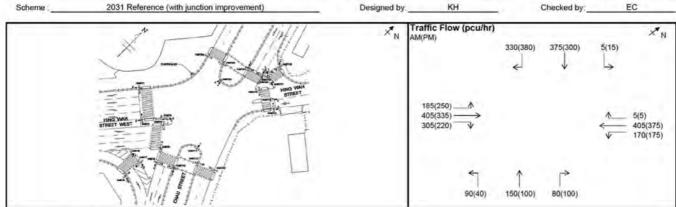
Notes:	AM Peak	1+2+10p+5	PM Peak	1+2+10p+5
	Sum of Critical y Y	0.724	Sum of Critical y Y	0.683
	Lost Time L (sec)	36	Lost Time L (sec)	36
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.647	Practical Y Ypr	0.651
	Reserve Capacity RC	-11%	Reserve Capacity RC	-5%

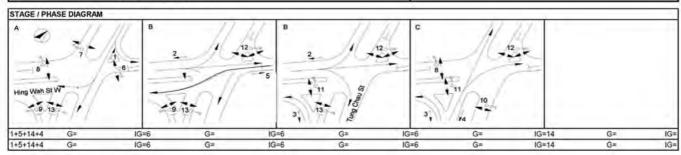
J12 -Tung Chau Street / Hing Wah Street West

 JOB NO.:
 5190641

 Design Year:
 2031

 Designed by:
 KH
 Checked by:
 EC





Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	Α	3.30	Y	N	15		348	1%	1940	0.179	315	5%	1935	0.163
18	А	3.30	N	N	40		362	91%	2015	0.180	380	100%	2010	0.189
Hang Wah S	Street West	EB												
2A	B,C	3.50	Y	N	25		185	100%	1760	0.105	250	100%	1760	0.142
2B	B,C	3.50	N	N			405		2000	0.203	335		2000	0.168
14A	С	3.50	N	N	20		153	100%	1860	0.082	111	100%	1860	0.060
148	С	3.50	N	N	18		152	100%	1840	0.083	109	100%	1840	0.059
Tung Chau	Street NB													
3A	C,D	3.60	Y	N	20		90	100%	1835	0.049	40	100%	1835	0.022
4A	D	3.60	N	N			116		2115	0.055	100		2115	0.047
48	D	3.60	N	N	40		114	70%	2060	0.055	100	100%	2040	0.049
Hang Wah S	Street WB													
5A	В	3.90	Y	N	20		575	30%	1960	0.293	550	32%	1960	0.281
6р	Α		5GM +	6FG =	11	sec		-						
7p	A		5GM +	7FG =	12	sec					_			
8p	A,D		5GM +	12FG =	17	sec		-						
9p	A,B		5GM +	8FG =	13	sec		-			_			
10p	D		5GM +	BFG =	11	sec	_				_			
11p	C,D		5GM +	9FG =	14	sec								
12p	B,C,D		5GM +	6FG =	11	sec								
13p	A,B,C		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+5+14+4	PM Peak	1+5+14+4
	Sum of Critical y Y	0.611	Sum of Critical y Y	0.578
	Lost Time L (sec)	28	Lost Time L (sec)	28
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.703	Practical Y Ypr	0.706
	Reserve Capacity RC	15%	Reserve Capacity RC	22%

 JOB NO. :
 5190641

 Junction :
 J12 -Tung Chau Street / Hing Wah Street West
 Design Year;
 2031

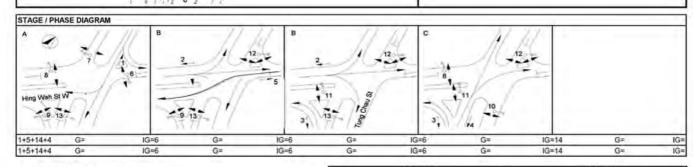
 Scheme
 2031 Design (with junction improvement)
 Designed by
 KH
 Checked by
 EC

 Image: Markett West
 Traffic Flow (pcu/hr)
 330(380)
 375(300)
 5(15)

 Image: Markett West
 185(250)
 ↑
 405(335)
 ↑

 Image: Markett West
 305(220)
 ↓
 405(375)
 ↓

 Interest West
 170(175)
 ↓
 170(175)
 ↓



Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	Α	3.30	Y	N	15		348	1%	1940	0.179	315	5%	1935	0.163
18	A	3.30	N	N	40		362	91%	2015	0.180	380	100%	2010	0.189
Hang Wah	Street West	EB						-						
2A	B,C	3.50	Y	N	25		185	100%	1760	0.105	250	100%	1760	0.142
28	B,C	3.50	N	N			405		2000	0.203	335		2000	0.168
14A	С	3.50	N	N	20		153	100%	1860	0.082	111	100%	1860	0.060
148	С	3.50	N	N	18		152	100%	1840	0.083	109	100%	1840	0.059
Tung Chau	Street NB													
3A	C,D	3.60	Y	N	20		90	100%	1835	0.049	40	100%	1835	0.022
4A	D	3.60	N	N			121		2115	0.057	107		2115	0.051
48	D	3.60	N	N	40		119	67%	2065	0.058	103	97%	2040	0.050
Hang Wah	Street WB													
5A	В	3.90	Y	N	20		575	30%	1960	0.293	550	32%	1960	0.281
6р	Α		5GM +	6FG =	11	sec								
7p	A		5GM +	7FG =	12	sec	_							
8p	A,D		5GM +	12FG =	17	sec		1						
9p	A,B		5GM +	8FG =	13	sec		-						
10p	D		5GM +	6FG =	11	sec		-						
11p	C,D		5GM +	9FG =	14	sec		-						
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,C		5GM +	6FG =	11	sec								
	11													

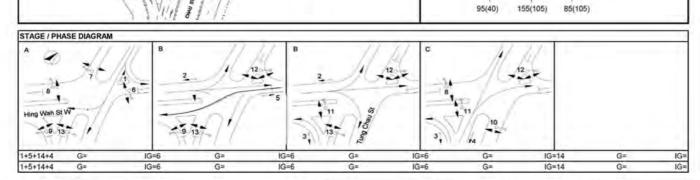
Notes:	AM Peak	1+5+14+4	PM Peak	1+5+14+4
	Sum of Critical y Y	0.613	Sum of Critical y Y	0.580
	Lost Time L (sec)	28	Lost Time L (sec)	28
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.703	Practical Y Ypr	0.706
	Reserve Capacity RC	15%	Reserve Capacity RC	22%

90(40)

160(110)

80(100)

JOB NO. : 5190641 J12 -Tung Chau Street / Hing Wah Street West 2037 Scheme __ 2037 Reference (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) AM(PM) XN 350(400) 395(315) 5(20) 5(5) 435(400) 180(190) 430(355) 330(230)

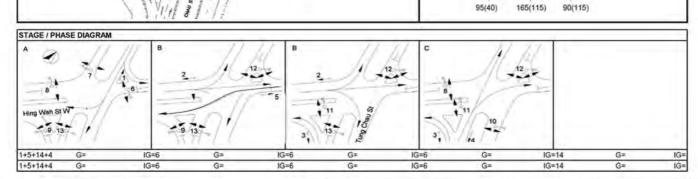


	Peak	PM F			Peak	AM F		- 4				ons	Calculati	Capacity
S facto	Saturation flow S (pcu/hr)	Proportion turning (%)	Design Flow q (pcu/hr)	Flow factor y	Saturation flow S (pcu/hr)	Proportion turning (%)	Design Flow q (pcu/hr)	Gradient in %	Radius for turning (m)	Opposed turn? (Y/N)	Nearside lane? (Y/N)	Lane Width (m)	Stage	Phase
												-	Street SB	Tung Chau
0.17	1935	6%	335	0.190	1940	1%	368		15	N	Y	3.30	A	1A
0.19	2010	100%	400	0,190	2015	92%	382		40	N	N	3,30	A	18
												EB	Street West	Hang Wah S
0.15	1760	100%	270	0.111	1760	100%	195		25	N	Y	3.50	B,C	2A
0.17	2000		355	0.215	2000		430			N	N	3.50	B,C	2B
0.06	1860	100%	116	0.089	1860	100%	166		20	N	N	3.50	С	14A
0.06	1840	100%	114	0.089	1840	100%	164		18	N	N	3.50	С	148
													Street NB	Tung Chau
0.02	1835	100%	40	0.052	1835	100%	95		20	N	Y	3.60	C,D	3A
0.05	2115		105	0.058	2115		122			N	N	3.60	D	4A
0.05	2040	100%	105	0.057	2060	72%	118		40	N	N	3.60	D	48
													Street WB	Hang Wah S
0.30	1960	32%	590	0.314	1960	29%	615		20	N	Y	3.90	В	5A
								sec	11	6FG =	5GM +		A	6р
							_	sec	12	7FG =	5GM+		A	7p
							_	sec	17	12FG =	5GM +		A,D	8p
_							_	sec	13	8FG =	5GM +		A,B	9p
_							_							
_							_							
							_							
								sec	13	6FG =	5GM +		A,B,C	13p
								sec sec sec sec	11 14 11 11	8FG = 9FG = 6FG = 8FG =	5GM + 5GM + 5GM + 5GM +		D C,D B,C,D A,B,C	10p 11p 12p 13p

Notes:	AM Peak	1+5+14+4	PM Peak	1+5+14+4
	Sum of Critical y Y	0.650	Sum of Critical y Y	0.614
	Lost Time L (sec)	28	Lost Time L (sec)	28
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.703	Practical Y Ypr	0.706
	Reserve Capacity RC	8%	Reserve Capacity RC	15%

JOB NO. : 5190641 J12 -Tung Chau Street / Hing Wah Street West 2037 Scheme: 2037 Design (with junction improvement) Designed by: Checked by:_ Traffic Flow (pcu/hr) AM(PM) X'N 350(400) 395(315) 5(20) 5(5) 435(400) 180(190) 435(360)

330(230)



Capacity	Calculat	ions						AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor y
Tung Chau	Street SB													
1A	Α	3.30	Y	N	15		368	1%	1940	0.190	335	6%	1935	0.173
18	A	3.30	N	N	40		382	92%	2015	0,190	400	100%	2010	0.199
Hang Wah	Street West	EB												
2A	B,C	3.50	Y	N	25		195	100%	1760	0.111	270	100%	1760	0.153
28	B,C	3.50	N	N			435		2000	0.218	360		2000	0.180
14A	С	3.50	N	N	20		166	100%	1860	0.089	116	100%	1860	0.062
14B	С	3.50	N	N	18		164	100%	1840	0.089	114	100%	1840	0.062
Tung Chau	Street NB													
3A	C,D	3.60	Y	N	20		95	100%	1835	0.052	40	100%	1835	0.022
4A	D	3.60	N	N			129		2115	0.061	115		2115	0.054
48	D	3.60	N	N	40		126	71%	2060	0.061	115	100%	2040	0.056
Hang Wah	Street WB													
5A	В	3.90	Y	N	20		615	29%	1960	0.314	590	32%	1960	0.301
6р	Α		5GM +	6FG =	11	sec								
7p	A		5GM +	7FG =	12	sec								
8p	A,D		5GM +	12FG =	17	sec		-						
9p	A,B		5GM +	8FG =	13	sec		-			_			
10p	D		5GM +	BFG =	11	sec	_	-			_			
11p	C,D		5GM +	9FG =	14	sec	_	-						
12p	B,C,D		5GM +	6FG =	11	sec	_							
13p	A,B,C		5GM +	6FG =	11	sec								

Notes:	AM Peak	1+5+14+4	PM Peak	1+5+14+4
	Sum of Critical y Y	0.654	Sum of Critical y Y	0.619
	Lost Time L (sec)	28	Lost Time L (sec)	28
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.703	Practical Y Ypr	0.706
	Reserve Capacity RC	8%	Reserve Capacity RC	14%

1+2+3

JOB NO. : 5190641 J13 - Sham Shing Road / Hing Wah Street West 2021 Scheme . Existing Designed by: Checked by: Traffic Flow (pcu/hr) 180(185) 515(480) 205(165) V 60(65) 405(340) STAGE / PHASE DIAGRAM G= 1+2+3 G= G=

Capacity	Calculat	tions				- 4		AM I	Peak			PM	Peak	
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Sham hing	Road EB													
1A	A	3.30	Y	N	23	-	181	100%	1825	0.099	176	100%	1825	0.096
18	A	3.30	N	N	25		194	100%	1965	0.099	189	100%	1965	0.096
1C	A	3.30	N	N	25		205	100%	1965	0.104	165	100%	1965	0.084
ling Wah S	Street West	NR.												
2A	B	3.40	Y	N	20		60	100%	1820	0.033	65	100%	1820	0.036
28	В	3.40	N	N	1.0		203	10079	2095	0.097	170	10010	2095	0.081
2C	В	3.40	N	N			202		2095	0.096	170		2095	0.081
Hing Wah S	Street West	SB												
3A	С	3.30	Y	N			140		1555	0.090	130	-	1555	0.084
3B	С	3.30	N	N			187		2085	0.090	175		2085	0.084
3C	С	3.30	N	N			188		2085	0.090	175		2085	0.084
3D	С	3,30	N	N	25		180	100%	1965	0.092	185	100%	1965	0.094
4p	A,B		5GM +	13FG =	18	sec								
5p	A		5GM+	11FG =	16	sec								
6р	B,C		5GM +	11FG =	16	sec								
7p	С		5GM +	14FG =	19	sec								
	11.													

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.293	Sum of Critical y Y	0.272
	Lost Time L (sec)	12	Lost Time L (sec)	12
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.816	Practical Y Ypr	0.817
	Reserve Capacity RC	179%	Reserve Capacity RC	201%

1+2+3

1+2+3

G=

G=

G=

Capacity	Calculat	ions				-		AM Peak				PM Peak			
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	
ham hing	Road EB		10000	1			- Germany		100		- dr		0	-	
1A	Α	3.30	Y	N	23		202	100%	1825	0.111	195	100%	1825	0.107	
18	A	3.30	N	N	25		218	100%	1965	0.111	210	100%	1965	0.107	
1C	A	3.30	N	N	25		230	100%	1965	0.117	185	100%	1965	0.094	
ling Wah S	treet West	NR.													
2A	B	3.40	Y	N	20		65	100%	1820	0.036	75	100%	1820	0.041	
28	В	3.40	N	N			238	,5070	2095	0.114	198	1.5010	2095	0.095	
2C	В	3.40	N	N			237		2095	0.113	197		2095	0.094	
Hing Wah S	treet West	SB													
3A	C	3.30	Y	N			170		1555	0.109	159		1555	0.102	
38	С	3.30	N	N			227		2085	0.109	213		2085	0.102	
3C	C	3.30	N	N			228		2085	0.109	213		2085	0.102	
3D	С	3.30	N	N	25		200	100%	1965	0.102	205	100%	1965	0.104	
4p	A,B		5GM +	13FG =	18	sec									
5p	A		5GM +	11FG =	16	sec									
6р	B,C		5GM +	11FG =	16	sec									
7p	С		5GM +	14FG =	19	sec									
												-			

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.340	Sum of Critical y Y	0.306
	Lost Time L (sec)	12	Lost Time L (sec)	12
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.816	Practical Y Ypr	0.817
	Reserve Capacity RC	140%	Reserve Capacity RC	167%

G=

1+2+3

G=

G=

Capacity	Calculat	tions						AM I	Peak		PM Peak			
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow
Sham hing	Road EB		44	49		- 3	(Breening)		April 100	-	(pate)	-	(paramy	-
1A	A	3.30	Y	N	23		202	100%	1825	0.111	195	100%	1825	0.107
18	A	3.30	N	N	25		218	100%	1965	0.111	210	100%	1965	0.107
1C	Α	3.30	N	N	25		230	100%	1965	0.117	185	100%	1965	0.094
ling Wah S	treet West	NB												
2A	В	3.40	Y	N	20		65	100%	1820	0.036	75	100%	1820	0.041
28	В	3.40	N	N	7		238		2095	0.114	198		2095	0.095
2C	В	3.40	N	N			237		2095	0.113	197		2095	0.094
Hing Wah S	treet West	SB												
3A	C	3.30	Y	N			170		1555	0.109	159		1555	0.102
38	C	3.30	N	N			227		2085	0.109	213		2085	0.102
3C	C	3.30	N	N			228		2085	0.109	213		2085	0.102
3D	С	3.30	N	N	25		200	100%	1965	0.102	205	100%	1965	0.104
4p	A,B		5GM +	13FG =	18	sec								
5p	A		5GM +	11FG =	16	sec								
6р	B,C		5GM +	11FG =	16	sec								
7p	С		5GM +	14FG =	19	sec								

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.340	Sum of Critical y Y	0.306
	Lost Time L (sec)	12	Lost Time L (sec)	12
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.816	Practical Y Ypr	0.817
	Reserve Capacity RC	140%	Reserve Capacity RC	167%

G=

1+2+3

1+2+3

G=

G=

G=

Capacity	Calculat	tions					AM Peak			PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Sham hing	Road EB													
1A	A	3.30	Y	N	23		214	100%	1825	0.117	209	100%	1825	0.115
18	A	3.30	N	N	25		231	100%	1965	0.118	226	100%	1965	0.115
1C	A	3.30	N	N	25		245	100%	1965	0.125	195	100%	1965	0.099
Hing Wah S	treat West	NR												
2A	B	3.40	Y	N	20		70	100%	1820	0.038	75	100%	1820	0.041
28	В	3.40	N	N	2.0		255	10070	2095	0.122	210	10079	2095	0.100
2C	В	3.40	N	N			255		2095	0.122	210		2095	0.100
Hing Wah S	treet West	SB												
3A	С	3.30	Y	N			181		1555	0.116	168		1555	0.108
3B	С	3.30	N	N			242		2085	0.116	226		2085	0.108
3C	C	3.30	N	N			242		2085	0.116	226		2085	0.108
3D	С	3.30	N	N	25		215	100%	1965	0.109	220	100%	1965	0.112
4p	A,B		5GM +	13FG =	18	sec								
5p	A		5GM +	11FG =	16	sec								
6р	B,C		5GM +	11FG =	16	sec								
7p	С		5GM +	14FG =	19	sec								

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.363	Sum of Critical y Y	0.327
	Lost Time L (sec)	12	Lost Time L (sec)	12
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.816	Practical Y Ypr	0.817
	Reserve Capacity RC	125%	Reserve Capacity RC	150%

1+2+3

1+2+3

G=

G=

G=

Capacity	Calculat	tions				-	AM Peak			PM Peak				
Phase	Stage	Lane Width (m)	Nearside lane? (Y/N)	Opposed turn? (Y/N)	Radius for turning (m)	Gradient in %	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor	Design Flow q (pcu/hr)	Proportion turning (%)	Saturation flow S (pcu/hr)	Flow factor
Sham hing	Road EB			1										
1A	A	3.30	Y	N	23		214	100%	1825	0.117	209	100%	1825	0.115
1B	A	3.30	N	N	25		231	100%	1965	0.118	226	100%	1965	0.115
1C	A	3.30	N	N	25		245	100%	1965	0.125	195	100%	1965	0.099
Jing Wah S	treet West	NR												
2A	B	3.40	Y	N	20		70	100%	1820	0.038	75	100%	1820	0.041
2B	В	3.40	N	N	20		258	10076	2095	0.123	213	10070	2095	0.102
2C	В	3.40	N	N			257		2095	0.123	212		2095	0.101
Hing Wah S	treet West	SB												
3A	С	3.30	Y	N			181	1 -	1555	0.116	168		1555	0.108
3B	С	3.30	N	N			242	1	2085	0.116	226	1	2085	0.108
3C	C	3.30	N	N			242		2085	0.116	226		2085	0.108
3D	С	3,30	N	N	25		215	100%	1965	0.109	220	100%	1965	0.112
4p	A,B		5GM +	13FG =	18	sec								
5p	A		5GM +	11FG =	16	sec								
6р	B,C		5GM +	11FG =	16	sec								
7p	С		5GM +	14FG =	19	sec								

Notes:	AM Peak	1+2+3	PM Peak	1+2+3
	Sum of Critical y Y	0.364	Sum of Critical y Y	0.329
	Lost Time L (sec)	12	Lost Time L (sec)	12
	Cycle Time c (sec)	128	Cycle Time c (sec)	130
	Practical Y Ypr	0.816	Practical Y Ypr	0.817
	Reserve Capacity RC	124%	Reserve Capacity RC	149%

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Appendix 6

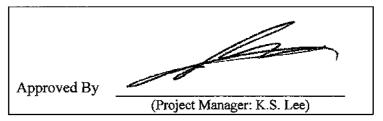
Environmental Assessment (EA) Report

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Environmental Assessment Report

(V1.0)

September 2021



REMARKS:

The information supplied and contained within this report is, to the best of our knowledge, correct at the time of printing.

CINOTECH accepts no responsibility for changes made to this report by third parties.

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1 INTRODUCTION

1.1 Background

- 1.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). This Environmental Assessment (EA) is to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.2 The Scheme SSP-018 consists of Sites A and B. Site A is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the south-western boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary. The location of the Scheme is shown in Figure 1-1.
- 1.1.3 The URA proposed to redevelop the Site A for high-density residential development, and the Site B to G/IC complex with a large public open space.
- 1.1.4 Cinotech Consultants Limited was commissioned by URA to carry out an Environmental Assessment (EA) to assess and envisage any potential environmental impact on the implementation of the proposed development of the Scheme and to recommend necessary pipe upgrading/diversion as necessary.

1.2 Purpose and Scope of Report

- 1.2.1 This EA is prepared to assess the potential environmental impact/benefit associated with the implementation of the Scheme in supporting the submission of the draft DSP to TPB's consideration. It has been undertaken with reference to the guidance for environmental considerations provided in Chapter 9 "Environment" of the Hong Kong Planning Standards and Guidelines (HKPSG).
- 1.2.2 This EA presents the study of the potential environmental impacts of the following aspects:
 - Air Quality
 - Noise
 - Waste Management
 - Preliminary Land Contamination
- 1.2.3 Drainage Impact, Sewerage Impact, Water Supply Impact and Air Ventilation Impact will be assessed in separate reports.

2 DESCRIPTION OF THE ENVIRONMENT

2.1 Overview of Existing Developments and Major Roads in the Surroundings

- 2.1.1 The Scheme is located in a core region of developed area. The immediately north and east of the Sites are mostly residential development. The immediately south of the Sites is a large public open area (Sham Shui Po Sport Ground). In the west of the Sites, there are some industrial developments mixed with commercial and residential developments. The Caritas Medical Centre is around 300m in the north of the Sites.
- 2.1.2 Both of the Sites are adjoining the primary distributor road Cheung Sha Wan Road. Primary distributor road Lai Chi Kok Road is around 300m & 100m in the south of Site A and Site B, respectively. Urban trunk road West Kowloon Corridor is around 400m & 200m in the south-west of Site A and Site B, respectively.

2.2 Overview of Potential Environmental Impact to the Sites

Potential Air Pollution Sources

- 2.2.1 The residential developments in the east and north as well as the Sham Shui Po Sport Ground in the south are not considered as air pollution source.
- 2.2.2 Base on the existing situation, the industrial developments in the west are unlikely to be noticeable air pollution sources as there is no industrial chimney identified. In addition, the industrial developments are closely packed with existing air sensitive receivers (residential and commercial developments) showings their surroundings are suitable for air sensitive uses.
- 2.2.3 In order to verify the potential air pollution source(s) in Caritas Medical Centre, inquiry through Access to Information had been conducted during April-June in 2021. According to the reply from Caritas Medical Centre, there are 10 chimneys in the hospital, but only 2 are active chimneys. The rest of the chimney are only for standby emergence generator, which are normally not active. Moreover, the 2 active chimneys are only using clean fuel (Town Gas). Therefore, the chimneys in Caritas Medical Centre are not considered as air pollutant sources.
- 2.2.4 Due to the heavy traffic, the road traffic emissions are the major air pollution source in the surroundings.

Potential Fixed Noise Sources

- 2.2.5 The residential developments in the east and north are not considered fixed noise source.
- 2.2.6 For the Sham Shui Po Sport Ground in the south, there are loud speakers identified within the covered stand. Considering the scale of the loud speakers and the traffic noise from the Cheung Sha Wan Road, it is unlikely that those loud speakers will adversely affect the Site A, which is >100m away and separated by Cheung Sha Wan Road. However, for Site B, there are potential impact from the loud speakers due to the proximity.
- 2.2.7 Some of the industrial developments in the west are having chiller plant and/or water cooling towers at the roof which are considered potential fix noise sources. For Site A, those fix noise

sources are more than 200m holistically away from the Site, and mostly blocked by high-rise commercial/residential buildings (e.g. China Shipbuilding Tower, & Charming Garden) thus no adverse impact is anticipated. However, for Site B, those fix noise sources are much closer thus attention may be required.

2.2.8 Due to the heavy traffic, the road traffic noise are the major noise source in the surroundings.

3 THE PROPOSED DEVELOPMENT

- 3.1.1 The proposed gross site areas of the Site A & Site B are 5,197m² and 13,857m² respectively, subject to site survey and detailed design. With the net site area of Site A of about 5,197 m² (subject to site survey), the proposed total Gross Floor Area ("GFA") of Site A is about 49,372 m² (Plot Ratio (PR) = 9.5), of which 38,978 m² is for domestic (PR=7.5), 5,197 m² for commercial/retail (PR=1.0), and 5,197 m² for GIC provision (PR=1) in the Scheme. The net Site area of Site B is about 4,212 m² (subject to site survey), the proposed total Gross Floor Area ("GFA") of Site B is about 33,969 m² (Plot Ratio (PR) = 8.0) for GIC provision in the Scheme.
- 3.1.2 Currently, the Site A comprises a single storey Cheung Sha Wan Sports Centre and its associate outdoor garden and playground. The Site B comprises a government land lot (GLA-TNK 1723) which currently is an open area with a few 1-2 storeys temporary structures, Cheung Sha Wan Path Sitting-out Area, and a garden associated with Sham Shui Po Sports Ground. (Figure 1-1).
- 3.1.3 Under the current notional design, the entire Site A is proposed to rezone to "R(A)" and redevelop the area for high-density residential development, with non-domestic uses always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of a building. The proposed development on Site A consists of a 2 floors of basement carpark, a 5 storeys podium (GFA: 5,197m² for retails; 5,197m² for G/IC) and two 34 storeys residential towers (838 flats, 140mPD). The western part of the Site B is proposed to rezone to G/IC to provide a G/IC complex of 95mPD with GFA of 33,696 m² for community and amenity. The rest of the Site B (about 9,645 m²) is proposed to be public open space. The proposed notional scheme is shown in Figure 3-1 & 3-2. The notional design is subject to change at detailed design stage.

4 AIR QUALITY IMPACT ASSESSMENT

4.1 Introduction

- 4.1.1 The purpose of this chapter is to demonstrate that the proposed development will not impose adverse air quality impact to the surrounding area during the construction phase and the air sensitive receivers (ASRs) of the proposed development will not receive insurmountable air quality impact from the surrounding area during operation phase according to the notional layout plan.
- 4.1.2 This chapter assessed the potential air quality impact from the following aspects: (i) Construction Phase the potential air quality impact generated from the construction activities of the proposed development to the surroundings; (ii) Operation Phase road traffic emission to the proposed developments in the Scheme. It also recommends appropriate mitigation measures to the potential impacts if any.

4.2 Legislation, Standards & Guidelines

- 4.2.1 The air quality impact assessment criteria were made reference to the Hong Kong Planning Standards and Guidelines (HKPSG) and the Air Pollution Control Ordinance (Cap.311) (APCO).
- 4.2.2 The Air Pollutant Control Ordinance (APCO) provides the statutory authority for controlling air pollutants from a variety of sources. The Hong Kong Air Quality Objectives (AQO) stipulate the maximum allowable concentrations over specific periods for the criteria pollutants. The concerned air pollutants during construction phase are the Total Suspended Particulates (TSP), Respirable Suspended Particulates (RSP) and Fine Suspended Particulates (FSP) arising from the construction work of the Proposed Development. The emission source during the operational phase of the road work would be the vehicular emission on the roads. There are no active industrial chimneys, besides the 2 chimneys in Caritas Medical Centre, which is using clean fuel (Town Gas), identified within the assessment area.
- 4.2.3 In Hong Kong, Sulphur Dioxide (SO₂) is primarily from the combustion of Sulphur-containing fossil fuels in power stations and marine vessels. A statutory minimum requirement has been enacted since April 2002 to restrict vehicles to use ULSD (Ultra Low Sulphur Diesel) with a sulphur content of only 0.005% and has been further tightened to a sulphur content of only 0.001% from 1 July 2010 onward. Therefore, emission of vehicular SO₂ is not a significant source. For marine vessel, according to Air Pollution Control (Fuel for Vessels) Regulation, starting from 1 January 2019, all marine vessels except for specified vessel types as set out in the Regulation, are required to use compliant fuel (i.e.: liquid fuel with sulphur content not more than 0.5% by weight, liquefied natural gas, or other approved fuel) within Hong Kong waters, irrespective of whether they are sailing or berthing.
- 4.2.4 It is understood that road transportation is the dominant source of CO emission; nevertheless, the air quality impact due to CO is still relatively minor. Although CO concentrations are not measured at Sham Shui Po Air Quality Station, the ambient air quality predicted for Year 2025 from PATH v2.1 (grid 38,35) shows that the predicted future hourly CO levels would be always lower than 1000 μg/m³ which comply with AQOs with large margins (1-hour criteria: 30,000 μg/m³; 8-hour criteria: 10,000 μg/m³). Hence, the emission of CO from the induced road transportation is not likely to have major impact on air quality, and hence is not considered as a key parameter for this assessment.

- 4.2.5 Ozone (O₃) is formed from dioxygen by the action of ultraviolet light and also atmospheric electrical discharges. It is not a primary pollutant emitted from vehicular emission thus is not considered as key criteria pollutants for the project.
- 4.2.6 Leaded petrol has been banned in Hong Kong since 1999. It is not considered concerned pollutants for vehicular emission.
- 4.2.7 To sum up, the Nitrogen Dioxide (NO₂), Total Suspended Particulates (TSP), Respirable Suspended Particulates (RSP), and Fine Suspended Particulates (FSP) are chosen to be the key criteria pollutants for the assessment of the air quality impact in this project. The relevant AQO are shown in Table 4-1.

Table 4-1 Hong Kong AQO for 1-hour, 24-hours Average and Annual Concentration for NO2, RSP, FSP & TSP

Pollutant	Maximum Concentration (μg/m³) ⁽¹⁾					
Fonutant	1-hour ⁽²⁾	24-hour ⁽³⁾	Annual			
Nitrogen Dioxide (NO ₂)	200	N.A.	40			
Respirable Suspended Particulates (RSP) ⁽⁴⁾	N.A.	100	50			
Fine Suspended Particulates (FSP) ⁽⁴⁾	N.A.	50	25			
Total Suspended Particulates (TSP) ⁽⁵⁾	500	N.A.	N.A.			

Note:

- [1] Measured at 293K (for NO2, RSP & FSP), 298K (for TSP) and 101.325 kPa;
- [2] Not to be exceeded more than 18 times per year;
- [3] Not to be exceeded more than 9 times per year for RSP; 35 times for FSP;
- [4] Suspended particulates in air with a nominal aerodynamic diameter of 10 μm or smaller for RSP and 2.5 μm or smaller for FSP.
- [5] Hong Kong AQO & HKPSG do not specific the criterion for TSP. Reference has been made to Annex 4 of EIAO-TM.

4.3 Background Air Quality

4.3.1 EPD has been closely monitoring the air quality in Hong Kong through their air quality monitoring station (AQMS). The closest AQMS to the scheme is the Sham Shui Po Monitoring Station. The monitoring result of Sham Shui Po Monitoring Station during year 2016-2020 are summarized in Table 4-2. The measured NO₂/RSP/FSP concentrations show a decreasing trend from Year 2016 to Year 2020. The most concerning parameter during the past few years is annual averaged NO₂ concentration, which has been exceeding AQO's criterion in 2016-2020.

Measured Air Quality of Sham Shui Po Monitoring Station (2016-2020) Table 4-2

D II .	Averaging	AQOs	Concentration [µg/m³]						
Pollutant	Time	[μg/m³] [i]	Year 2016	Year 2017	Year 2018	Year 2010	Year 2020		
RSP	24-hour (10th Max)	100 (9)	77.2	71.3	60.0	66.3	58.3		
[PM ₁₀] Annu	Annual	50	34.5	33.2	32.5	32.8	27.5		
FSP [PM _{2.5}]	24-hour (36th Max)	50 (35)	38.5	36.7	33.6	28.8	24.9		
	Annual	25	23.0	21.4	21.4	18.2	13.9		
NO ₂	1-hour (19th Max)	200 (18)	161.0	194.0	152.0	176.0	151.0		
	Annual	40	<u>57.6</u>	54.4	48.6	47.8	45.4		

The numbers in brackets () refer to number of exceedance allowed per year.

4.3.2 PATH-v2.1 is a macro-scale air quality model developed by EPD to predict future air quality over the whole Pearl River Delta region including Hong Kong. For the purpose of this assessment, the predicted values from PATH-v2.1 are adopted as the background air quality. The PATH grids corresponding to the Scheme is (38,35) as shown in Figure 4-1. Table 4-3 give the predicted ground level (0-17mAG) background air quality for Year 2022 to Year 2025.

Table 4-3 Background Ground Level Air Quality of Grid (38, 35) of PATH-v2.1

D 11	Averaging	AQOs	PATH Model Concentration [µg/m³]					
Pollutant	Time	[µg/m³] [i]	Year 2022	Year 2023	Year 2024	Year 2025		
RSP	24-hour (10th Max)	100 (9)	63.4	63.1	62.7	62.4		
[PM ₁₀] Annu	Annual	50	27.4	27.4	27.3	27.3		
FSP	24-hour (36th Max)	50 (35)	24.3	24.1	23.9	23.7		
[PM _{2.5}] Annu	Annual	25	15.0	15.0	14.9	14.9		
NO ₂	1-hour (19th Max)	200 (18)	129.7	127.3	125.3	123.7		
	Annual	40	24.5	23.9	23.0	22.8		

Note:

The numbers in brackets () refer to number of exceedance allowed per year.

4.3.3 All predicted background pollutant concentrations show a decreasing trend from Year 2022 to Year 2025 as shown in Table 4-3, and it is likely to continue to reduce after Year 2025. The background RSP, FSP and hourly NO2 concentrations are well below the AQO criteria and providing more margin in later years.

Daily and Annual averaged were calculated from hourly data.

The 10th highest daily RSP concentrations predicted by PATH-v2.1 are adjusted by adding 11.0μg/m³, according to EPD's Guidelines on Choice of Models and Model Parameters (updated July 2021)

⁽iii) The annual RSP concentrations predicted by PATH-v2.1 are adjusted by adding 10.3 μg/m³, according to EPD's Guidelines on Choice of Models and Model Parameters (updated July 2021).

(iv) The 36th highest daily FSP concentrations predicted by PATH-v2.1 are adjusted by adding 0.0µg/m³, according to

EPD's Guidelines on Choice of Models and Model Parameters (updated July 2021).

The annual FSP concentrations predicted by PATH-v2.1 are adjusted by adding 3.5 μg/m³, according to EPD's Guidelines on Choice of Models and Model Parameters (updated July 2021).

4.4 Construction Phase Air Quality Impact Assessment

- 4.4.1 Major dust emitting construction activities will be the demolition of existing structures, excavation for basement construction, foundation works and construction activities (e.g. the construction of superstructure). Fugitive dust would be generated. The concerned air pollutants during the construction phase are the Total Suspended Particulates (TSP), Respirable Suspended Particulates (RSP) and Fine Suspended Particulates (FSP) arising from the construction work of the Project.
- 4.4.2 Dust control measures under the Air Pollution Control (Construction Dust) Regulation (Cap. 311R) and good site practice shall be implemented to mitigate dust impact arising from demolition work by preventing dust generation and/or by screening, suppressing and removing dust generated:
 - Enclose the whole wall of the building to a height of at least 1m higher than the highest level of the structure to be demolished with impervious dust screens or sheeting on façade abutting or fronting upon a street
 - Existing structures are proposed to be demolished by non-percussive equipment such as hydraulic crusher to reduce dust emission; no blasting will be involved.
 - Water or a dust suppression chemical shall be sprayed immediate prior to, during and immediately after demolition/excavation works
 - Cover stockpile or dusty materials with tarpaulin to prevent wind erosion
 - Any dusty materials remaining after a stockpile is removed shall be wetted with water and cleared from the surface of roads or streets
 - Every vehicle shall be washed to remove any dusty materials from its body and wheels before leaving the construction site
 - Where a vehicle leaving a construction site is carrying a load of dusty materials, the load shall be covered entirely by clean impervious sheeting to ensure that the dusty materials do not leak from the vehicle
 - Store cement bags in shelter with 3 sides and the top covered by impervious materials if the stack exceeds 20 bags
 - Maintain a reasonable height when dropping excavated materials to limit dust generation
 - Limit vehicle speed within site to 10 km/h and confine vehicle movement in haul road
 - Minimize exposed earth after completion of work in a certain area by hydroseeding, vegetating or soil compacting
 - Cover materials on trucks before leaving the site to prevent dropping or being blown away by wind
 - · Regular maintenance of plant equipment to prevent black smoke emission
 - Throttle down or switch off unused machines or machine in intermittent use
 - Plan the site layout so that machineries, dust causing activities and stockpilings are away from receptors as far as possible.
 - Site hoarding higher than 2.4m should be implemented where there are receptors at close proximity to the construction site and dusty activities.
 - Haul road shall be away from the project boundary as much as possible

- 4.4.3 No significant dust impact on the surrounding air sensitive receivers (ASRs) is expected with proper implementation of mitigation measures. No quantitative construction dust assessment is considered necessary.
- 4.4.4 Operation of Powered Mechanical Equipment (PME) during demolition/construction work would emit gaseous air pollutants such as nitrogen dioxide (NO₂) via fuel burning. According to Air Pollution Control (Non-road Mobile Machinery) (Emission) Regulation, only approved or exempted Non-Road Mobile Machinery (NRMM) with a proper label are allowed to be used in specified activities and locations including construction sites. Supportive information and documents (e.g. third-party emission certificates, model and serial numbers of machines and engines, etc.) for each NRMM would be provided to EPD to prove that the concerned NRMM is in line with the prescribed emission standards. Since the number of PME expected to be used on-site will be limited and much less than vehicles travelled on surrounding roads (e.g. Cheung Sha Wan Road), no significant impact is anticipated.

4.5 Operation Phase Air Quality Impact Assessment

General Flow of the Assessment

- 4.5.1 Firstly, the assessment year will be determined by comparing the daily vehicular emission of the different years and the year with highest vehicular emission will be adopted as assessment year.
- 4.5.2 Then, the cumulative pollutant concentration will be computed. Besides the PATH-v2.1 background, the following pollutant sources will be considered:
 - Vehicular Emission from open public road sections within 500 m assessment area
 - Other major emission sources within 4 km of the scheme area
- 4.5.3 If any of the representative ASRs exceed the AQO criteria, feasible locations for openable windows and/or fresh air intake will be suggested.

Air Sensitive Receivers

- 4.5.4 During operation phase, no major emission is anticipated from the residential, G/IC and commercial components of the proposed development. On the other hand, the residential flats, shops and G/IC areas of the Scheme are ASRs which should be assessed.
- 4.5.5 The residential flats in the Scheme rely on openable windows for ventilation; the shops and G/IC in the podium and in the G/IC Complex would rely on air-conditioning with fresh air intake. Therefore, façades of the Residential Towers, as well as the potential fresh air in-take locations of the podium and the Low Block should be assessed. The locations of the assessment points are illustrated in Figures 4-2 & 4-3 and listed in Table 4-4.

Table 4-4 Summary of the Assessment Points (Air Quality)

Locations	ID	Assessment Height (mAG)
	AP-01 to AP-05	G/F - 01.50 1/F - 06.35
Façade of the Podium Structure of the Site A	AP-06 to AP-15	G/F - 01.50 1/F - 06.35 2/F - 10.85 3/F - 14.50 4/F - 18.00 5/F - 21.50
Façade of the Residential Tower A	TA-01 to TA-13	Residential 1/F – 29.35 Residential 2/F – 32.50
Façade of the Residential Tower B	TB-01 to TB-12	Residential 3/F – 35.65 Residential 4/F – 38.80 Residential 5/F – 41.95
Façade of the G/IC Complex of Site B	BC-01 to BC-10	G/F - 01.50 1/F - 08.00 2/F - 11.60 3/F - 15.20 4/F - 18.80 5/F - 22.40 6/F - 26.00 7/F - 30.50 8/F - 35.00

- 1] The Ground level of the Scheme is 5.05mPD.
- [2] The Assessment Height is 1.5m above slab level.
- 3] The notional design including the elevation is subject to change.
- [4] The residential towers has it own floor number.

Meteorological Data

For AERMOD, AERMET, & CALINE4

- 4.5.6 The hourly meteorological data from PATH model and the hourly stability classes calculated by PCRAMMET has be adopted. The PCRAMMET model can estimate the stability class based on the existing meteorological data for CALINE4 (for traffic emission). As CALINE4 imposes the limitation of wind speed on each of the stability class, the adopted stability class has been shifted toward class 3 for classes 1 & 2, and the adopted wind speed has been reduced for other cases, when necessary, for conservative assessment.
- 4.5.7 The hourly data from PATH Model has been prepared into on-site data as AERMET input. The output meteorological data form AERMET was later be used by AERMOD (for non-road traffic emission). The input mixing height data was restricted to between 121m and 1667m, which were the observed extreme values by the Hong Kong Observatory in year 2010. To avoid the occurrence of calm hours in the model, a minimum wind speed of 1.0m/s was adopted and any wind direction <0.1° was replaced by 360°.
- 4.5.8 The surface characteristics of the AERMET input were prepared following the recommendations in "AERMOD Implementation Guide" revised in August 2015 by USEPA. The Albedo and Bowen ratio adopted are the average values based on the land use of the 10km × 10km region centred on the study area. The surface roughness lengths were

determined based on the land use of 1km upwind in sector widths no smaller than 30 degrees. The surface roughness, Albedo and Bowen of different land use are adopted with referenced to Table 4-2 to Table 4-6 of User's Guide for the AERMOD Meteorological Preprocessor (AERMET).

For Road Traffic Emission factor from EMFAC v4.3

4.5.9 Hong Kong Observatory's hourly temperature and relative humidity at King's Park during year 2020 has be adopted for determining the road traffic emission factor. Meteorological data at King's Park is representative as it is located at core of developed area, similar to the Subject Site.

Assessment Year

- 4.5.10 The proposed development is planned to be completed by Year 2034, the assessment year for traffic air quality impact shall be predicted based on the worst scenario within 15 years after the completion of the proposed development.
- 4.5.11 The traffic flow forecast for Years 2034, 2042 & 2049 has been provided by traffic consultant. The predicted traffic flow has been submitted to the Transport Department (TD) for agreement with the methodology. The Endorsement of Traffic Forecast from TD will be enclosed in Appendix 4-1 when available.
- 4.5.12 Sensitivity test for traffic emission has been conducted using traffic data of Years 2034, 2042 & 2049. The NOx emission of Year 2049 and the RSP/FSP emission of Year 2034 are found to be highest, thus NOx/NO₂ emission of Year 2049 and RSP/FSP emission of Year 2034 has been adopted. The result of sensitivity test is enclosed in Appendix 4-2. The methodology of the sensitivity test is explained in the following paragraphs.

Methodology - Road Traffic Emission Factors & Sensitivity Test

- 4.5.13 The latest version of EMFAC HK V4.3 which was issued by EPD in early 2021 has been adopted to compile the traffic emission inventory. "Emfac Mode", which can provide RUN emission per vehicle kilometre travelled (in g/VKT) and START emission per trip (in g/trip) under which different temperature, relative humidity and traffic speed has been selected for the assessment. As a conservative approach, the highest START emission across various soak time will be adopted. The START emission has been converted into emission/VKT using the trip/VKT ratio from EMFAC v4.3¹ of the corresponding year and combine with the RUN emission. Therefore, a set of emission factors (NOx, NO2, RSP & FSP) for vehicles emission with cold start and another set of emission factors for vehicles emission without cold start has been obtained.
- 4.5.14 It should be noted that the HKSAR Government are promoting electric vehicle and targeting zero emissions before 2050². In practice, besides the cost-effective reason, the number of electric vehicles is restrained by the technologies such as battery capacity and charging speed. The prevailing of charging facility would also be another factor. There are too many uncertainties about the projected ratio of electric vehicles during assessment year (2034-2049). Therefore, for conservative assessment, the electric vehicle is not considered.

¹ The adopted VKT for the start emission calculation has been corrected by a −13% factor according to Appendix 3.4-3 of Approved EIA report for Liantang / Heung Yuen Wai Boundary Control Point and Associated Works (AEIAR-161/2011).

² Hong Kong Roadmap on Popularisation of Electric Vehicles, https://www.evhomecharging.gov.hk/downloads/ev_booklet_en.pdf

- 4.5.15 In this assessment, the road has been categorized into 2 road types as summarized in Table 4-5. For roads with cold start (Type 1), both RUN emission and START emission will be adopted. For roads without cold start (Type 2), only RUN emission will be adopted. It should be noted that, Franchised Buses (FBSD & FBDD) are not expected to perform cold start on normal public roads. Therefore, the START emission for FBSD & FBDD has not been included in the determination of road traffic emission. Instead, the cold start emissions of the Buses will be handled separately.
- 4.5.16 There are industrial buildings fall within the 500m assessment area, with loading/unloading/parking areas for heavy vehicle. In addition, there are terminus for public light buses (Cheung Sha Wan Bus Terminus) at around 150m in the west of site B. As the current broad brush approach assumed the start emission from vehicles (except FBSD & FBDD) happened in all the Type 1 road (including the Cheung Sha Wan Road, which is the major road adjoining the Sites A & B), and the highest START emission across various soak time has been adopted (except FBSD & FBDD), the current approach is considered conservative. The list of roads for the air quality impact assessment including the cold start availability has been included in Appendix 4-1.

Table 4-5 Road Types within the Study Area

Road Type	Description	
Type 1	Roads with cold start	
Type 2	Roads without cold start	

- 4.5.17 For mapping the corresponding emission factor to each road section more precisely, the yearly temperature and relative humidity from Hong Kong Observatory has been broken into 4 seasons, namely Q1: Dec-Feb, Q2: Mar-May, Q3: Jun-Aug, & Q4: Sep-Nov. Daily profiles for each season with the lowest hourly temperature and relative humidity in each season (Table 4-6) has been adopted to identify the corresponding hourly emission factors for each road section conservatively. Then, the hourly road traffic emission of each road section was calculated by multiplying the vehicle counts, road length and the corresponding emission factor.
- 4.5.18 Finally, sensitivity testing has been conducted by comparing the daily road traffic emissions under 4 seasons of different scenarios (i.e. traffic flow for years 2034, 2042 and 2049). The year with the highest daily emission has been be adopted as the assessment year for the respective pollutant.

	Q1		(Q2		Q3	Q4	
Hour	Temp (°C)	RH (%)	Temp (°C)	RH (%)	Temp (°C)	RH (%)	Temp (°C)	RH (%
1	8	27	16	37	24	77	18	40
2	8	28	16	36	24	76	17	47
3	8	29	16	38	23	69	17	45
4	7	32	15	39	24	70	16	43
5	7	26	15	37	24	76	16	38
6	7	25	16	36	23	74	16	37
7	7	24	16	35	23	76	16	35
8	7	24	16	33	23	74	15	37
9	8	21	16	27	24	68	16	39
10	9	19	15	23	24	63	17	37
11	10	15	16	22	25	56	18	36
12	11	13	16	19	26	54	19	39
13	12	16	16	19	25	56	21	40
14	12	17	16	20	25	53	21	41
15	13	18	16	27	26	55	21	44
16	13	17	16	29	25	58	21	41
17	10	20	16	32	25	60	20	42
18	10	21	16	34	25	63	19	40
19	10	21	16	35	25	69	19	38
20	10	22	17	36	25	72	19	34
21	11	22	16	31	25	73	18	37
22	10	20	17	25	24	72	18	34
23	10	25	16	31	24	75	18	36
24	9	24	16	33	24	78	18	39

Table 4-6 Diurnal Temperature and Relative Humidity Profile for each Seasons

Methodology - CALINE4

- 4.5.19 The total hourly road traffic emission of each road section has been divided by the total hourly vehicle count and the road length (in <u>Mile</u>) to obtain the hourly fleets averaged emission factors (emission/Vehicle Mile Travelled, in g/VMT).
- 4.5.20 The hourly fleets averaged emission factors in each season together with the hourly traffic flow of each link (road section) were then utilized in CALINE4 to simulate the dispersion of the vehicle exhaust pollutants from the surrounding open road network.
- 4.5.21 The surface roughness adopted in CALINE4 is 370cm according to EPD's recommendation for urban area. The molecular weight for NO_x & NO₂ in CALINE4 is 46.

Cold Start Emission for Franchised Buses (FBSD & FBDD) - AERMOD

- 4.5.22 According to Calculation of Start Emissions in Air Quality Impact Assessment (EPD, Jan 2021), the start emission of diesel vehicles with SCR should spread over 700m.
- 4.5.23 The identified buses from the bus terminus (Cheung Sha Wan Bus Terminus) and the adopted Road ID are illustrated in Figures 4-3a & 4-3b, respectively. The bus schedule is list in Appendix 4-4. Although there is no bus schedule for 2034-2049 available at the moment, considering the current tendency and the policy, the number of diesel-powered buses should not increase, if not reduce. It is because the diesel-powered buses will be gradually replaced by electric-powered buses. Using the existing bus schedule for the cold start emission calculation in the future is considered conservative.

The hourly temperature and relative humidity at King's Park during year 2020 (rounded-down to the nearest integer) have been adopted.

- 4.5.24 For consistence with other road traffic emission, the assessment years are chosen as Year 2049 for NOx/NO₂ emission and 2034 for RSP/FSP. As a conservative assessment, the start emission of diesel FBDD at the lowest temperature (7 °C) will be adopted. From on-site survey, it is found that soak time of the buses are either <30 minutes or overnight (actual soak time unknown). Therefore, soak time of 30 minutes (7:00 − 1:00) and 720 minutes (5:00 − 7:00) have been adopted. The adopted emission factors for buses are list in **Table 4-7**. The emission elevation and initial vertical mixing height of the buses has been referenced to Appendix 3.6 of Revised Austin Road Flyover EIA Report. The adopted emission rate for each road sections are listed in **Appendix 4-4**.
- 4.5.25 Dispersion modelling has been be undertaken using USEPA approved AMS/EPA Regulatory Model (AERMOD) to assess the Marine Emission.

Table 4-7	Adopted Emission	Factory	for Buses'	Cold Start Emission

Pollutant	NOx	NO2	RSP	FSP
Year	2049	2049	2034	2034
Temperature (deg C)	7	7	7	7
Vehicle Type	FBDD (DSL)			
Soak Time (min)		Emission pe	r trip (g/trip)	
30	1.1379	0.3300	0.0000	0.0000
720	10.7100	3.1059	0.0000	0.0000

Industrial Chimney within 500m assessment area

- 4.5.26 As stated in Sections 2.2.2-2.2.3, active chimneys are identified in the Caritas Medical Centre. However, those chimneys are either not active (for standby emergence generator) or using clean fuel (Town Gas). Therefore, those chimneys are not included in the quantitative assessment.
- 4.5.27 Besides the Caritas Medical Centre, no active industrial chimney has been identified within the assessment area.

Major emission sources within 4 km

4.5.28 The nearest major emission sources are: Kwai Chung Crematorium (3983m), & To Kwa Wan Gas Plant (4396m). As both of them are ~4km from the Scheme, and their source strength are relatively small (compare to other major source such as cruise terminal). Therefore, no major emission sources are included in the quantitative assessment.

Cumulative Pollutant Concentration

4.5.29 The cumulative pollutant concentration at each of the assessment point has been calculated by summing the background concentration (from PATH-v2.1)³, the road traffic emission (from CALINE4), and other emissions (from AERMOD). It should be noted that background

³ Different background concentration from PATH-2016 has been adopted based on the elevation of the assessment point. i.e. L1: 0 to 17mAG; L2: 17 to 35mAG; L3: 35 to 55mAG.

- vehicular, industrial and marine emissions have been included in PATH-v2.1, adding the emissions from CALINE4 and AERMOD will result in conservative results.
- 4.5.30 The Ozone Limiting Method (OLM) and maximum equilibrium NO₂:NO_x ratio of 0.9 ⁴ has been adopted for the conversion of NO_x to NO₂ based on the hourly O₃ concentrations predicted by PATH-v2.1 in the corresponding grid.
- 4.5.31 The NO₂/NO_x conversion has been calculated as follows:

[NO₂]_{pred} = Min{ [NO₂]_{init} + MIN {[NO_x]_{pred} - [NO₂]_{init}, (46/48) × [O₃]_{PATH} }, 0.9 x [NO_x]_{pred}} where,

[NO₂]_{pred} is the predicted cumulative NO₂ concentration

[NO₂]_{init} is the sum of initial NO₂ concentration from CALINE4, AERMOD and PATH v2.1 [NO_x]_{pred} is the sum of predicted NO_x concentration from CALINE4, AERMOD and PATH v2.1

[O₃]PATH is the O₃ concentration from PATH v2.1

- 4.5.32 For all vehicle emissions, the calculated initial NO₂ concentration based on NO₂ emission factor of Emfac v4.3 has been adopted. For all non-vehicular emissions, initial NO₂/NO_x ratios reported in the Heathrow Airport EIA report are adopted, which is 10%.
- 4.5.33 Due to the nature of OLM, and conservative approach for the traffic emission and PATH-v2.1 background, the cumulative NO₂ concentration at each ASR is considered very conservative.

Results and Discussion

- 4.5.34 The detailed results are listed in Appendix 4-5. The summary of the annual NO₂ concentration is provided in Appendix 4-6. The results are also summarized in Table 4-8 & Table 4-9.
- 4.5.35 The assessment result shows that, apart from Annual Averaged NO₂ concentration at ground of southeastern boundary of Site A (1.5mAG at AP-03, AP-04 & AP-05), other assessment points at Site A and Site B show compliance with AQO's NO₂/RSP/FSP criteria.
- 4.5.36 Under current notional design, the predicted air quality at all residential flats comply with the AQOs. The fresh air in-take for the podium structures of Site A would be designed to be located at or above 6.35mAG (11.4mPD). The fresh air in-take for the G/IC complex at Site B should not be restrained by air quality. Subject to the CE in C's approval of the draft DSP, URA/ future joint venture partner should explore and implement all practicable design in order to ensure all openable windows for ventilation and fresh air intakes comply with the AQO criteria at the detailed design stage.
- 4.5.37 It should be noted that the exceedance is partially due to the conservative approach. Considering the Government's measures to promote the use of electric vehicles, it is expected that the future background pollution concentration as well as the road traffic emission should be much lower than that in the current calculation up on complete of the Scheme (Year 2034).

Additional Clarification Regarding Application of Appendix W Modeling Guidance for the 1-hour NO2 NAAQS", U.S. EPA, March 1, 2011

Table 4-8 Summary of the Predicted Pollutant Concentration

	Pollutant Concentration (µg/m³)									
	Daily 10th Maximum RSP	Annual RSP	Daily 36th Maximum FSP	Annual FSP	Hourly 19th Maximum NO2	Annual NO ₂				
Criteria	100	50	50	25	200	40				
Podium T1	62.56 -	27.20 -	23.75 -	23.08 -	130.94 -	23.08 -				
	63.76	28.13	24.82	43.92	177.14	43.92				
Podium T2	62.08 -	26.97 -	23.31 -	19.22 -	116.64 -	19.22 -				
	62.51	27.17	23.75	22.32	128.52	22.32				
Low Block	62.09 -	26.98 -	23.31 -	19.27 -	116.62 -	19.27 -				
	62.60	27.21	23.82	23.43	128.85	23.43				
Tower T1	62.53 -	27.17 -	23.77 -	22.27 -	124.09 -	22.27 -				
	63.67	27.76	24.79	34.70	155.46	34.70				

Table 4-9 Summary of the Predicted Annual Averaged NO₂ Concentration

		A	nnual Av	eraged N	O2 Cone	centratio	n (μg/m³)	at differ	ent Heig	ht
Location	mAG	1.5	6.35	10.85	14.5	18	21.5			
	mPD	6.55	11.4	15.9	19.55	23.05	26.55			
Site A - Podium	min	34.40	32.91	29.69	27.97	23,80	23.08	11 - 1	11	
	max	43.92	33.92	31.01	29.32	24.86	23.84	-		
		A	nnual Av	eraged N	O2 Cone	centratio	n (μg/m³)	at differ	ent Heig	ht
Location	mAG	29.35	32.5	35.65	38.8	41.95				
	mPD	34.4	37.55	40.7	43.85	47				
Site A - Podium	min	21.97	21.64	19.69	19.43	19.22				
	max	22.32	21.91	19.91	19.62	19.38	11 11		= ::	- ==
Site A - Tower A	min	22.09	21.73	19.76	19.50	19.27				
	max	23.43	22.87	20.73	20.31	19.95				
		A	nnual Av	eraged N	O2 Cond	centratio	n (μg/m³)	at differ	ent Heig	ht
Location	mAG	1.5	8	11.6	15.2	18.8	22.4	26	30.5	35
	mPD	6.55	13.05	16.65	20.25	23.85	27.45	31.05	35.55	40.05
Site A - Podium	min	31.43	30.73	30.04	29.25	25.29	24.50	23.77	22.95	22.27
	max	34.70	32.91	31.55	30.26	25.97	24.96	24.10	23.22	22.49

Note: Criteria = 40 μg/m³

4.6 Conclusion

- 4.6.1 The air quality impact arising from the proposed development to the surrounding area and air quality impact from the surrounding area to the proposed development has been assessed.
- 4.6.2 With the implementation of dust suppression measures stipulated under the Air Pollution Control (Construction Dust) Regulation and the adoption of good site practice, no adverse air quality impact associated with the construction works is expected.
- 4.6.3 Air emission is not anticipated from the proposed development during operation phase. Air quality model based on the current notional design with conservative approach has been conducted. The model results show that the predicted air quality at all proposed residential flats comply with the AQOs. The fresh air intake for the podiums structure Site A would be designed to be located at or above 6.35mAG (11.4mPD). The fresh air in-take for the G/IC complex at Site B should not be restrained by air quality. The air quality upon completion of the Scheme will be similar to, if not better than, the existing situation and no insurmountable air quality impact is anticipated.

5 NOISE IMPACT ASSESSMENT

5.1 Introduction

- 5.1.1 The purpose of this chapter is to demonstrate the noise sensitive receivers (NSRs) of the proposed development within the Scheme comply with the noise criteria of The Hong Kong Planning Standards and Guidelines (HKPSG).
- 5.1.2 The potential noise impact from the following aspects have been assessed: (i) Construction noise the potential noise impact generated from the construction activities of the proposed development to the surroundings; (ii) Traffic noise the potential noise impact generated from the nearby road networks to the proposed development during operation phase; (iii) Fixed noise the potential noise impact generated from the surrounding fixed noise sources to the proposed development.
- 5.1.3 Effective mitigation measures and recommendations are proposed to mitigate the excessive noise level to achieve an acceptable compliance level under the current notional design.

5.2 Standards and Guidelines

Road Traffic Noise

5.2.1 HKPSG provides guidance on acceptable road traffic noise levels at the openable windows of various types of noise sensitive buildings. The relevant criteria are shown in **Table 5-1**.

Table 5-1 HKPSG Road Traffic Noise Planning Criteria

Uses	Road Traffic Noise L ₁₀ , (1hr) dB(A)		
Domestic Premises	70		
Hotel and Hostels	70		
Offices	70		
Educational institutions	65		
Hospital & Clinics	55		
Places of public worship and courts of law	65		

Note: The above criteria apply to noise sensitive uses which rely on opened window for ventilation.

Fixed Noise Sources

5.2.2 Acceptable Noise Levels (ANL) shown in Table 2 of the Technical Memorandum for the Assessment of Noise from Places Other than Domestic Premises, Public Places or Construction Sites (IND-TM). According to IND-TM, the ANLs for different Area Sensitivity Ratings (ASRs) are given in Table 5-2.

Table 5-2	Acceptable Noise Levels for Fixed Noise Impact (ANLs), dB(A), Leq,
	(30mins)

Time Period	ASR A	ASR B	ASR C	
Day (0700 to 1900 hours)	60	(5	70	
Evening (1900 to 2300 hours)	60	65	70	
Night (2300 to 0700 hours)	50	55	60	

- 5.2.3 The Scheme is located in the urban area of Sham Shui Po. According to TD's Annual Traffic Census (ATC2019), the daily traffic of the Cheung Sha Wan Road section (Street No. 3427) is more than 35,000. Therefore, the Scheme and its surroundings are considered directly affected by Influencing Factor (IF); the ASR of the site would be classified "C".
- 5.2.4 As the site is subject to traffic noise impact from Cheung Sha Wan Road (primary distributor road), it is expected that the prevailing background noise level would be higher than ANL-5dB for both daytime and night-time, thus ANL-5 dB would be adopted as the planned fixed noise sources criterion. The planning criteria would be 65 dB(A) for day and evening time and 55 dB(A) for night time.

5.3 Construction Noise Impact Assessment

- 5.3.1 The use of powered mechanical equipment (PME) will generate construction noise impact to the nearby NSRs. The major noise emitting activities will be the demolition of existing structures and foundation works of future development.
- 5.3.2 As the site is situated in a well-developed urban area, the number of PME that it can accommodate is limited, however, the noise from construction activities may still be an impact if the construction works are not planned and arranged properly.
- 5.3.3 The "Practice Note for Professional Persons Environmental Consultative Committee" (ProPECC) "Noise from Construction Activities –Non-statutory Controls" (PN 2/93) suggests assessment criteria relating to construction noise and some practical noise abatement measures to reduce the construction noise.
- 5.3.4 To minimize noise generation, non-percussive equipment such as hydraulic crusher is proposed for demolishing existing building and structure. Also, adoption of non-percussive piling method for foundation work is also recommended. As these activities would only last for a short period of time, significant noise impact on sensitive receivers is not expected with proper implementation of mitigation measures:
 - Adopt good site practice, such as throttle down or switch off equipment unused or intermittently used between works
 - Regular maintenance of equipment to prevent noise emission due to impairment
 - Position mobile noisy equipment in locations away from nearby NSRs and point the noise sources to directions away from NSRs
 - Make good use of other structures for noise screening
 - Use of quiet plants and working methods to mitigate at source
 - Use of mobile noise barriers/enclosures along the path of noise propagation
 - Schedule work to minimize concurrent activity and duration of impact

5.3.5 With the aforementioned noise mitigation measures implemented during the construction phase, no adverse noise impact arising from the construction activities is expected.

5.4 Operation Noise Impact Assessment

Representative Noise Sensitive Receivers during Operation Phase

Road Traffic Noise

- 5.4.1 All flats of the residential towers were identified as NSRs according to the nature of use. Commercial & retail area, clubhouse and GIC facilities in the podium and the G/IC complex will be provided with air-conditioning system and will not rely on openable windows for ventilation, and thus the noise standard is not applicable. The noise assessment points were located 1.2m above the slab level and 1m away from the façade. All potential windows locations of all residential flats are covered.
- 5.4.2 There are (Tower A (Low Zone): 22 floors x 13 flats + Tower A (High Zone): 12 floors x 12 flats + Tower B: 34 floors x 12 flats) = 838 residential flats based on the notional layout of typical floor. It should be note that the Tower A consist of high zone and low zone, with identical Flat 01- 08 and different Flat 09 13. To avoid confusion, high zone and low zone are using different flat IDs and assessment points IDs.
- 5.4.3 For assessment purpose, the traffic noise level at all 838 flats have been assessed. The representative assessment points are summarized in Table 5-3 and their locations are illustrated in Figures 5-2a, 5-2b & 5-2c. It should be noted that the notional layout of the Scheme is for assessment purpose only and subjected to change.

Planned Fixed Noise Sources

5.4.4 Large building service equipment of Site A & B are the potential planned fixed noise during operation phase of the Scheme. It should be noted that there are no representative NSR in the north, west and south from Site B has been selected as the NSRs are either very far or the view to Site B are completely blocked. The representative NSRs of the proposed residential developments and in the surrounding have been identified, listed in Table 5-4 and illustrated in Figures 5-3.

Table 5-3 Summary of Representative Noise Sensitive Receivers and Assessment Points for Traffic Noise Impact Assessment

Tower	Number of Flats per floor	NSR ID [1]	Number of Floor	Elevation of the Assessment Point [2][3]
A	13	TAL01-1 to TAL13-3 13 flats and 38 assessment points on	22 floors (1 st – 22 nd residential floor)	34.10mPD for the 1st residential floor
	each floor	1	+ 3.15m for each floor	
A 12	12 12 flats and 38 assessment points on each floor		12 floors (23 rd – 34 th residential floor)	103.40mPD for the 23 ^r residential floor
		,	+3.15m for each floor	
В	12	TB-01-1 to TB-12-3	34 floors (1st - 34th residential floor)	34.10mPD for the 1 st residential floor
- 71	assessment points on each floor	residential floor)	+ 3.15m for each floor	

NSR ID is in the form of TTXYY- Z, where "TT" is tower identity = TA or TB, "X" is zone identifier = H (High Zone), L (High Zone) or "-" (N/A, for Tower B), "YY" is flat number = 01 - 13; Z is assessment point number within a flat = 1 - 5. [1]

Representative Noise Sensitive Receivers for Fixed Noise Impact Table 5-4 Assessment

NSR ID	Daniel de	Horizontal Distance from		
	Description	Podium of Site A	G/IC Complex of Site B	
NSR01	Tower B - Flat 01	N/A	204m	
NSR02	11A Cheung Wah Street	39m	197m	
NSR03	Charming Garden	76m	155m	
NSR04	Cheung Sha Wan Catholic Secondary School	16m	244m	
NSR05	Un Chau Estate - Un Hong House	44m	272m	
NSR06 Hang Chun Court - Chun Yin House		149m	208m	

The elevation of the assessment points for the 1st residential floor = 5.05 mPD (Ground) + 25.35m (Podium & Club House Height) + 2.5m (Transfer Plate) + 1.2m (1.2m above slab level) = 34.10mPD The notional design including the elevation is subject to change. [2]

Road Traffic Noise

Assessment Methodology

- 5.4.5 An in-house noise model (MARC) was used to predict the traffic noise levels arising from the road network. It adopts the methodology provided in the UK Department of Transport's Calculation of Road Traffic Noise (CRTN) 1988, which is stipulated in Chapter 9, Section 4.2.7 of the HKPSG for assessing road traffic noise impact. Road traffic noise levels are presented in terms of noise levels exceeded for 10% of the one-hour period for the hour having the peak traffic flow [L10 (1-hour) dB(A)].
- 5.4.6 The assessment was based on the projected peak hour flows for the worst year within 15 years after completion of the Project in Year 2034. Based on the traffic forecast provided by the traffic consultant, the AM peak hour flows in Year 2049 will be the maximum projected peak hour traffic flow within 15 years from the completion of the Scheme. The major roads within 300m from the boundary of the Scheme have been included in the assessment and are shown in Appendix 5-1.
- 5.4.7 To minimize the traffic noise impact to the Scheme, the following architectural design consideration has been adopted:
 - Both Towers A & B have been setback from the major road traffic from the road traffic noise.
- 5.4.8 Two scenarios have been considered in the traffic noise impact assessment. The first one is a (A) Base Scenario which only considered architectural design and location of the openable windows; the second scenario is a (B) Mitigated Scenario with Acoustic Windows.

Impact Identification and Assessment

- 5.4.9 The peak hour traffic flow of individual roads in the assessment year (Year 2049) is listed in Appendix 5-1. The traffic forecast has been submitted to the Transport Department for their endorsement. As hourly traffic flow of AM Peak are higher than that of PM Peak, especially for the nearby primary distractor road Cheung Sha Wan Road, thus the traffic noise for AM peak hours were calculated.
 - a) Base Scenario: Careful Buildings Disposition & Windows Locations
- 5.4.10 In the Base Scenario, residential towers have been arranged to have setback from the main roads (i.e. Cheung Sha Wan Road) and in the way that the view angle from the windows to the main road has been minimized by buildings deposition, buildings orientation and windows locations. Without this design, the traffic noise level in the base scenario is expected to be much higher.
- 5.4.11 The detailed results of Base Scenario are presented in **Appendix 5-2**. This Base Scenario results in about 17% flats complying with the noise criteria of 70 dB(A). The maximum exceedance is 9 dB, i.e. 79 dB(A), at the 1st 3rd residential floor of Flat TB-01 & TB-12 of Tower B, which having a wide view angle to Cheung Sha Wan Road.
- 5.4.12 The maximum traffic noise exceedance of each facdes under Base Scenario are illustrated in Figure 5-4a 5-4c.

- b) Mitigated Scenario: With Acoustic Windows
- 5.4.13 Subject to detailed design, mitigation measures are proposed in this mitigated scenario:
 - Top-hung Type Acoustic Window (Noise Reduction: -5 dB(A))
 The design of a top-hung window with a horizontal fin on the bottom of the window coupled with Micro-perforated absorbers (MPA) on the inner side of the window and a pelmet in the indoor area behind the top-hung window, can effectively resist noise from entering domestic premises directly and hence minimize the impact caused to the residents. The design is similar to the type adopted in Hong Tsuen Road Residential Development at Sai Kung (Park Mediterranean). The ratio of vertical distance from opening of the top-hung window to the length of the horizontal acoustic fin (aspect ratio) will be less than the aspect ratio (0.55) of the acoustic window in Park Mediterranean.
- 5.4.14 Top-hung Type Acoustic Window⁵ has been proposed in the current assessment as it has been adopted and well proven in private housing for years. Therefore, the calculated traffic noise level is reliable and conservative.
- 5.4.15 It should be noted that at-receiver mitigation measure with higher acoustic performance exist. However, their noise reduction effect and ventilation performance are highly depended on the detailed design. For example, the Baffle Type Acoustic Windows⁶ broadly adopted in public house in recent years can reduce the traffic noise by 4-8 dB depended on the dimensions of the room and windows. With acoustic linings, suitable orientation and nearby acoustic fins, its noise reduction effect could be even higher. The major issue of adopting Baffle Type Acoustic Windows at the current stage is that, with room dimension may be significantly changed in the later stage, it is hard to estimate whether any combination of window pane separation, windows height, window opening and windows overlapping, etc. can provide both sufficient ventilation and acoustic performance. Therefore, adopting Baffle Type Acoustic Windows at the current stage may lead to under-estimate of acoustic performance if we go for conservative, or lead to impossible scenario if the adopted acoustic performance is too optimistic.
- 5.4.16 Despite the uncertainties, the use of acoustic windows with higher noise reduction effect is encouraged in detailed design stage. As more information is available at that stage for the designer/engineer to choose the most suitable acoustic windows design with consideration of both acoustic and air ventilation performance.
- 5.4.17 Section drawings of the typical Top-hung Type Acoustic Windows with/without balcony are illustrated in **Figures 5-5a & 5-5b**. Mitigation measures have been proposed to all locations with traffic noise exceedance. The locations of the proposed mitigation measures are illustrated in **Figures 5-6a 5-6c** and listed in **Appendix 5-3**.
- 5.4.18 The detailed predicted noise levels with acoustic windows are presented in **Appendix 5-3**. Given specific noise reduction measures at different assessment points, the compliance rate by flat has been increased to ~80%. Only low-mid level residential flats that directly affected by the traffic noise from Cheung Sha Wan Road are expect to experience traffic noise exceedances, while it is expected to completely comply at higher level (23rd residential floor or higher). The maximum exceedance is 4 dB, i.e. 74 dB(A), at the 1st 3rd residential floor

https://www.epd.gov.hk/epd/Innovative/greeny/eng/content/king-tai-court.html?type=ftab 20

⁵ Sample for Top-hung Type Acoustic Window https://www.epd.gov.hk/epd/Innovative/greeny/eng/content/hong-tsuen-road-residential-development-sai-kung.html?type=ftab_21

⁶ Sample for Baffle Type Acoustic Windows

of Flat TB-01 & TB-12 of Tower B. The exceeded facades under Mitigated Scenario are highlighted in Figures 5-6a – 5-6c.

Table 5-5 Summary of Traffic Noise Impact Assessment

	Number of Flat	Base S	cenario	Mitigated Scenario		
		Complied Flat	Compliance Rate	Complied Flat	Compliance Rate	
Tower A - Low Zone	286	45	15.7%	202	70.6%	
Tower A - High Zone	144	24	16.7%	144	100.0%	
Tower B	408	70	17.2%	328	80.4%	
Total	838	139	16.6%	674	80.4%	

Existing Fixed Noise Sources in the Surroundings

- 5.4.19 For the fixed noise sources in the surrounding affecting the proposed Scheme, no adverse fixed noise impact is anticipated and no quantitative assessment is necessary due to the following information:
 - As stated in the overview of the existing potential fixed noise sources to the Sites (Section 2.2), majority of the Site A is not expected to experience adverse impact from existing fixed noise sources. More specifically, Site A is surrounded by residential building in west, north and east directions. In the south of Site A, it is a large open area (Sham Shui Po Sport Ground) and potential fix noise sources in south to south west directions are either weak (the loud speaker within the covered stand of Sport Ground) or very far (in the west of Site B). Some high-level flats may have direct view to the chiller plants on the roof of China Shipbuilding Tower. If necessary, the project proponent will provide noise mitigation measure on sources to mitigation this potential noise impact.
 - Although Site B may suffered from potential fixed noise impact, Site B do not rely on openable windows for ventilation thus fix noise criterion is not applicable.

Planned Fixed Noise Sources of the Scheme

5.4.20 The Scheme will provide central air ventilation for commercial & retail area, clubhouse, GIC facilities and basement carpark. The associated HVAC system may cause noise impact to surrounding NSRs. Although the large exhaust fans are usually located indoor enclosed within the air ducts, the fan noise will transmit via the ventilation pipe and emit at the duct exhaust. Therefore, the potential planned fixed noise sources of the Scheme are the large exhaust fans and the outdoor units of air conditioner. Other equipment such as water pumps and lift motors will be located in enclosed rooms thus no adverse noise impact to the surrounding is anticipated.

Site A

5.4.21 For Site A, the non-residential portion will be closed outside operation hours and the associated HVAC system are expected to stop during night time. Besides, the expected ventilation requirement of the basement carpark during night-time is expected to be very low thus the primary exhaust fan is unlikely required. Due to the relatively small size of the served zones, Variable Refrigerant Volume (VRV) system is preferred over chiller plants and/or water-cooling tower as VRV provide flexible cooling capacity with high efficiency over large range of loading. To avoid the noise from fixed plants affecting the residential portions, the large plants and large ventilation exhaust pipes are planned to be located at semi-confined areas such as plant rooms and/or entrance/exit of the carpark, with acoustic louvers if necessary. The ventilation pipes will be equipped with silencer to reduce the induct noise level. As there is no direct line of sight between the fixed noise sources of Site A and the residential flats of Site A, no adverse noise impact from the fixed noise sources of Site A to the residential flats of Site A is anticipated. As the fixed noise source of Site A, including the louvers serving the fixed noise sources, may visible from the NSRs in the surrounding, maximum allowable sound power levels will be recommended.

Site B

5.4.22 For Site B, chiller plants and large ventilation exhaust pipes are also planned to be located at semi-confined areas. The ventilation pipes will also be equipped with in-line silencer to reduce the in-duct noise level. As the fixed noise source, or the louvers connected to the fixed noise sources, of Site B may visible from the NSRs in the surrounding, including the NSRS in Site A. Maximum allowable sound power levels will also be recommended.

Maximum Allowable Sound Power Levels (SWL)

- 5.4.23 Calculations based on the planning criteria and distance to the nearest NSRs are present in **Table** 5-6.
- 5.4.24 According to the calculation based on the nearest NSR (NSR04 for Site A and NSR03 for Site B), the cumulative SWL of the building service equipment at podium of Site A should not exceed 88 dB(A) during day and evening time, and should not exceed 78 dB(A) during night time. For the G/IC complex in Site B, the limits of the cumulative SWL are 108 dB(A) during day and evening time, and 98 dB(A) during night time.
- 5.4.25 It should be noted that a 6 dB correction has been adopted accounting for the tonality, intermittency and impulsiveness characteristics for assessment purpose. In case the noise exhibits tonality, intermittency and impulsiveness characteristics during the operation, the maximum allowable SWLs of the fixed plants should be corrected based on the recommendation given in Section 3.3 of the IND-TM.
- 5.4.26 Although the Scheme is still in early stage thus no detailed design including the location of the noisy plants is available, no adverse fixed noise impact to the NSRs is anticipated if the choice of equipment, installation locations, installation and mitigations are properly designed. To ensure the compliance in the final design, the project proponent (URA) should incorporate the fixed source noise planning criteria, i.e. At NSR noise level of 65 dB(A) for day and evening time and 55 dB(A) for night time in Leq,30min, to the tender document of this Scheme.

Table 5-6 Allowable Sound Power Level for the Building Service Equipment of the Proposed Development

Time Period	Maximum	Horizontal Distance from the		Maximum Allowable Sound Power		
	Allowable SPL at NSR, dB(A)	Project Site Boundary to the Nearest NSR, m	Distance	Facade	Tonality/ Intermittency/ Impulsiveness [1]	Level at Source, dB(A)
		Site A (Nea	rest NSR - NS	SR04)		
Day and Evening Time (07:00-23:00)	65	16	32	-3	-6	88
Night Time (23:00 – 07:00)	55	16	32	-3	-6	78
		Site B (Nea	rest NSR - NS	SR03)		
Day and Evening Time (07:00-23:00)	65	155	52	-3	-6	108
Night Time (23:00 – 07:00)	55	155	52	-3	-6	98

For assessment purpose, a 6 dB of tonality, intermittency & impulsiveness correction has been adopted.

[2] The Maximum Allowable Sound Power Level at Source should be corrected by the tonality, intermittency, & impulsiveness correction of the selected equipment, according to Section 3.3 of the IND-TM.

5.5 Conclusion

- 5.5.1 The overall noise impact during the construction phase is considered insignificant. Mitigation measures shall be implemented in accordance with ProPECC PN 2/93 during construction to minimize construction noise impact on the nearby NSRs.
- 5.5.2 Traffic noise impact has been taken into consideration when designing the notional layout of the residential development. The view angle from the windows to the road traffic has been minimized by buildings deposition, buildings orientation and windows locations. In the base scenario where tower setback, buildings deposition, buildings orientation and windows locations are considered, only ~17% of flats complies with the 70 dB(A) traffic noise assessment criterion as demonstrated. In the mitigated scenario where acoustic windows are considered, the compliance rate by flat has been dramatically increased to ~80%. Given the notional design is at planning stage and the proposed development is subject to detailed design upon CE in C's approval of the Scheme, the current assessment is based on a notional design and anticipated results. It should also be noted that the traffic noise assessment is based on a typical Top-hung Type Acoustic Window. By using acoustic windows with higher noise reduction performance in the detail design stage, it is feasible to achieve a higher compliance rate.
- 5.5.3 A preliminary study of fixed noise sources based on the existing situation and the available information for planned developments show that no adverse fixed noise impact to the Scheme is anticipated.
- 5.1 The existing significant fixed noise sources are only identified in the west of Site B which is far away from the residential portion of the Scheme in Site A, which rely on openable windows for ventilation. The planned fixed noise source from the proposed Scheme should not introduce adverse noise impact to the surroundings with proper design. To ensure the compliance in the final design, the project proponent (URA) should incorporate the fixed source noise planning criteria to the tender document of the Scheme.

6 WASTE MANAGEMENT CONSIDERATION

6.1 Legislations and Requirements

- 6.1.1 In general, sustainable approaches to waste management should be adopted to produce less waste and reuse or recover value from waste. The consideration on waste management for the Project will take into account of the below Ordinances/Guidelines/Practice Notes adopted in Hong Kong.
- 6.1.2 The following legislations/guidelines related to the handling, treatment and disposal of waste in Hong Kong are listed:
 - Waste Disposal Ordinance (Cap. 354) (WDO)
 - Waste Disposal (Chemical Waste) (General) Regulation (Cap. 354C)
 - Waste Disposal (Charges for Disposal of Construction Waste) Regulation (Cap. 354N)
 - Land (Miscellaneous Provisions) Ordinance (Cap. 28)
 - Code of Practice on the Packaging, Labelling and Storage of Chemical Waste
 - Air Pollution Control Ordinance (Control of Asbestos (sections 51 to 84))
 - ProPECC PN2/97 Handling of Asbestos Containing Materials in Buildings
 - ADV-19 Practice Note for Authorized Persons, Registered Structural Engineers and Registered Geotechnical Engineers – Construction and Demolition Waste
 - ADV-21 Practice Note for Authorized Persons, Registered Structural Engineers and Registered Geotechnical Engineers – Management framework for Disposal of Dredged/Excavated Sediment
 - ETWB TCW No. 34/2002 Management of Dredged/Excavated Sediment
 - Code of Practice on the Handling, Transportation and Disposal of Asbestos Wastes
- 6.1.3 Waste collection and disposal is covered by the Waste Disposal Ordinance (Cap. 354) (WDO). This provides a licensing system for the disposal of certain wastes and for the control of certain wastes by regulation. All wastes should be properly stored and disposed in accordance with relevant waste management regulations and guidelines.
- 6.1.4 Waste Disposal (Chemical Waste) (General) Regulation (Cap. 354C) outlines the requirement for chemical waste handling and disposal.
- 6.1.5 Under the Waste Disposal (Charges for Disposal of Construction Waste) Regulation (Cap. 354N), construction waste delivered to a landfill for disposal must not contain more than 50% by weight of inert materials. Construction waste delivered to a sorting facility for disposal must contain more than 50% by weight of inert materials, and construction waste delivered to a public fill reception facility for disposal must consist entirely of inert materials.
- 6.1.6 Land (Miscellaneous Provisions) Ordinance (Cap. 28) provides control over placing and maintaining of C&D materials on unleased land. If the occupier does not hold the relevant license, the Department of Lands will take action accordingly.
- 6.1.7 Both the Practice Note for Authorized Persons, Registered Structural Engineers and Registered Geotechnical Engineers (ADV-21) and Technical Circular ETWB TCW No.

- 34/2002 cover the approval of dredging/excavation proposals and marine disposal of dredging/excavated sediment.
- 6.1.8 Practice Note for Authorized Persons, Registered Structural Engineers and Registered Geotechnical Engineers (ADV-19) provides mitigation measures on waste generation and management during the planning stage of a building development to minimise waste disposals at landfills.

6.2 Waste Management for Construction Phase

Waste Types

- 6.2.1 The demolition and construction activities to be carried out for the proposed development would generate a variety of waste that can be divided into distinct categories based on their composition and ultimate method of disposal. The identified waste types include:
 - Construction and demolition (C&D) materials, comprising inert and non-inert materials, from the demolition and construction works;
 - · Potential asbestos containing materials;
 - · Excavated Sediment;
 - · Chemical waste from any maintenance of construction plant and equipment; and
 - · General refuse from the workforce

Inert and non-inert C&D Materials

- 6.2.2 Inert C&D Material (or public fills) includes construction debris, soil, rock and concrete, should be re-used on-site as filling materials or off-site as public fill at public fills reception facilities. Non-inert C&D Material (or C&D waste) includes metal from the existing structures, wood from formwork, equipment parts, and materials and equipment wrappings, etc. should be re-used or recycled as far as possible.
- 6.2.3 As the Scheme involves demolition of existing buildings and construction of 2 floors of basement, there will be generation of inert C&D materials during construction. It is estimated that about 60,000 m³ excavated materials would be generated and about 10,000 m³ would be suitable for backfilling during site formation stage. It is also estimated that about 3,500 m³ C&D materials will be generated during the demolition work.
- 6.2.4 To account the quantity of C&D materials to be generated from construction of the new building, C&D materials generation rate of 0.1 m³ per m² of GFA constructed is adopted in accordance with the "Reduction of Construction Waste Final Report, Hong Kong Polytechnic University (March 1993)". The total GFA of the proposed development from the Scheme will be around 73,000 m² (Domestic: 49,372 m²; Non-domestic (Site A): 10,394 m²; Non-domestic (Site B): 33,969 m²). The C&D materials generated from superstructure construction is approximately 7,300 m³. Hence, the total amount of inert C&D materials generated by the Project is projected at 70,800 m³.
- 6.2.5 The volume of non-inert C&D material, such as maintenance and packaging waste, generated during site clearance and construction of superstructure works is projected at 1,080m³, which will be subject to specific construction procedures and site practices. The estimated amount of non-inert C&D material generated would be minimal with careful design, planning, good site management and control of ordering procedures etc.

6.2.6 The estimated quantities of inert and non-inert C&D material generated from the construction of the Scheme are presented in **Table 6-1**.

Table 6-1 Estimated Quantities of C&D materials to be Generated, Reused and Disposed of

					Wastes to be Reused/Recycled/disposed of (m³)						
	Sum (m³)	Inert C&D materials		Non-inert C&D materials			Excavated Sediment				
Construction Activities		Reused /Recycl ed On- Site	Reused /Recycl ed Off- Site	Disposed Off-Site (a)	Reused /Recycl ed On- Site	Reused/Re cycled Off-Site (b)	Disposed Off-Site	Reused/Rec ycled On- Site	Reused/Rec ycled Off- Site	Disposed Off-Site	
Excavation	60,000	10,000	0	40,000	0	0	0	0	0	10,000	
Site Clearance / Demolition of Existing Buildings	3,500	0	0	3,150	0	35	315	0	0	0	
Superstructure Construction	7,300	0	0	6,570	0	73	657	0	0	0	
All	70,800	10,000	0	49,720	0	108	972	0	0	10,000	
	1		59,720			1,080			10,000		

Note

a) The inert C&D materials not reused on-site shall be disposed off-site to the Fill Bank at Tseung Kwan O Area 137

6.2.7 It is estimated that about 14% of inert C&D material to be reused on-site. It is proposed to dispose the rest of inert C&D materials to the Fill Bank at Tseung Kwan O Area 137. The remaining non-recyclable C&D materials are not suitable for public fill and requires disposal to licensed landfill facilities (the closest landfill is the South East New Territories (SENT) Landfill).

Excavated Sediment

- 6.2.8 In addition, as the land of the Site is within reclamation ground, approximately 10,000m³ of excavated sediment is estimated to be generated and disposed off-site from the Project. The marine disposal of the sediment should be disposed in accordance to the ETWB TCW No. 34/2002 and ADV-21. The rationale for sediment removal must be provided to the Secretary of MFC for agreement, as early as possible, the allocation of sediment disposal space at sea will not be considered until the need for removal of the sediment has first been satisfactorily demonstrated.
- 6.2.9 To minimize waste generation and off-site disposal, Sediment should be reused on-site as far as possible. However, if Sediment cannot be reused on-site or on alternative sites, marine dumping of Sediment is required. For Sediment dumping, the Contractor who will be undertaking the works must make a formal application to DEP for a dumping permit, in accordance to ETWB TC(W) No. 34/2002, and if the permit is granted, it will be the contractor's responsibility to ensure that the permit conditions are met to DEP's satisfaction. All necessary documents (i.e. SSTP, PSQR / SQR) must be submitted to EPD for agreement before the Marine Fill Committee can allocate the Sediment Disposal Site for the marine dumping.

b) Non-inert C&D materials should be reused or recycled as much as possible before disposed off-site, estimated to be 10% of the total generated.

Chemical Waste

- 6.2.10 Chemical waste, such as cleaning fluids, solvents, spent lubricants and fuel for equipment or waste battery, may be generated. As far as the scale of the works is small, the quantity of chemical waste generated would be minimal. It is expected that the approximate quantity of the lubrication oil is about 100L/month and hence approximately 6 m³ of chemical waste will be generated during construction period of 60 months (general assumption of construction time for URA redevelopment projects adopted). A licensed collector should be employed to handle and dispose of the chemical waste. Furthermore, the chemical waste should be handled in accordance with the Waste Disposal (Chemical Waste)(General) Regulation. The Works Contractor should register as a Chemical Waste Producer under the WDO.
- 6.2.11 Since the existing structure (Cheung Sha Wan Sports Centre) to be demolished was built in 1970s, asbestos containing materials may be present at the existing structures which would be demolished. Asbestos investigation would be carried out before the commencement of demolition works. Asbestos investigation and asbestos abatement plan will be made in accordance with Air Pollution Control Ordinance, Waste Disposal (Chemical Waste) (General) Regulation and other Codes of Practice listed in Appendix III in ProPECC PN2/97 Handling of Asbestos Containing Materials in Buildings if any asbestos is found in the Site.
- 6.2.12 In addition, other chemical waste, if any, to be generated during the demolition works will be handled and disposed of in accordance with the Waste Disposal (Chemical Waste) (General) Regulation (Cap. 354C). For asbestos wastes, if any, will be handled and disposed of in accordance with the Code of Practice on the Handling, Transportation and Disposal of Asbestos Wastes.
- 6.2.13 With the implementation of proper chemical waste management measures listed in Section 6.2.25, the impact is anticipated to be insignificant.
- 6.2.14 No hazardous materials or hazardous wastes are expected to be generated during the construction of the Site.

General Refuse

- 6.2.15 General refuse such as food scraps, waste paper, empty containers, etc., would be generated from construction workforce during construction phase.
- 6.2.16 The maximum number of construction workers to be employed will be approximately 100 workers per day. The daily arising of general refuse from the construction workforce can be estimated based on a generation rate of 0.65kg per worker per day, the estimated quantity of the general refuse is 65kg (= 100 workers x 0.65kg/worker/day).
- 6.2.17 Such refuse should be properly managed so intentional or accidental release to the surrounding environment does not occur. If the general refuse is recyclable, such as paper, plastics and aluminum materials, the reuse and recycling of such waste is encouraged. Effective collection of site wastes such as providing enclosed bins or compaction units would be required to prevent waste materials being blown around by wind, flushed or leached into nearby waters, or creating an odour nuisance or pest and vermin problem. Waste storage areas should be well maintained and cleaned regularly.

6.2.18 With the implementation of good waste management practices as suggested in Section 6.2.24 at the site, adverse environmental impacts are not expected to arise from the storage, handling and transportation of general refuse generated by construction workers.

Mitigation Measures

6.2.19 Prior to the commencement of the construction works, the contractor will identify the types and amount of waste generated, and handle, store, collect and dispose waste in accordance with Waste Disposal Ordinance (Cap. 354). The associated mitigation measures and good site practice should be implemented as follows:

C&D Materials

- 6.2.20 In general, minimization/reuse/recycling of C&D materials (i.e. both inert and non-inert C&D materials) should be considered prior to disposal. Waste minimization measures should be adopted during construction phase, measures may include:
 - · On-site sorting of C&D materials;
 - · Recycling of construction materials for on-site use;
 - Avoidance and minimization to reduce the potential quantity of C&D materials generated;
 - Reuse of materials as practical as possible;
 - Recovery and Recycling as practical as possible;
 - Provide training to workers on the importance of appropriate waste management procedures, including waste reduction, reuse and recycling.
- 6.2.21 The Contractor should submit a waste management Plan (the Plan) to the project proponent for agreement, covering the types of waste and their estimated quantities, timing of waste arising; measures for reducing waste generation etc. as recommended in Section 3 of ADV-19. If the project will produce more than 300,000 m³ of construction and demolition material, advice from the Director of Environmental Protection should be sought prior to the acceptance of the Plan.
- 6.2.22 The Contractor should adopt good housekeeping practices such as waste segregation prior to disposal. Stockpiling and segregating areas should be provided at site. Effective collection of site wastes would be required to prevent waste materials being blown around by wind, flushed or leached into nearby waters, or creating an odour nuisance or pest and vermin problems. Waste storage areas should be well maintained and cleaned regularly.
- 6.2.23 During inclement weather (e.g. heavy rainstorm), the stockpile should be covered by tarpaulin or other water-resistant fabric. This can prevent dust and waste from being blown away by wind or washed into watercourses/drainage system.

General Refuse

6.2.24 General refuse should be stored in enclosed bins or compaction units separate from C&D materials. 3-color recycle bins for the collection of recyclable municipal waste should also be provided. A reputable waste collector should be employed by the Contractor to remove or recycle general refuse from the Site, separately from C&D materials. Preferably an enclosed and covered area should be provided to reduce the occurrence of "wind-blown" light materials.

Chemical Waste

- 6.2.25 If chemical waste is produced at the construction site, the Contractor will be required to register with the EPD as a chemical waste producer and to follow the guidelines stated in the Waste Disposal (Chemical Waste) (General) Regulation (Cap. 354C). Chemical waste should be stored in appropriate containers and collected by a licensed chemical waste collector. The chemical waste management measures should include, but not limited to the following:
 - Minimize the production of Chemical Waste
 - Registration of Chemical Waste Producers with EPD should be carried out for any person who produces chemical waste
 - Give notification of certain Chemical Waste for Disposal to EPD as required in Section 4 of the Regulation & Section 17 of the Ordinance
 - Carry out Packaging, Labelling and Storage of Chemical Wastes as per Sections 9 to 19
 of the Regulation
 - Collection of Chemical Waste and the "Trip Ticket" System as per Sections 20 to 29 of the Regulation
 - Precautions Against Dangers from Spillages, Leakages or Accidents involving Chemical Waste as per Sections 30 to 32 of the Regulation
- 6.2.26 Provided that good site practices are strictly followed, there would be no adverse impacts related to waste management during construction phase.

6.3 Waste Management for Operation Phase

- 6.3.1 Domestic wastes will be expected as the major type of waste from the redevelopment, including food residues, plastic and metal products, and paper. No chemical or hazardous waste is anticipated. Wastes generated will be collected and disposed of on a regular basis. Building management will be arranged by the future owners to manage the development including waste disposal.
- 6.3.2 As the domestic waste will be collected (at a refuse collection point) and regularly disposed of at landfill or regularly sent to recyclers, waste recycling would be carried out during operation phase. Adverse impacts due to waste management will not be anticipated.

6.4 Conclusion

6.4.1 A variety of wastes including inert C&D material, C&D waste, chemical waste, asbestos-containing materials, excavated sediment, and general refuse would be generated during the construction phase and domestic waste would be generated during operation phase. Provided that the wastes generated would be managed with appropriate measures, no adverse environmental impacts arising from the handling, storage, transportation or disposal of the wastes generated during the construction and operation stage of the Scheme would be envisaged.

7 POTENTIAL LAND CONTAMINATION

7.1 Introduction

7.1.1 This chapter identifies and evaluates any potential land contamination impact within the scheme boundary of the proposed development. Preliminary assessment has been conducted with reference to the applicable legislation and guidelines.

7.2 Legislations, Standards & Guidelines

- 7.2.1 Legislations and guidelines related to land contamination are given below:
 - Environmental Impact Assessment Ordinance (Cap. 499);
 - Waste Disposal (Chemical Waste) (General) Regulation (Cap 354C);
 - Dangerous Goods Ordinance (Cap 295);
 - Practice Guide for Investigation and Remediation of Contaminated Land (PG);
 - Guidance Note for Contaminated Land Assessment and Remediation; and
 - Guidance Manual for Use of Risk-Based Remediation Goals (RBRGs) for Contaminated Land Management.

Potential Land Contamination Impact

- 7.2.2 According to Guidance Note for Contaminated Land Assessment and Remediation and EIAO-TM Annex 19 and PG, the industrial uses that may result in land contamination include but limited to the following:
 - Boat / ship building or repairing works
 - Chemical manufacturing / processing plants, dangerous goods stores power plants
 - Concrete and asphalt production
 - Golf courses
 - Motor vehicle /equipment depot, repairing, service centres
 - Open area storage
 - Petroleum Products and coal industrial operations (including oil depots and gas works)
 - Power plants, individual power generation units
 - · Scrap yards
 - Steel mills / metal workshops
 - Waste recycling workshops
 - Dumping ground

7.3 Assessment Methodology

- 7.3.1 With reference to the PG, Site Appraisal shall be carried out to assess the land contamination potential via the following methods for the preliminary assessment:
 - Review of available historical and recent aerial photos
 - Inquiry with the Environmental Protection Department (EPD) and Fire Services Department (FSD) on potential land contamination issues in past years

Apart from the existing Cheung Sha Wan Path Sitting-out Area, the other areas are still
occupied and inaccessible during this assessment period. As land contamination issue
arising from the sitting-out areas are not expected, site walkover is not carried out for
this assessment. Nevertheless, the Sites shall be re-appraised upon land resumption.

7.4 Site Appraisal

Aerial Photos

7.4.1 Aerial photos between 1945, the first available year, and 2020, the latest available year, were inspected at the Map and Aerial Photograph Library of the Lands Department. Aerial photos overlaid with the boundaries of areas of concern is provided in **Appendix 7-1**. The land use history of the Site are summarised in **Table 7-1** as below:

Table 7-1 Historical Land Use

abic /-1	able 7-1 Historical Land Use			
Site	Photo No./ Reference	Observations		
Site A				
1945	681_5-4110	The Site was part of the former Cheung Sha Wan (Bay), adjacent to the reclaimed land of Cheung Sha Wan.	N/A	
1963	1963-5948	The reclamation of the land at the Site was completed. Temporary structures assumed to be c structures are recorded in the site.	Open area / Squatting	
1967	1967-5500	Temporary structures at the Site have been removed, and barren land are observed.	Open space	
1968	1968-1067	Temporary structures are observed and the land is assumed to be used open area storage of construction materials as piping materials are observed.	Storage of construction materials	
1975	1975_11994	The building for the existing Cheung Sha Wan Sports Centre was erected.		
1984	1984_56990	No significant change for the building. Some shrubs were grown on the site.	Recreational facilities (Community)	
2000	CN28212	No major change in the Site is observed.		
2020	E116762C	No major change in the Site is observed.		
Site B				
1945	1945 681_5-4110 The Site was part of the former Cheung Sha Wan (Bay)		N/A	
1967	1967-5500	The land of the Site was reclaimed and vehicles in the Site are observed.	Car park	
1968	1968-1066	The Site was generally paved. More vehicles and some open area storage of construction materials are recorded in the site.	Storage of construction	
1973	06890	No significant change was recorded.	materials / Car park	
1975	11994	The temporary structures and vehicles were removed.	Open space	
Apart from some shrubs that were being grown of Site, no major change in the Site are observed, we existing Sham Shui Po Sports Ground near the Sunder construction and the development in the		Apart from some shrubs that were being grown on the Site, no major change in the Site are observed, while the existing Sham Shui Po Sports Ground near the Site was under construction and the development in the surrounding areas was also in progress.	Open space	

Site	Photo No./ Reference Observations		Assumed Land Use	
1987 A14737		In the southwest of the Site, the construction of the existing Cheung Sha Wan Path Sitting-out Area was substantially completed and the area was fully paved apart from the landscaped areas, while the remaining area of the Site remained unchanged. The construction of Sham Shui Po Sports Ground was completed.		
1993	No significant change was recorded in the Cheung Sha		Open space / Car park	
2004	The northern boundary of the Cheung Sha Wan Path Sitting-out Area was extended. The remaining area of the Site was fully paved and was occupied by temporary structures, assumed to be site offices, and vehicles.		Open space / Car park / Office	
2015 CW114351		More temporary structures and vehicles were also recorded in the site. Open area storage of construction materials are also observed.	Open space / Car park / Office / Storage area	
2020	E053114C	More temporary structures and vehicles were recorded in the site.	Open space / Car park / Office / Storage area	

7.4.2 The review of historical land use from aerial photos has indicated that the major land use of the Sites during 1945-2020, after the lands were being reclaimed, are open space, storage area of construction materials and recreational facilities for Site A; the open space, car park, and open space for Site B. Although the previous use of open area storage was recorded at the Sites, as only inert construction materials were involved, based on findings from the aerial photos, land contamination issue arising from the land use is not anticipated.

7.5 Inquiry with EPD & FSD

- 7.5.1 Information was requested from FSD and EPD's Regional Office (West) on the history of operation and land use of the sites. The EPD was consulted with regard to any records of chemical waste producer (CWP). The FSD was consulted with regard to any records of dangerous good producer(s). Both departments were also inquired on any reported accidents or spillage/leakage incidents within the three areas of concern. The correspondences from EPD and FSD are documented in Appendix 7-2.
- 7.5.2 **Table 7-2** below shows the summary of the responses from Government Departments.

Table 7-2 Summary of Response from Government Departments

Government Department	Response
Environmental Protection Department Regional Office (West)	No record of reported accidents of spillage / leakage of chemicals at the concerned sites. For chemical waste producer (CWP), the records were checked on 3 rd August 2020 and no record of CWP was found for the Sites.
Fire Services Department	No dangerous goods license or reported accidents of dangerous goods leakage or spillage is recorded.

7.6 Conclusion

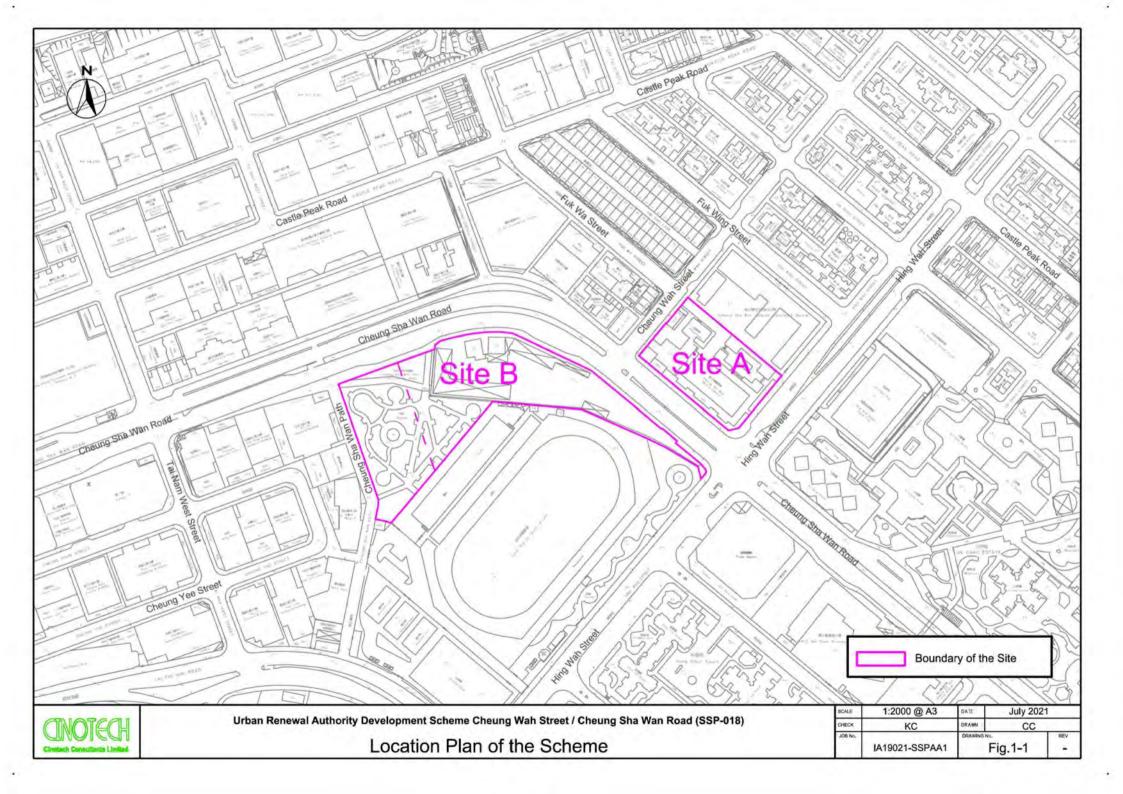
The available information from aerial photos, records from authorities suggest that the no potentially contaminating activities were recorded for the Sites. Although the previous use of open area storage was recorded at the Sites, as only inert construction materials were involved, based on findings from the aerial photos, land contamination issue arising from the land use is not anticipated. Apart from the existing Cheung Sha Wan Path Sitting-out Area, the other areas are still occupied and inaccessible during this assessment period. As land contamination issue arising from the sitting-out areas are not expected, site walkover is not carried out for this assessment. Nevertheless, the Sites shall be re-appraised upon land resumption. Detailed Land Contamination Assessment and Remediation (if needed) should be completed with reference to the prevailing guidelines on land contamination assessment prior to the development of the proposed development site.

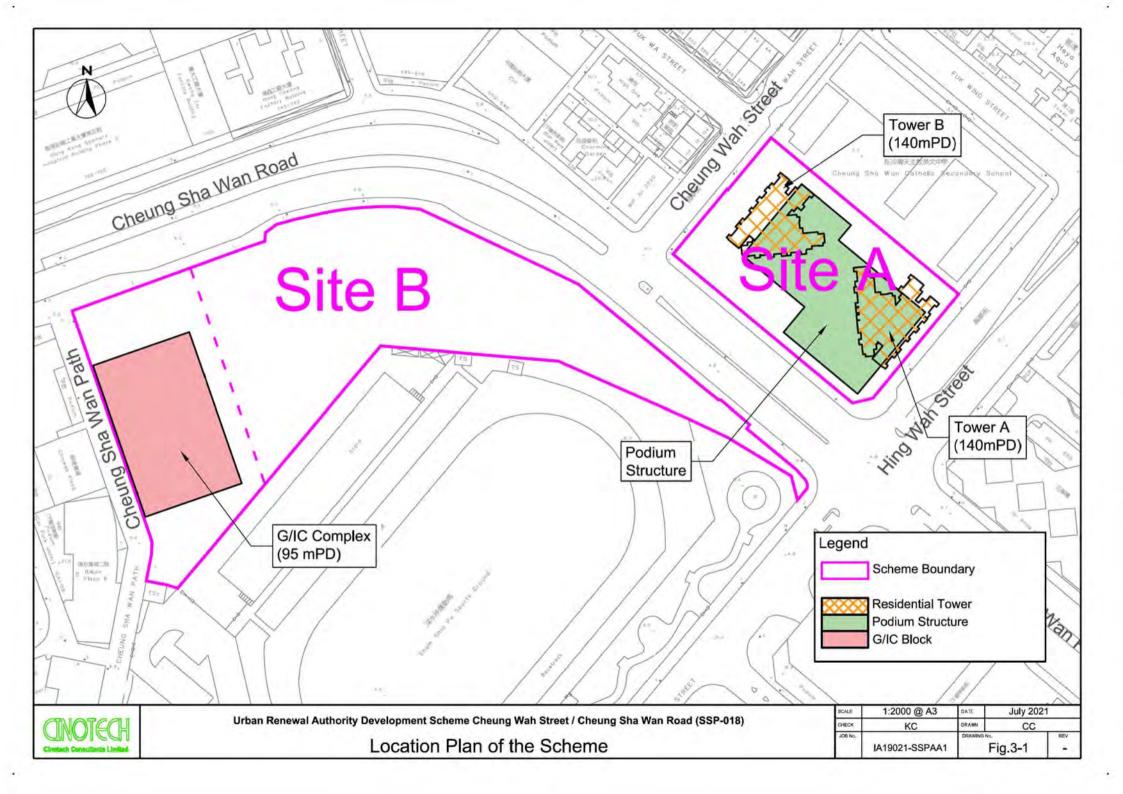
8 CONCLUSION

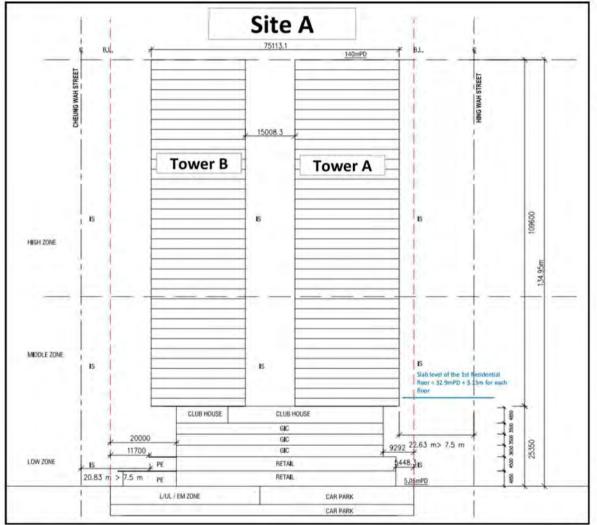
- 8.1.1 An Environmental Assessment has been carried out to evaluate the potential environmental benefits and impacts likely to arise from the proposed Scheme. The key environmental issues associated with the Scheme are construction dust impact, construction noise impact and waste management during the construction phase and potential air quality and noise impact during the operational phase.
- 8.1.2 With the implementation of dust suppression measures stipulated under the Air Pollution Control (Construction Dust) Regulation and the adoption of good site practice, no adverse air quality impact associated with the construction works is expected.
- 8.1.3 Air emission is not anticipated from the proposed development during operation phase. Air quality model based on the current notional design with conservative approach has been conducted. The model results show that the predicted air quality at all proposed residential flats comply with the AQOs. The fresh air intake for the podiums structure Site A would be designed to be located at or above 6.35mAG (11.4mPD). The fresh air in-take for the G/IC complex at Site B should not be restrained by air quality. The air quality upon completion of the Scheme will be similar to, if not better than, the existing situation and no insurmountable air quality impact is anticipated.
- 8.1.4 Construction noise impact is considered insignificant with proper implementation of the recommended mitigation measures.
- 8.1.5 Traffic noise impact has been taken into consideration when designing the notional layout of the residential development. The view angle from the windows to the road traffic has been minimised by buildings deposition, buildings orientation and windows locations. In the base scenario where tower setback, buildings deposition, buildings orientation and windows locations are considered, only ~17% of flats complies with the 70 dB(A) traffic noise assessment criterion as demonstrated. In the mitigated scenario where acoustic windows are considered, the compliance rate by flat has been increased to ~80%.
- 8.1.6 A preliminary study of fixed noise sources based on the existing situation and the available information for planned developments show that no adverse fixed noise impact to the Scheme is anticipated. The existing significant fixed noise sources are only identified in the west of Site B which is far away from the residential portion of the Scheme in Site A, which rely on openable windows for ventilation. The planned fixed noise source from the proposed Scheme should not introduce adverse noise impact to the surroundings with proper design. To ensure the compliance in the final design, the project proponent (URA) should incorporate the fixed source noise planning criteria to the tender document of the Scheme.
- 8.1.7 If the draft DSP is approved by CE in C, a detailed design of the proposed development will be carried out and if the block layout is changed and subject to requirement by relevant government departments, a revised noise impact assessment would be carried out to demonstrate the noise compliance.
- 8.1.8 A variety of wastes including inert C&D material, C&D waste, chemical waste, asbestos-containing materials, excavated sediment, and general refuse would be generated during the construction phase and domestic waste would be generated during operation phase. Provided that the wastes generated would be managed with appropriate measures, no adverse environmental impacts arising from the handling, storage, transportation or disposal of the wastes generated during the construction and operation stage of the Scheme would be envisaged.

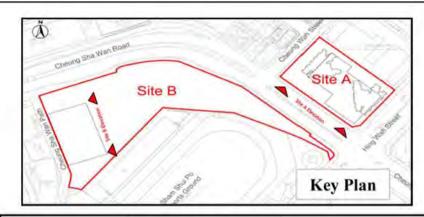
8.1.9 The available information from aerial photos, records from authorities suggest that the no potentially contaminating activities were recorded for the Sites. Although the previous use of open area storage was recorded at the Sites, as only inert construction materials were involved, based on findings from the aerial photos, land contamination issue arising from the land use is not anticipated. Apart from the existing Cheung Sha Wan Path Sitting-out Area, the other areas are still occupied and inaccessible during this assessment period. As land contamination issue arising from the sitting-out areas are not expected, site walkover is not carried out for this assessment. Nevertheless, the Sites shall be re-appraised upon land resumption. Detailed Land Contamination Assessment and Remediation (if needed) should be completed with reference to the prevailing guidelines on land contamination assessment prior to the development of the proposed development site.

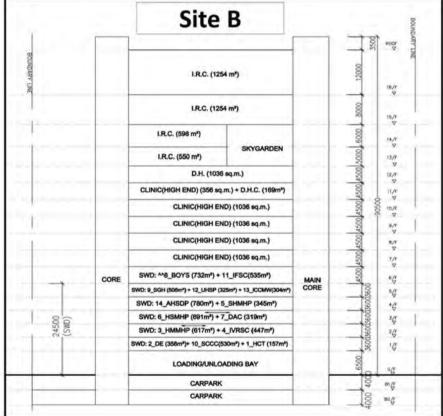












Remark:

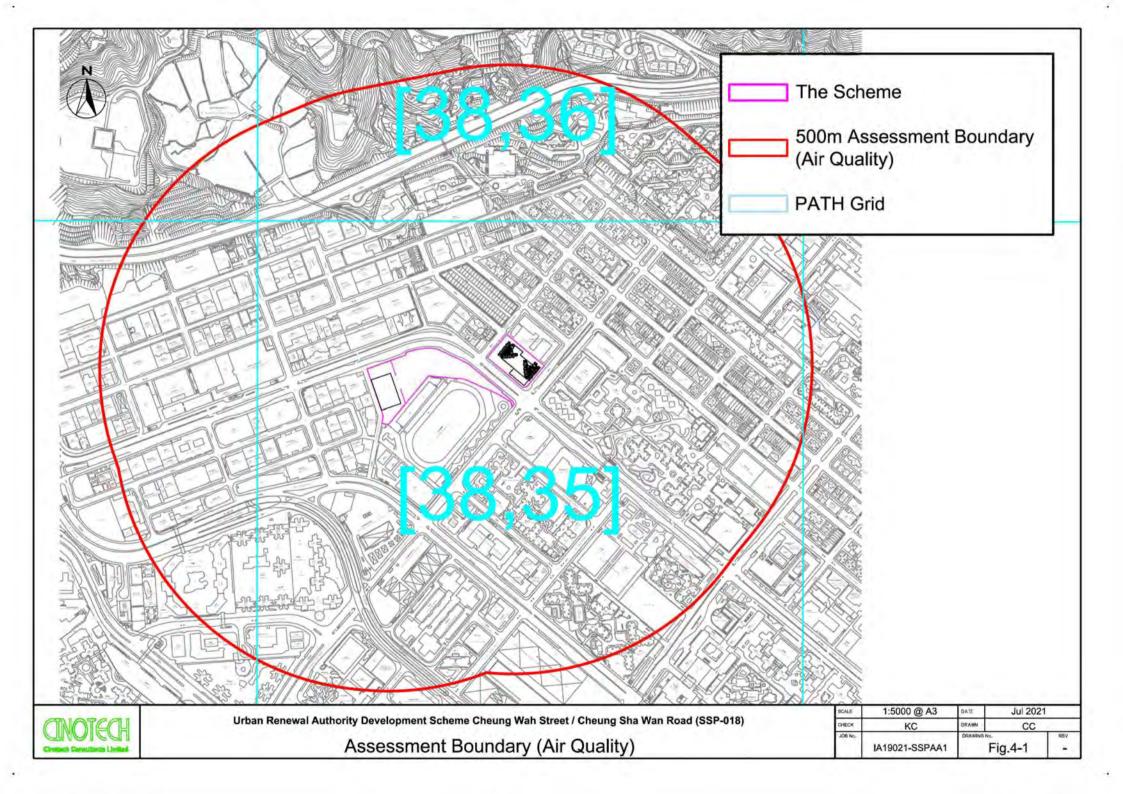
Notional Design subject to change at detailed design stage

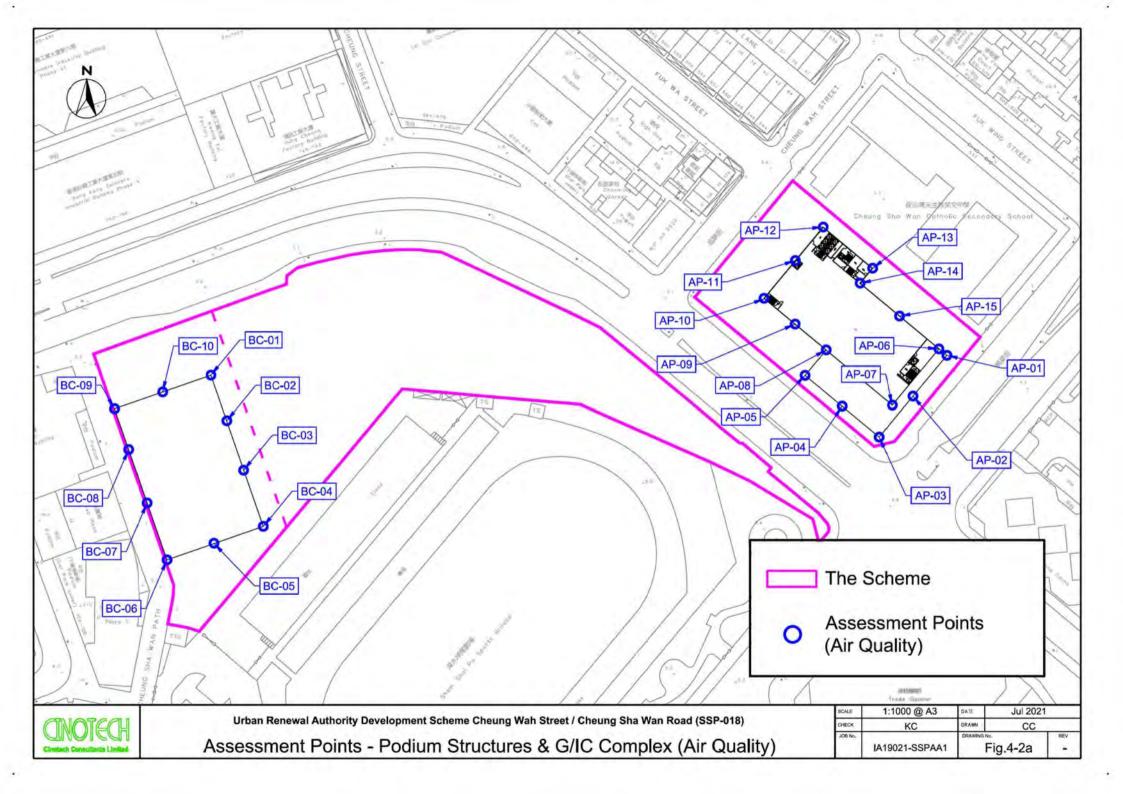


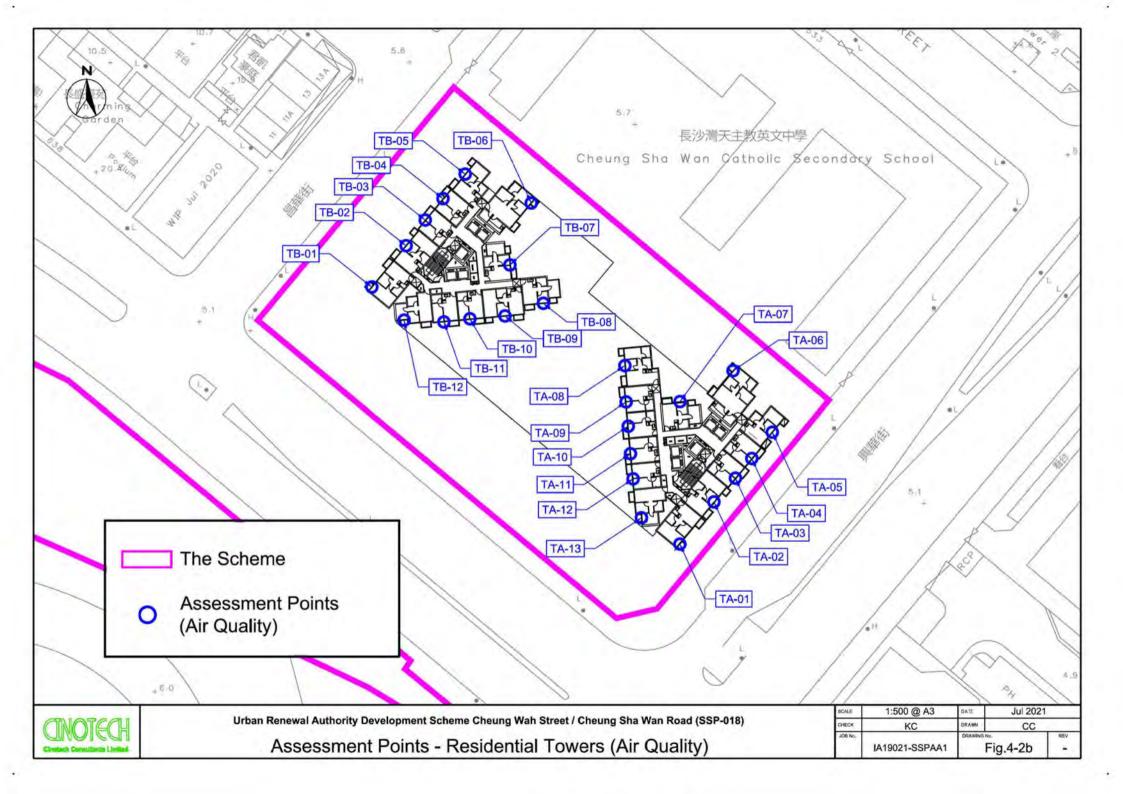
Urban Renewal Authority Development Scheme Cheung Wah Street/ Cheung Sha Wan (SSP-018)

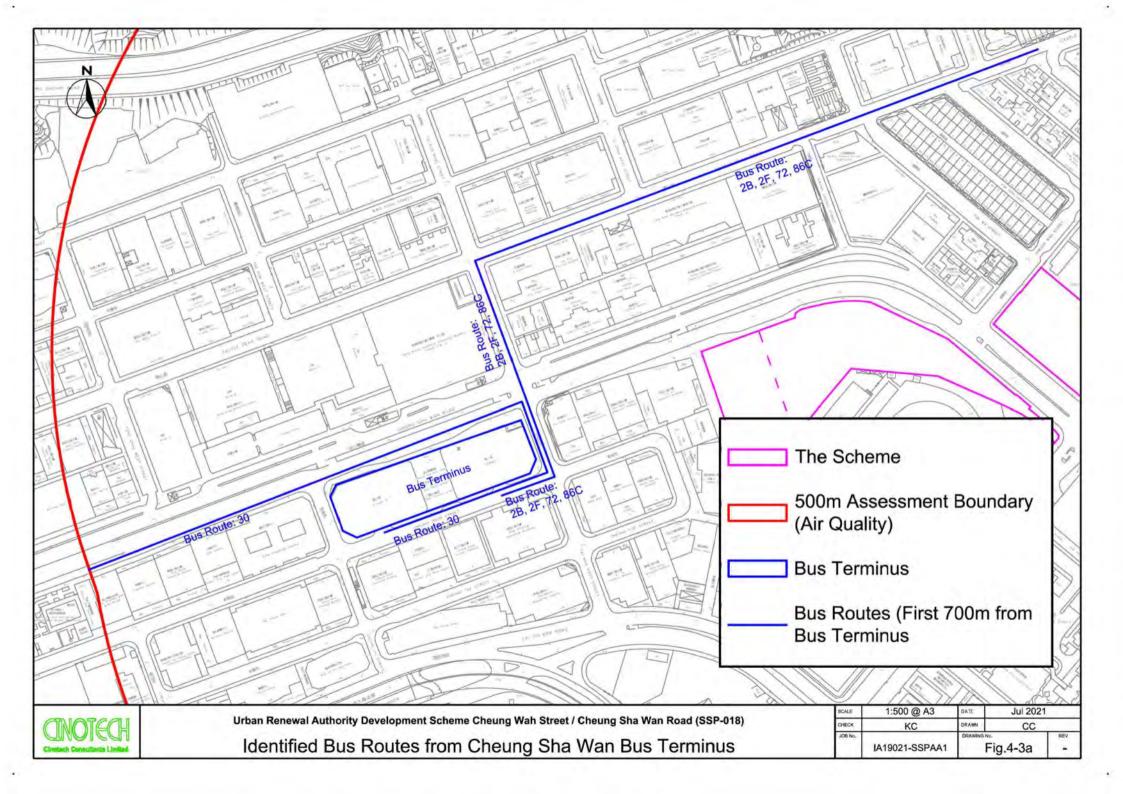
Notional Section Plan of the Proposed Scheme

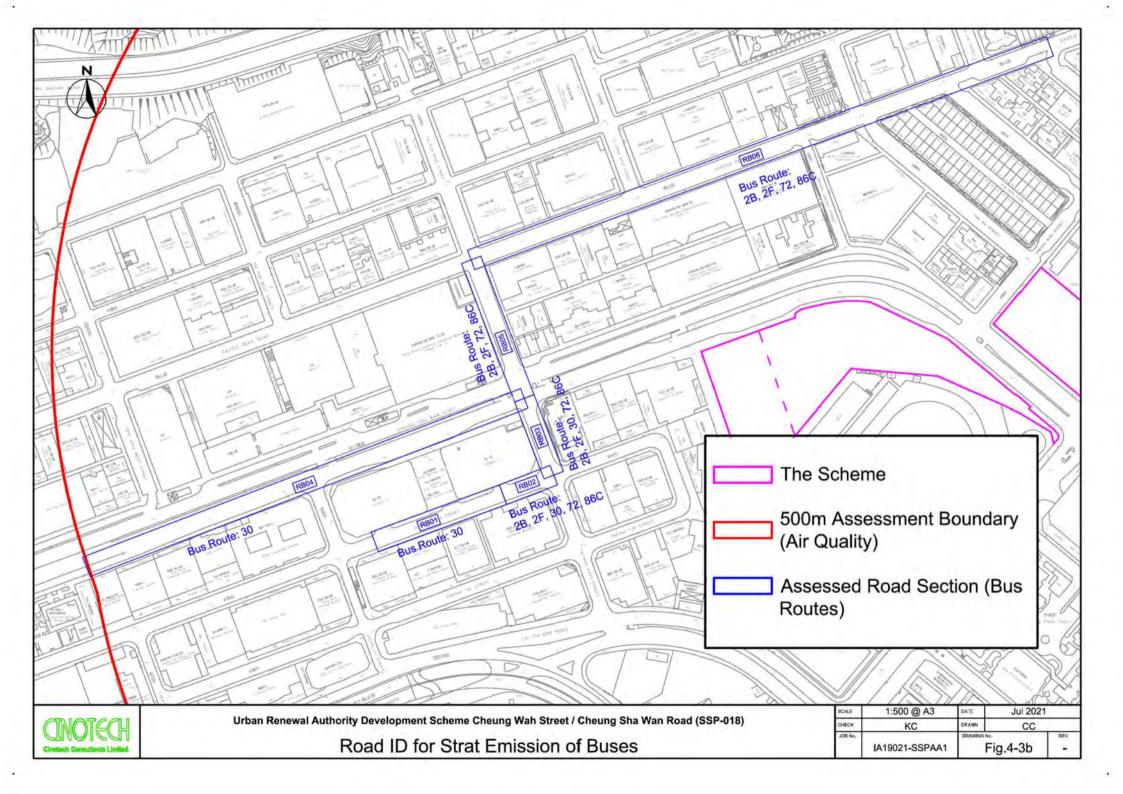
SCALE CHECK		DATE	Jun-21 CC	
		DRAWN		
JOB NO.	IA9021-5SPAA1	FIGURE NO.	3-2	REV.

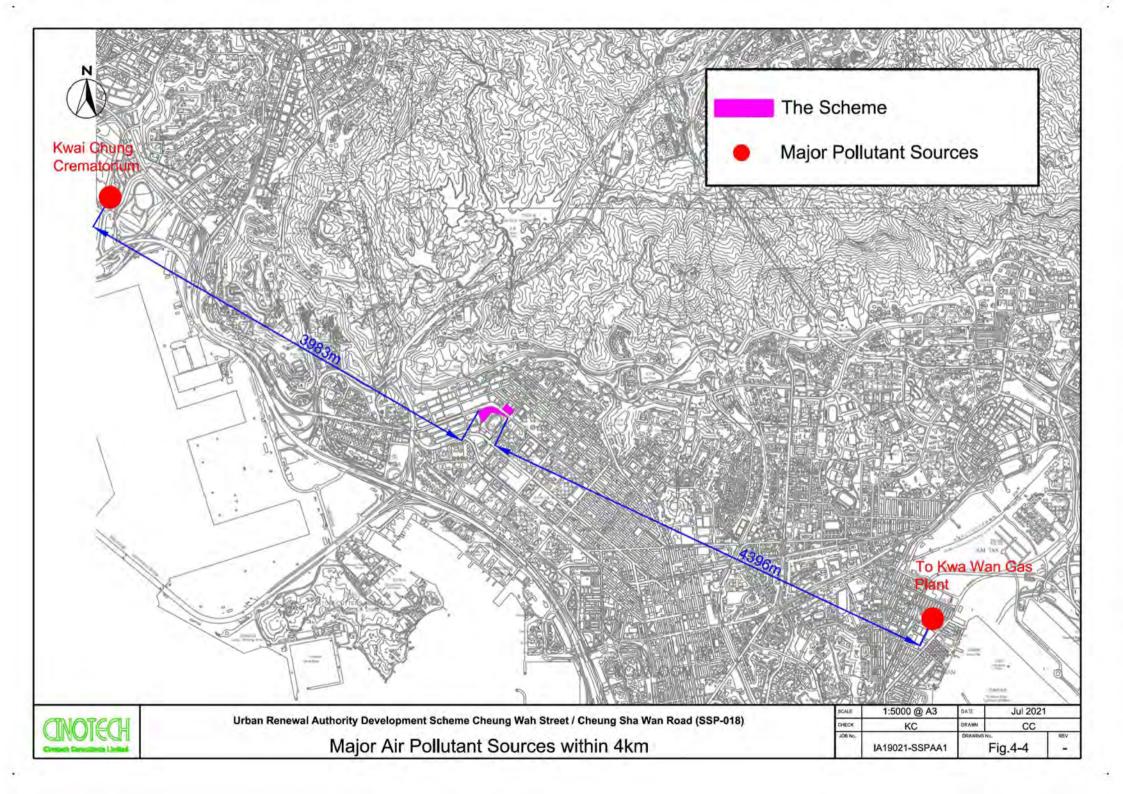


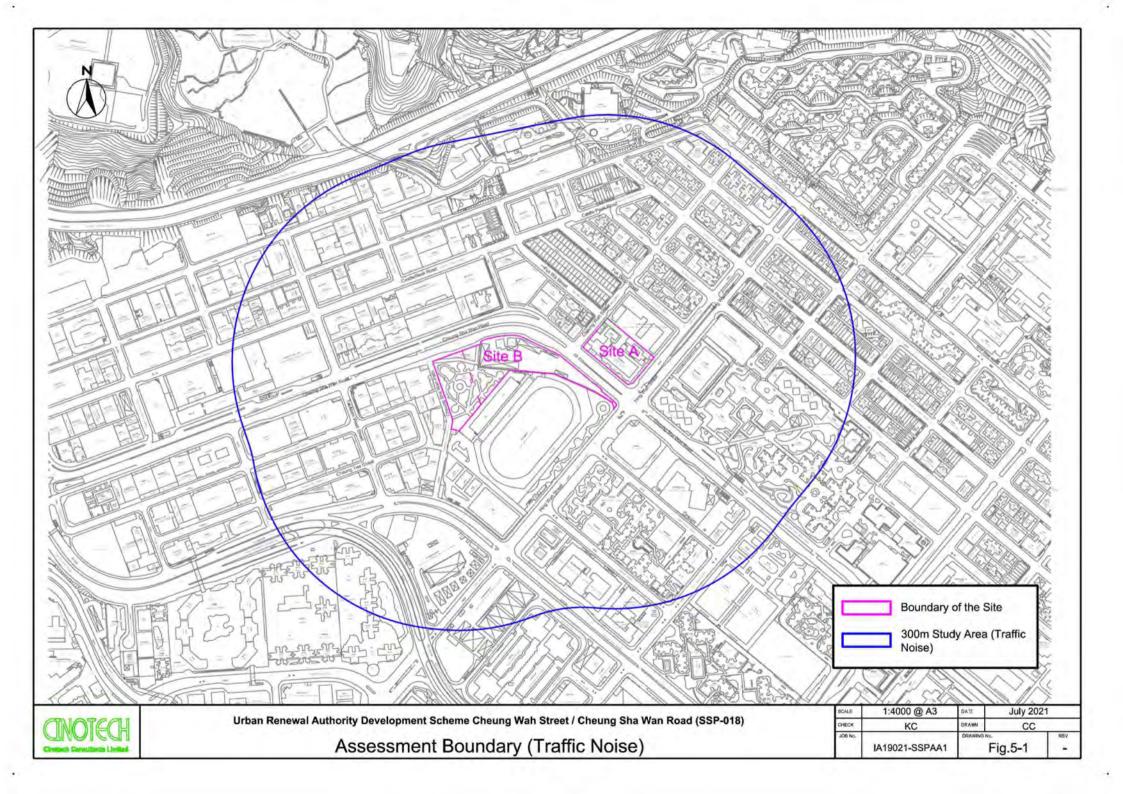


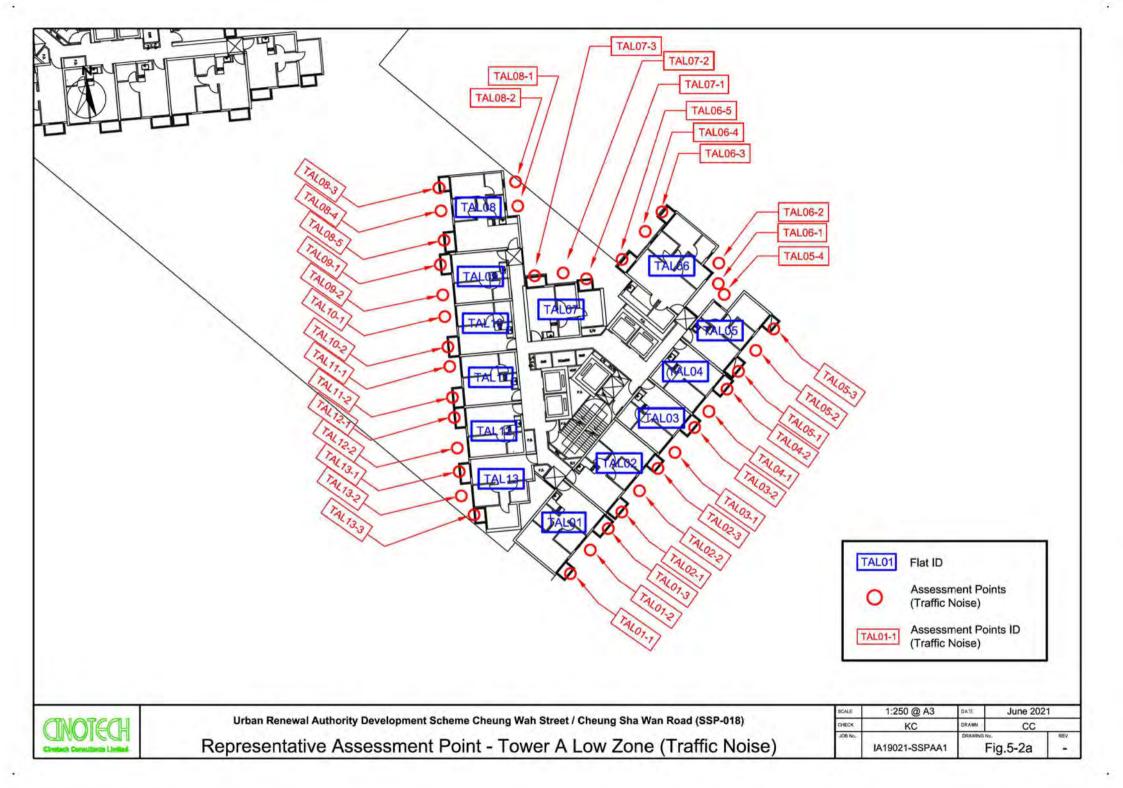


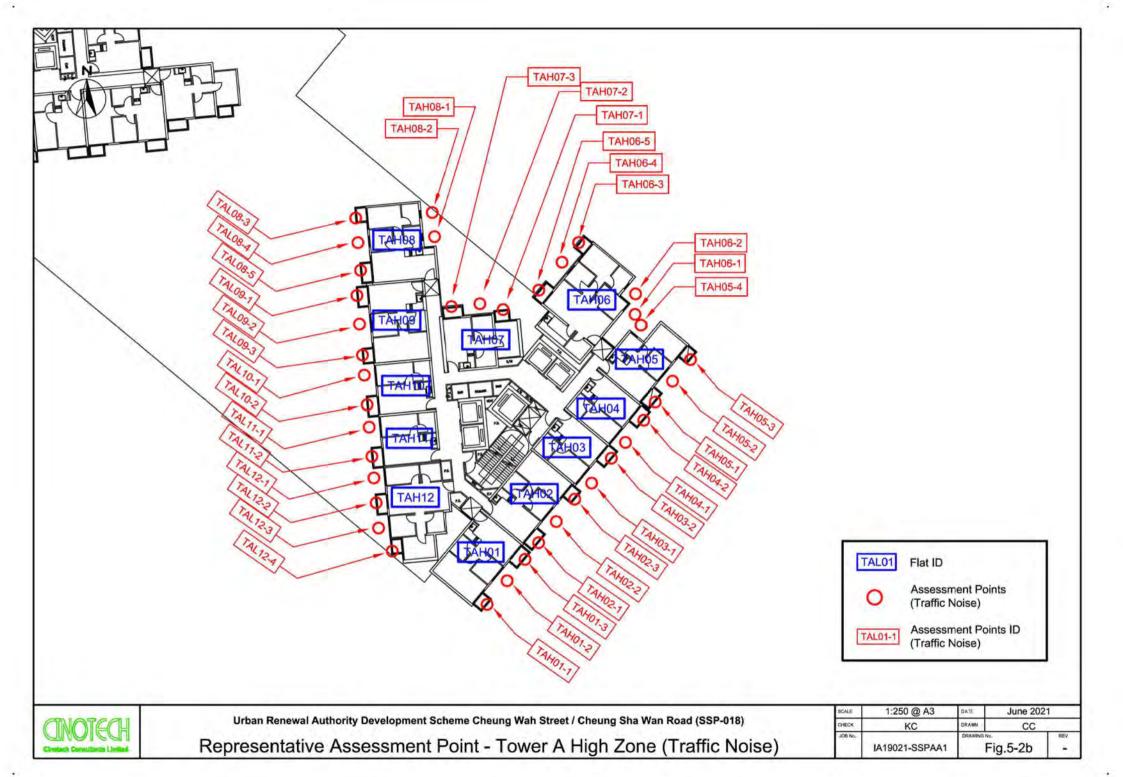


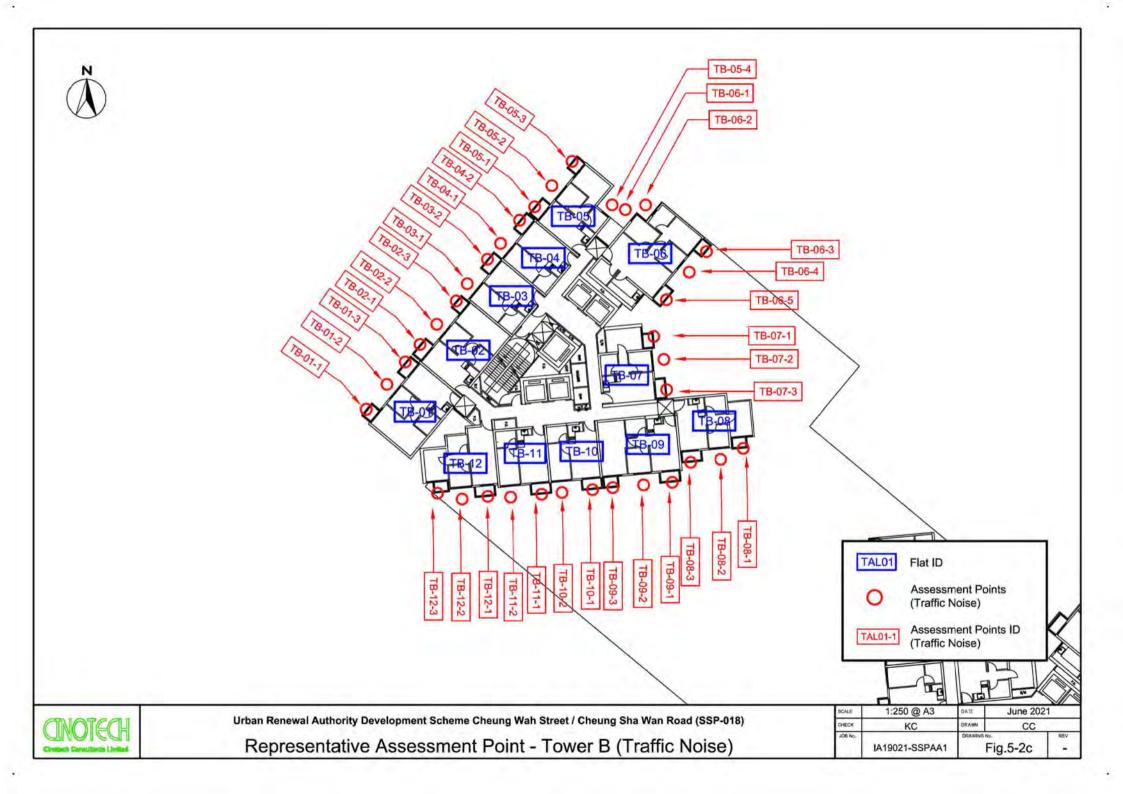


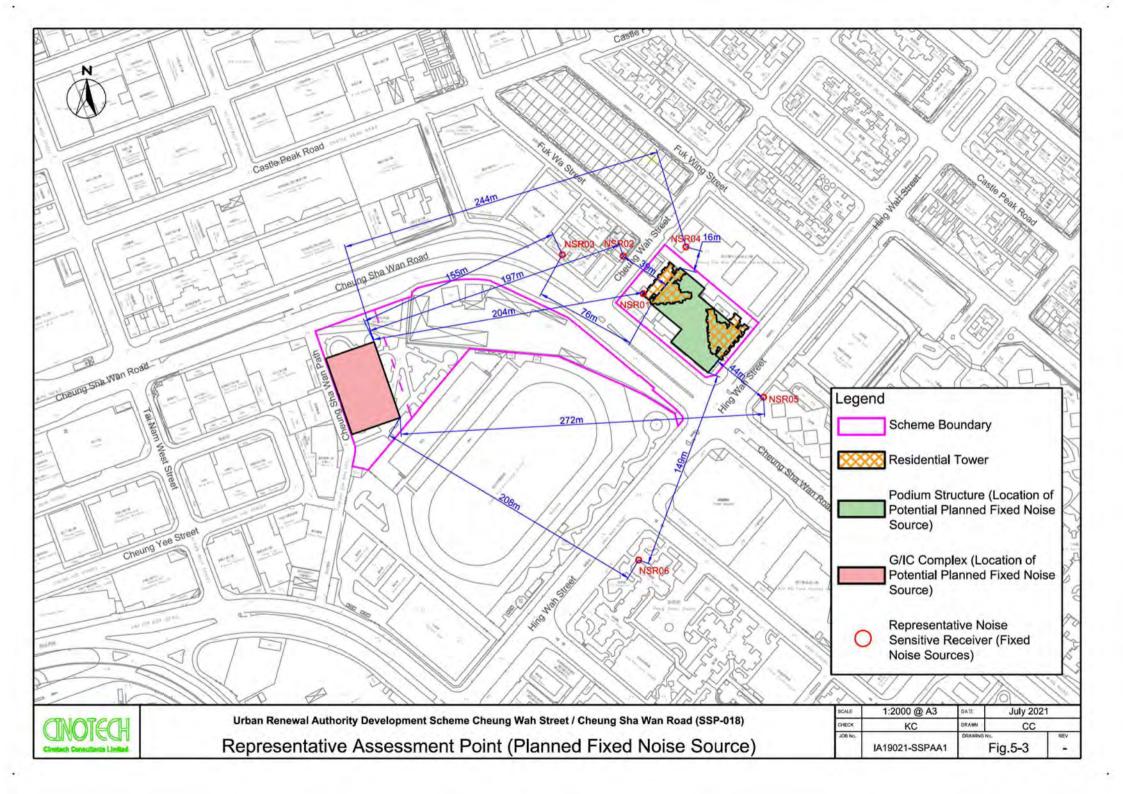


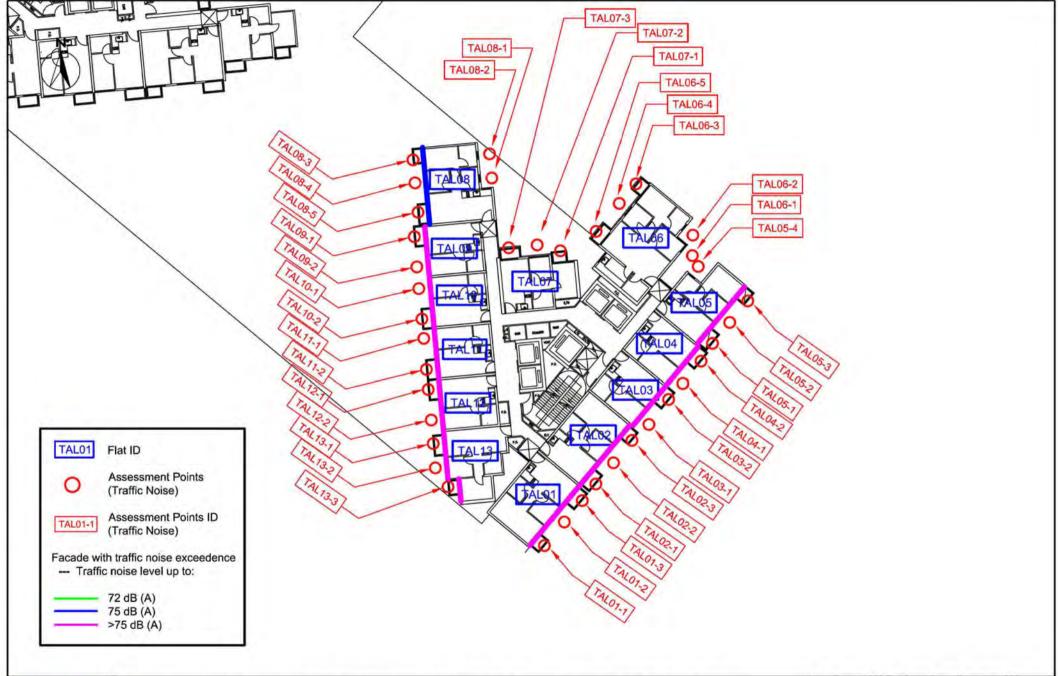










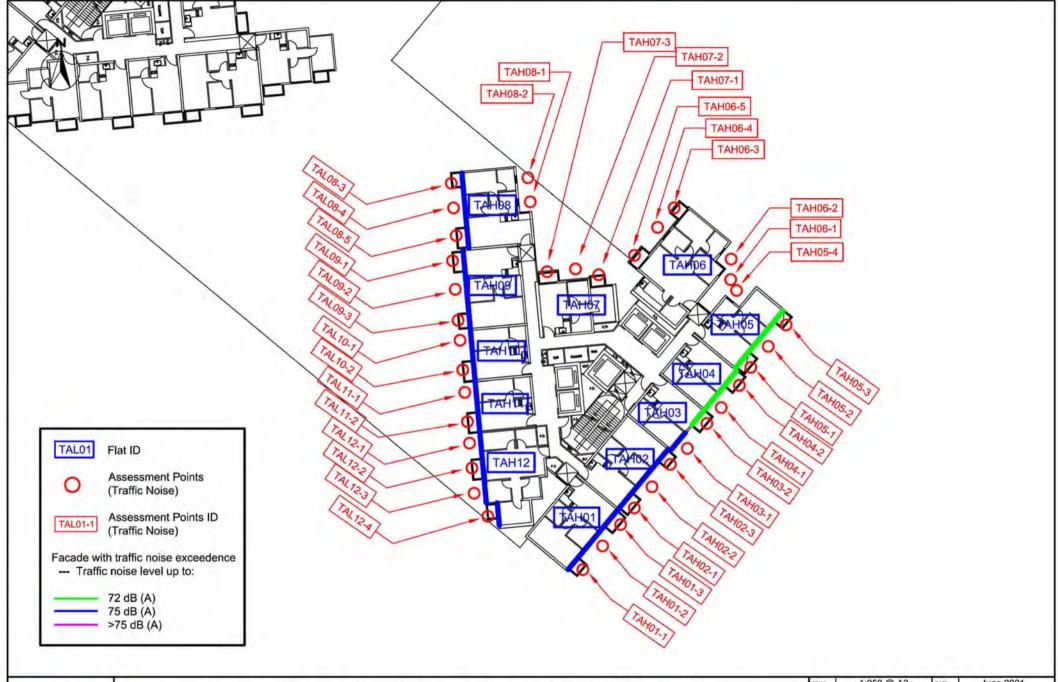




Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Noise Exceedance in Base Scenario - Tower A Low Zone (Traffic Noise)

SCALE	1:250 @ A3	DATE	June 2021	
CHECK	KC	DRAWN	CC	
JOB No.	IA19021-SSPAA1	DRAWING No	ig.5-4a	REV

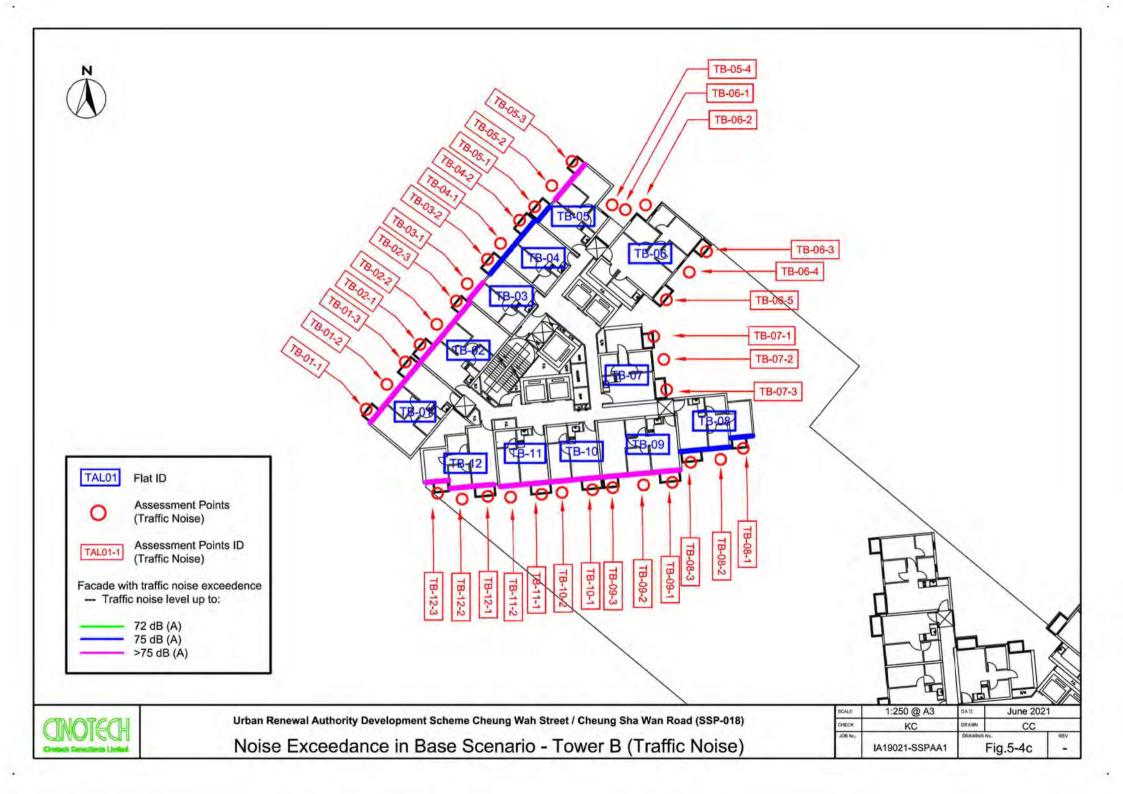


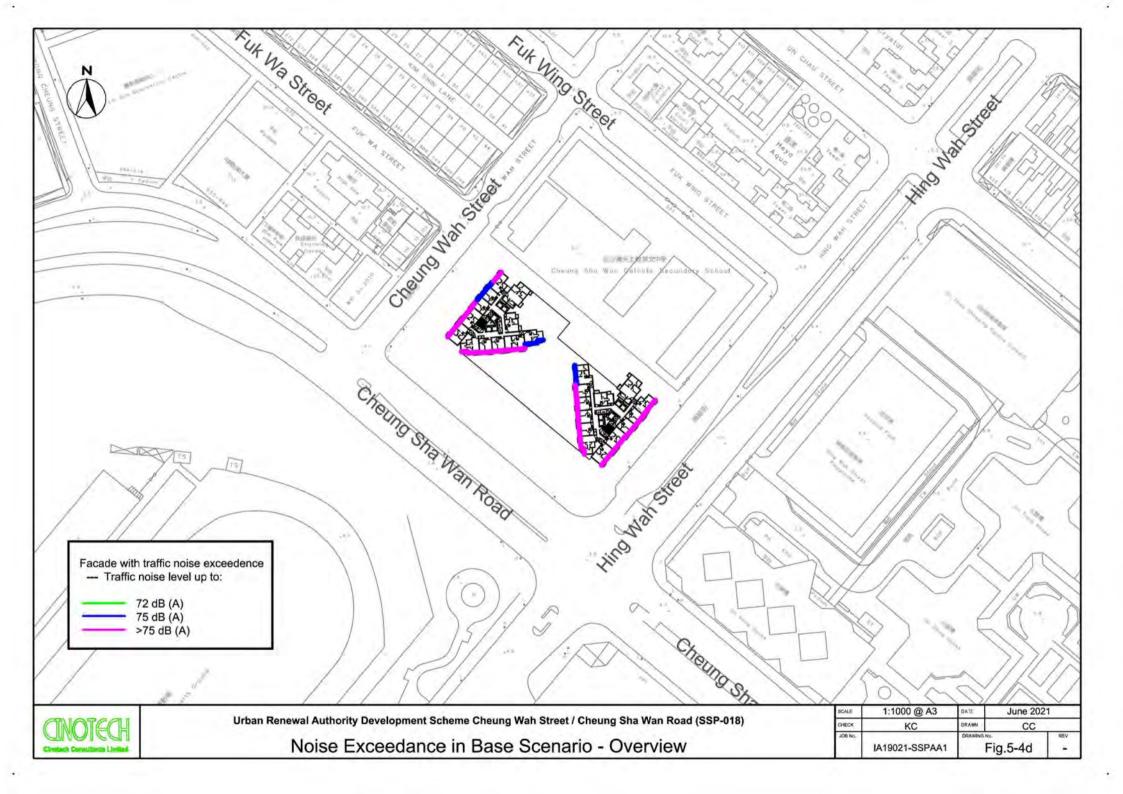
CNOTECH

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

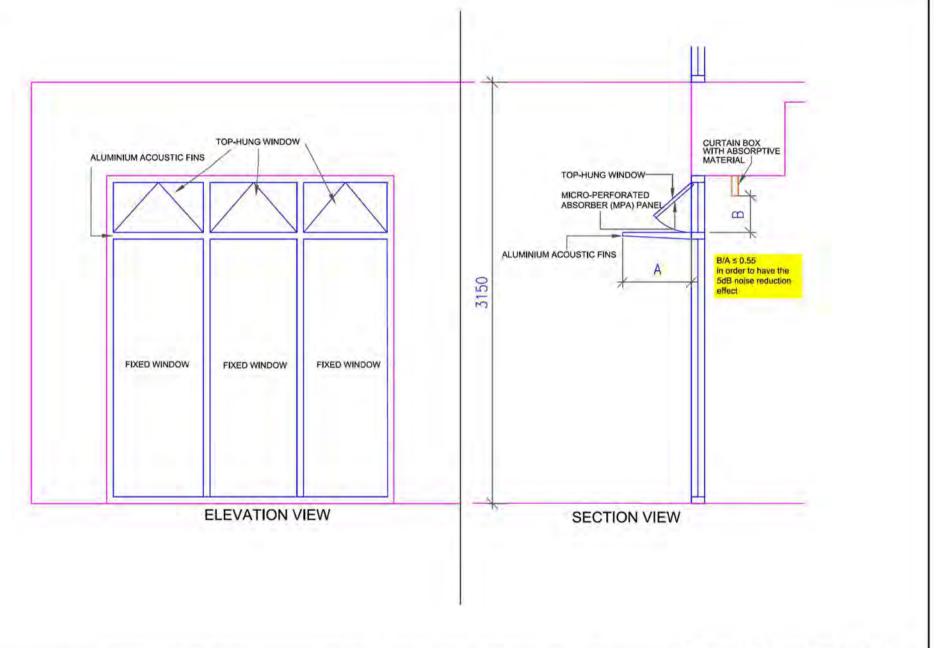
Noise Exceedance in Base Scenario - Tower A High Zone (Traffic Noise)

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CHECK	KC DRAW	DRAWN		
JOB No.	IA19021-SSPAA1	Fig.5-4b		REV







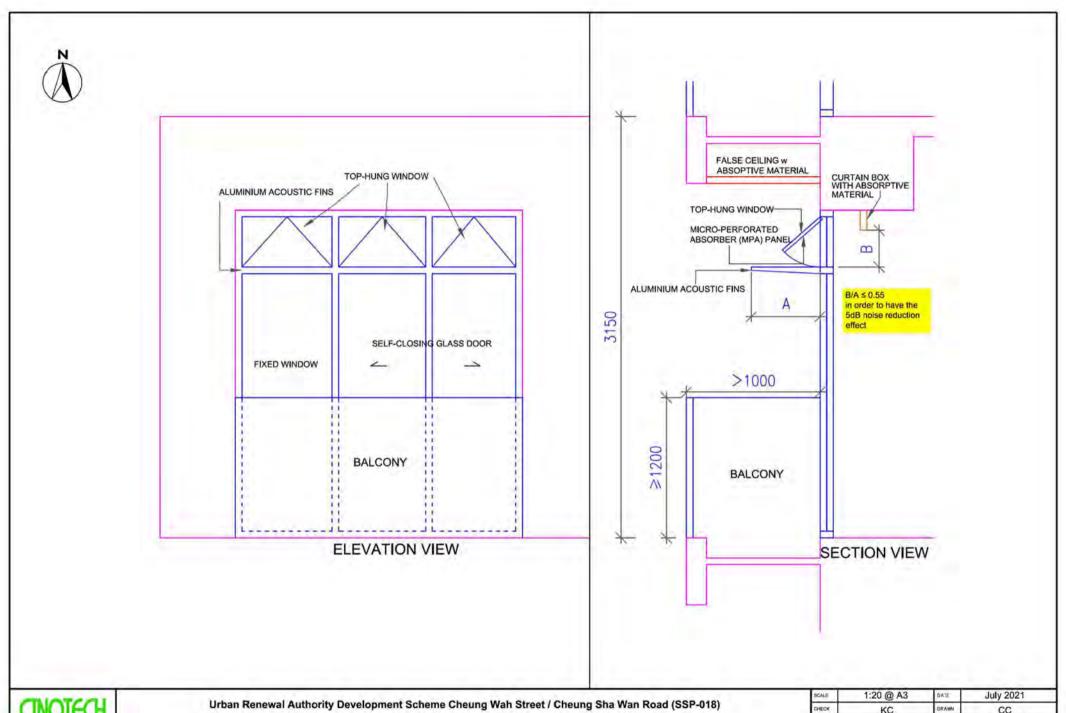




Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Typical Section for Acoustic Window (Top-hung type)

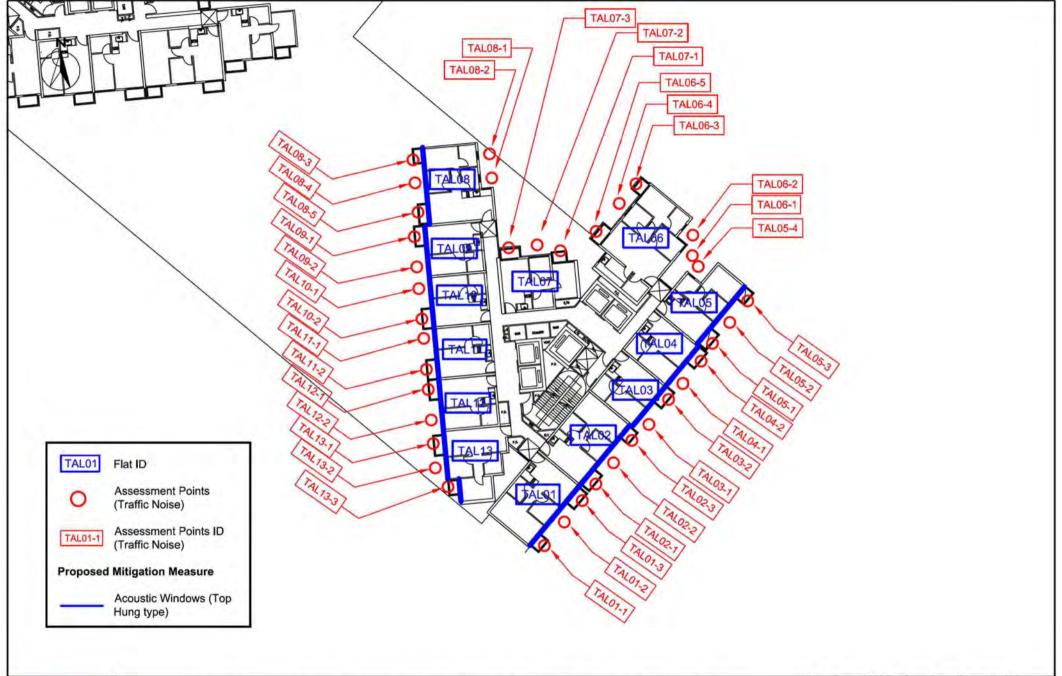
SCALE	1:20 @ A3	DATE July 2021		1
CHECK	KC	DRAWN	CC	
JOB No.	IA 19021-KCAA101	DRAWING N	5-5a	REV



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Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Typical Section for Acoustic Window with Balcony

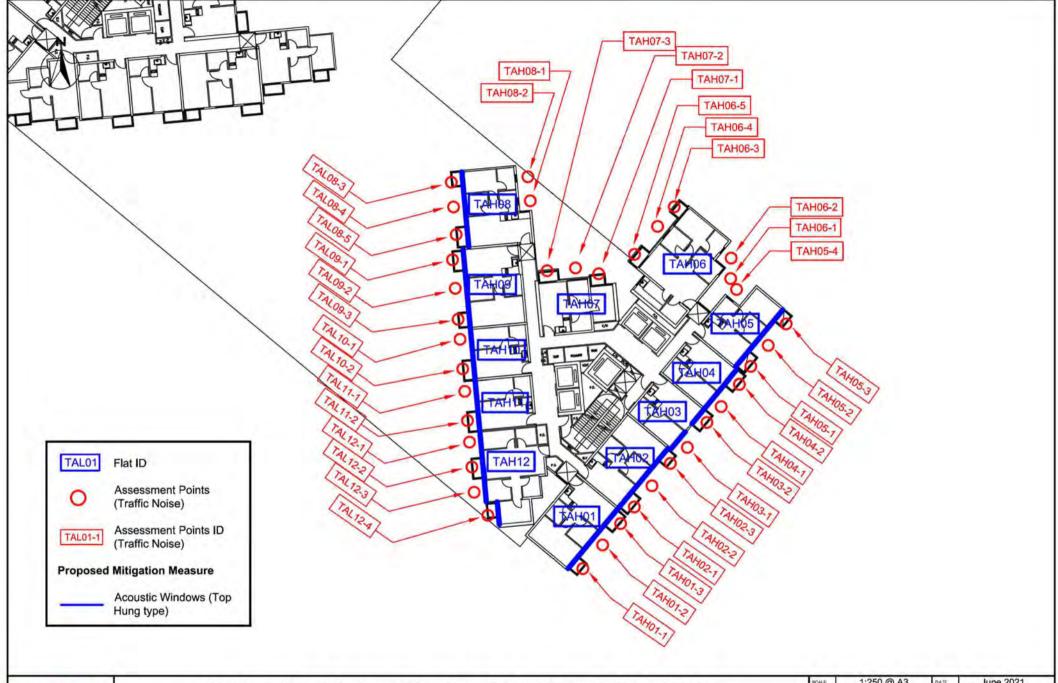


CNOTECH

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Proposed Mitigation Measures - Tower A Low Zone (Traffic Noise)

SCALE	1:250 @ A3	DATE	June 2021	
CHECK	KC	DRAWN	CC	
JOB No.	IA19021-SSPAA1	Fig.5-6a		REV

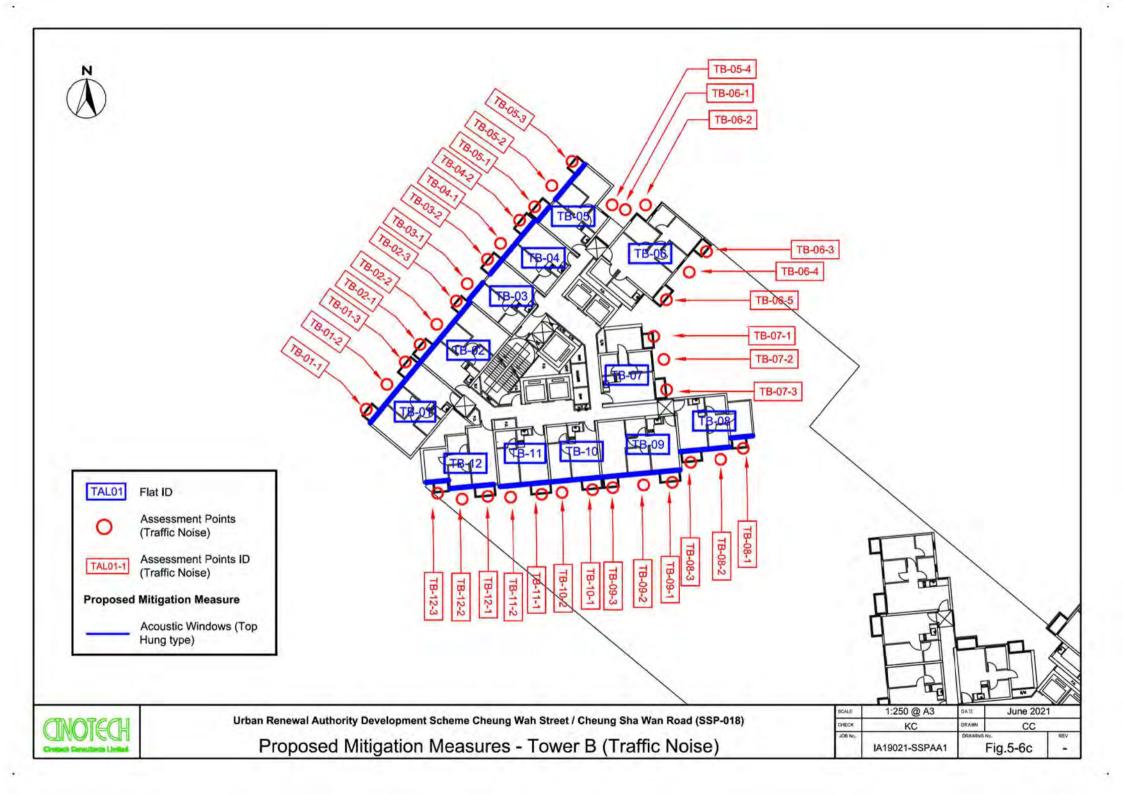


CNOTECH

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

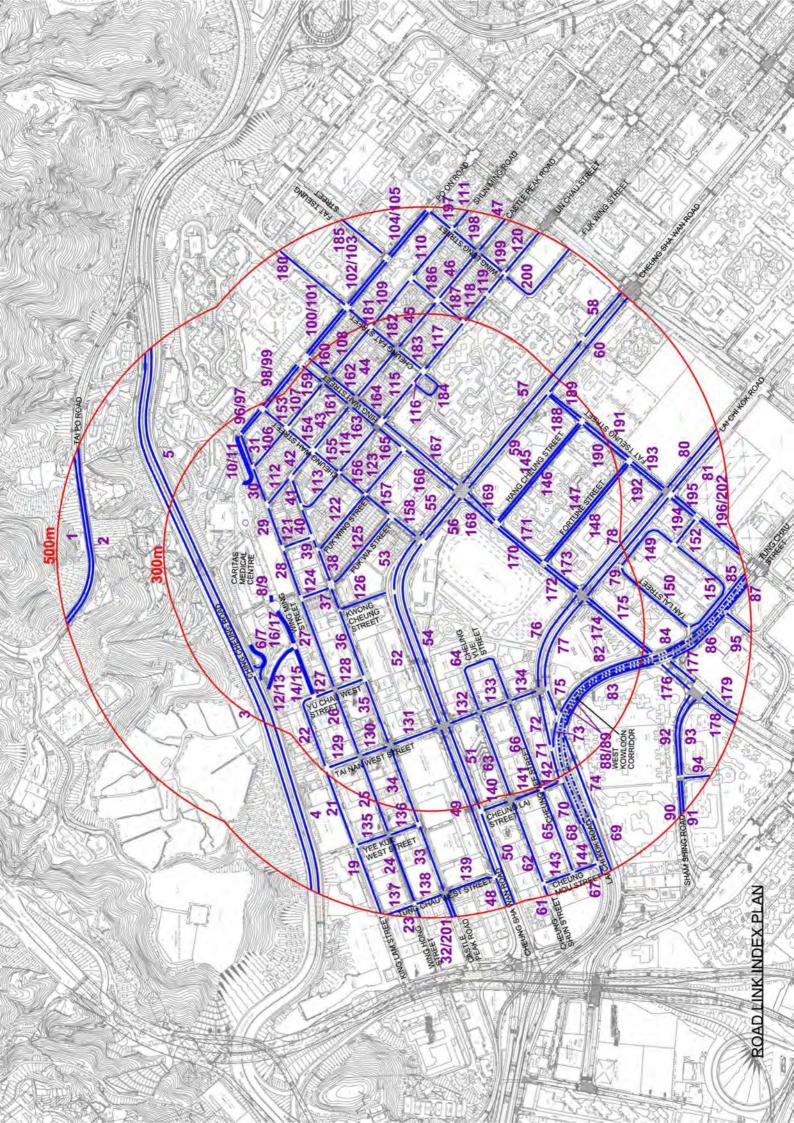
Noise Proposed Mitigation Measures - Tower A High Zone (Traffic Noise)

SCALE	1:250 @ A3	DATE	June 2021	
CHECK	KC	DRAWN	CC	
JOB No.	IA19021-SSPAA1	Fig.5-6b		REV



APPENDIX 4-1

List of Road Sections and Endorsement from Transport Department



Road sections with cold start are indicated as 1
 Road sections without cold start are indicated as 0

Road ID	Road Name	Travel Direction	Road Length (m)	At grade / Flyover	Speed Limit (km/hr)	Cold
1	Tai Po Road	EB	320	At grade	50	1
2	Tai Po Road	WB	350	At grade	50	0
3	Ching Cheung Road	EB	1070	At grade	70	0
4	Ching Cheung Road	WB	425	At grade	70	0
5	Ching Cheung Road	WB	650	At grade	70	0
6	Access Road of Caritas Medical Centre	EB	70	At grade	50	0
7	Access Road of Caritas Medical Centre	WB	80	At grade	50	0
8	Access Road of Caritas Medical Centre	EB	15	At grade	20	0
9	Access Road of Caritas Medical Centre	WB	15	At grade	20	0
10	Access Road of Caritas Medical Centre	EB	100	At grade	50	0
11	Access Road of Caritas Medical Centre	WB	105	At grade	50	0
12	Access Road to St. Raphael's Catholic Cemetery	NB	90	At grade	50	1
13	Access Road to St. Raphael's Catholic Cemetery	SB	95	At grade	50	1
14	Wing Ming Street	EB	90	At grade	50	1
15	Wing Ming Street	WB	90	At grade	50	1
16	Wing Ming Street	EB	70	At grade	50	1
17	Wing Ming Street	WB	70	At grade	50	1
18	King Lam Street	EB	130	At grade	50	1
19	King Lam Street	WB	130	At grade	50	1
20	King Lam Street	EB	150	At grade	50	1
21	King Lam Street	WB	150	At grade	50	1
22	King Lam Street	EB	150	At grade	50	1
23	Wing Hong Street	WB	45	At grade	50	1
24	Wing Hong Street	WB	45	At grade	50	1
25	Wing Hong Street	WB	150	At grade	50	1
26	Wing Hong Street	WB	125	At grade	50	1
27	Wing Hong Street	WB	170	At grade	50	1
28	Wing Hong Street	WB	95	At grade	50	1
29	Wing Hong Street	WB	80	At grade	50	1
30	Wing Hong Street	WB	70	At grade	50	1
31	Wing Hong Street	WB	65	At grade	50	1
32	Castle Peak Road	2-way	50	At grade	50	1
33	Castle Peak Road	EB	135	At grade	50	1
34	Castle Peak Road	EB	150	At grade	50	1
35	Castle Peak Road	EB	130	At grade	50	1
36	Castle Peak Road	EB	135	At grade	50	1
37	Castle Peak Road	EB	45	At grade	50	1
38	Castle Peak Road	EB	65	At grade	50	1
39	Castle Peak Road	EB	20	At grade	50	1
40	Castle Peak Road	EB	55	At grade	50	1
41	Castle Peak Road	EB	50	At grade	50	1
42	Castle Peak Road	EB	60	At grade	50	1
43	Castle Peak Road	EB	105	At grade	50	1
44	Castle Peak Road	EB	115	At grade	50	1
45	Castle Peak Road	EB	115	At grade	50	1
46	Castle Peak Road	EB	115	At grade	50	1
47	Castle Peak Road	EB	80	At grade	50	1
48	Cheung Sha Wan Road	EB	60	At grade	50	1
49	Cheung Sha Wan Road	WB	300	At grade	50	1
50	Cheung Sha Wan Road	WB	185	At grade	50	1
51	Cheung Sha Wan Road	WB	170	At grade	50	1
52	Cheung Sha Wan Road	WB	265	At grade	50	1
53	Cheung Sha Wan Road	WB	110	At grade	50	1
54	Cheung Sha Wan Road	WB	360	At grade	50	1
55	Cheung Sha Wan Road	WB	120	At grade	50	1
56	Cheung Sha Wan Road	WB	120	At grade	50	1
57	Cheung Sha Wan Road	WB	365	At grade	50	1

Road Section List

 Road sections with cold start are indicated as 1 Road sections without cold start are indicated as 0

	Road sections without cold start are indi						
Road ID	Road Name	Travel Direction	Road Length (m)	At grade / Flyover	Speed Limit (km/hr)	Cold Start	
58	Cheung Sha Wan Road	WB	110	At grade	50	1	
59	Cheung Sha Wan Road	WB	240	At grade	50	1	
60	Cheung Sha Wan Road	WB	230	At grade	50	1	
61	Cheung Shun Street	2-way	25	At grade	50	1	
62	Cheung Shun Street	EB	165	At grade	50	1	
63	Cheung Shun Street	EB	175	At grade	50	1	
64	Cheung Yue Street	EB	225	At grade	50	1	
65	Cheung Yee Street	WB	165	At grade	50	1	
66	Cheung Yee Street	WB	175	At grade	50	1	
67	Lai Chi Kok Road	EB	25	At grade	70	1	
68	Lai Chi Kok Road	EB	80	At grade	70	1	
69	Lai Chi Kok Road	WB	100	At grade	70	1	
70	Lai Chi Kok Road	EB	90	At grade	50	1	
71	Lai Chi Kok Road	EB	60	At grade	50	1	
72	Lai Chi Kok Road	EB	110	At grade	50	1	
73	Lai Chi Kok Road	EB	55	At grade	50	1	
74	Lai Chi Kok Road					-	
75	Lai Chi Kok Road	WB WB	185 70	At grade	50 50	1	
76						1	
77	Lai Chi Kok Road	EB	205	At grade	50	1	
	Lai Chi Kok Road	WB	190	At grade	50	1	
78	Lai Chi Kok Road	EB	250	At grade	50	1	
79	Lai Chi Kok Road	WB	250	At grade	50	1	
80	Lai Chi Kok Road	EB	150	At grade	50	1	
81	Lai Chi Kok Road	WB	140	At grade	50	1	
82	Tung Chau Street	EB	225	At grade	50	1	
83	Tung Chau Street	WB	230	At grade	50	0	
84	Tung Chau Street	EB	65	At grade	50	1	
85	Tung Chau Street	EB	150	At grade	50	1	
86	Tung Chau Street	WB	145	At grade	50	- 1	
87	Tung Chau Street	WB	65	At grade	50	1	
88	West Kowloon Corridor	EB	655	Flyover	70	0	
89	West Kowloon Corridor	WB	640	Flyover	70	0	
90	Sham Shing Road	EB	70	At grade	50	1	
91	Sham Shing Road	WB	65	At grade	50	1	
92	Sham Shing Road	EB	175	At grade	50	1	
93	Sham Shing Road	WB	175	At grade	50	1	
94	Access Road connecting Sham Shing Road	2-way	55	At grade	50	0	
95	Lai Hong Street	2-way	60	At grade	50	1	
96	Po On Road	NB	60	At grade	50	1	
97	Po On Road	SB	60	At grade	50	1	
98	Po On Road	NB	120	At grade	50	1	
99	Po On Road	SB	120	At grade	50	1	
100	Po On Road	NB	125	At grade	50	1	
101	Po On Road	SB	125	At grade	50	1	
102	Po On Road	NB	115	At grade	50	1	
103	Po On Road	SB	115	At grade	50	1	
104	Po On Road	NB	115	At grade	50	1	
105	Po On Road	SB	115	At grade	50	1	
106	Shun Ming Road	NB	95	At grade	50	1	
107	Shun Ming Road	NB	120	At grade	50	1	
108	Shun Ming Road	NB	125	At grade	50	1	
109	Shun Ming Road	NB	115	At grade	50	1	
110	Shun Ming Road	NB	120	At grade	50	1	
111	Shun Ming Road	NB	45	At grade	50	1	
112		NB	65		50	_	
113	Kwong Shing Street Un Chau Street	NB NB	100	At grade At grade	50	1	
	CONTRACTOR OF THE PROPERTY OF	LIND	100	i At urage	:00		

Road Section List

 Road sections with cold start are indicated as 1 Road sections without cold start are indicated as 0

Road ID	David Name	Travel	Road	At grade	Speed Limit	100000000000000000000000000000000000000
Road ID	Road Name	Direction	Length (m)		(km/hr)	Start*
115	Un Chau Street	NB	95	At grade	50	1
116	Un Chau Street	NB	25	At grade	50	1
117	Un Chau Street	NB	120	At grade	50	1
118	Un Chau Street	NB	65	At grade	50	1
119	Un Chau Street	NB	50	At grade	50	1
120	Un Chau Street	NB	105	At grade	50	1
121	Tsap Fai Street	NB	60	At grade	50	1
122	Fuk Wing Street	SB	135	At grade	50	1
123	Fuk Wing Street	SB	110	At grade	50	1
124	Fuk Wa Street	NB	60	At grade	50	1
125	Fuk Wa Street	NB	170	At grade	50	1
126	Kwong Cheung Street	SB	95	At grade	50	- 1
127	Yu Chau West Street	SB	40	At grade	50	1
128	Yu Chau West Street	SB	60	At grade	50	1
129	Tai Nan West Street	NB	65	At grade	50	1
130	Tai Nan West Street	NB	60	At grade	50	1
131	Tai Nan West Street	NB	105	At grade	50	1
132	Tai Nan West Street	NB	70	At grade	50	0
133	Tai Nan West Street	NB	60	At grade	50	1
134	Tai Nan West Street	NB	60	At grade	50	1
135	Yee Kuk West Street	SB	65	At grade	50	1
136	Yee Kuk West Street	SB	60	At grade	50	1
137	Tung Chau West Street	NB	65	At grade	50	1
138	Tung Chau West Street	NB	60	At grade	50	1
139	Tung Chau West Street	NB NB	105	At grade	50	-
140	Cheung Lai Street		65		50	1
		NB		At grade		
141	Cheung Lai Street	NB	60	At grade	50	1
142	Cheung Lai Street	NB	40	At grade	50	0
143	Cheung Mou Street	NB	60	At grade	50	1
144	Cheung Mou Street	NB	50	At grade	50	1
145	Hang Cheung Street	NB	245	At grade	50	1
146	Hang Cheung Street	SB	245	At grade	50	1
147	Fortune Street	NB	250	At grade	50	1
148	Fortune Street	SB	250	At grade	50	1
149	Tan Lai Street	SB	145	At grade	50	1
150	Tan Lai Street	NB	165	At grade	50	1
151	Tan Lai Street	WB	220	At grade	50	1
152	Yee Kuk Street	2-way	65	At grade	50	1
153	Cheung Wah Street	NB	55	At grade	50	1
154	Cheung Wah Street	NB	65	At grade	50	1
155	Cheung Wah Street	SB	65	At grade	50	1
156	Cheung Wah Street	SB	65	At grade	50	1
157	Cheung Wah Street	SB	65	At grade	50	1
158	Cheung Wah Street	SB	70	At grade	50	1
159	Hing Wah Street	NB	55	At grade	50	1
160	Hing Wah Street	SB	55	At grade	50	1
161	Hing Wah Street	NB	65	At grade	50	1
162	Hing Wah Street	SB	65	At grade	50	1
163	Hing Wah Street	NB	65	At grade	50	1
164	Hing Wah Street	SB	65	At grade	50	1
165	Hing Wah Street	NB	65	At grade	50	1
166	Hing Wah Street	NB	135	At grade	50	1
167	Hing Wah Street	SB	200	At grade	50	1
168	Hing Wah Street	NB	90	At grade	50	1
169	Hing Wah Street	SB	90	At grade	50	0
170	Hing Wah Street	NB	115	At grade	50	0
171	Hing Wah Street	SB	115	At grade	50	0

Road Section List

Road sections with cold start are indicated as 1
 Road sections without cold start are indicated as 0

Road ID	Road Name	Travel Direction	Road Length (m)	At grade / Flyover	Speed Limit (km/hr)	Cold Start
172	Hing Wah Street	NB	95	At grade	50	1
173	Hing Wah Street	SB	95	At grade	50	1
174	Hing Wah Street	NB	180	At grade	50	1
175	Hing Wah Street	SB	180	At grade	50	1
176	Hing Wah Street	NB	100	At grade	50	1
177	Hing Wah Street	SB	90	At grade	50	1
178	Hing Wah Street	NB	90	At grade	50	1
179	Hing Wah Street	SB	90	At grade	50	1
180	Cheung Fat Street	2-way	165	At grade	50	1
181	Cheung Fat Street	NB	60	At grade	50	1
182	Cheung Fat Street	NB	65	At grade	50	1
183	Cheung Fat Street	SB	65	At grade	50	1
184	Un Chau Street	NB	100	At grade	50	1
185	Fat Tseung Street	2-way	110	At grade	50	1
186	Fat Tseung Street	SB	65	At grade	50	1
187	Fat Tseung Street	NB	65	At grade	50	1
188	Fat Tseung Street	NB	80	At grade	50	0
189	Fat Tseung Street	SB	80	At grade	50	1
190	Fat Tseung Street	NB	115	At grade	50	1
191	Fat Tseung Street	SB	115	At grade	50	1
192	Fat Tseung Street	NB	85	At grade	50	1
193	Fat Tseung Street	SB	85	At grade	50	0
194	Fat Tseung Street	NB	65	At grade	50	1
195	Fat Tseung Street	SB	65	At grade	50	1
196	Fat Tseung Street	2-way	105	At grade	50	1
197	Wing Lung Street	NB	55	At grade	50	1
198	Wing Lung Street	NB	65	At grade	50	1
199	Wing Lung Street	SB	65	At grade	50	1
200	Wing Lung Street	SB	175	At grade	50	1

APPENDIX 4-2

Sensitivity Test for Traffic Emission

Result of Sensitively Test (Traffic Emission)

Scenario	Year 2034	Year 2042	Year 2049				
Quarter		NOx Emission (kg/daγ)					
Q1 (Dec - Feb)	124.01	123.59	131.46				
Q2 (Mar - May)	117.89	117.13	124.67				
Q3 (Jun - Aug)	100.39	99.59	106.03				
Q4 (Sep - Nov)	113.42	112.57	119.84				
Average	<u>113.93</u>	<u>113.22</u>	<u>120.50</u>				
Quarter		RSP Emission (kg/day)					
Q1 (Dec - Feb)	3.68	3.12	3.31				
Q2 (Mar - May)	3.68	3.12	3.31				
Q3 (Jun - Aug)	3.68	3.12	3.31				
Q4 (Sep - Nov)	3.68	3.12	3.31				
Average	3.68	3.12	<u>3.31</u>				
Quarter		FSP Emission (kg/day)					
Q1 (Dec - Feb)	3.38	2.88	3.06				
Q2 (Mar - May)	3.38	2.88	3.06				
Q3 (Jun - Aug)	3.38	2.88	3.06				
Q4 (Sep - Nov)	3.38	2.88	3.06				
Average	3.38	2.88	3.06				

Note:

[1] Cold Start of FBSD & FBDD not included

APPENDIX 4-3

Caline4 Input

| Califor # Input for 2034 Q1 | Note | Page
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| 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 1770 | 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Caline 4 input for 2034 Q1

Road		Coordin	rate (m)		Width	Height	Road Type
Pair	X1	Y1	X2	¥2	mixing room	(m)	(calline 4)
RSAT	833254.35	821947.25	885315.56	821691.57	13	0	- 1
8162	833329.69	621353-67	ED31534	621691.04	13	0	7
R143	A33129.75	621689.31	#33160.67	#21#34.07	- 13	0	- 1
R164	833,160,17	62183A.07	#33,878.74	821782.15	- 12	0	- 1
Riss-Ries	823817.49	621976.5%	£345/458	621516.03	- 32	0	
2147+R144	833734-44	#21886:3K	SELECTED S	821727.34	18	0	- 1
R146	833728.61	821749.82	632607.73	821684.38	14	0.00	- A
R149	833774.00	621643.62	032807.73	821684.38	13	0	1
R150	833756.67	#21786.23	853607.71	821603.81	- 0	0.	
R151	833612.61	821610.98	833663.50	821663.70	13	0	4.
R151	WINGER OF	621543.70	#3377628	#21842.83.	14	0	1
WIR2	8357F4.08	621043.52	\$13EE 17	821500.58	20		7
R193	833991.31	622369.76	834678.77	622454.27	78.	0	- 1
R194	\$33950.66	222530-65	##XWZ.00	\$22189.07	18		1
8100	£33'909.46	\$22,271.36	X33000.66	922120.45	16	0	- 1
#186	833688.78	622222.16	#11M09/85	022277.30	18		- 1
8197	E23666.58	62222234	65360777	622172.96	98	0	
P153	833827.77	822172.95	#15772.49	\$22113.30	18	0	
HIRK	634070.01	622299.62	ESANTERO	622384.34	18	0	1
M160	834090.39	622287 A3	#345774T	622332.11	16		- 1
891	E34014 NO	#22250.52	834075.61	822209.62	15	0	- 1
R162	634049.42	822238.28	834800.19	822287.53	15	0	1
#163	E33993.00	62220186	834634.00	022250.02	- 10		- 1
R164	834007.86	622194-31	#34/94%AZ	ACCESS 28	15		1
RIES	#33957.31	622151.78	#259/A47	62222125	36	0	4
B158	835872.14	822651.29	82191475	822190.50	18	0	- 1
R167	633,683,47	822042.45	E34007.E8	822180.33	18	0	1
R163+R169	833813.72	\$21 87 E 47	EDWEN	027050.03	21	. 0	1
R179-9171	833716.44	421 FEB 2.15	#.E1812.49	621978-50	18	0	1
R172+R173	833864.92	821823.12	811719.26	821487.65	26	. 0	1
R174×R173	#33064.78	621407.56	£13M3.36	621623.55	16	0	1
ROL	E33496.77	f21508.45	#11560.47	621680.73	20	0	4
R177	E335(3.09	821599.24	SPAN	621688.A7	29	0	1
W172	R335410.44	621529.99	ED-PARES	621608.41	16	0	7
9179	X23451.04	621624.31	#30511.33	821400.38	12	0	1
8190	E34218.31	622286.35	\$34375.90	621585.39	18	0	1
R191 R192	E3A161.98 E3A140.62	822212.72	834391.76	022258-36	16	0	1
#182 #183	834099.34	622113.33	#34140/62	022212.3# 022162.67	18	0	1
R134	834099,34 834077.01	622113.33	#34440.62 #54851.51		10	0	1
R154	83ADE1.51	822192.68 822100.84	E3407130	822084.18	13	0	- 1
H184	#34071.00	822100.94 822084.18			14	0	- 1
	-	-	834007.30	022115.02	19	0	1
MIES.	634369-95	\$22185.5A	83438244	833187.A4			_
RIFE	E34221.54	62236 à 63	EM27134	622136.83	19	0	- 1
RIST	83A190.59	822037.73	83423176	622086.A5	- 9	0	- 1
R183+R197	834004.93	#21315 CD	834965.24	821600.22	16	0	- 1
R190-R191	823921,12	921737,74	834004.08	621816.03	39	0	- 1
#182×R (82	633876.32	621460.75	A12410.60	621727.50	29	0	1
R394-R 195	833825,79	621600.86	813867.51	621651.AB	20	0	- 1
R595+R292	8337E4.01	621523.38	#11816.17	82169558	20	0	1
R197	634364.00	622040.04	E3440E18	822104.71	- 17	0	1
RISE	834323.77	822010.68	8343M436	822060.94	18		- 1
R199	139/20193	421561.17	EJANIZACO	822010:AB	-39	0	1
R100	634239.47	#21914.13	834210.06	021003.18	44	0	1

										Vet	nicle count	for each	road										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
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150	100	100	100	50	50	150	300	350	360	300	300	300	300	300	300	350	350	356	300	250	200	200	150
200	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	350	300	250	250	700	150
200	150	150	100	100	100	200	400	500	450	450	450	450	500	500	500	550	600	600	500	400	350	150	250
150	100	100	100	50	100	150	300	400	350	300	300	300	350	300	300	350	350	350	300	250	200	200	130
150	100	100	100	50	100	150	300	400	350	300	300	300	350	350	350	350	400	350	300	250	250	200	150
300	250	200	150	150	150	250	600	750	650	600	600	600	650	650	650	700	700	700	550	500	450	400	300
750	700	150	150	100	100	200	450	600	500	500	450	500	550	500	500	550	550	550	450	400	350	350	230
400	150	300	200	200	200	350	H50	1050	950	900	900	900	1090	1050	1050	1150	1250	1150	950	850	750	700	550
350	300	250	200	150	200	350	750	950	900	800	800	900	950	900	1000	1050	1150	1100	900	800	700	650	450
450	350	250	250	200	250	400	850	1100	1000	950	900	950	1050	1050	1050	1100	1200	1100	950	800	700	700	550
450	390	300	250	200	250	450	900	1150	1000	950	950	950	1050	1000	1000	1090	1100	1300	900	750	650	930	500
300	250	200	150	150	150	300	650	800	700	650	600	600	600	600	550	600	600	550	450	400	350	350	250
250	200	150	150	100	100	200	500	600	550	580	500	500	550	550	550	600	650	600	500	458	350	350	250
300	750	200	150	150	150	250	600	750	650	600	600	600	1600	600	550	1900	600	550	450	400	350	3500	250
300	250	200	150	150	150	250	600	750	650	600	600	650	700	700	700	750	600	800	650	950	500	490	150
150	150	100	100	100	100	150	350	450	350	350	300	350	350	150	300	350	150	350	300	250	200	200	150
12	9	8	7	- 5	6	-11	50	150	50	50	-50	50	50	50	50	50	50	50	50	50	50	50	20
50	24	19	17	13	14	50	50	100	50	50	50	50	90	50	50	50	50	50	50	50	50	50	50
24	20	16	19	11	12	- 72	50	50	50	50	50	50	50	50	50	50	50	50	50	24	21	20	16
50	21	16	34	12	13	- 12	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
100	50	50	50	50	30	100	150	200	200	200	200	200	200	200	200	200	250	200	200	150	150	150	100
19	16	12	35	8	11.	17	50	50	50	50	50	50	50	50	50	50	50	50	50	22	19	18	14
100	50	50	- 50	50	50	100	150	200	200	150	150	150	150	150	150	150	150	150	100	100	100	100	50
64	62	59	58	57	58	- 63	150	70G	200	150	150	200	200	200	200	290	200	200	200	150	150	150	119
71	68	64	62	29	33	60	150	150	150	150	150	200	200	200	200	250	250	250	200	200	150	150	119
36	79	25	22	17	19	32	100	100	100	75	73	73	73	70	70	68	65	155	64	64	51	64	25
60	-59	57	55	55	35	39	173	200	171	171	119	117	117	116	114	314	112	112	1.00	58	57	51	55
100	100	44	38	- 31	35	100	150	200	150	100	100	100	100	100	100	100	100	100	100	100	100	100	71
5	7	5	A	4	4	7	17	21	17	14	12	11	13	9	7	7	4	4.	4	3	3.	3	1
16	13	11	- 3	2	8	114	50	50	90	50	50	50	50	22	19	18	15	15.	13	11	10	9	6
20	17	14	- 11	8	10	19	50	50	50	50	50	50	50	50	50	21	20	19	17	13	11	n	3
50	25	20	17	15	16	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	50	90
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	(Including	mining zone)	20	20	30	400				**	92	10		**	14	14	14	- 0	-	11	11	13	10	10	01				31	48	91	91	100	14	**	,																10	- 16	18	10	- 63	18	11	17				1.6		18			10	10	94	91	6)	**	18	13	0	16	10	92	=	15	18	18	18	*	**	110	- 52	11
101	5	822306.25	82234678	822409.45	822541.55	BUTTER VE		***************************************	873474 66	877.45K C.R.	#22454.65	822426.09	822626.54	#22465.21	822464.47	822441.65	822458.02	822387.55	\$2286034	82242288	822462.AS	122456.07	822556.02	622462.07	125425.39	822300.48	49 191724	400000	872308.34	83321878	822293.72	82234613	\$22316.78	822125.44	822-078-67	877257.83	832278 92	435144 73	10.000.00	20,307,000	*******	852484 58	822672.A7	*******		1000000	82222121	20,000,000	100000	100000		872348.57	822330.45	822250.62	822162.67	R22006.AS	622011.22	82196758	821877.95	922086.76	822007.07	822067.62	822174.73	822163128	822174.73	82212203	822164.43	822152.89	822349.92	022128.55	622115.33	822206(3)	822039-CE	621814.78	821738.42	821888 22	821727.AS	021889.31	821947.78	622007.97	#2200B72	621163.31	821863.31	821891.67	821062.74	821763.88	82181288	621795.91	121802.67
~	ate (m)	83347737	833231.06	833434.80	823900.46	22300164			*******	A1167151	43341347	833973.71	834046.15	831527.55	833712.87	833782.11	833840.51	83196159	83384185	83389664	83388354	833846.51	83342249	833418/08	933447.92	93354464	93398736	4446444	4 833.044.47	RAYBORDS	63338666	83546561	83348948	833100.53	833237.0K	821477.80	83155134	41141143		40,000	41101741		83311178		4000000		***************************************	1000000	74.1.		*********	91190216	83395646	834034.90	534540.62	83423428	83432121	134394.01	833158.58	957	833274.46	170	83368833	3734.68	833468.33	1268671	33649.55	83161368	833713.85	833747.83	835778.45	83367234	833867.20	93410921	934255.10	83406834	034341.81	63343974	93328678	93346651	13364373	131543.70	833563.70	832315.56	833481.00	933476.47	93125216	833254.16	93332666
4 input for	Coordinate	11 PEZZZZZ	822330.25	822345.74	827408.48	BOTE 43 00	*********	***************************************		ETANTAM.	822466.68	832614.05	822628.09	822419.61	822455.21	832494.47	822441.00	822398.31	822297.16	822463,30	82243288	822462.40	822567.47	832554.02	522462.05	82242838	222394	PERSONAL BILL	877774.01	823162 63	822239.76	877783772	822345.13	822119.68	823428.64	AD1478.02	822222.03	*******		BOTTE SE	417464.74	*******	ATTORE TO	********	200760		Maria M	200000				#2235.17	822360.57	822320.48	877750.57	\$22162.67	822084.85	873010.68	621955.43	821977.96	821642.33	822004.80	822088.21	822 (23.88	822163.25	8270027.29	82212203	822144.40	622152.80	822149.62	622122.55	822123.04	822113.30	822062.66	621814.78	822(1)9-23	821889.22	821680.28	621889.31	821547.50	822008.03	822028.72	\$21952.82	70.54.05.00	8214891.68	821775.07	821783.15	821757.87	821820.73
e 4 in	*	633126.78	12,771228	833231.06	833454 80	STATES AS		10.20.010	******	61361676	813673.76	131533.67	633973.71	633527.00	833627.68	E33732.87	633782.11	633661.17	613693.59	833978.15	13,0696.04	633883.54	623387.36	633423.09	633476,08	633447.62	20394.04		41161147	#310k3 47	E33209.07	633355.00	RESARD OF	833073.42	833166.83	K13233.04	611177.60	235443.69	*******			835647.83	813074.00		200,000	27777	#13.77# TA				**********	RESESTA 16	12	833950.40	634034.90	SMARKED ST	614231.72	834322.77	833097.20	613156.56	613101.67	833274.00	833434.15	613736.86	833734.06	833438.83	633586.71	25,649,55	833683.66	833713.66	533757,63	633734.53	832778.49	833873,29	634195.21	613867.79	EDADSS 34	#3311E.37	633139.76	£13298.66	633460.69	832543,73	633480.98	11.001.01	833315.06	633154.01	633178,74	F13168.60	833249.00
Caline	Road	R003	R003	R003	8003	2000	2000	-	8000	Bares	8000	R005	REGES	RESTS+RIGOT	R006-R007	R006*R007	MIDDS-ROOT	RS18+R009	REDDR - R-DOR	Rp10+Rp11	R010-H011	RECU-ROCE	Rotz-Rot2	R013+R013	MO12-MO13	R012+R013	MOLES HAVE	David-Bite?	Berris Berr	Rote	8.621	Bett 2	R422	R023	R024	BASSA	meze	RAST	*****	Dane.	Bette	H03+	EM17+ B 10+	- Contraction	1	Willes .	West a	Berry	and a	-	-	1994	N042	N943	ROAA	Bass	Ross	R847	HOAR	8549	mose.	Rost	R052	RESES	NOS3	H054	H054	R05.4	NO84	H054	R054	ROSS	Moto	H057	Resa	BOXO	NONO	1 00 H	ROSZ	RINGS	NO4	*100*	1094	ROKS	RONG	1106F	ROSE	RONG	HOTO

Caline 4 input for 2034 Q1

| 87.10.0 | 447640 | 10000 | 107516 | |
 | Lowers | 1.704 | T TOTAL | 20000 | 247014 | Lesson |
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8510.0	9510'0	1210.0
 | 0.0164 | ZZ10'0 | \$610.0 | Z210.0
Z210.0 | 0,010,0 | 8510.0 | 15100
 | 0.0211 | 0.0220 | 50100 | 0,0190
 | 0120.0 | 80200 | 0.0152
 | 0.0154 | 0.0212 | 5210.0
7150.0 | £210.0
 |
| 85100 | 0510.0 | 9ETO C | 1510.0 | SSTOO | #£100
 | E310.0 | 95100 | \$5100 | 0.0150 | t9t0.0 | 0.0139 | 05100
 | 9410.0 | P\$100 | 29100 | 6810.0
 | \$5100 | 05100 | 8610.0
 | SETO 0 | 09100 | 55100 | 6010.0
 |
| 8510.0 | 09100 | DETG'0 | 1210.0 | \$\$100 | 82100
 | E910'0 | 95100 | \$5T00 | 0.0150 | 1910'0 | 66100 | 0.0150
 | 9910'0 | P\$100 | 89100 | 681070
 | 95100 | 09100 | 86100
 | 8E1U 0 | 0.0160 | 55100 | 69100
 |
| 1/100 | PS10'0 | 0510'0 | £910'0 | 0510.0 | 1619.0
 | 6710.0 | 69100 | 6910'0 | \$9t0.0 | 9510.0 | £510'0 | 59100
 | 6510'0 | 1710.0 | £810'0 | T020.0
 | 5910'0 | 05100 | 05100
 | 0.0150 | 00120 | 94100 | \$9100
 |
| 502010 | £510'0 | 9610'0 | E550.0 | 6810,0 | 0.0204
 | E610.0 | 5610'0 | 6610'0 | 1610.0 | 5070'0 | 0.0183 | 56100
 | 5610'0 | 8810.0 | 46100 | 0.0260
 | 1550.0 | 8750.0 | 098070
 | 9410.0 | 9/160/0 | 1050.0 | 1920'0
 |
| 8210.0 | 6910.0 | 0910 C | 2910.0 | S810'0 | 0.0210
 | 640.0 | 8710.0 | 6810.0 | 0.0187 | 1610.0 | 64100 | COTRY
 | 18100 | 6610.0 | 0.020.0 | 8050.0
 | 9210.0 | 16100 | 0.0211
 | 0.0221 | 0.0207 | 9610'0 | 2810.0
 |
| 1/100 | E\$10'0 | 0.0154 | 1/10.0 | 0810.0 | 0.0211
 | £610.0 | 1810.0 | 1610.0 | 0.0199 | 4050.0 | 0,0200 | 0.0208
 | 0.0207 | 0.0224 | 0.0214 | 0.0222
 | 1610.0 | 0.0212 | 0.0232
 | 0.0242 | 0.0231 | 0.0215 | 1020.0
 |
| 21100 | 8010.0 | 2,0115 | 0.0121 | 2110.0 | 0.0130
 | 0.0126 | 0.0120 | 0.0129 | 0.0132 | 8£10.0 | 1910.0 | 0.0143
 | 8310.0 | 09100 | 91100 | 1410.0
 | 7610.0 | 67100 | 65100
 | £910.0 | 1910'0 | 1910'0 | 95100
 |
| 9910'0 | 0410.0 | 94£0,0 | 620.0 | 0910/0 | 98100
 | E710.0 | 5710.0 | 6910.0 | 0.0160 | £510.0 | 0.0154 | E910.0
 | 6510.0 | 8710.0 | 06100 | £020.0
 | £910°0 | 19100 | \$910.0
 | 1910.0 | £910.0 | 1910.0 | £910.0
 |
| 19100 | 99100 | 2010.0 | 0910.0 | 19100 | ENTOD
 | 1710.0 | 19100 | 79100 | 7210.0 | 9910'0 | 59100 | 85100
 | 25100 | E9100 | 1710.0 | \$610.0
 | 7210.0 | 2510.0 | Z\$10°0
 | 7210.0 | Z510'0 | 7210.0 | 2510.0
 |
| 29100 | 5910'0 | TMO.0 | 8510.0 | 5910.0 | 0.0187
 | E710.0 | E9100 | 6,0163 | 6510.0 | 8910'0 | T\$10.0 | 6210.0
 | 951010 | 19100 | 8710.0 | 9610'0
 | 8510.0 | 85100 | 85100
 | 0.0158 | 8510.0 | 8510.0 | 8510.0
 |
| 0.0182 | 2910.0 | 9910'0 | 77,10.0 | 8110.0 | 0.0204
 | 0eto.0 | 0.0183 | 6210.0 | \$710.0 | 1810.0 | 69100 | 52100
 | 6910'0 | 92100 | 8810.0 | 8050.0
 | 9210'0 | 82100 | \$410.0
 | 2510.0 | 1710.0 | 9210.0 | 92100
 |
| 0.0184 | 9910.0 | 6910'0 | A810.0 | \$810.0 | 11700
 | £610.0 | 8810.0 | 9810.0 | 2810.0 | 2610.0 | 2710.0 | 0.0185
 | 67.10.0 | 7810.0 | 66100 | 0.0215
 | £810.0 | 0.01mg | 0.0184
 | 0.0183 | 1810.0 | 0.0184 | 1810.0
 |
| 9550.0 | 0.0142 | TSTO C | 0.0164 | 0.0230 | 0.0262
 | 0.0242 | 0.0228 | 11/20.0 | 8710.0 | 0.0183 | \$6200 | 0.0236
 | 0.0177 | 0.0190 | 1610.0 | 0.0215
 | 0.0221 | 0.0214 | 0.0183
 | 0.0240 | 0.0220 | 0.0184 | #870°C
 |
| 66100 | 1120.0 | 9120.0 | \$310.0 | 10200 | 0.0272
 | 8020.0 | 0.0202 | 0.0203 | 0.0200 | £810.0 | 98100 | 96100
 | 0610 0 | 2020.0 | 0 0 0 0 0 1 | 9150.0
 | 1610.0 | 16100 | 8810.0
 | 0610.0 | 5610.0 | Z610.0 | 1610.0
 |
| 19100 | 2510.0 | PETO,0 | P210.0 | 6910.0 | P5100
 | OELO.O | 2910.0 | 0/10/0 | 10000 | 884D.0 | 99100 | 0.0160
 | \$510.0 | Z9100 | 06100 | 0020.0
 | 1919.0 | 09100 | 0910.0
 | Z910'0 | 1910.0 | 19100 | 2910.0
 |
| 28100 | 0910.0 | 9510,0 | Z810 0 | SRIGO | 01200
 | 8610.0 | N810.0 | 06100 | 5810.0 | 6610.0 | 84100 | 26100
 | /810.0 | 46100 | 10200 | 0.0219
 | 8810.0 | 20200 | 90539
 | 1220.0 | 51200 | 0.0204 | 56100
 |
| 00000 | 5610.0 | 9910.0 | 9610.0 | \$610.0 | 7120.0
 | 6610.0 | P8100 | \$810.0 | 1810.0 | 8610.0 | Eato.0 | 92700
 | 8910.0 | 8210.0 | SHIDO | 1150.0
 | \$710.0 | 64100 | 9/100
 | 0.0181 | 0.0172 | 82100 | 84100
 |
| 6,00217 | 8020'0 | 1020.0 | 2020.0 | 0.0214 | 86.70.0
 | 8120.0 | EIZO'O | 8770'0 | N120.0 | 4110.0 | 9070'0 | 0.0210
 | 0.0207 | 1120.0 | 0.0214 | £520.0
 | 8610'0 | 86100 | 4610.0
 | 100,000 | 0,0203 | 7610.0 | 96100
 |
| NTZO O | 1050.0 | 6020°C | E020.0 | 9170'0 | 967070
 | 6t20.0 | EIZOO | Stzoo. | 0.0214 | 9110.0 | 9070'0 | 0.0208
 | 4050.0 | 8020'0 | 8020'0 | 2220.0
 | \$610.0 | 6610'D | 86100
 | 0.0302 | 1610.0 | 1610.0 | 461010
 |
| BISCOO | 7050.0 | 0.920.0 | 0.0203 | 0.0216 | 96200
 | 0.0219 | P120'0 | 8170.0 | 0.0215 | 0.0216 | 9020'0 | 0.0209
 | 5020.0 | 9020'0 | 0.0209 | 0.0221
 | 4610.0 | 16100 | 0.0205
 | 6810.0 | 0.0198 | 96100 | 66100
 |
| 8150.0 | 1050,0 | 0.0207 | 0.0203 | 0.0214 | 0.0235
 | 0.0219 | 802010 | \$120°0 | 0.0214 | 7150.0 | 10020.0 | 0.0210
 | 0.0207 | 1020.0 | 00210 | 0.0223
 | 8610.0 | 56100 | 90200
 | 0610.0 | 8610.0 | £610'0 | 002010
 |
| 21100 | 8050.0 | 0.0207 | E020.0 | \$120.0 | SEZO'O
 | 0.0219 | 6.0212 | 0.0218 | 0.0215 | 7150.0 | 1020.0 | 0.0210
 | 0.0207 | 6,020.0 | 00270 | \$£50.0
 | 6610.0 | 0.0203 | 6,0203
 | 1010.0 | 5610'0 | E610.0 | £610.0
 |
| 7250.0 | 95200 | 6550.0 | 0.0340 | 1520'0 | 2150.0
 | Z520'0 | P970'0 | 6920'0 | 0.0272 | \$450.0 | 6420'0 | 0.0278
 | 0.0282 | 0850.0 | 1920 0 | 2550.0
 | 7202.0 | 65200 | 0.0362
 | \$570.0 | 6520.0 | 0.0262 | /520 C
 |
| 0.0220 | 0.0212 | 0.0212 | 0.0210 | 0.0222 | D.0247
 | 0.0226 | 0.0221 | 1520.0 | 8,550.0 | 0.0230 | 6120.0 | 0.0223
 | 0.0220 | 0.0224 | 0.0223 | 0.0232
 | 0.020.0 | 0.0204 | 0.0203
 | 0.0207 | 7610.0 | 0.0203 | 9070
 |
| 0.0325 | 66100 | 0,0214 | 5610.0 | 0.0206 | 0.0231
 | 0.0215 | 0.0205 | 0.0213 | C020.0 | 8050.0 | 76£0.0 | 0.0203
 | 8610.0 | 66100 | 9070'0 | 6,0223
 | 0.0204 | 0.0220 | 0.0155
 | 8910'0 | 1510.0 | 0.0200 | 0810.0
 |
| 6050.0 | 2110.0 | OZEO.0 | 9820,0 | \$0E0/0 | SEEOO
 | 6060.0 | E6Z0'0 | £1/E0.0 | 2250.0 | raed.o | 8950.0 | 0.0369
 | 0.0384 | IBEO.0 | SEEOO | NZEO.O
 | SEED.O. | 0.0354 | \$SED'O
 | 6,6377 | 9260,0 | HA-EO.O | 1550.0
 |
| 0.0230 | 1550.0 | MISQ.C | 0.0212 | 0.0220 | 972010
 | 0.0224 | \$150.0 | 0.0226 | E550.0 | 2550.0 | 11200 | 51200
 | 91200 | EISO.0 | 7150.0 | P.ESO.0
 | 6050.0 | 0.0202 | 0.0221
 | 9220-0 | 0.0210 | 5610.0 | 2120 0
 |
| 0.0225 | 0,0214 | 0.0223 | 0.0218 | 0.0222 | 30.000
 | 6550.0 | 8150.0 | 0.0225 | 0.0221 | 0.0224 | 60200 | 0.0214
 | 0.0211 | 1120.0 | 91200 | 9650.0
 | 0.0204 | 66100 | 0.0214
 | 8120.0 | 6,0203 | ELSO.O | 90200
 |
| 0.0244 | 0.0315 | 0.0230 | 1120.0 | 0.0223 | 0.0250
 | £220.0 | 0.0220 | 0.0230 | 0.0220 | 85,00.0 | 6120.0 | 0.0218
 | 0.0210 | 0.0212 | 5120'0 | 0.0232
 | 8610.0 | 80200 | 0.0227
 | 6ES0.0 | 7150,0 | 7610.0 | 10000
 |
| 0.0139 | 0.0230 | 0.0219 | 0.0234 | 0.0226 | 9970°0
 | 0.0229 | 0'0333 | 1620.0 | 0.0224 | 0.0228 | 60200 | 0.0215
 | 01200 | 91200 | 61200 | 0.0231
 | 0.0199 | 0.0208 | 0.0236
 | 1850.0 | 6120.0 | 1050.0 | 20200
 |
| 0.0239 | 0.0230 | 5220.0 | 0.0233 | 0.0233 | 79200
 | 6.0229 | 60223 | 6EZ0.0 | 2650.0
2650.0 | 8550.0 | 2120'0 | 02200
 | 0.0221 | 0.0224 | 8220.0 | 8620.0
 | 60707.0 | 50200 | 65550.0
 | 8270'0 | 0120/0 | 100.0 | Z1Z0'0
 |
| 69200 | 55200 | 5520.0 | BES0.0 | 8EZ0:0 | 1/200
 | 9420.0 | SEZO:0 | 9520.0 | 1/20'0 | £820.0 | 5970'0 | 9970'0
 | 1420.0 | 1620.0 | 5/200 | 2620.0
2650.0
 | 9/200 | 87200 | 0520.0
 | 0920.0 | \$E20,0 | \$820.0 | 09200
 |
| 19200 | 6550.0 | 9350.0 | E#70.0 | 0.0241 | SEZOO
 | 0.0252 | 0.0253 | 64200 | N750.0 | 7950.0 | 9060.0 | 5060.0
 | £1(0,0 | P0E0.0 | 0.0284 | 2620.0
 | 0.0297 | 98200 | 0.0278
 | 1650.0 | 0,0262 | 80£0.0 | 2620.0
 |
| 58200 | 69200 | 5/200 | 0.0262 | 0.0273 | 0.0302
 | 6/20.0 | 99200 | 10000 | 9060.0 | LIED.O | STEGO | Q.0317
 | 0.0314 | 7550.0 | 1620.0 | E150.0
 | 8750.0 | 90000 | 0.0281
 | 6820'0 | 94200 | E750.0 | LEZO
 |
| 8750.0 | 9820'0 | 0.0282 | 0.0258 | 0.0280 | 6160.0
 | 6620.0 | 9450.0 | 0.0323 | 0.0332 | 0.0339 | 0.0350 | 0.0349
 | P300.0 | ETEO.0 | SZEGO | 0.0337
 | \$2E0.0 | 61500 | 0.0334
 | 1000.0 | 0.0303 | 9150'0 | 4000
 |
| 2650.0 | 1520'0 | 0.0241 | 0.0234 | 0.0243 | 0.0280
 | 0.0241 | E920'0 | 0520'0 | 1920'0 | 8520'0 | 19200 | 0.0246
 | 11700 | 4920'0 | 0.0260 | 8520.0
 | 87700 | 12100 | 19100
 | £910.0 | 0910'0 | Z820'0 | TSZ0'0
 |
| E\$20.0 | 5920'0 | 0.0244 | Z#20.0 | ZÞZ0'0 | 6250.0
 | 80.00.0 | 89200 | 15200 | 1520.0 | £250.0 | 6520.0 | 5520.0
 | 7250.0 | 9570'0 | 0.0254 | 0.0250
 | 6453.0 | 0.0247 | 0.0249
 | 1950.0 | 0.0247 | 99200 | 2520.0
 |
| \$800°0 | 0100,0 | \$100.0 | 780070 | 0800.0 | \$8100.0
 | £600°0 | 06000 | 26000 | 16000 | 5010.0 | 96000 | 50100
 | 10100 | E1100 | 00110 | 8110.0
 | 0.010 | 11100 | 1110.0
 | 6010.0 | 60100 | 01100 | 60to 0
 |
| 90200 | 0.020.0 | earo,c | 5610.0 | 01200 | 0.0240
 | 0.0224 | 902010 | 0.0215 | 0.0210 | 0.0214 | 1610.0 | 0.0204
 | 0.0204 | 0.0210 | 0.0221 | 0.0233
 | 2610.0 | 66100 | 86100
 | 86100 | 7610.0 | Z6100 | 2610.0
 |
| 0.0206 | 0.0200 | 6810.0 | 5600.0 | 0.0210 | 0.0240
 | 0.0224 | 90200 | ST20'0 | 0.0210 | 0.0214 | 16100 | 0.0204
 | 0.0204 | 0.0210 | 1550.0 | 6.620.0
 | 2610.0 | 66100 | 8610.0
 | 8610.0 | £610.0 | 7610.0 | 5610.0
 |
| Eff0.0 | £610,0 | 7810.C | 7eto.o | 6050.0 | 6EZ0'0
 | 0.0222 | 0.0210 | 0.0220 | 0.0214 | 9110.0 | 0.0203 | 0.0209
 | 9000'0 | \$150.0 | 5220.0 | 2850.0
 | \$610.0 | \$610.0 | 0.0189
 | 8810.0 | 8810.0 | 5610.0 | £610.0
 |
| 5500.0 | 7200.0 | 2800.0 | 8200.0 | PS00'0 | 65000
 | 1900 0 | 29000 | 6900'0 | 8900.0 | 0,000.0 | 1/00.0 | 2000.0
 | 0.0085 | P800.0 | 99000 | £600.0
 | Z800 0 | 0.0083 | 6,0083
 | 5,800.0 | 0.0082 | Z800.0 | 2800.0
 |
| 5500'0 | Z500'0 | 5500.0 | 8500.0 | 15000 | 6500'0
 | 1900.0 | 29000 | 6900'0 | 8900.0 | 0700.0 | 4/00.0 | 5700.0
 | 2800.0 | 4800.0 | 9800.0 | £600.0
 | 0.0082 | 5800.0 | 6800.0
 | £800.0 | 2800.0 | Z800'0 | 2800.0
 |
| 5500'0 | 7200.0 | 5500.0 | 8500.0 | 1500'0 | 6500.0
 | 1300.0 | Z900'0 | 6900'0 | 8900.0 | 0100.0 | 6700.0 | 52000
 | 5800.0 | 4800.0 | 98000 | £600.0
 | 7800.0 | 0.0083 | £800.0
 | £800.0 | \$800.0 | Z800.0 | Z80010
 |
| 550010 | £500'0 | 5500'0 | 8500.0 | \$500°0 | 6500'0
 | 1900.0 | Z900'0 | 6900'0 | 8900.0 | 0100.0 | 0.0074 | 52000
 | 5800.0 | 4800.0 | 98000 | £600.0
 | \$800.0 | 5800.0 | 5800.0
 | 6.800.0 | 1800.0 | Z800.0 | 7800
 |
| 0.0055 | £500'0 | 2500.0 | 8500.0 | 1/500/0 | 65000
 | 1900.0 | \$900.0 | 6900'0 | 8900.0 | 0700.0 | 4100.0 | 52000
 | \$800.0 | \$800.0 | 99000 | £600.0
 | 5800.0 | £800'0 | 0,0083
 | 6,0083 | 1800.0 | Z800'0 | \$800.0
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| 5500'0 | £500'0 | 2200.0 | 8500.0 | 9500'0
9500'0 | 65000
 | 1900'0 | 2900'0
0'000'5 | 6900'0 | 8900.0 | 0700.0 | VL000 | 52000
 | 0.0085 | 1/800.0 | 99000 | 6600.0
 | Z800.0 | 0.0083 | 6800.0
 | 0.0063 | 0,0082 | 2800.0 | 2800.0
 |
| \$500°0
5500°0 | 2500'0
2500'0 | 5900°C | 8500.0 | \$500°0 | 6500°0
 | 1900'0 | 79000 | 6900'0 | 8900.0 | 0500.0 | \$500.0
\$500.0 | 5200°0
 | 0.0085 | 0.0084 | 9890'0 | £600.0
 | 7800.0 | £800'0 | £800.0
£800.0
 | 6800.0 | 7800'0 | C800.0 | 78000
 |
| 9500'0 | PS0070 | 9500,0 | R200.0 | 9500'0 | E3000
 | 5900.0 | \$9000 | 6,0073 | 1/00/0 | £500.0 | 6100.0 | 64,000
 | 1600'0 | 5600'0 | 10100 | 8600.0
 | £800 0 | 28000 | Z800.0
 | 0.0083 | E800.0 | 0.0082 | E800 C
 |
| 9500'0 | 9500'0 | 9906'0 | 8500'0 | 95000 | 19000
 | 5900.0 | \$900'0 | £4000 | 1/00.0 | £200.0 | 6100.0 | 62000
 | 1600'0 | \$6000 | 10100 | 8600.0
 | 6,808.3 | 2800.0 | 0.0082
 | 0.0083 | £800.0 | C 00083 | £900°C
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| 9500'0 | 8500,0 | 9900'0 | 8500.0 | 9500'0 | 19000
 | 90000 | 99000 | \$2000 | 1700.0 | £400.0 | 6400.0 | 62000
 | 1600 0 | \$6000 | Tetoe | 8600.0
 | 0.0083 | 7800'0 | Z800'0
 | 0.0083 | E800.0 | 2800.0 | £800.0
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| 9500'0 | 8500'0 | 9500'0 | 8500.0 | 9500'0 | 89000
 | 5900'0 | \$9000 | £700.0 | 1700.0 | £100.0 | 6400.0 | 6/,0070
 | 1600'0 | \$600'0 | 10100 | 8600.0
 | £800.0 | 0.0083 | C800.0
 | 5800.0 | \$800.0 | Z800.0 | £900°C
 |
| 9500'0 | 9500'0 | 9900'0 | 8500.0 | 9500'0 | 19000
 | 5900.0 | \$900'0 | 6,000.3 | 1700.0 | £400'0 | 6400'0 | 67.00.0
 | 16000 | 56000 | 10100 | 8600.0
 | E803 0 | Z800 D | Z800'0
 | 0.0083 | 0.0083 | 0.0082 | E900°C
 |
| 9500'0 | R\$00'0 | 9900'0 | 8500.0 | 99000 | 19000
 | 5900'0 | \$9000 | 6,000.3 | 1400'0 | £400'0 | 64000 | 64000
 | 16000 | \$600'0 | 10100 | 8600.0
 | 0.0083 | 0.0082 | 0.0082
 | 6,0003 | £800.0 | 0.0082 | 5800.0
 |
| 9500'0 | 8500'0 | 9900'0 | 8500.0 | 9500'0 | 1900'0
 | 5900'0 | \$9000 | ££00'0 | 1400'0 | E100,0 | 6500,0 | 62000
 | 160000 | \$600'0 | 1010'0 | 8600.0
 | 6.8083 | 2800.0 | Z800'0
 | 6,0083 | £800'0 | Z800'0 | £800°C
 |
| 0.0214 | 9110.0 | TIXO.C | 91700 | 2150.0 | 62200
 | 0.0219 | 61100 | 0.0220 | 0.0220 | 0.0132 | 91700 | 0.0219
 | 81000 | 6120.0 | 61200 | 1110.0
 | 0.0214 | 0.0214 | 0.0215
 | 2150.0 | 5120'0 | 2150.0 | 5110.0
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| 0.0182 | ££10.0 | BZ10.0 | 6/10/0 | 6210/0 | 26100
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 | 8/10/0 | 8710.0 | 8710.0
 | 8710.0 | 8710.0 | 8710.0 | BATO
 |
| 0.0182 | 44100 | 8210.0 | 6710.0 | 64100 | 26100
 | 0.0182 | 84100 | 6210.0 | 8710.0 | 2810.0 | 0710.0 | 0.0180
 | 0.0172 | 09100 | 18100 | 0.0202
 | 8710.0 | 87100 | 8/10/0
 | 8510.0 | 0.0178 | 8710.0 | 84100
 |
| 2610.0 | 9810'0 | 6810.0 | 1610.0 | 2610/0 | 2120.0
 | 6610.0 | P610.0 | 9610'0 | 1610.0 | 8610.0 | 8810.0 | 26100
 | 0610.0 | 9610'0 | 96100 | 0.0211
 | 5810 0 | 78£0.0 | 8810.0
 | 8810.0 | 7810.0 | 7810.0 | 9810.0
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| 2610'0 | 9810.0 | 9810.0 | 0.0194 | 2610.0 | 0.0212
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 | 0610'0 | 9610'0 | 96100 | 0.0211
 | 0.6185 | 4810.0 | 0.0188
 | 8810.0 | 7810.0 | V810.0 | 9810.0
 |
| 26100 | 9810'0 | 6WIO.0 | ME10.0 | 2610.0 | 21200
 | 6610.0 | 9610'0 | 96100 | 0.0194 | 8610.0 | 88100 | 26100
 | 0610'0 | 96100 | 96100 | 1150.0
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| 6810.0 | £810.0 | 0010.0 | 0610.0 | 8810.0 | 1120.0
 | \$610°0 | 68100 | \$610.0 | 0.0190 | 8610.0 | 0.0182 | 0.0190
 | \$810.0 | 0610.0 | 1610.0 | 6050.0
 | 1810.0 | 08100 | 1810.0
 | 1810.0 | 1810.0 | 0810.0 | 64100
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| | Z\$10'0 | 9210.0
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 | 8510.0 | 82100 | 7£10.0 | 5510.0
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| | | 9510.0 | | SETOTO | 0.0142
 | 9610.0 | EE100 | 19100 | 7E10.0 | 6,0143 | 19100 | 00100
 | 09100 | 60126 | 75100 | 9610.0
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| 01100 | 2010.0 | 9510'0 | 6610.0 | |
 | | | 5020'0 | 2020.0 | 0.0205 | 26100 | 0.0200
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	ń	- 02	PC-GABISE	92349558	421632.93	26,500,033	
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	Pair	X4	44		Y2	prichating princip	gua	(Califoli 6)	Hroo	Hro
	5141	655295.35	821847,25		821881.67	-63			0.0219	100
2008 MIN MARIA (2014) CORTINATION (2014) CORT	8142	822222.88	121153.47			13			0.0139	0.012
December December Decembe	RT48	835139,75	BRIDGER	133700-17	821534.07	18.	10 mm	1.	0.0210	0.023
100 100	0.144	11316517	121834.07	833118.74	621153.15	13.			0.0213	0.023
100 100	R145+B146	633812-69	821975.50	83100438	823 B16.03 -				9,0076	0.017
1979 1979	RIGT-RIGH	E2373E-84	SQUARK 28	932931.13		- 44			0.0171	0.016
No.	R140	E33728.61	821749.32	033897,73	\$21684.38	14	0		9910.0	0.016
Company Comp	8149	633774.06	E21343.52	83380773	621684.36	13	9		0.0166	0.616
1916-190 1916-190	R150	633736.67	821739:20	83386731	82180187	. 11			9910'0	0.016
1977-14 1976	RtSt	623613.61	8211111 SE	62268250	\$21542.79	11	. 0		99100	0.016
	RTS1	E21693.00.	E21543.7V	10377528	821642.53	14	0	4	0.0166	0.016
10,000 1	R152	813774.08	221543.52	833828.17	821609128	2.0	0	. 4	9910'0	0.016
1979 1979	R153	613391.31	812389.74	834018.77	922414.27	- 13	0		0.0186	0.017
	R154	E23950.86	\$22,125.45	83389200	\$22,269.87	1/8	9		0.0186	0.017
COMMENT RESTRICT STREAM 1 COMON COMMENT RESTRICT STREAM 1 C C COMON REFERENCE REFERENCE STREAM 1 2 1 C C C REFERENCE REFERENCE REFERENCE 1 2 1 C	R156	833309.65		13390046	822320.45	18.	0.		0.0157	0.017
CARRANTO SERVICA STATES 11 2 1 0.02000 CARRANTO STATES 11 2 1 0.02000 CARRANTO STATES 11 2 1 0.02000 CHORGES MARCHAN STATES 11 1 0.02000 CHORGES MARCHAN STATES 11 1 0.02000 CHORGES MARCHAN STATES 11 0 0.02000 CHORGES MARCHAN STATES 11 0 0 0.02000 CHORGES MARCHAN STATES 11 0 0 0.02000 CHORGES MARCHAN STATES 12 0 0.02000 0 CHORGES MARCHAN STATES 12	R156	633668.76	811777318	83280845	\$2,172,52	10			0,0223	0.023
Part	Britis	EX3862.56	8222238	83382727	82217238			*	0.0204	0.020
Company Comp	Rtta	613827.77	822172.06	83277258	\$2231525	- 13	9		0.0200	0.020
Particle	RTSS	134075.91	#22398.62	154117290	622344.34	12			0.0190	0.019
	6,16.0	834(980,29	127.117.53		11.222.52	18	e	1	0.0194	0.520
	RISE	834134.9E	822259 53		822298.62	- 80	-		0,0104	9100
Section Sect	B162	E34046-42		83406E38	622287.53	18			0.0193	0.019
Charge C	R162	622993.06		13403430	14 462229	99	0	-	0.0158	0.019
1,000 1,00	R164	854(07,86	\$22111.33	93404842		2	6	-	0,0184	0018
1,000 1,00	RIES	613953.31	822151.70	93389447		. 91	0		0,000	0.023
	RISS	833672.14	822051.58		622160.50	19	9	-	0.0176	0.017
	RTST	131015.47	173042.45		622409-33		0	-	0.0275	0.027
	RIGA-RIGS	612611.72				11	0	-	0.0108	0.011
123-124 124-	RETU-RETE					83			0.0125	0.012
	RITZ+R17.		82182233	83377628		20		-	0.0186	0.018
COURT COUR	N174-R176		E21077.30	83368338				-	0.0200	0.020
	Betze	653496.77	621608.49	833565.47		26			0,0200	0.020
Part	RITT	813813.08	821899.24	83167168		75			0,0189	8100
	RITE	833440.44	821529.50	353453.00	#21609.61	48	-		67200	d
PROPERTY CLUSTON PROPERTY CLUSTON PROPERTY CLUSTON C	RITE	13261.64	E11626.29	13381132	621609.28				0.0216	0
	6180	634216.31	\$27.558.35	93433599	822286.38				0.0208	0
Design Control Contr	1	200.00	2000	1000000	277.00.77		-		0,010	9
	2	20111000	10741000		46577778		-	I	0.000	1
	W193	E34098.34	B2211233	25666656	10.250.220				0.0008	9 6
Heartown Dishear Dade Date	B184	#12061 CT	80701775	834071.94					0,000	3 6
SERVIN STRIKE 194544 153974 19 0 1 1 0.000	4117	814071 80	875/06.4.18	0.740047.0		,			2000	3 0
SECTION SECT	6110	634309.05	822180.58	93428246	822287.44				0.0302	0.030
Debarder Chicago Chi	0.186	634231.54	19 940728	83427334	822136.83	91		. 4	0.000	0.022
Company Comp	R187	E34190.59	822057.73	03423176	\$22046.45	36	a		0.0215	0.023
CORPUT C	R188+R189	834004.88	821814.03	93499834	#21089.31	**			0.0151	6100
CHESTA STATES STATES STATES STATES COURT	9100-N191	633831.13	621727.34	88,900,858	621815.03	. 81			0.0212	0
March Marc	R162+R195	\$33 ET 27	82169.75	833800.85	821727.98	2.0			0,0057	0.0
DESCRIPTION	R154+R198	£13£2£.79	621905.50	833847.51		- 13	9		0.0217	0.022
	#199-K302	833761.01	824923.38	\$33828.17	821509.66	50			0.0210	0.023
	1619	834384.36	SECOND 19		822104.71	11			0,0169	0.017
84335.0 67404.0 634360-0 62364.0 14 6 7 0.024	R19F	636322.77	89/01/229		82200E 94	18	-		0,0169	9000
ENGLISH STREET, STREET	8199	834281.93	62(16.1.17	034331200	822010.48	18		-	0.0234	0
	M200	834239.17				*			0.0184	8100

Control Cont	Hr02 Hr03	Hr04	Hr05	H/06	Hr07	Hr08	60JH	011	-	Hr12	Hr13	Hr14	H	HITE	Hr17	HITE	Hr19	Hr20	HEZ	777
Coling C	0.0176	80172	0.0173	0.6209	0.6230	0.0234	0.0224	0.0214	0.0205	0,0157	0.0208	00100	49100	6,000	0.0162	0.0196	0,0173	99100	0.0151	0,0147
Coling C	0.0104		0.0128	0.0159	0.0154	0.0144	0.0163	0.0063	0.0165	0.00.75	0.0171	0.0173	0.0173	99100	92100	0.6181	0.0174	0.0177	0.0206	- 96100
Coling C	Н	ŭ	0.0206	0.0036	0.0237	0.0221	0.0233	0.0216	0.0215	0.0202	0.0210	0.039	0.0197	0.0155	26100	0.0203	0.0183	0.0172	0.0160	7510.0
1,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0	Н		0.0207	0,020	0.6239	0.0220	0.0222	0.0214	0.0210	0.0196	0.000E	0.0193	0.0193	0.0183	0.0158	0.0200	0.0180	0.0172	0.0161	95100
Control Cont	0,0169	Ц	0.0179	0.0374	0.0210	9.0194	0.0177	0.0054	0.0169	0,0153	0.0173	0.0161	59100	0.0163	0.0173	0.0386	0.0161	0.0146	0,0121	97100
	0.0172	_	0.0176	0.0173	0.0308	0.0154	0.0173	0.0161	0.0165	0.0150	0.0170	0.0159	0.0163	65100	0.0169	0.0182	0.0157	0.0139	0.0134	0.0124
	0.0169		0.0165	0.0165	0.0206	0.018.1	0.0168	0.0160	0.0165	0.0155	0.0175	0.0165	0.0171	0.0170	0.0179	0.0195	0.0171	0.0172		
	0.0169	ľ	0.0165	0.0165	0.0206	0.0183	89100	0.0360	0.0165	0.0153	0.0175	0.0165	0.0171	0.0170	6,0179	0.0195	0.0171	0.0172		-
	0,0169		0.0165	0,60,65	0.0206	0.0183	0.0168	0.0160	0.0165	0,0158	0.0175	0.0165	00171	00176	60100	0.0195	0.0171	0.0572		-
	9,0169	F	0.0165	0.0166	0.0706	0.0183	90168	65100	0.0166	0.0153	0.0175	0.0165	69100	07100	0.0178	0.0194	0.0171	0.0172	-	H
Correct Corr	0.0199	-	0.0165	0.0186	0.0206	0.0183	0.0158	0.0159	0.0166	0.0153	0.0175	0.0165	0.0159	0.0170	RELIGIO	0.0194	0.0171	0.0172	H	-
	H	ŀ	0.0165	0.6165	0.0306	0.0181	0.01168	0.0160	0.0165	0.0157	0.0376	0.0154	00110	0.0171	0.0178	AP10.0	0.0369	0.0169	30155	H
0.02 0.02 <th< td=""><td>of mars</td><td>H</td><td>2000</td><td>0.6189</td><td>O DOOR</td><td>0.0301</td><td>2000</td><td>A 111.75</td><td>nethon</td><td>0,000</td><td>P(11)0</td><td>0.0121</td><td>92100</td><td>Arriga</td><td>0.0177</td><td>1000</td><td>99100</td><td>0.0158</td><td>+</td><td>+</td></th<>	of mars	H	2000	0.6189	O DOOR	0.0301	2000	A 111.75	nethon	0,000	P(11)0	0.0121	92100	Arriga	0.0177	1000	99100	0.0158	+	+
	+	+	2000	0.0400	CONTRACT	0.0100	00000	0.000	100000	TOTAL DE	COUNTY OF	2000	2000	20000	2000	O COUNTY	COLOR	0.000	+	+
0.001 0.001 <th< td=""><td>+</td><td>+</td><td>Carrier</td><td>0.0105</td><td>0.0200</td><td>20200</td><td>00000</td><td>0.007/4</td><td>0.000</td><td>COLD</td><td>Course</td><td>0.000</td><td>0.000</td><td>27170</td><td>6/fan</td><td>00000</td><td>001100</td><td>901010</td><td>+</td><td>+</td></th<>	+	+	Carrier	0.0105	0.0200	20200	00000	0.007/4	0.000	COLD	Course	0.000	0.000	27170	6/fan	00000	001100	901010	+	+
0.0199 0.0199<	0.0003	+	20100	0.0163	0.0000	0.0000	2000	0.0179	COUNTY.	Maron	0.0483	0.0104	2/100	22000	0.0350	William .	0.000	0.0350	+	+
COLORIA 01179 COLORIA	+	+	10700	0,0217	0.0278	0.0259	10700	0.0028	00700	0.0023	0.0241	0.0224	\$2700	0.0213	0.0227	0.700	0,0203	0.0190	ł	+
0.0014 0.0104<	+	+	00200	0.0205	0.0254	80738	22200	0.0216	0.0234	0,01399	0,0022	0.0204	00207	60200	0.0230	67700	0,0195	0.0384	+	+
0.0077 0.0078, 0.0189, 0.0189, 0.0036, 0.0036, 0.0036, 0.0036, 0.0036, 0.0038,	4	-	10200	10000	0.0253	0.0216	0.0207	96100	0.0199	0.0386	0.0201	0.0189	0.0191	0.0187	26100	0.0205	0.0184	0.0174	1	+
COUNTY COUNTY<	-		00155	0.0192	0.0330	26100	0.0190	0.0156	DOLLES	0.0179	0.0203	76100	0.0196	0.0133	0.0190	0.020M	0.0190	0.0178		2
0.0188 0.0188 0.0288 0.0289 0.0299<	-	1	0.0199	0.0198	0.6230	0.0206	90200	0.0201	0.0136	0.0188	0.0199	8510.0	0.0186	0.0177	0.0186	0.0198	0.0180	0.0171	0.0172	0,0173
0.01/15 0.01/15 <t< td=""><td>H</td><td>-</td><td>0.0189</td><td>0.0187</td><td>0.0221</td><td>0.0203</td><td>55100</td><td>0.0193</td><td>95100</td><td>0.0187</td><td>0.000</td><td>10.033</td><td>56100</td><td>660189</td><td>0.0198</td><td>0.0217</td><td>0.0188</td><td>0.0186</td><td>H</td><td>-</td></t<>	H	-	0.0189	0.0187	0.0221	0.0203	55100	0.0193	95100	0.0187	0.000	10.033	56100	660189	0.0198	0.0217	0.0188	0.0186	H	-
0.01299 0.01299 0.01299 0.01291 0.01211 0.01211 0.01211 0.01211 0.01212 0.0121	Н	L	0.0192	0.0192	0.0224	0.0205	90200	0.0195	0.0194	0.0184	0.0200	0.0285	0.0187	60179	0.0284	0.0136	0.0173	0.0169	-	-
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COUNTY COUNTY<	٠	ŀ	Option .	O fines	GRINE	90108	00100	0.00	0.0183	0.0171	0.0156	0.0175	20100	00000	22100	0.0194	0.0172	0.0167	t	+
COUNTY COUNTY<	t	÷	00000	0.0000	Orthon	10000	00033	- State	0.0007	Coope	Others	0.000	90000	00100	0.0000	0.0018	0.0106	0.0163	+	+
COUNTY COUNTY<	÷	+	2000	O COTTO	0,0000	00100	00100	00000	2000	00000	2000	90000	and a	S COLUMN	20000	20000	0.0000	O Outo	+	+
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OLIGINA OLIGINA <t< td=""><td>+</td><td>4</td><td>0.0126</td><td>8ZW 0</td><td>0.0153</td><td>0.0123</td><td>60119</td><td>0.0133</td><td>0.0135</td><td>0.0116</td><td>0.0037</td><td>0.0131</td><td>0.0111</td><td>60123</td><td>0.0128</td><td>0.0112</td><td>0.0122</td><td>0.0126</td><td>0.0136</td><td>62100</td></t<>	+	4	0.0126	8ZW 0	0.0153	0.0123	60119	0.0133	0.0135	0.0116	0.0037	0.0131	0.0111	60123	0.0128	0.0112	0.0122	0.0126	0.0136	62100
0.0200 0.0201<	+	1	0.0185	0.6157	0.0221	0.0199	0.0197	0.0100	0.0193	0.0134	96100	06100	0.0193	0.0156	0.0195	0.0211	0,0186	0.0178	0.0173	0.0174
OCCURS OLIVERS OLIVERS <th< td=""><td>7</td><td>4</td><td>0.0201</td><td>0.0201</td><td>0.0236</td><td>0.0221</td><td>0.0216</td><td>0.0211</td><td>0.0212</td><td>50000</td><td>0.0219</td><td>0.0210</td><td>0.0212</td><td>0.0202</td><td>0.0232</td><td>0.0228</td><td>0.0201</td><td>0.0193</td><td>0.0190</td><td>06100</td></th<>	7	4	0.0201	0.0201	0.0236	0.0221	0.0216	0.0211	0.0212	50000	0.0219	0.0210	0.0212	0.0202	0.0232	0.0228	0.0201	0.0193	0.0190	06100
Q. 0.0.13. O. 0.0.15. O. 0.0	+	4	0.0203	0.6203	0.0233	0.0215	0.0216	0.0211	0.0209	0.0202	0.0210	0.0206	90200	96100	0.0204	0.0219	0.6200	0.0194	0.0395	95100
0.0214 0.0215 0.0215 0.0224<	Н		0.0157	0.0187	0,0216	80194	0.0194	0.0190	0.0198	0.0136	0,0097	0.0192	10191	0.0185	10197	0.0209	0.0187	0.0179	6,000	82300
0.0210 0.0217<	Н		50215	0.5220	0.0542	0.0228	6:0234	97234	0.0721	0:0215	0.0220	20200	0:0211	0.0200	0.0705	0.0219	0.0202	0.0300	0.0203	20250
CORTY GRING CORTY CORTY <th< td=""><td>Н</td><td>L</td><td>0.0217</td><td>0.0215</td><td>0.0239</td><td>0.0221</td><td>0.0229</td><td>0.0236</td><td>0.0227</td><td>0.0229</td><td>0.0237</td><td>0.0233</td><td>0.0234</td><td>0.0218</td><td>0.0227</td><td>0.0246</td><td>0.0223</td><td>0.0514</td><td>3.0226</td><td>0.0234</td></th<>	Н	L	0.0217	0.0215	0.0239	0.0221	0.0229	0.0236	0.0227	0.0229	0.0237	0.0233	0.0234	0.0218	0.0227	0.0246	0.0223	0.0514	3.0226	0.0234
OFFICE ORDER ORDER <t< td=""><td>H</td><td></td><td>0.0212</td><td>0.6213</td><td>0.0245</td><td>0.0228</td><td>0.0221</td><td>0.0217</td><td>0.0239</td><td>0.0259</td><td>0.0223</td><td>0.0215</td><td>0.0216</td><td>0.0205</td><td>0.0234</td><td>0.0234</td><td>0.0207</td><td>0.0205</td><td>0,0199</td><td>6510'0</td></t<>	H		0.0212	0.6213	0.0245	0.0228	0.0221	0.0217	0.0239	0.0259	0.0223	0.0215	0.0216	0.0205	0.0234	0.0234	0.0207	0.0205	0,0199	6510'0
0.0271 0.016s 0.016s 0.026s 0.026s<	H	L	0.0163	0.0171	0.0236	0.0209	50200	-0.0203-	0.0204	15100	0.5230	0.0222	0.0221	0.0204	0.0231	0.6230	0.0213	0.0235	0.0195	26100
CONTION OF COUNTY OF COU	٠	Ł	0.0166	0.0001	0.0381	00000	0,0203	0.0000	0.000%	0.0105	0.0008	0.0199	0.0000	0.0102	0.0199	0.0017	0.0197	0.0001	0.0181	0.0180
COLOTY C	٠	+	0.0160	0.0014	0.6789	0.0016	0.0014	0.0013	0.0016	0.0011	0.0924	0.0090	0.0147	0.0189	0.0100	0.6017	0.0198	0.0049	90000	+
COUNTY 0.01747 0.01747 0.01754 0.01875 0.01815 0.01825 0.01782 0.01825 0.01712 0.01712 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01824 0.01825 0.01825 0.01825 0.01824 0.01825 0.01825 0.01825 0.01824 0.01825 0.018	٠	H	0.0174	0.6875	0.0210	9,010,0	0.0178	5,0163	0.0167	0.0152	0.0472	0.0160	9000	0.0162	0.0171	DOUBLE	92100	0.0346	30121	-
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COURTY C	۰	ŀ	0.0211	0.006	0.0238	0.0216	0.0215	0.0212	0.0210	0.0295	0.0019	0.0212	0.0213	0.0203	0.0218	0.00.00	0.0204	0.0500	0.0200	-
COURTY ORDERS COURTY ORDER	H		0.0257	0.0233	0.0247	0.0216	0.0234	0.0235	0.0231	0.0222	0.0229	90100	0.0250	061100	0.0200	61200	0.0199	0.0200	-	60200
COURS GARIS GARI	٠	0.0207	0.0205	61030	0.0746	6.0225	0.0223	0.0224	0.0239	0.0222	0.0232	0.0228	0.0232	0.0222	0.0231	0.0247	0.0222	0.0216	H	-
CONTINE GLODIO COLUMN	H	-	00100	O.DANE	0.0208	56100	0.0000	0.0186	0.0189	0.0185	0.0200	26100	0.0191	0.0183	0.0389	0.0205	0.0186	0.0184	3.0175	-
CUTI GLONG DADY ORD	۰	F	0.0197	0.0217	0.0242	0.0216	0.0219	0.0208	0.0217	0.0204	0.0218	0.0208	0.0209	0.0198	0.0208	0.0227	0.0202	0.0199	0.0186	0.0188
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40166 DOIGH OFFIT O COST DUZZI GUZZI	0.0384	+	0.0004	0.0010	0.0334	0.0371	0.0307	0.0000	900000	0.0197	0.0210	0.0302	0.0208	90000	0.0000	0.6016	0.0204	0.0003	+	₽
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4	3	K13125.78	123177.37	833231.06	833434.85	633360.46	E3311E28	833185.93	633425.15	633596.26	623673.75	132833,67	633973,71	633527.00	833627.55	R23732.97	633782.11	633661.17	613693.59	83397£75	19,000,01	613883.54	623387.36	633423.89	633416,00	613447.62	233544.64	133488,77	833587.56	613633.17	423002.07	103266101	00000000	20,000,000	22002	644700,84	833232.00	20,277,000	*********	BA207.04	B11 54 74	815647.83	813076.98	AUSTON TO	233263.50	833398.77	833624.34	613653.40	\$13694.68	835761.98	833763,11	813833.16	E33902.04	833950.40	KANAD CZ	834231.72	834322.77	833097.20	823158.55	E13101.67	833274.00	833434.18	613736.86	833736.06	833438.83	*******	#31683 68	813713.66	£33757 £3	613734.63	833778.89	833873.30	634155,21	et3167.79	E34055.34	83311E.37	633139.75	E13258-66	633460.69	133543,73	633460.99	B11514.00	818184 04	411111	SALLING GA	100 00 000	
Caline	Road	8003	R003	R003	R003	R003	R004	H100-4	H004	Ross	R-0016	RIODIE	REGE	PS16+R901	R006+R007	R006+R1007	RESS-ROOT	RDIS+R009	ROOM-MOON	R010-R011	6010-H011	RECU-RECT	RD12+R013	R013+R013	R012+R013	RBC2+RBC3	ROT2+ROT2	R014+X-016	8016-H017	MOLES HOLD	Mara	200	Marke	Tares.	Water a	Marke	4754	1	1000	2000	Bank a	HODE	6032×R201	BELLS	Bet 4	8638	8.636	R437	Relie	ROZB	6,040	1041	NG42	HINES.	977	Ross	FISA7	HOM	8958	1105G	Rost	R452	RDK3	RIGHTS	H054	Britis.	NO.	2000	R654	ROSS	Moto	R057	. R05a	6,000	NONO	1601	ROSZ	RDES	NOR4	*000	1004	BASE .	1000	Bode	1000	Moro	

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Road	R074	R472	ROTA	H57.4	R075	Rate	8476	RETT	F1077	F1077	H578	BG79	Ribbo	RO#1	ROBZ	B962	RIN'Z	MO83	HO\$3	Pot:	NO84	ROBA	ROPS	MORS	MORE	M080	1000	100	Muse	8088	ROSS	ROKE	ROBB	HIGHW.	ROSS	9.03.9	R089	R089	RUES	Ribes	Robs	8,008	9000	On the State of	COLD. Eddy	TANK TANK	Date .		Market .	000-H001	0000-000	100-00-000	104.8.104	BINE	R-10.7	Ritor	Redd	8418	0110	HI I	MILE	Rtt3	Atta	RIES	RTES	RHIT	RITE	RTES	R120	R121	RIZZ	R123	R124	R125	RIZE	R127	R128	R129	R136	RESE	R132	K133	RESA	BEESE	R126	R137	RESE	

1910 299	ZP10'0 etto'0 4110'0 5910'0 1810'0 5510'0 5510'0	9610.0 \$910.0 8810.0 8810.0	8510°0 8510°0 8510°0 8510°0 1510°0 H450	99100 99100 99100 99100	0810.0 0810.0 0810.0 0810.0 0810.0 0810.0	5210.0 5210.0 5710.0 6710.0	99100 00122 00122 00123 HUB	5710.0 5310.0 5310.0 8710.0	2710.0 2210.0 2810.0 7710.0	1610.0 8210.0 1610.0 1610.0	19100 19100 19100 19100	00100 00100 00100 HU1	6610'0 0510'0 2610'0	50200 60100 60100 90200	1610.0 1610.0 1610.0	0550.0 1410.0 1410.0	2610 0 9010 0 2610 0	95100 95100 95100 904H	\$610.0 \$610.0 \$610.0	0.0302 0.0302 0.0303 0.0304 0.0304	0.0153 0.0153 0.0153 0.0153	9610'0 0110'0 5410'0 104H	0193 0193 1400
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1910 1910	0.0118						69100	2510'0 ·	Reto o	6510/0	1FIOO	9510/0	15100	2910/0	651070	2610.0	09100	15taa	G0152	95100	2910'0	19100	1910
1910 1910	0.0142		6210.0	0.0144	29100	5510.0	C0100	05100	0.0146	9510'0	85100	7510.0	60100	65100	69100	0.0190	6510.0	19100	8510.0	8210.0	6210.0	95100	\Z\$10
1900 1900 1900		97100	B210.0	Z5100	ELTO D	5910.0	95100	45100	Sero.o	19100	10100	25100	49100	SSTOO	88100	8810,0	ZSTO O	15100	95100	95100	52.00,0	95100	ESTO
1910 1910 1910	79100		RSTO 0	45100	ACTO U	5910.0	95700	£ST0.0	Z/10/0	1910.0	THIOD	25100	C910'0	5510.0	8910.0	8810.0	0.0152	estoo .	951070	95100	rstoo .	95100	1510
1910 1910	59100	9vto'c	BS 10'0	25100	£100	5910'0	9510'0	. 45to-e	2510'0	19100	1110.0	25100	29100	\$510°0	19100	BE10.0	2510'0	25100	95100	95100	75100	9510'0	2510
1910 1910 1910	\$\$100	0410.C	B610.0	Z\$10'0	87.10.0	20.0364	95100	00120	\$200.0	COTOTO T	TOTOTO	2500.0	6 0147	SSTOO	19100	8810.0	£810.0	25000	0.0156	957070	0.0153	95taro	ESTO
1910 1910	Z#10'D	0,010,0	#510 G	25100	2/100	1310.0	953070	95100	7510.0	1910.0	Totto'o	75100	£910'0	OUTZZ	\$910 U	8910'0	£510'0	ESTOD	9510'0	95100	25100	95100	£511
1910 1910	SVIOO	EMOC	951010	95100	W100	1910'0	0.0157	9510'0	0.0151	5910.0	0.0140	2510.0	AV10'0	9210.0	19100	88.00.0	2510.0	12510.0	0'0126	95100	5210.0	95100	PST
1910 1910 1910	PE10/0	TETO'G	90100	#\$10°0	94100	Eato.o	95100	19100	M210.0	9100	EPIOO	29100	Z910 Q	22100	gatao	1050.0	EXTO O	94100	ECTOD	0.0170	29100	4910.0	TEX
1910 1910	1610.0		9970'0	75100	E/10/0	0.0165	95100	29100	BSTO'0	TZTD'O	5510'0	0.0164	0.0160	9410'0	98100	1020.0	E410.0	17100	EL10.0	0.0170	0'0767	59100	TET
1910 1910	PETO'0		astora	25100	MIDD	9910'0	R510'0	99100	1910-0	69100	75100	DUTOD	99ID 0	44100	16100	902010	P/10'0	14100	0.0173	0410.0	8910.0	59100	241
1910 1910	9510'0		52100	68100	0.0215	0.0209	20200	90500	0.0206	5550,0	4020.0	0.0221	6150.0	0.0231	BE200	0.0255	0.020.0	06100	0.0185	067070	56100	1610.0	502
1910 1910	1510'0		£910'0	62100	50700	E610.0	28100	06100	8810.0	\$020.0	\$8t00	7910.0	6610 O	0.0209	0.0220	0.0233	8810.0	#S10'0	28100	0.0184	EN10.0	\$810.0	78.f
1910 1910	05100		1910.0	00100	0.01299	7710.0	2710.0	94100	5210.0	2810.0	52400	16100	T810/0	16100	36100	5150.0	SETOO	Sittoo	28100	SET0'0	ENTO.0	E810.0	191
1910 1910	6910'0		0.0165	94100	16100	ESTOR	59T0'0	THIO	TRIOG	6810.0	0.0165	52100	2210.0	5210'0	94100	0.0201	22100	25100	00100	9610 0	76100	IRIO.0	SAT
1900 2910 2910 200 0000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 000000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 00000 1910 200 000000 1910 200 000000 1910 200 000000 1910 200 000000000000000000000000000000000	65100		0.0158	99t00	1310.0	1/10.0	£9100	1/10.0	0.0174	£810.0	ELIGO	1910.0	4810.0	06100	COLNY	0.0210	0.0182	8/100	22100	9/10/0	0.0184	98100	521
1910 1910	6910'0		1/10/0	£210'0	OUTO D	\$20.0	17/100	62100	4210.0	0.0184	2410.0	12100	4410.0	62100	28100	20200	£210'0	#2100	99100	2410.0	89100	69100	170
1900 2910 2910 2910 2910 2910 2910 2910	05100		9510.0	65100	080.00	M20.0	0.0165	27100	1710.0	E810.0	6910'0	82700	08100	68100	\$8100	5020.0	7710.0	1710.0	18100	0.0182	££100	0810.0	845
1910 1910	Z\$100		2910'0	29100	66100	B.0174	69100	1910'0	6710.0	6810.0	08100	0.0169	1610.0	96100	16100	2120.0	E810.0	SETOD	2810.0	0.0125	5810.0	E810.0	ESS
1900 2910° 490° 200 0000 1910° 410° 1910° 410° 510° 410° 1910° 410° 510° 410° 510° 1910° 410° 510° 410° 510° 1910° 410° 510° 510° 1910° 410° 510° 510° 510° 510° 510° 510° 510° 5	69100		5510 0	65100 65100	00000	9800.0	25100	16100	1610.0	1710.0	1610'0 6510'0	estoro	0.0165	90700	0.0203	9610.0	Z610.0	16100	96100	2410 0	1610.0	69100	021
1910 1910	2510,0		BETO II	\$\$100	14100	1910.0	85100	19100	£510.0	£910'0	15100	Z9100	1910 0	593070	THICG	£610.0	0910 0	19100	E9100	79100	1910.0	09100	791
1900 29100 499 200 0000 1910 4910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 0000 1910 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 00000 1910 2010 0000000 1910 2010 000000 1910 2010 000000 1910 2010 0000000000000000000000000000000	££50.0		0.0218	0.0221	B000	0.0228	2550.0	9970'0	1500 a	6200.0	9970'0	E820.0	A1100.0	7750.0	15000	0.0267	617010	0.0251	152010	1520.0	0.0252	1250.0	600
1910 1910	7800,0		9600'0	2600°D	SHOT	OUTOO	20100	9010/0	A010.0	90to'0	5010.0	90100	90100	50100	PLUC	ZITO'B	CO10.0	00100	20100	00000	Sataro	0.0104	100
1910 1910	etto.o		9110.0	2110.0	IXIOD	#tt0.0	pitto	12100	0.0120	0.0126	SELOO	0.0124	65100	82100	Strag	ESTO.O	8110.0	7110.0	91100	0.0120	21100	9110.0	911
1900	0.0159		ESTOD	14100	\$6100	97.00.D	15100	44100	2710.0	C810.0	0/10/0	77,000	67175	19100	18100	5050.0	22100	02100	0/100	6,0172	1710.0	1/100	121
1910 1910 1910	54100		8410.0	2810.0	0.0209	2010.0	3810.0	\$610.0	EGTO 0	1059.0	6810.0	20135	7610.0	66100	0.0204	9170.0	DELOLO	SELGG	20100	98100	1810.0	ESIGO	190
100 1910	0.0180		62100	48t00	107.010	Nate.o	tatoo	0610'0	0610.0	0.0194	9810.0	Beto.o	9610 O	86100	16100	0.0213	7810.0	1810.0	82100	\$810.0	8810.0	98100	885
190	\$9100		9910.0	0.0172	15100	1810.0	1510.0	8/10/0	5510.0	0.0182	1410.0	R/100	5210.0	8710.0	62100	5610.0	E510.0	ECTOR	2100	1520.0	P£100	EVICO	134
190	3810.0	ZITO'D	0.0184	98100	10700	9810.0	18100	0 0.194	0.0395	0.0202	3610'D	EDGOLO	100000	51700	0.0210	0.0221	0.0202	86100	66100	0.0550.0	0.0200	66100	202
100 29100 290 200 0000 15100 0000 15100 0000 15100 0000 15100 0000 00	T050.0	8050.0	£610°0	0.0205	92200	0.0208	0.020.0	0.0215	0.0214	V150.0	0.0210	0.0209	0.0208	11200	0.0203	.6150.0	8610.0	6610'0	0.0200	0.0197	6610 D	66100	667
100 1910	£810.0	PKID,C	0610.0	16100	graste	NELO.O	06100	66100	6610.0	5070.0	£510'0	0.0202	0,000	0.0204	60200	\$££0.0	56100	56100	DSIGD	ERTOD	SETO'O	ESIGO	760
1910 1910	5530.0	ORTO,C	B610.0	9610'0	Etzon	1610.0	0.0188	£9700	0.0204	0.0211	9/10.0	MEE0.0	9810'0	68100	16100	9150.0	2510'0	05100	G0152	85T0'0	9510'0	1510.0	951
100 1910c 499 200 0000 4910 100 1510c 000 100 1510c 000 100 8410t 500 100 8410t 500 100 1510c 9910c 100 10	99100		2810.0	28100	0.0199	E810.0	8120.0	48100	E810.0	0.0192	62100	MATO D	981D 0	98100	88100	0.0213	Z810'0	15100	15100	0.020.0	7910,0	Z8100	Z81
100 2910 490	0670'0		1/510'0	2810/0	66100	0.0183	14100	19100	0.0177	9020'0	96100	0.0202	9610 0	16100	16100	0.0219	7919.0	95100	25100	1220'0	0.0210	66100	2610
100 2910°C 290 200 0000C 290 200 00000C 290 200 0000C 290 200 0000C 290 200 0000C 290 200 0000C 290	SITO'O		0.013A	90100	39100	Z\$10.0	DSTOO	1510'0	891070	8510/0	0.0140	E\$100	05100	19100	0710.0	2610'0	1910.0	0510:0	tetor	£910.0	0910'0	29100	tett
10'0 2910'C 299 20'0 0920 C 1510 10'0 1510 C 098 10'0 1510 C 098 10'0 8210 C 591 10'0 5910 C 991 10'0 5910 C 991 10'0 992 C 650 10'0 992 C 650 10'0 992 C 991 10'0 992 C 992 10'0 992 C 99	81100		\$610.0	99100	89100	7210.0	05100	TSTOO	8410.0	8510'0	0.0140	12100	este e	\$9100	02700	5610.0	1919.0	poten	19100	5910.0	0910'0	Z910'0	1910
10'0 2910'0 290 20'0 0970'0 110 20'0 1100 1510 0999 10'0 8210'0 5910'0 5910 10'0 2910'0 5910 10'0 0910'0 5910 10'0 0910'0 5910 10'0 0910'0 5910 10'0 0910'0 5910 10'0 0910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910 10'0 9810'0 5910'0 5910'0 5910 10'0 9810'0 5910'0	STT0'0		NETO-0	96100	3910.0	ZSTO:0	05100	15100	9,0149	85100	0970'0	1210.0	05100	19100	0/100	2610.0	1910.0	09100	TOTOD	£910.0	0.0160	29100	1910
10°0 2910°C 290 20°0 0920°C 910°C 10°0 1510°C 091 10°0 1510°C 091 10°0 1510°C 1910°C 1910	#810'0		2810.0	281IL0	ZIZOG	1020.0	LSTOO	96TU 0	2610.0	0.02002	6810'0	16100	961010	86TUO	66100	8120.0	6810.0	\$6100	66100	0.0192	7810.0	Z610'B	983.0
10°0 2910°0 290 20°0 0970°0 910 10°0 1510°0 0910 10°0 8210°0 5910°0 800 10°0 5910°0 800 10°0 5210°0 800 10°0 5910°0 690	2610'0		\$10.0	£810.0	10200	SELOG	2710.0	#810.0	0.010.0	LISO.0	0.0204	0.0213	0.0207	90200	66100	9550.0	90200	9650.0	95100	9670'0	8550.0	0.0210	2021
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hicle count for	1300	calo	200	050	450	450	08	980	750	980	700	700	250	250	300	900	600	089	250	400	2650	2690	2650	25.50	2650	2050	0502	2050	3050	2050	2050	2050	200	750	300	034	250	650	2051	300	5	150	250	300	300	000	069	009	700	100	350	200	300	052	300	980	GUD	000	200	212	9	
91	DASO	090	900	200	300	900	1080	0501	900	200	200	750	300	300	250	750	200	200	300	450	2750	2750	2750	05/2	2750	2050	2050	2050	2000	2050	2050	2050	800	900	200	134	250	200	150	250	300	300	250	150	100	082	650	900	750	900	350	200	300	951	300	990	006	059	200	212	95	
	1650	750	950	000	055	088	1300	1200	950	250	988	650	350	350	650	058	650	850	950	005	3300	3200	3300	3200	1300	2350	2350	2350	2350	2350	2350	2350	1000	3000	250	98	360	250	200	250	200	250	300	150	150	250	750	700	850	900	400	250	200	250	300	90,00	1150	200	008	32 22	9	
1	1750	909	980	020	900	909	1250	1250	1000	550	006	906	350	350	000	00 5	650	090	350	005	3400	3400	3400	3400	3400	2450	2450	2450	2450	2450	2450	2450	1000	1000	250	000	950	005	300	230	300	300	300	150	150	300	700	000	750	100	350	250	300	200	300	002	1200	050	200	21	5	
4911	1350	906	650	900	900	400	920	850	900	900	909	009	250	52	009	909	250	530	350	350	2550	2550	2550	9552	2550	1800	1300	1800	0081	1800	1800	080	930	050	51	20	121	250	100	100	100	100	31	100	20	350	350	905	400	900	200	001	100	100	100	350	082	300	350	11	91	
1	500	300	092	150	150	150	350	350	300	150	250	250	100	100	250	82 5	250	250	100	150	1300	1300	1300	1300	1300	850	850	880	820	850	980	098	250	. 052	8	200	13	100	2 27	8	9 5	8 8	9	8 8	9	150	200	150	300	230	100	9 5	2	9 9	2	300	300	920	200	0 5		
44.0	300	150	150	100	100	100	300	200	052	100	18	82 5	S	9 5	150	951	150	150	88	100	080	95	283	939	050	400	400	900	400	007	900	900	150	150	5	100	25	73	91	34	20	17	3	15	32	88	05	3 3	100	100	205	77	30	22	19	100	002	8 8	300	5 2	-	
1000	NG NG	100	130	100	300	100	300	300	150	300	150	150	205	5. 5	2 95	951	100	300	9 5	3	330	2 2	350	380	98	250	250	2 5	82	250	2	8 8	150	150	S	8 -	17	33	11	36	2 2	15	22	10	80	2 2	9	51 5	9.	9.4	9	13	14	15	12	100	150	905	3,	, ,		
1000	250	100	150	100	100	100	300	200	150	100	3	150	98	8 9	150	951	150	150	2 3	95	350	350	150	350	350	250	250	350	250	750	250	052	051	150	28	8 4	14	11	30	15	77	a	13	6	2	9 9	90	8 9	95	900	34	13	111	13	11	100	150	100	05		-	
	250	100	150	100	100	100	200	200	150	100	150	951	9	8 8	150	150	130	150	9 9	100	005	88	200	905	905	320	350	350	350	350	350	055	150	951	8	9 =	77	77	2 22	12	17	17	R	12	30	9 8	a	8 8	8	9 4	98	8 5	17	19	36	100	200	90 8	8	1		
	300	150	130	100	300	100	300	300	150	100	350	150	2 2	53 5	200	51 5	150	130	8 5	100	220	2 2	DS2	750	2 5	380	950	989	200	980	989	280	951	350	52	300	- 55	300	23	2	53 53	2 3	9 5	2 12	3.7	900	300	300	300	100	52	2 5	3	98	9	100	300	100	100	3		
	000	051	500	051	150	150	057	057	200	001	00	88	8 8	8 8	8 8	88	8 8	8	8 8	001	090	950	050	050	950	750	750	9.5	052	750	95	05/	050	550	20	200	. 09	100	90	9	9.5	8 8	93	2 3	8	8 9	150	9.9	000	90	00	9 5	9	9.9	2	8 8	053	8 9	200 100		4	

	Road Type											-													1	140.00		1			*			*								,											-										e																													-
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	[including	minima repair	38	17.	30	40	,	48	. 96	- 0	17.	17.	10	16	- 18	70	2	14	14	14	- 14	1.0	13	13	14	. 11	14	17	- 17	- 12	47	11	17	11	44	. 21	- 11	- 60	18	- 0.0		10	18	10	10		200	20	20	- 10	17	=	- 10	18	10	10			10		17	83	- 19	16	1.0	100	18	- 18	. 61	- 83	18			80			. 5	1.0	- 94	9.		1.0									91	11
102	2	17.2	421607.07	621875.23	821880.64	20,000,00	424 849 77	821586.69	62162232	82188436	\$21871.28.	821812.09	62198275	821861.4E	\$21387.94	951592.08	\$21621.12	821766.92	\$21687.58	621833.12	8211123	29755575	621564.65	621603.87	\$21676.52	\$21545.20	62151239	621253.09	\$21546.45	62150630	\$21886.64	#2186A.01	821841.09	\$21786.ST	421407.75	821805.62	#21511.57	\$21546.57	821852.03	621626.28	824768.53	621726.47	821683.57	821884.44	821528.87	********	11000	821646.31	\$21899,24	\$21576.AY	621548.43	822414.33	11 22222	822256.35	822180.58	633099.51	82230839	822287 S3	82224222	62279.48	6220cm 94	823028 83	622360.57	032371.31	82230123	8221228	622115.02	622407.73	62156128	\$21684.AS	821896.55	622316.08	8732578	822 1 60 KG	10 May 17 1	62217238	82255473	\$22278.AS	622221.21	822255.72	822578.17	62200076	623007.07	824162.74	20,000,00	407434	4512434	The same of	822129.44	822072.07	821877.98	621367.58
r 2034	ate (m)	A2757724	833564.75	833287.14	11146150	********	93377518	833863.43	823484.92	8338557	833600.48	83367384	83347832	833867.57	03289654	833583708	83181875	#3351E39	83387013	13349518	12357436	933588.81	9336628	833407.71	833645.24	833881.67	63375852	13365341	63364623	93388649	033306550	63341650	833467,63	83362163	111574.10	83360516	833712.08	93137608	8334677.58	61340040	411477.44	83354236	833.842.67	8336668	4316663			933449.08	832913/08	83334153	833648.49	83492877	134117.62	12121631	03430805	834497.44	93389176	1340HL3F	834181488	107.176	83439429	83840074	83390256	#33909EE	853884.47	934017.01	834097.20	BOATHOUSE	83424326	2173270	634388.17	43375411	411814.74	ATTRACTA	********	133827.77	83368833	933563.51	83355435	833355.00	011356.77	833464.10	TO MICE	133481.00	11,508.57	******	43321338	********	133100.03	63343458	83316856	133250.10
input for	Coordin	621869.28	621675.23	E2186654	ESTREE N		421897.40	821864.77	621099129	82169414	E2163128	E1414	411622.35	821811.62	\$21,061.13	821669.88	\$21814.41	\$21823.43	821785.92	E258551T	DI BIBLE	85177239	821887.03	821644.08	821605.64	821673.52	821545.20	E21644.69	\$21583.53	\$215128	821/E11.68	E21894.69	621865.51	\$2184T.00	821786.07	827500128	\$21505.22	621801.44	825646.07	821882.03	80183838	SECTION NO.	824738 47	E21663.37	**********	.,	William	825633.93	621640.21	62163473	621501.73	122454.38	\$22414.ZZ	WZCCZZ8	622256.38	822184/68	872431.91	84737894	822238.08	DIAL DE	622136.63	822053-98	622405.79	\$2223A.17	80227158	11'902728	822131.54	RELIVERAL	\$2.500.7.TS	851993.88	821981.17	82337A.16	627311.13	82222248	833344.72	E22384.07	927289.00	822215.78	822278.88	802113203	82223203	822478.54	823084170	831007.68	271962.74	#15 14 64 W	#22478.06	Brett ave	822182.03	827(29.44	822472.03	122007.07
4	3	A1327.61	823397.24	833451.80	8112261.64	20,100,00	expense as	R33548.06	633663.43	53386.57	e13853.67	831600.48	812082.38	613(613.29	123175.67	833867,01	633452.18	63353676	625536.79	833438.83	ELDANGER	813524.36	833567.54	622003.09	613605.34	623640.24	197189178	832550,79.	812661,68	etterr es	833354.34	833348.00	653416.50	823.687.61	133553333	832074.85	61369016	613256.06	833370.08	833427.54	K11420 60	#15522.48	833643.19	633562.07	ATS 454.06	********	M Alanna	833337.92	633.648.06	63337.84	£13609.59	821060.09	\$34028,TY	634927.62	124216.31	834303.00	613817.63	STANKE S	838090.64	1071	57773.X	634363.46	822848.76	833833.16	633309.66	\$13998.00	834076.02	834097.30	634190.59	634242.94	634251.93	833768.63	611781 84	CUSINES. 72	813473.82	833684.86	633653.40	235493.66	833503.61	833377.88	833377.60	£1539£.42	811.617.02	H354th at	F13481 DE	**************************************	225252.03	PARAMETER.	633060.91	633 100 53	#13121.EE	\$33274.88
Caline	Road	2014	NOT2	MOTX	8274	2000	8076	R076	847.6	RE77	NS77	ROTT	8:27.6	PETS	Date:	F081	8465Z	F-04.2	Fat2	K.00 X	REGIS	Pick2	H384	NOR.	ROSS	Ross	ROBE	H109-0	9609	5007	中央日化	8600	Rose	ROLE	Robb	N6036	2509	8,000	R089	8000	RANG	Ribbs	R088	8659	9000	Design State of	1000	NIN2+R092	MIND 2 - FORES	6094	RESE	HIBS-R007	10000-1000	R100-8101	PHO2+R101	R104-R108	400 M	Riff	Ride	M109	R110	Ritt	Rett2	R112	R1ts.	Rics	RTTE	RILL	R118	8349	R120	8121	6477	Be22	RTZA	REST	6126	8127	R128	8128	R13G	Rebe	Real	W13.Y	BUSA	Bette	Real	West P	R137	8438	Ress	RT40

Road		Coardin	rate (m)	-	Width	Height	Road Typ
Pair	X1	Y1	X2	¥2	proclusting proclusting	(m)	(caline 4
Rist	B33254.33	521947.25	885315.56	821691.57	13	0	1
R162	833329.69	821353.87	ED31534	621691.04	13	0	7
R143	633129.75	621689.31	#33460.67	#21#34.07	- 13	0	1
R144	833,160,17	621834.07	#33.878.74	821783,18	13	0	- 1
BLES-RIAL	823812.43	421974.5%	\$3497458	621516.03	- 32	0	1
2147+2140	E23734.44	#21886:3K	E2301/12	821727.34	16	0	-1
R148	833728.61	821749.82	632607.73	821694.38	14	0.0	- 4
R149	833774.00	621643.62	032807.73	821684.38	13		1.
R150	833756.67	#21786.23	853607.71	821603.81		0-	- 1
R151	\$33612.61	821610.98	833663.50	821663.70	13	0	4.
R151	AMDERI 60	021543.70	#3377628	#21842.83.	14	0	1
WIR2	635774.DB	621843.52	\$13EE 17	821500.58	20		1
R193	833991.31	622389.76	834G/8.77	622454.27	78.	0	1
R194	\$33960.66	222330-65	#EXWZ.00	#22189.07	18	0	1
RIBE	833909.46	122271-36	X33000.66	932130.45	16	- 0	1
#186°	8130848.78	622222.16	#11M09/85	022271.30	18		- 1
B197	H33866.58	622722.34	6550777	8221T2.98	98	- 0	
P153	833827.77	822172.95	815772.46	822113.30	18	0	
HITT	634070.01	622299.62	E34312.00	632384.34	18.	0	1
RIES	834090.38	\$2228 F 65	#34577-61	622332.11	15		- 4
B191	834014.60	822250.52	834075.91	822209.62	15	0	- 1
R162	634049.42	822238.28	234(NO.19	822287.53	15	0	1
#143	E33993.00	622201.66	#34634.00	032250.01	10.	0.	1
8164	834007.86	622194:35	#34/94% AT	022230.20	15		1
R165	E23957.31	622151.78	#ESSWAA7	622221 25	36	0	
R156	835872.14	822651.39	82196475	#22190.50	18	0	1
R147	633,683-47	822042.45	E34007.88	#22100.33	18	0	1
R163+R160	833813.72	\$21 87 E 47	EDWEST	WETOSD AT	29		1
R179-9171	E33716.44	821 FEB 2.35	#31812.49	821978.50	18	0	1
R172+R173	833864.92	821823.12	811719.26	821687.65	26	. 0	-1
RUA-RUS	#33061,78	621407.56	£12M(3-34)	821623.58	36	-0-	1
804	E33496.77	f21508.49	\$11580.47	621680.73	20	-0-	- 4
R177	E33513.09	821599.24	2237344	621688.A2	29	0-	1
RITE	R35440.44	621529:00	STATES OF	#21F08.41	16	0	7
9.173	X23451.04	621626.31	#30511.33	821400:38	17	. 0	- 1
R 120	E34218.31	622256.35	\$54375.90	621585.39	18	. 0	1
R131	E3A181.98	4223° 1.72	#34Z1831	822258-36	18	0	1
#182	K3A140-62	822162.47	834191.76	027212.3#	18	0	1
#182·	834099.34	622113.33	E3440/62	822162.67	18	0	- 1
R134	E34077.01	622152.66	#54851.51	822100.94	13	0	- 1
P184	STADE 1.51	E22100.94	83407130	822094.18	13	0	- 1
H184	#34071.00	07204 s. to	834007.30	822115.02	14	0	- 1
mies-	834309-95	\$22180.5A	834382.60	833167.A4	10	0	- 1
B196	824221.54	62238 à 63	634273.34	622136 83	39	0	- 1
RIST	834190.59	822037.73	83420176	622086.A5	- 91	0	- 1
R153+R199	834004.93	#21915 CD	834945.34	821600.22	10	0	1
R190-R191	B33921,13	921727.74	834004.08	621816.03	19	0	1
#192-R (92	633575.32	\$21460.75	812810.60	621727.50	29	0	1
R394-R 195	833825,79	621600.86	613867.51	621631.AB	20	0	- 1
R395+R292	633784.01	621323.38	#11816.17	821650.58	20	0	-
RIST	634364.00	827040.94	E34400 13	62210471	17	0	- 1
Rtss	834323.77	822010.68	83436436	622060.94	78		- 4
R199	839/201-93	421961.17	63A323.00	622015.AB	-38	0	- 1
R100	834239.67	#21914.12	834210.00	821983.18	14	0	1
#100	834239,67	821914.13	#34327.69	021840.33	18.		- 1

			7							Val	nicle count	for each	road										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	13	9	6	7	10	50	50	100	100	180	150	150	150	200	200	150	250	300	250	150	150	100	100
50	19	12		10	14	-50	50	150	150	150	150	150	150	200	200	150	200	200	150	100	100	100	50
100	50	50	50	50	50	100	250	450	500	450	400	400	400	450	400	300	400	450	300	200	200	150	130
100	50	50	25	50	50	100	200	400	450	400	350	350	350	150	350	250	150	350	250	200	150	150	100
21	12	7:	4	5	3	22	160	72	73	70	69	119	118	120	139	115	169	220	166	112	109	58	57
29	16	10	-7 -	7	12	11	63	150	150	150	150	150	100	150	100	100	100	150	100	100	100	100	71
14	- 6	5	4	.4.	5	15	50	50	50	50	50	50	90	50	50	-21	50	- 23	19	13	10	10	1 2
14	8	5	4	4	5	15	50	50	50	50	50	50	50	50	50	2.5	50	23	19	13	10	10	1 7
14		- 5	4	- 4	- 5	15	50	50	50	50	50	50	50	50	50	- 31	50	23	.19	13	10	10	1 7
14	8	- 3	- 4	-4	5	14	50	50	50	50	50	50	50	50	50	23	50	24	19	13	11	10	
14	- 8	- 5	4	A	- 3	14	50	50	50	50	50	50	50	50	50	23	50	24	19	13	- 11	10	- 3
14	. 8	5	4	.4.	5	15	50	50	50	50	50	50	50	50	50	50	50	50	24	D.	14	13	10
100	100	50	50	50	50	100	200	250	200	200	200	200	200	200	200	200	200	150	150	150	100	100	100
100	100	50	50	50	50	100	200	250	250	200	200	250	250	250	250	300	300	300	250	200	200	150	150
100	100	50	50	50	30	100	200	250	200	200	200	200	200	200	200	200	200	200	150	150	100	100	100
450	350	300	250	700	250	400	1100	800	800	800	800	800	100	750	700	700	700	650	550	450	-400	400	300
500	400	350	300	250	250	450	1050	1300	1100	1050	950	950	1000	950	900	950	900	900	750	650	550	300	400
450	350	300	250	200	250	400	900	1100	950	900	850	850	900	650	800	BS0	550	850	700	600	500	500	900
23	19	15.	14	10	12	22	50	50	50	50	50	50	50	50	50	50	100	50	50	50	50	50	50
100	50	50	50	50	50	100	200	250	200	200	150	150	150	150	150	150	150	150	100	100	100	100	50
150	100	100	100	50	50	150	300	350	360	300	300	300	300	300	300	350	350	350	300	250	200	200	150
200	150	100	100	100	100	150	350	450	480	350	350	350	400	350	35G	400	400	350	300	250	250	700	150
200	190	150	100	100	100	200	400	500	450	450	450	450	500	500	500	550	600	600	500	400	350	150	250
150	100	100	100	50	100	150	300	400	350	300	300	300	350	300	300	350	350	350	300	250	200	300	130
150	100	100	100	50	100	150	300	400	350	300	300	300	350	350	350	350	400	350	300	250	250	200	150
300	250	200	150	150	150	250	600	750	650	600	600	600	650	650	650	700	700	700	550	500	450	400	300
750	200	150	150	100	100	200	450	600	500	500	450	500	550	500	500	550	550	550	450	400	350	350	230
400	150	300	200	200	200	350	850	1050	950	900	900	900	1090	1050	1050	1150	1250	1150	950	850	750	700	550
350	300	250	200	150	200	350	750	958	900	800	800	900	950	900	1000	1050	1150	1100	900	800	700	650	450
450	350	250	250	200	250	400	850	1100	1000	950	900	950	1050	1050	1050	1100	1200	1100	950	800	700	700	550
450	390	300	250	200	250	450	900	1150	1000	950	950	950	1050	1000	1000	1090	1100	1100	900	750	650	650	500
300	250	200	150	150	150	300	650	800	700	650	600	600	600	600	580	600	500	550	450	400	350	350	250
250	200	150	150	100	100	200	500	600	550	500	500	500	550	550	550	600	650	600	500	450	350	350	250
300	750	200	150	150	150	250	600	750	650	600	600	600	600	600	550	600	600	550	450	400	350	350	250
300	250	200	150	150	150	250	600	750	650	600	600	650	700	700	700	750	800	800	650	550	500	450	150
150	150	100	100	100	100	150	350	450	350	350	300	350	350	350	300	350	150	350	300	250	200	200	150
12	9	8	7	5	6	11	50	-50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	20
50	24	19	17	13	14	50	50	100	50	50	50	50	90	50	50	50	50	50	50	50	50	50	50
24	20	16	19	11	12	72	50	50	50	50	50	50	50	50	50	50	50	50	50	24	21	20	16
50	21	16	34	12	13	12	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	- 50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	90	50	50	50	50	50	50	50
100	50	50	50	50	50	100	150	200	200	200	200	200	200	200	200	200	250	200	200	150	150	150	100
19	16	12	11	8	11.	17	50	50	50	50	50	50	50	50	50	50	50	50	50	22	19	18	14
100	50	50	50	50	50	100	150	200	200	150	150	150	150	150	150	150	150	150	100	100	100	100	50
64	62	59	58	57	58	63	150	200	200	250	150	200	200	200	200	290	200	200	200	150	150	150	119
71	68	64	62	29	33	60	150	150	150	150	150	200	200	200	200	250	250	250	200	200	150	150	119
36	79	25	22	17	19	32	100	100	100		73	71	73	70	70	68	65	150	64	64	51	64	25
60	59	57	55	- 55	35	39	173	200	172	171	119	117	117	116	114	314	112	112		58	57	51	55
		44																	100				
100	100		338	- 31	35	100	150	200	150	100	100	100	100	100	100	100	100	100	100	100	100	100	71
. 6	7	5	A	A	4	7	17	21	17	14	12	11	11	9	7	3	4	4.		3	3.	2	1
16	-13	11	- 3	7	3	14	50	50	90	50	50	50	50	22	19	18	15	15.	13	- 11	10	9	- 6
20	17	14	- 11	8	10	19	- 50	50	50	50	50	50	- 50	50	- 50	21	20	19	17	- 13	- 11	11	9
50	25	20	17	15	16	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	-50	90
50	25	20	17	15	16	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50

707	WIGHT
input for 2034	Consultante fort
Caline 4	Desired

2 H	88 0,0	88 0	88	88	98	98	85 0.	85 0.0	52 0.0	25 00	52 0.0	68	15 00	15 00	71 07	71 00	71 00	71 00	26 06	26 0.6	38 0.0	30 00	97	97	29 00	90	88 0.0	90 62	25 0.0	18 0.0	81	96	90	06	28	21	14 0.0	77 0.6	90	78 0.0	70 97	99	77 0.0	73 04	32 0.0	37 0.0	20 1 49	98 00	90 69	13 00	13 0.0	13 0.6	13 0.0	88	71 00	00 00	91	72 00	25 07	25 00	78 00	0.0	
Hr2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	000	100	1000	100	100	100	100	100	10.0	0.02	200	7000	2000	200	200	0.033	0.02	20'0	0.02	0.013	0.00	0.020	0.015	0.02	000	0.002	1002	0.024	0.02	0.02	0.0024	0.02	0.002	2000	0.02	0.024	0.02	0.026	100	0.03	100	0.03	800	200	1 0.036	0.02	100	0.002	200	100	0.020	
H/21	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0,005	0.005	0.005	0.000	0.011	0.011	0.017	7100	0.017	0,017	0.012	0.011	0.023	0.022	0.023	0.023	0.023	0.023	0.019	0.023	0.023	0.022	0.018	0.071	0.020	0,019	0.026	0.027	0.021	0.027	0.026	0,027	0.028	0.026	0.027	0.027	0.024	0.023	0.027	0.029	0.027	0.032	0.032	0.032	0.032	9000	0.027	0.030	0.023	0.018	0.021	0.021	0.027	0.020	
Hr20	0.0093	0.0093	0.0093	0.0093	0.0090	0.0030	0.0090	0.0090	0.0063	0.0063	0.0063	0.0066	0.0103	0.0103	0.0182	0.0182	0.0182	0.0182	0.0140	0.0140	0.0236	0.0226	0.0222	0.0222	0.0227	0.0232	0.0215	0.0231	0.0224	0.0246	0.0203	0.000	0.0204	0.0186	0.0245	0.000	0.0210	0.0257	0.0235	0.0258	0.0257	0.0240	0.0253	0.0251	0.0217	0.0216	0.0238	0.0252	0.0241	0.0273	0.0273	0.0273	0.0220	0.0306	0.0243	0.0261	0.0232	0.0181	0.0216	0.0016	0.0180	0.0196	
Hr19	0.0089	0.0089	68000	0.0089	0.0091	0.0091	0.0091	0.0091	0.0068	0.0068	0.0068	0,0067	11100	0,0111	0.0175	0.0175	0.0175	0.0175	0.0156	0.0156	0.0239	0.0226	0.0231	0.0738	0.0240	0.6242	0.0218	0.0242	0.0240	0.0235	0.0207	0.0313	0.0212	0.0199	0.0254	0.07777	0.0223	0.0268	0.0255	0.0267	0.0268	0.0258	0.0268	0.0265	0.0725	0.0222	0.0249	0.0256	0.0249	0.0281	0.0281	0.0283	0.0226	0.0311	0.0248	0.0276	0.0230	0.0184	0.0222	0.0222	0.0324	0.0210	
Hr18	0.0094	0.0094	0.0094	0.0094	0.0097	0.0097	0.0097	0.0097	0.0073	0.0073	0.0073	0,0073	0.0115	0.0115	0.0199	0.0199	0.0199	0.0199	0.0181	0.0181	0.0254	0.0255	0.0252	0.000	0.0268	0.0274	0.0233	0.0271	0.0263	0.0246	0.0241	MC00	0.0239	0.0227	0.0270	0.0749	0.0245	0.0295	0.0280	0.0295	0.0296	0.0288	16200	0.0293	0.0252	0.0246	0.0281	0.0280	0.0277	0.0310	0.0310	0.0310	0.0310	0.0333	0.0269	0.0298	0.0232	0.0216	0.0248	0.0248	0.024	0.0236	
HH17	0.0095	0.0095	0.0095	0.0095	0.0097	0.0097	0.0097	0.0097	6.000.0	0.0079	6.0079	0.0078	0.0117	0.0117	0.0182	0.0182	0.0182	0.0182	0.0172	0.0169	0.0243	0.0235	0.0236	0.0249	0.0242	0.0247	0.0229	0.0247	0.0245	0.0239	0.0220	0.0215	0.0219	0.0209	0.0245	0.0230	0.0231	0.0275	0.0251	0.0275	0.0275	0.0268	0.0270	0.0273	0.0234	0.0228	0.0256	0.0255	0.0255	0.0281	0.0281	0.0781	0.0230	0.0303	0.0250	0.0274	0.0228	0.0202	0.0231	0.0231	0.0251	0.0221	
Hr16	66000	66000	66000	660000	0.0099	0.0099	0.0099	66000	0.0073	0.0071	0.0071	0.0072	01100	0.0110	0.0174	0.0174	0.0174	0.0174	0.0160	09100	0.0229	0.0224	0.0279	0.0236	0.0227	0.0234	0.0229	0.0234	0.0230	0.0250	0.0219	0.0308	0.0210	0.0199	0.0238	0.0774	0.0222	0.0269	0.0255	0.0269	0.0264	0.0256	0.0264	0.0262	0.0224	0.0218	0.0245	0.0247	0,0244	0.0268	0.0268	0.0268	0.0268	0.0295	0.0247	0.0267	0.0228	0.0201	0.0224	0.0224	0.0203	0.0206	
Hr15	86000	86000	86000	0.0098	0.0097	0.0097	0.0097	0.0097	0.0082	0.0082	0.0082	0,0074	0.0120	0.0120	0.0174	0.0174	0.0174	0.0174	0.0161	0.0161	0,0242	0.0239	0.0239	0.0248	0.0245	00250	0.0224	0.0250	0.0242	0.0232	0.0215	0.00219	0.0219	0.0207	0.0261	0.0244	0.0242	0.0305	0.0291	0.0305	0,0301	0.0292	66200	0.0297	0.0251	0.0244	0.0276	0.0284	0,0279	0.0301	0.0301	0.0301	0.0301	0.0344	0.0286	0,0311	0.0227	90200	0.0233	0.0231	0.0212	0.0220	
Hr14	0.0095	0.0095	0.0095	0.0095	0.0094	0.0094	0.0094	0.0094	0.0077	0.0077	0.0077	0.0072	0.0115	0.0115	0.0171	0.0171	0.0171	0.0171	0.0159	0.0156	0.0239	0.0238	0.0237	0.0347	0.0244	0.0244	0.0216	0.0249	0.0239	0.0220	0.0213	0.0217	0.0219	0.0202	0.0264	0.0245	0.0246	0.0316	0.0300	0.0315	0.0311	0.0301	806010	0.0307	0.0256	0.0249	0.0278	0.0294	0.0290	0.0307	0.0307	0.0307	0.0307	0.0356	0.0300	0.0322	0.0233	0.0204	0.0233	0.0233	0.0209	0.0221	
Hr13	0.0097	0.0097	0.0097	0.0097	96000	960000	9600.0	0.0096	0.0086	0.0086	0.0086	0.0074	0.0120	0.0120	0.0184	0.0184	0.0184	0.0184	0.0163	0.0163	0.0245	0.0244	0.0241	0.0243	0.0243	0.0249	0.0236	0.0254	0.0242	0.0240	0.0214	0.0021	0.0022	0.0202	0.0265	0.0253	0.0254	0.0314	0.0303	0.0313	0.0314	0.0305	9060'0	0.0310	0.0259	0.0252	8720.0	0.0292	0.0292	0.0304	0.0304	0.0104	0.0264	0.0351	0.0270	0.0315	0.0227	0.0199	0.0238	0.0238	0.0213	0.0220	
Hr12	\$600'0	0.0095	0.0095	26000	0.0093	0.0093	0.0094	0.0094	0,0074	0.0074	0.0074	0.0071	0.0119	0.0119	0.0158	0.0158	0.0158	0.0158	00144	0.0143	0,0229	0.0233	0,0234	0.0234	0.0237	0.0243	0.0204	0,0246	0.0239	0.0199	0.0207	0.0014	0.0213	0,0199	0.0264	0.00523	0.0254	0.0338	0.0325	0.0336	0,0332	0.0325	0.0322	0.0327	0.0267	0.0263	0.02N9	0.0318	0,0312	0,0319	0.0319	0.0319	0.0319	0.0380	0.0329	0,0343	0.0232	0.0203	0.0228	0.0228	0.0228	0,0215	
Hrti	660000	0.0099	660070	66000	0.0097	0.0097	0.0097	0.0097	0.0082	0.0082	0.0082	0,000	0.0123	0.0123	0.0174	0.0174	0.0174	0.0174	00156	0.0156	0.0239	0.0237	0.0236	95700	0.0238	0.0242	0.0224	0.0245	0.0238	0.0219	0.0204	0.0317	0.0218	0.0198	0.0257	0.0255	0.0260	0.0330	0.0321	0.0330	0.0331	0.0322	12800	0.0325	0.0266	0.0262	0.0285	0.0314	0.0304	0.0309	60000	0.0309	0.0309	0.0386	0.0326	0.0334	0.0233	0.0201	0.0235	0.0235	0.0215	0.0218	
Hr10	0.0038	86000	0.0098	0.0098	96000	96000	9600 0	960000	0.0084	0.0084	0.0084	0.0077	0.0130	0.0130	0.0166	99100	99100	0.0166	0.0152	0.0152	0.0237	0.0237	0.0234	45700	0.0236	0.0240	0.0224	0.0250	0.0239	0.0216	0.0194	0.0000	0.0216	0.0192	0.0253	0.0050	0.0264	0.0350	0.0334	0.0349	0.0344	0.0334	0.0333	0.0337	0.0276	0.0272	0.0291	0.0327	0.0321	0.0315	0.0315	0.0815	0.0285	0.0350	0.0343	0.0350	0.0231	0.0198	0.0230	0.0230	0.0216	0.0212	
Hr09	86000	86000	86000	86000	56000	26000	36000	20000	98000	0.0086	98000	7/000	0.0124	0.0124	0.0175	30175	00175	0.0175	19100	00100	0,0234	90239	0.0238	18700	30240	96200	9.0238	0.0252	0.0239	0.0229	90208	30218	0.0217	0.0190	25200	0.0762	99700	0.0346	98800	0.0345	0,0340	0.0331	16500	0.0335	0.02E1	0.0273	0.0293	0.0320	0,0320	0.0309	0.0309	0.0309	0.0309	99800	90238	0,0337	62200	0.0199	28200	20232	0.0213	0.0211	
Hr08	90106	00106	90109	00100	00100	00100	00100	00100	06000	06000	06000	20083	10125	50125	10184	00184	10184	10184	10181	10181	10531	10232	10235	10237	00336	10236	00260	0.0248	30236	10252	10237	10011	10215	10202	50255	10350	10254	80308	56503	30308	10308	10295	10299	00299	30256	10253	10252	10289	10282	10277	10277	10277	10257	10313	10201	10300	0030	90209	10229	00229	10213	00212	
1107	0105	0105	0105	0105	0010	0010	0010	0100	6600	0093	.0093	1900	0112	0112	0208	0208	9020	0208	0202	0201	0252	0257	0258	8570	0254	0250	0268	0252	.0258	0267	0246	0281	0232	0214	0269	0253	0268	0324	0315	0324	0324	0317	0315	0320	0254	1920	0273	0295	0295	0256	0286	0286	0273	0333	0256	0316	0234	0222	0251	0251	0283	.0227	
100	0 7600	0092 0	0092 0	0092 0	00055	0 2500	0092 0	0092	0 9800	0 9800	0 9800	0072	0118 0	0118 0	0181	0181 0	0181	0181 0	0 6510	0 6510	0232 0	0 8123	6223	0 8770	0 01.03	0 213	0203 0	0231 0	0 9170	0184 0	0182 0	0130	0 6000	0173 0	0530	NO SECON	0242 0	0 5970	0 8620	0279 0	0833	0 6629	0 5060	0302 0	6241 0	0240 0	0 2520	0 9629	0 9820	0 222	0 7700	0277 0	0 1970	6832 0	6907 0	0307 0	0 (12)	0188 0	0520	0220	0204 0	0201 0	
r05 H	0092 0	0092 0	0002	0092 0	0001	0 1600	0092 0	2692 0	0 6600	0093 0	0093 0	9000	0110	0110	0 0510	0150	0150	0150 0	0160	0160 0.	0223 0	0212 0	0235 0	3195 0	0196	3225 0.	0202 0	0216 0	0228 0.	0 1610	0184	3171	0205 0.	0182 0	0526 0	3539	0243 0	0277 0	0301 0.	0285 0	1338 0	0300	0222 0.	0276 0	0231 0.	0241 0	0257 0.	0277 0	0273 0	0277 0.	0277 0	0277 0	0277 0	0333 0	0251 0.	0308 0	0219 0	0184 0	0185 0	0185 0	0193 0	0190 0	
H H	0 160	0091 0	1600	1600	091 0	0 000	0065 01	0000	0 +90	0064 0	0000	900	080	080	0 0511	0 00	0510	0510 071	0 721	157 0	0 052	1234 0	252	200	1180	1248 0	1230 00	1231 0	1260 0.0	163 0	1178	0 001	1205	1178 0.	227 0	0 38.0	1242 0	1276 D.	303 0	1281 0.	1289 0.	1302	0 612	1276 0	1231 0	1241 0	1257 D.	272 0	277	1278 0	0 0 0	278 0	00 000	333 0	279 0	0 000	222 0	1188 0	1611	0 161	1201	196	
03 H	091 00	091 0.0	091 0/0	001 00	260	260	092 0.0	092 00	900	000	064 0.0	000	082 0.0	000	150 00	150 00	150 00	150 0.0	159 00	159 0.0	260 0.0	241 00	261 0.0	179 0.0	177 00	257 00	213 00	235 0.0	272 0.0	165 0.0	182 0.0	169 001	205 00	178 0.0	977	717	241 00	274 0.0	301 00	285 0.0	288 0.0	662	214 0.0	276 0.0	231 0.0	240 0.0	257 0.0	272 0.0	272 00	778 0.0	278 0.0	278 0.0	261 0.0	926	280 00	305 0.0	218 00	190 0.0	169 00	169 0.0	200 002	196 0.0	
)2 Hr	92 0.0	92 0.0	92 0.0	92 0.0	0.0	200	91 0.0	91 0.0	0'0 E64	93 0.0	93 0.0	994	17 0.0	0.0	20 00	200	50 0.0	20 0.0	00 09	90 09	34 0.0	19 0.0	30 0,0	96 0.0	99 0.0	34 0.0	0.0	22 0.0	0.0	0'0 96	177 0.0	00 99	0.0	71 0.0	32 0.0	30 00	43 0.0	0.0 29	0.0	0.0	35 0.0	0.0	95 0.0	273 0.0	29 0.0	35 0.0	5.6 0.0	71 0.0	271 0.0	77 0.0	77 0.0	77 0.0	59 0.0	132 0.0	71 0.0	00 90	18 0.0	88 0.0	87 0.0	0.0	97 0.0	00 06	
H HR	92 0.00	92 0.00	92 0.00	92 0.00	91 000	31 0.00	91 0.00	91 000	86 0.00	86 0.00	86 0.00	73 000	27 0.03	27 0.01	20 0.03	000	200	50 0.01	000 09	000	10 0,00	31 000	22 0.00	31 000	91 001	14 0.02	02 005	29 0.02	12 0.02	85 0.01	80 000	84 0.01	03 0.02	67 0,03	36 0.0	36	43 0.02	200 95	96 0.02	73 0.02	29 0.03	95 0.03	97 00	65 0,02	28 0.02	41 0.02	57 0.02	76 0.02	70 0.02	77 0.02	77 0.03	0.0277 0.0277 0.0278	59 0.02	27 0.0	54 0.02	000 000	18 0.02	58 0.01	82 0.03	82 0.01	91 0.01	94 0.03	
Hro	0.00	2 000	2 000	0000	000	000	1 000	0000	0000	9000	0000 6	000	1 001	1 0.01	100	1 001	100	1000	8 0.016	100 8	4 0.02	2 002	0.02	200	2 0.014	5 002	4 0.02	3 0.02	0 002	1000	2 001	1000	5 0.020	7 0.014	9 0.02	200	4 0.024	8 0.02	1 0.02	7 0.02	000	0.02	2 0.01	2 002	0 0.02	0 002	6 0.02	5 0.02	5 002	7 0.02	7 002	7 0.02	9 0.02	0 003	7 0.02	003	0.02	0.01	100	4 0.01	1 001	2 001	
Hroo	0.003	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.006	0.008	0.007	0.012	0.012	0.018	0.018	0.018	0.018	0.015	0.015	0.023	0.022	0.022	0.0224	0.023	0.023	0.020	0.022	0.022	0.018	0,018.	0.0316	0.020	0.016	0.024	0.0736	0.024	0.030	0.029	0.030	0.030	0.029	0.030	0.030	0.0340	0.024	0.025	0.030	0.028	0.027	0.027	0.027	0.025	0.033	0.030	0.030	0.034	0.018	0.022	0.022	0.019	0.020	ĺ

	(Calling 4)		-					+		1.4						٠	*	-	-			-					-			1	-	-	-							٠					,								.40			٠															*																
	(m)	9	0	0	e	a			0	0.	9	ø	9	0	0	0	0	0	0	a	0	0			0	0	0			0	0 4	0	0	0	ø		0	0		6	0	0	a	9								9	0	0		0	0	0		a		-	0	0	0	a	0	0	0	. 0	0	0	0		0	0	0	0	0	0	9		0	0		0	0
WIGH	(Including	2.6	20	2.0	26	63		- 10	43	18	119	14	14	14	14		12	11	12	23	10	10	10		01		13					91	14	*										11					**			- 16	- 41	18	- 10	18	- 18	17	16	12	98	100	1.0	+4	- 48	1.6	- 18	94	16	18	16	1.0	15	- 0	16	16	. 91	1.6	15	18	1.5	118		*	= =	52	113
4 02	Y2	82233625	822409.45	622562.00	822545.7E	822316.62	873434 AK	822496.53	822614.65	1224.05.09	822526.54	922465.27	822494.47	822441.65	\$22454.02	822367.55	\$22866.34	152432.00	822462.45	822456.02	822568.02	10 299629	122425.39	822380.A8	827384.59	822394.80	SZZZA BI	2000000	277778	2 ((()))	022340.13	822348.78	122125.44	622178.07	822252.03	822278.92	822341.T2	822376.93	82240579	822431.11	822484.38	822072.07	H22126.94	822176.17	*******		200400000	400,000,00	STATES AND A P.	833444 63	872 Mile 6.7	822320.45	822250.62	622162.67	AZZDBEAS	8220T1 22	621367.56	821877.95	922086.76	822007.07	822967.62	822346128	622174.73	82212203	822144.43	822162.89	522149.92	622128.55	822115.33	822206(3)	\$22039.KZ	82181428	821738.42	82188122	821727.AS	10'688120	821967.78	122000287	#22008.72	621363.31	821863.31	821891.67	92196276	821763.88	82181181	\$21796.91	\$24822.5F
203	X2	83317737	833434.80	833969.46	83396546	8331124.93	411010	93367378	19219228	12297271	83404615	831827.55	833712.97	833712.11	833840.51	83386359	83284185	13389664	83388354	833846.51	83342240	633416.08	933447.92	93354454	933587.50	833587.54	111111111111111111111111111111111111111	Total Control	03355007	00000000	0334850	93346965	833100.53	133232.06	833377.80	83356334	633673.82	833768.11	83384678	833917.83	833986E8	833111179	83325339	83130477	1000000	47700000		94,104,10	27720444	***************************************	A1104716	83396646	834034.90	834540.82	83423428	83432121	134384.01	833158.58	63343410	933274.46	033438.70	833775668	83368833	83355671	03364955	83168368	833713.85	633747.83	833778.49	83387234	833867.20	93410921	834255.10	83405834	1811816	83313976	93328674	93346651	83354373	1331543.70	833563.70	832315.56	833481.00	933476.47	63325348	83255638	83332688
input for	Y1	822324.11	822345.74	622408.45	822543.00	622308.10	27178841	627421.55	822496.58	132614.65	822628.09	822419.91	822455.21	833494.47	822441.05	10 865228	822297.16	822463,30	822432.88	82248238	822567.47	822554.02	522482.07	8CX77738	822390.48	822318.11	522354.80	P. C.	2074178	1000000	27.282.28	622345.13	822119.68	122129.44	822178.07	82225203	822278.46	822341.72	822376.15	822405.79	822431.11	822055.71	822672.07	822129.94		200100				******	SPECIAL STR	822360.57	822320.48	522250.52	\$22.62.67	822081.65	822010.68	621955.43	821977.96	621842.33	822006.80	40000	82216126	827067.29	82212203	822144.40	622152.80	822148.62	622128.55	822 (23.04	822113.30	822052,66	621814.78	822039.23	821889.22	821689.28	621889.31	821947.50	822008.03	822028.72	621952.62	821834.07	821491.68	821775.07	821783.15	821757.87	821820.73
4	X	633125.78	833231.08	833454.89	633360.46	E31118.28	E11454.14	633516.26	87.578559	131533,67	633973.71	633527.00	833627.55	E33732.87	633782.11	633681.17	613693.59	833978.15	633696.64	633883.64	623387.36	633423.69	633416,08	813447.62	633544.64	133483,77	832587.96	2000000	477092.07	1935678,07	633393.09	613A88.61	833073.42	833100.63	633232.06	613377.64	833503.61	833673.62	633764.65	813848.76	833917.83	833076.99	833121.78	811261.50	*******	1000000	20000000		*******	**********	F13231.16	E13502.96	833 950.40	634034.90	534140.62	834231.72	834322.77	835097.20	613154.66	613101.67	833274.00	£13738.64	833734.04	83343883	633586.71	25.649.55	833683.68	833712.65	533757,63	633784.53	833778.89	833873,20	634155.21	E13167.79	E340963	83311E.37	633139.75	£13294.66	63.034.03	833543,73	633480.98	71.081.023	833315.06	833154.01	613176.74	£13168.00	833249.00
Caline	Pair	R003	R003	11003	R003	R004	100 m	Rock	H-00.H	F100/E	800H	RS16+R307	R006+R007	R006+R:007	REDS-R007	R018+R009	ROOM-HOOM	R010-R011	6010-H011	RECE-REC	RO12+R013	R012+R013	R012+R013	MOLZ+ROKS	HOT 2+NOT2	HO14+KO15	MON G-MONT	The same	Moto	200	2754	R222	R023	R024	R625	meze.	R027	H028	820H	Rest	H001	F033*R301	RESTS	Reta	BANA	WALL OF THE PARTY OF	2000	Batte .	2000	8040	Bees	NG42	R043	HO44	Bass	Rock	HD47	RNR	8048	BONG.	ROBT	8563	R083	H054	H054	11084	H084	H054	R054	ROSS	ROM	F1057		9100	NONO	1001	ROSZ	RDES	HD64	#100 W	H054	RORS	MONG	11097	HOSe	RONS	MOTO

210.0	9510'0	1510'0	4910'0	\$2100	20200	0.0185	LETOO	\$610'0	Z610'0	2020.0	16100	0.0200	0.0211	0.0220	1120.0	0.0242	012010	80200	6,0217	£220.0	0.0212	7150.0	315
510.0	2910.0	5910.0	9510.0	9510/0	62100	P3f0.0	7210.0	2510'0	5210.0	0,0160	8E10.0	15100	0.0145	£510'0	89100	0610,0	£510'0	0.0154	ZST0'0	6210.0	0.0154	95100	153
\$10.0	0410.0	9E10.0	1510.0	SSTOO	87.000	E310.0	95100	55100	0.0150	t9t0:0	0.0139	05100	0.0144	PS10.0	29100	6840.0	\$510.0	05100	8610.0	SETO D	09100	0.0155	601
510'0	09100	DETO'0	1210.0	5510.0	82100	E910.0	95100	\$5100	0.0150	1910.0	65100	0.0150	9910.0	P\$100	89100	681070	9510.0	09100	86100	8510.0	0.0160	55100	691
100	FS10'0	0510.0	£910'0	0510.0	16190	6710.0	69100	6910'0	99t0.0	9510.0	£5100	59100	6510'0	1710.0	£810.0	T050.0	5910.0	05100	05100	0.0150	00120	9410.0	\$91
0.00	7910,0	9610'0	0.0223	6810.0	0.0204	£610.0	5610'0	9810.0 9910.0	het0.0	1610.0	0.0183	56100	2610.0	8810.0	16100	0.0260	1550.0	8750.0	098070	9410.0	9/20/0	1050.0	192
10:0	29100	0910°C	79100			E610.0	82100	1910.0	V810.0		64100	COTRY	1810.0	£6100	0.020.0	8050.0	92100	EETOO	1150.0	1720 0	0.0207	9610'0	
100	80100	0.0115	0.0121	0810.0	0.0130	6010.0	00130	62100	0.0132	0.0138	0.0200	0.0208	0.0148	0.0224	0.0146	0.0141	0.0137	00575	6210.0	0.0342	1650.0	0.0215	951
100	00100	2110.0	6510.0	0910.0	98100	E710.0	0.0172	6910.0	0.0160	EC10.0	P5100	E910.0	6510.0	8710.0	06100	1410.0	£910.0	1910D	\$910.0	1910.0	13100	1910.0	551
100	9910.0	2010.0	0910.0	19100	ENTOD	1/10.0	0.0163	29100	ZSI0'0	9910'0	SM100	8210.0	25100	£9100	7710.0	\$610.0	2510 O	45100	ZS100	4510.0	45100	7210.0	151
0100	5910'0	ZM0.0	95100	19100	0.0183	E410.0	E9100	5910.0	6510.0	8910.0	49100	6210.0	\$510.0	19100	8/100	96100	8510 O	85100	85100	8ST0'0	8510.0	8510.0	851
8100	99100	9910'0	2210.0	8410.0	0.0204	0610.0	£810.0	6510.0	\$710.0	\$810.0	E9100	5/100	6910'0	92100	8810.0	8020.0	9410.0	8/100	\$410.0	5410.0	\$710.0	94100	921
8100	9910.0	9910 C	\$610.0 -	0.0184	11700	EETO,0	E810.0	3810.0	2810.0	2610.0	27100	5810/0	6/10/0	7810.0	66100	0.0215	2510.0	92100	0.0184	2510.0	1810.0	9510.0	181
0.023	\$520.0	5170 C	9 0555	0.0230	0.0262	0.0242	0.0228	11/20.0	7550.0	0.0243	96200	9EZ010	0.0236	9620.0	00234	6450.0	1229.0	0.0214	0.0233	0.0240	0.0220	0.0234	922
910'0	Z#10'0	1210.0	1910'0	0.0172	7610.0	0.0185	9/100	5810.0	8/10.0	£810.0	7910.0	COTES	ZZ10:0	0610'0	16100	2150.0	\$810°0	THIOD	6810.0	0.0182	\$810.0	1810.0	181
610.0	1120'0	91200	Z120'0	0.0201	17720.0	8020.0	70700	60203	0.0200	11150.0	98100	96100	0610'0	2020.0	00201	9150.0	1619.0	16100	0/0188	0610.0	\$610.0	Z610.0	161
9100	5510'0	ÞETD'C	P210.0	6910'0	P510'0	060.0	9910'0	0/10/0	p910.0	89.tb.0	99100	0.0160	\$510.0	7910.0	06100	0050.0	1910.0	09100	09100	Z910'0	19100	19100	791
8100	09100	9510,0	Z810.0	\$810'0	01700	8610.0	M810.0	06100	5810.0	6610.0	84100	26100	Z810.0	£6100	10200	0.0219	8910.0	20200	91200	0.0227	51200	0.0204	561
0.000	5610.0	66TO'U	9610.0	\$6100	Q.0217	6610.0	P8100	\$810.0	1810.0	8610.0	ESTO'O	92700	8910.0	8210.0	SHLOO	4150.0	CL10.0	62100	9/100	0.0181	0.0172	82100	821
0.021	8020.0	7.020.0	Z020.0	0.0214	86,700	8150.0	E110.0	0.0218	MIZO.O	71150.0	9020'0	0.0210	0.0207	TTZ0'0	0.0214	££50.0	8610 0	86100	4610.0	0.0301	0.0203	7610.0	961
1700	1050.0	9,020.0	0.0203	91100	0.0236	0.0219	£1100	8120.0	4150.0	9110.0	9020'0	0.0208	4050.0	8070'0	8050.0	0.0322	\$610.0	6610'0	861070	0.0302	1610.0	7610.0	461
0.021	7050.0	0.020.0	0.0203	0.0216	0.0236	0.0219	D0214	8170.0	0.0215	0.0216	9020'0	0.0209	5020.0	9020'0	0.0209	0.0221	2610.0	16100	0.0205	6810.0	86100	96100	661
0.021	1020,0	0.0207	0.0203	0.0214	0.0235	0.0219	8020.0	£120.0	0.0214	7150.0	10000	0.0210	0.0207	7020.0	00210	0.0223	8610.0	56100	90200	0.0190	8610.0	£6100	002
1700	8050.0	7050.0	E020.0	0.0214	SEZO'0	6,0219	6.0212	0.0218	0.0215	7150.0	1020.0	0.0210	0.0207	£020'0	00270	\$£20.0	6610.0	0.0203	6,0203	2020.0	5610'0	E610.0	261
570.0	9520/0	6550.0	0.0340	1520.0	24200	2520.0	120.0	6920'0	5/20.0	\$150.0	64200	0.0278	5850.0	0850.0	1920 0	2550.0	72503.0	65200	0.0362	\$520.0	65200	0.0262	152
0.022	0.0212	0.0212	0.0210	0.0222	10.0247	0.0226	0.0223	1520.0	8,550.0	0.0230	0.0219	E250.0	0.0220	0.0224	0.0223	0.0232	0.0204	0.0204	0.0203	0.0207	7010,0	0.0203	900
0.022	6610.0	0.0214	56t0 0	9020.0	0.0211	0.0215	0.0205	0.0213	5050.0	8050.0	7610.0	0.0203	8610.0	6610'0	9070'0	6,0223	0.0204	00220	0.0155	8910.0	1210.0	0.0200	081
0.030	2150.0	OZEO'O	9820.0	10E0.0	SEEOD	6060.0	E6Z0'0	£1/E0.0	2250.0	raed.o	8950.0	0.0369	0.0384	IBEO.0	SEEOO	NZEO.O	SEED.O.	1550.0	\$SED'O	5520.0	9250.0	HAEO.O	158
0.033	1550.0	PIZG.C	0.0212	0.0220	今7000	6.0224	\$150.0	0.0226	ESSO.0	2550.0	1120.0	0.0215	91200	ETZO-0	7150.0	P.ESO.0	6050.0	0.0202	0.0221	9220'0	0.0210	5610.0	212
0.022	0,0214	0.0223	0.0218	0.0222	30.50.0	6550.0	8150.0	0.0225	1550.0	0.0224	60200	0.0214	0.0211	11200	91200	0.0236	0.0204	66100	0.0214	8120.0	£050.0	6,0213	908
0.024	51000	0EZ0,0	0.0211	0.0223	05700	0.0227	0.0220	0.0230	0.0220	85,00.0	6120.0	0.0218	0 0310	0.0212	51200	0.0232	8610.0	80200	0.0227	6ES0.0	7150.0	7910.0	100
0.013	0.0227	6120'0	0.0214	0.0226	8970'0	0.0229	0.0222	52200	0,0224	0.0222	60200	0.0215	0.0210	0.0211	51700	0.0231	6610.0	0.0208	0.0226	8250.0	7150.0	7610.0	706
0.032	0.0230	0.0231	0.0223	0.0223	15700	0.0229	0.0223	1520.0	8650.0	8550.0	0.0212	0.0217	5100'0	91200	61200	6,0243	0.0207	0.0212	0.0231	1920.0	61200	10200	100
0.023	0.0224	0,0255	0.0219	0.0238	0.0262	0.0246	0.0235	6EZ0'0	1750.0	0.0262	0.0222	0.0220	0.0271	0.0224	8550.0	2620.0 3620.0	0.0209	90200	0520.0	0.0260	0,0210	\$610°0	513
970.0	6250.0	6920,0	0.0243	8620.0	12200	2520.0	0.0239	6/200	M/20.0	£950.0	90600	9920.0	£1(0,0	0.0304	52200	2620.0	9620.0	98200	8/200	1620.0	0,0262 0,0254	MOEG.0	762
8200	6920.0		0.0262		0.0302	6,0279	99200	10000	9000'0	IIED.0	STEGO	7150.0	91100	75E0.0	1650.0	£150.0	8750.0	90200	0.0281	6820'0		E750.0	-
2200	2850.0	0.0282	0.0258	0.0273	6150.0	6750.0	9450.0	0.0323	0.0332	0.0339	OSEO O	0.0349	P9100	ETEO.0	5250.0	C160.0	\$550.0	61500	0.0334	1000.0	94500	9150.0	LEE
E50.0	1570'0	0.0261	#20.0 #20.0	0.0243	08700	1420.0	92.000 E9200	05200	1970'0	820.0	1970'0	00200	11700	£2£00	0.0260	BSZO.0	82200	1/100	1910.0	1010.0	0910.0	Z820'0	157
0.0074	5920'0	1350.0	Z#20.0	Z9Z0'0	£5700	8420.0	E9200	1570'0	1520.0	£20.0	85700	55200	/S20.0	9570'0	15700	0620.0	60.0249	Z\$Z0'D	6910.0	1910.0	7650.0	9920'0	752
8000	0100,0	\$100.0	Z900'0	0800.0	\$5000	E600.0	06000	26000	16000	5010.0	96000	50100	1010 0	E1100	01100	8110.0	0110.0	11100	11100	60100	60100	01100	601
0.020	0.0200	2810.0	5610.0	0.0210	0 0500	0.0224	90200	0.0215	0.0210	0.0214	26100	0.0204	0.0204	01200	12200	0.0233	2610.0	66100	86100	0.0198	7010.0	76100	761
0.020	00200	9810.0	2600.0	0.0210	0.0240	\$520.0	90200	STZ0'0	0.0210	\$150.0	26100	0.0204	90000	0.0210	1550.0	££50.0	2610.0	66100	8610.0	8610.0	7910.0	7610.0	261
1200	£610,0	7810.C	7610.0	6050.0	5EZ0'0	0.0222	0.0210	0.0220	0.0214	9150.0	0.0203	0.0209	9020'0	0.0214	52200	2820.0	\$610.0	96100	0.0189	8810.0	8810,0	5610.0	1 661
5000	Z500'0	5900°C	8500.0	#S00'0	65000	1900 0	290070	6900.0	8300.0	0400.0	P/000	52000	0.0085	P800'0	99000	6,000.0	Z900 0	0.0083	0,0083	5300.0	0.0082	78000	750
500'0	Z500'0	5500.0	8500.0	15000	65000	1900.0	Z900'0	6900'0	8900'0	0700.0	4700.0	52000	5800.0	4800.0	98000	£600.0	Z800°0	£800.0	E800.0	6,000.0	Z800'0	Z800'0	786
500'0	£500'0	5500'0	8500.0	#S00'0	6500'0	1900.0	Z900'0	6900'0	8900.0	0100.0	P/.00'0	52000	\$800.0	4800.0	98000	5600.0	7800'0	0.0083	£800.0	£800.0	0.0082	Z800.0	790
500'0	£500'0	5500'0	8500.0	\$500°0	6500'0	1900.0	Z900'0	6900'0	8900'0	0100.0	6,0074	52000	580010	4800.0	9800'0	£600'0	2800.0	0.0083	£800.0	6,000.0	£800.0	Z800.0	780
500'0	£500'0	5900'0	RS00.0	1/500'0	65000	1900.0	£900'0	6900'0	8900.0	0100.0	4100.0	52000	\$800.0	0.0084	9900'0	£600.0	2800'0	£800'0	0,0083	0.0083	Z800.0	Z800'0	290
0000	4500'0	5500.0	8500.0	P\$00'0	65000	T900'0	2900'0	6900'0	8900.0	0400.0	¥4000	52000	\$800.0	1/800.0	99000	6600.0	\$800.0	0.0083	0.0083	0.0083	0,0082	0.0082	280
500'0	Z500'0	5900'0	8500.0	\$500°0	65000	1900'0	7,900.0	6900'0	8900'0	0700.0	8400.0	5/00'0	0.0085	4800.0	9800'0	£600'0	0,0082	E800'0	6,0083	0.0063	2800'0	0.0082	780
500'0	£500'0	5500'0	8500.0	\$5000	65000	1900.0	79000	6900'0	8900.0	0700.0	\$100.0	52,000	2800.0	4800.0	9800'0	£600.0	0.0082	£800'0	6.0083	6800.0	Z800'0	0.0082	780
500 a	8500'0	9500'0	NS00.0	9500'0	19000	5900'0	99000	£100.0	14000	£400'0	6400.0	67,00.0	0.0091	\$600'0	10100	8600.0	0.0083	2800.0	0.0082	0.0083	£800.0	0.0082	£80
500'0	8500.0	99000	8500.0	95000	19000	5900 0	5900.0	£700.0	1700.0	£400.0	6100.0	64000	160000	\$6000	10100	8600.0	£800.0	0.0082	0.0082	0.0063	£800.0	0.0082	- 680
500'0	8500'0	9900'0	8500.0	9500'0	6,000.0	5900.0	\$9000	£100,0	1700.0	£400'0	6200'0	62000	1600 0	\$6000	Totoo	8600.0	0.0083	2800.0	G,0082	0.0083	E800.0	5800.0	180
500.0	8800.0	9500'0	8200.0	9500'0	89000	5900.0	\$900.0	£700.0	1700.0	£100.0	6100.0	64,000.0	16000	\$600.0	totoo	8600.0	£800.0	1800.0	5800.0	5800.0	\$800.0	Z800.0	580
500'0	8500'0	99000	8500.0	9500'0	£900'0	2900.0	\$900'0	6,0073	1700.0	£400'0	6200'0	67.00.0	1600'0	\$6000	10100	8600.0	E803.0	0.0082	Z80010	0.0083	6800.0	0.0082	690
500'0	P\$800	9900'0	8500.0	99000	19000	99000	\$900.0	6,000.3	1400.0	£100.0	6100.0	6200.0	1600'0	\$600.0	10100	8600.0	6,800.0	0.0082	0.0082	6,0063	£800.0	0.0082	880
500'0	8500.0	9900'0	8500.0	9500'0	1900'0	2900.0	\$9000	£700.0	1/00.0	E100.0	6700.0	6200.0	16000	\$600'0	1010'0	8600.0	6800.0	5800.0	S800.0	£800.0	£800,0	Z800.0	£80
120.0	9110.0	TIZO.C	9170'0	2150.0	62200	0.0219	61100	0.0220	0.0220	0.0222	91700	0.0219	81100	6120.0	0.0219	1110.0	0.0214	0.0214	0.0215	\$120.0	5120.0	2150.0	517
810.0	7710.0	BY10.0	6/10.0	6210/0	7610.0	5510.0	BZ10/0	6710.0	NY10.0	2810.0	0710.0	0.0100	5710.0	0.0150	ratoro	5050.0	8710.0	82100	8710.0	8710.0	8/10/0	8710.0	BZT
0.018	11100	8210.0	6710.0	6410/0	76100	2810.0	82100	6210.0	8710.0	\$810.0	0710.0	0.0180	0.0172	00100	28100	0.0202	82100	82100	8/10/0	8710.0	82100	8710.0	841
0.019	9910'0	6810.0	0.0194	2610.0	0.0212	6610.0	P610'0	9610'0	0.0194	8610.0	8810.0	0.0192	0610.0	9610'0	96100	0.0211	5810 0	28100	8810.0	8810.0	7810.0	7810.0	981
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8100	£810.0	0610.0	0610.0	8810.0	11500	2610.0	68100	2610.0	0.0190	8910.0	S810.0	00100	\$810.0	0610.0	16100	6050.0	TRIO.0	08100	1810.0	1810.0	1810.0	0810.0	641
p100	Z#10'0	9510.0	9E10.0	SETO,0	13:00	2610.0	66100	1510.0	0,0137	8610.0	19100	00100	0.0140	9E10.0	2E100	9610.0	7E10.0	09100	42100	0.0128	82100	0610.0	EET
P10'0	50,0142	9510.0	6610.0	SETUTO	20100	0.0136	EETGO	19100	0.0137	EA10.0	10100	0.0140	0.10.0	6E100	CETOO	9E10.0	7£10.0	00100	00157	0.0128	82100	7ETOO	251
0.014	Z#10.0	95100	6610.0	SETO'0	0.0142	9610.0	0.0133	19100	\$510°0	0.0143	19100	00100	0+10-0	60126	75100	9610.0	7E10.0	00100	42100	8210.0	82100	7E10.0	EEI
0.020	5610'0	9610.0	6610.0	0.0200	0.0234	0.0207	5610.0	5020'0	2020.0	0.0205	26100	0.0200	2610.0	7910.0	86100	2150.0	2810.0	98100	8810'0	\$810.0	7810.0	5810.0	181
0.020	5610.0	9610.0	6610.0	0/0200	0.0224	0.0207	6610'0	0.0205	2020.0	2020.0	26100	0.0200	0,0192	7910.0	86100	2150.0	5810.0	98100	8810.0	\$810.0	7810.0	58100	481
0 0 3 0	\$610'0	96100	6610'0	0.0200	0.0224	0.0207	66100	50200	0.0202	5020.0	26100	0.0200	2610.0	26100	86100	0.0215	5810.0	98100	881070	0.0187	C810.0	5810.0	781
510'0	##10°0	2010.0	05100	£\$10'0	1/100	B210.0	E510'0	£510'0	5510'0	0.0162	69100	Z5100	\$5100	0910'0	9910'0	\$10.0	8510'0	85100	9510'0	0910'0	0910'0	8510'0	851
(10.0	B310.0	1710.0	0.0165	Z910/0	0.0188	Z/10.0	E910.0	6510.0	9/10.0	2810.0	5710.0	E810.0	2810.0	9810'0	EBITO'O	0.0204	1810.0	1810.0	6/10/0	6510.0	8/10/0	0810.0	661
100	1910.0	Z\$10°C	7510.0	tsto'o	69100	9510'0	05100	\$510.0	ESTO'O	6510.0	59100	55100	2510.0	8510'0	59100	6,610.0	9510'0	95100	6210.0	2510.0	45100	5510'0	951
510'0	1810.0	D.OIBM	B/10'0	28100	0.0202	9810.0	1810.0	0.0201	0.0205	0.0212	6.0213	0'0530	0.0225	0.0228	91200	0.0235	0.0214	0.0214	0.0212	8120.0	5120'0	0.0217	EU
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910'0		5510'0	Z\$10°0	1910'0	18100	99t0'0	[9100	6910'0	8910.0	5/10.0	\$9100	E/10.0	0.0172	££100	8710.0	8610.0	1710.0	1710.0	0/10/0	£710.0	5710.0	1710.0	02
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910'0	2210.0	E210 C	0/10/0	S/10/0	96100	0.0180	\$4100	1610.0	E610.0	0,0200	8610/0	10200	807010	0.0212	00204	1,550,0	6610'0	0.0202	46100	0,0204	2020/0	0.0200	861
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B141	813295.35	821847,25	83331558	821881.67	13			0.0219	H	06100
R142	223329.89	421453.47	833318.98	621691.54	- 13			0.0139	H	00120
RTAR	833538/75	S2188V31	133/110:17	821534.07	11	-		0.0230	F	0.0235
0.144	11.001.008	121838.07	833118.74	621753.15	- 63	-		0.0211	-	0.6236
R145+8146	63512.63	821775.50	831004.98	827816.03:	- 13			92000	-	94100
RACT-RACE	RESTREES	SQ1505 28	822921.13	\$21727.74	16			Trivo	0.0	69100
R149	833728.61	82174432	033807.73	821684.38	14	0		9910:0		0.0169
8149	833774.08	E21943.52	61708008	821684.36	13	0		0,0166		69190
R150	633736.67	\$217316.20	83386731	821855.87	. 11	0		0,0166	-	69100
R151	19.519.519	82TEVE.98	83368250	\$2154179	11	0		99100	-	69100
Rtf1	E31693 DJ.	SPISHS 70.	83377528	821642.53	14	0		0.0166	-	169
R152	813774.08	22.542.52	1135555	821609158	218	ø		9910'0	9.0	0.0169
R163	613391.31	84.888.238	834018.77	822414.27	- 118	ø		0.0186	20.0	20179
R154	813950.86	\$22335.at	83389200	\$22369.87	16	9		0.0186	00	0.0179
Ress	833309.65	822777.58	833900.46	88702020	18	0	. 4	0.0157	-	67100
R154	633668.76	81177738	83280845	822271.35	100	4		0,0229	0.0	0.0211
Britis	82.388.E.S.	81277238	83362777	86723428	. 83	0		0.0304		0.0204
Rtsa	e11827.77	822172.06	83277228	\$2214238	- 13			0.0200	-	00200
M-159	834075.91	#72798.62	33411250	622344.34	11			06100		7610.0
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PISE	STATISA DE	15 052229	162/0108	S22298.62	. 83			0,01184	30	20183
B162	E34049.42	822228.28	83406839	622287.53	16			0.0193	0.0	0.0195
R162	822993.06	822201.46	13403430	822280.01	16	0	A	0.0198	0.0	96100
R154	654(07,86	62211123	83404642	822239.28	15	0		0,0184	H	DOLEA
RIES	10,000,000		93389447	\$22705.23	. 91	6.	100	0,0009		0.0212
RISS	833672.14	822051.38	833164.75	622160.50	19.	. 0		0.0175	-	0.0174
RTST	131015.47			622109-33	10	0		0.0270	-	0.0272
STAR-R165				622056.03	21	0		0.0108	-	0.0112
ATTE-RITE				121976.51	63			0.0125	-	0.0125
RITZ+B17:	823654.02		83377628	821367.65	20		+	0.0186	1	0.0185
N174-R175	633541.76	-	83368338	42122.55	100			0.0300	0.0	0.0200
Berrie	653496.77	621693.45	833565.47	82168073	2.6		3	0.0200	-0.0	0.0202
R177	803313.08	821899.34	83357368	\$21558.47	378			0.01189	-	88100
R178	833440.44	821529.00	353453.00	#21609.61	42	•	1	0.0219	-	0.0235
6119	833851.64		833.811.32	821600.28	11	-		0.0216	-	0.0236
8180	634236.31		93433499	822396.33				0.0208	+	0.0220
Brig C	83419158		03621631	822208.35			-	0,008	+	0.0167
R182	834140.62		83488438	-	- 16	-	-	0.0198	+	0.0204
64193	634099.34		834149.62	-				0.0208	+	0.0236
R184	634077.01		834881.51	82210294	0			0.0175	7	00177
W184	#24851.51		834077.90	822084.18	2			0,000	100	4/100
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B186-B181	613831.13		63656488	631818.03			-	0.6347	+	0.6230
R162+R195	27.371673	-		82177738	28			0.0067	H	96100
R134+R138		-		621681.48	22	,		0.0217	H	0.0723
H186+K202		824623.3s	#33828.17	821600.66	39			0.0210	P	0.0230
		MINUS	83440018	822104.71	11	-		0.0169	H	0.0172
Rise	534322.77	89/01/0729	82436436	\$2238E.94	118	-		0.0168	H	20168
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M200	834339.17	821814.13	834388346	81396338	147		1.45	0.0184	Н	28100
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Y2	82234678	822409.45	822543.00	82254£7E	822316.62	822388.41	823421.55	********	822426.04	822424.54	#22465.2Y	822464.47	822441.65	822454.02	822367.55	62346634	822422.88	822462.45	W22456.07	822566.02	622462.07	822425.39	822395.48	622384.69	822384.EB	822374.91	822398.31	822228	822293.72	822346.13	\$2234£.78	822125.44	822178.07	833363.83	E 22 27 E 63		25.00.000	20,000,000	4000000	853464 58	822012.07	WWW. 200 10.4	10000000	Beering 1	82227.21	822269.00	822264.07	822308.81	822330.76	622235.17	822368 57	\$22320.45	822200.02	622162.67	822006.AS	822011.22	82196158	821977.95	822086.76	822007.07	822067.62	822474.73	82216328	522174.73	622422.03	622364.43	8221228	26 69 778	40,000,000	400000		21,000,000	#21738.42	82188122	821727.4S	10'688128	821967.78	822007.97	#224038.72	621163.31	821863.31	821891.67	821862.76	821763.88	8218128	404704.01	821785.01
X2 X2	833231.06	833434.80	833969.46	831985.46	8331154.93	033425.15	02391620	431,000	833973.74	834046.15	833827.55	833712.07	833762.11	833848.51	83196118	83384185	83389664	83388354	PATERICA	83342248	633416.08	833447.52	83354454	833587.56	92,789,008	633633.17	833861.17	83320907	63335500	03348561	03348945	833100.53	833252.06	411477.80	*********	4000000	200,000	40,000	03300070	413-810-61	83311175	9113010	0.33455.59	92224677	033624.35	833843.40	83309420	833761.79	93377845	833833.16	93396236	83395646	634034.90	934140.92	834Z3478	83432121	13439401	933158.50	63343410	933274.46	133438.70	63368433	933734.66	83368833	83358871	033649.55		03371285	20/11/200		********	10.000.00	83425610	83406834	034241.81	833139.76	83328678	83346651	83354373	833543.70	633563.70	832315.56	833481.00	933175.47	93125368	413%118	STEERING !
Y	822330.25	822345.74	622408.45	822543.00	622308.10	822315.62	522386.41		BETS14 SK	827428.09	822419.61	822465.21	837484.47	822441.65	E22398.31	8222957.18	872463.30	822452.88	877.667.40	822567.67	822554.02	522482.05	82242X38	822350.48	522318.11	\$22354.80	1672228	822192.93	822339.76	27.282.238	822345.13	822119.68	122129.64	A2547A.02	10 4 5 6 6 8	*********	044444	BOTTE OF	20,000	827.614.61	822045.71	807073.03	2077075	200000000000000000000000000000000000000	822175.17	522221 21	90.662228	12234.50	822311.12	822318,98	822338.17	822360.57	177320.48	822250.52	822182.67	822084.66	823010.68	671955.43	821977.96	621642.33	822004.80	622088.21	822 (23.44	822163.28	877067,29	822 (22 03		92213290	10.000.000		100000000000000000000000000000000000000	BUT 147 AG	821814.78	822039.23	821880.22	821680.29	621889.31	821947.50	\$22008.03	822028.73	621952.62	821834.07	821691.68	821775,07	62(783.15	494747.67	BANAL BY 1
1X	12,177,128	833231.06	833434.89	633960.46	E3311E28	833185.93	633425.19	*******	131613.67	633973.74	833527.00	831627 66	833737 97	633782-11	633681.17	611693.69	833978.15	613696.64	RESIDED OF	613387.36	835423.89	613416.00	E13.647.62	233544.64	133488,77	833587.56	513 633 17	823082.67	10,805.02	633355.00	F13ABB.61	833073.42	833100.63	K13232.06	2011112 60	244444 24	84429474		20.00.00	833647.83	833076.99	BESSEDS TO	8777769	2000000	833298.77	633524.35	633653.40	E13594.68	R33761.98	833763,11	813 (53 (53)	E13502.94	833950.40	634034.90	ENABEZ	E34231.72	834322.77	633097.20	623156.06	613101.67	833274.00	833434.18	613736.86	833736.06	833438.83	633586.71	20044000	823183.00	100/1/000	20/12/200	-	20.0000	E3418531	et31667.29	834058.34	83311E.37	633139.75	833298-86	49.044.03	833543,73	633.460.98	77.091573	833315.00	633154.01	633176,74	P13166.60	CHINE OF 1
Pair	R1003	R003	R003	R003	R004	H004	N004	2000	ROOF	REGES	Rolfs+RigoT	9006+R007	900 6 - R 1007	1008+8007	S018+R009	SOUR - HOOS	1010+H011	010×H011	SECO-BOCK	Otz-Rot1	011+R043	1012+R013	MC2+RBC3	OC2+ROC3	SOL4+ROIS	1016+R017	SECR-RECT	ROTE	81021	RGZZ	R422	R023	R024	BEFF	Barre		1000	Batta	BA10	8400+	03.2×K201	Bette	2002		Maga	9000	16037	REIR	H029	6040	1041	N942	RDAS	ROAA	Bas	Model	HOAT.	HOAR	BOAS	RONG	Rost	Resz	RING	NISKS	M054	11004		NO.	2000	and a	and a	2000	Beks	ROKE	NONO	1001	ROSZ	RDE3	HDE4	#100 M	R054	ROKE	ROSS	1100H	ROSe	1000	HON

Road Type (caline 4)

H103 10,0084 10,0084 10,0084 10,0082 10,008	0.00166 0.00166 0.00166 0.00166 0.00166 0.00166 0.00170	0.0214 0.0214 0.0176 0.0176 0.0135 0.0137 0.0117
0.0081 0.0081 0.0081 0.0082 0.0073 0.0074 0.0073 0.	0.00157 0.00157 0.00157 0.00159 0.00118 0.00118 0.00119 0.00119 0.0019 0	0.0207 0.0207 0.0207 0.0163 0.0129 0.0129 0.0129
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 <th 0,0164 0,0163 0,0 0,0175 0,0173 0,0 Road Type (caline 4) Height Width (Including | Caline 4 in purt for 2034 Q 22 | Prop. 2 | P

0/10/0	- 20100	SALGE	1910'0	69100	62100	0.0172	TATOO	69100	0.0160	44100	PST0'0	eston	19100	18100	HETED	0.0204	Octoro	92100	8/100	0.0174	2410.0	0/100	1 0/10'0
02100	20100	BM10.0	1910.0	£9100	6/100	5,710.0	14100	69100	0.0160	4410.0	\$510°0	0.0163	TOTO	THIOD	16100	1020.0	04100	92100	8/10/0	6710.0	0.0172	0710.0	0.10.0
4100	Z910'0	2910'0	(910.0	24100	0.0123	6/10/0	04100	69100	1910.0	0.020.0	EBIO 0	6010.0	8810 0	0.0214	6,025.7	Z170'0	0.0210	0.0244	99100	0.0364	9/0525	0.0214	90000
510 a	£520'0	0.020.0	0.0214	61700	92200	MOSO O	F6100	0.0201	1610.0	8610.0	DOTES	enton	#810°0	0.0154	swtora	6050.0	ESTO U	95100	95100	#Storu	.4510'U	tstoo	9510 0
0.013	CA10.0	1510.0	091070	£\$10'0	5/100	ZSLOTE	5510'0	95T0'0	ENTO:0	£910'0	0,0142	ESTOO	0.022A	51700	60200	0.0230	8510.0	95100	951070	9510'0	0.0152	85100	9510 0
0.020	7510.0	8710.c	5810.0	4810'0	36100	5610.0	96100	TETOD	95000	6,0193	18100	60100	9810'0	06100	50200	9050.0	£619.0	LETOO	8910.0	\$810.0	8810.0	1610.0	5610.0
0.021	2050.0	9,0504	5050.0	6050.0	4120.0	0.0210	0.0204	50200	1020.0	6050.0	0.0201	E120.0	91700	91200	21200	0.0217	1023.0	ETZOO	SL20.0	£170'0	0.0208	E020.0	6610.0
9100	9910'0	1910 C	0.0184	\$\$100	21100	PP10'0	ostoo	45100	201030	4510'0	11100	15100	49100	V\$100	65100	36100	45100	3810.0	06100	0.034	AMIO.O.	0810.0	ELLO
BICO	5710.0	EGIÓD	0.0183	9810.0	60200	Z6T078	E8100	0.0192	2610'0	10700	38100	0.0200	76100	707070	66100	0.0221	0.0199	18100	2810.0	002010	0.0192	0.020.0	96100
8100	Z510'0	0310.0	E810.0	T4100	60700	5610.0	69100	94100	5,0177	19100	Ittoo	0.0176	14100	98100	62100	1610.0	1410.0	52100	08100	6710.0	7810.0	94100	1910 0
1200	P6100	9020.0	6540 U	0.0204	82200	6.0213 2510.0	00200	81700	0.0211	\$150.0	50200	0.0211	90000	90200	6,020.0	3110.0	0.0202	\$2100 \$2100	06100	0.0394	6610.0	E810.0	8670.0
	Z610'0				10200								0.0207		66100	0.0226	9020 0			9620.0		0.0230	20203
0.021		SMIG C	1610.0	5810.0		2810.0	2510.0	#210'0	0810.0	1150.0	0.0204	0.0213		90200				9650.0	95100		0.0228		
6100	1810.0	DOTES	0.0145	8810.0	ZIZOU	1020.0	LSTOTO	96TU 0	5610.0	0.0202	estoro	M6100	961010	86TU 0	66100	2150.0	6810.0	16100	66100	5910.0	7810.0	Z610'B	983.0 (
10.0	arro,o	5110.c	NETO-D	9610.0	3910.0	72£0.0	05100	15100	9,0149	8510.0	09100	1210.0	05100	19100	02100	0.0192	1910.0	09100	THION	£410.0	0.0160	2910.0	1910.0
10.0	8110,0	5,110,6	NETO D	3610.0	50,000	7210.0	06300	tstoo	8410.0	8510.0	0.0140	6200.0	estero	\$9100	0.0170	5610.0	1919.0	00700	60160	2970'0	09100	79100	1910.0
#10'0	ELIGO.	TITO,C	AE 10.0	99100	89100	2510.0	05100	1510.0	8410.0	8510.0	0.0140	E210.0	05100	19100	0710.0	2610:0	1910.0	0510:0	19100	\$9t0.0	09100	2910.0	1910
0.021	06100	BALLOC	1510.0	2810.0	66100	0.0183	14100	19100	0.0177	9070.0	\$6100	0.0202	9610 0	16100	1610.0	ets0.0	7919.0	95100	45100	17200	0.0210	66100	2510
8100	99100	7810.0	0.0185	Z8100	0.0199	E810.0	5520.0	7810.0	E810.0	0.0192	6210.0	881C0.0	M810.0	9810.0	81100	0.0213	7810.0	12100	15100	0.0204	7910.0	7810.0	\$810.0
6100	5530.0	OLIO.C	B610.0	9610.0	Etzon	1610.0	0.0188	£9700	M050.0	0.0211	9610.0	ME £0.0	981010	68100	16100	9150.0	2510.0	05100	ZS10.0	85T0'0	9510'0	1510.0	9510
6100	5810.0	MILO.C	0610.0	1610/0	grasse	NETO:0	06100	66100	6610.0	5020'0	£510'0	0.0202	0,000	0.0204	0.0209	5220.0	5610'0	56100	06100	ERTOD	5610'0	ESIGD	COLD
0.021	T050.0	8050.0	7610.0	502070	92200	0.0208	0.0200	0.0215	0.0214	TISD.0	0.0210	0.0200	8020.0	11200	0.0203	.6150.0	8610.0	6610'0	0.0200	16000	6610.0	66100	65707
6100	3810.0	ZRTO'C	M810.0	98100	107.90	9810.0	18100	0 CLT 90	26(0.0	0.0202	3610 D	EDCOLO	10000	51700	00510	0.0221	0.0202	86100	66100	0.0220.0	0.0200	66100	2020
2100	\$910,0	2010.C	9910.0	0.0172	1910.0	0.0181	1510.0	8710.0	£210.0	0.0182	1410.0	R2100	2510.0	8710.0	62100	\$610.0	E710.0	27,100	2100	1110.0	0.0134	EV10.0	65101
8100	08100	6/10 C	6/10 0	\$810°0	10200	NSto.o	(8100	0610'0	0610.0	0.0194	9810/0	Feto.o	9610 O	86100	16100	0.0213	7819.0	1810.0	82100	\$810.0	9810.0	98100	88101
810.0	54100	SATOR	8410.0	2810.0	0.0209	2010.0	38100	\$610.0	E610.0	1059.0	6810.0	2610.0	7610.0	66100	0.0204	9120'0	DELLA	SELCO	4100	98100	1810.0	ESIGO	1810
0.017	0.0159	6510'0	E910 D	14100	96100	6/10.0	14100	44100	5210.0	0.0182	0/10/0	1/100	\$210.0	18100	18100	0.0202	22100	07,100	0/100	0.0172	1710,0	1/100	1210
Ting	6110.0 ·	5210'0	at to a	2110.0	IZTOD	atto.o	PILLO	0.0171	0.0120	0.0126	SELOO	0.0124	62300	82100	STIGO	6210.0	81100	41100	91100	0.0110	SILIGO	91100	SITO
0100	7.B00,0	SMOC.C	9600'0	8600'D	50100	OTTO O	cotor	9010/0	\$010.0	'9010'0	0.0102	9010°0	90100	SOTO	FILTRO	Z110.0	ZOTO O	00100	20100	OCTO D	SOLOTO	0.0104	00101
2200	0.0233	9520.0	0.0218	0.0221	0.0248	9220 O	5550.0	9970'0	P200	6250.0	9970'0	ENZ0.0	0.0274	7750.0	HSE010	0.0267	69709 0	ESZOU	0.0251	15280	0.0252	0.0251	69/00
510'0	2510,0	8110.0	BETO D	\$\$100	14100	1910'0	95100	ISTOO	£510'0	£910'0	0.0151	ZYTOU	19100	59100	THICG	0.0193	09100	ESTOO	E9100	29300	19100	09100	79101
810.0	0.0172	1/10.0	E410.0	6/10/0	0'0500	9810.0	0610.0	16100	1610.0	6610.0	16100	90100	007910	507070	0.0203	6150.0	7610'0	16100	96100	8510'0	1610'0	5610'0	86100
9100	69100	6010 C	5510'0	estuo	5/100	19100	25100	19100	1910'0	1710.0	6510'0	@100	59100	PZ10'0	outoro	9610'0	7910.0	1/100	99100	22100	3910.0	6910'0	0210
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arco	05100	9510'0	9510.0	65100	08000	W20.0	0.0165	27100	1710.0	6810.0	6910'0	BLTOO	0810	68100	\$810.0	5020.0	7710.0	1710.0	18100	0.0182	17.10,0	0810.0	84701
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march entities do aptitut annuale	En 624822.67	19.		

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Hr18 1650 900 800 800 800 550 550 550 550 1200 1200 1200 1200 1	12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1700 900 900 800 800 800 600 600 1200 1200 1200 1200 1200 1200	85 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1500 1500 1500 1500 1500 1600 1660 1660	757 757 757 757 757 757 757 757
H115 1450 300 300 900 900 900 900 1050 1050 1050 1050 1	25 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
H144 2460 7460 7560 7560 560 560 1600 1600 1600 560 560 560 560 560 560 560 560 560	700 700 700 700 700 700 700 700 700 700
H13 650 650 700 700 700 700 650 650 650 650 650 650 650 650 650 6	25 C C C C C C C C C C C C C C C C C C C
Hr12 5400 660 660 660 660 660 660 660 660 660	10 10 10 10 10 10 10 10
Hr11 1300 1300 1300 1300 1300 1300 1300 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1470 1438 600 800 300 300 300 1000 1100 1100 300 300 30	1750 1750
1408 1450 1450 1450 1450 1450 1450 1450 1450	85 60 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
H108 800 800 800 800 800 600 1250 1250 600 1250 600 1250 600 1250 600 1250 600 1250 1250 1250 1250 1250 1250 1250 12	900
H107 11587 200 850 850 400 400 400 850 850 850 850 850 850 850 850 850 8	660 600 600 600 600 600 600 600
H106 200 200 200 200 150 150 150 150 200 200 200 200 200 200 200 200 200 2	250 250 250 250 250 250 250 250 250 250
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H-104	
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(California d.)	
969 m m m m m m o o o o o o o o o	
28	

Road		Coordi	nate (m)	-	WHAT	Height	Road Typ
Pair	X1	Y1	X2	¥2	producting	(m)	(calline 4)
Rist	100254.35	521947.25	******	621631.57	mixing rocal	0	1
R162	833329.89	E21552-E7	ED3:534	621691.04	11	0	1
R143	633129.75	421489.31	#33160.67	#21#34.07	- 13	0	1
E144	833760.07	621834.07	#33.87E.74	821783,18	13	0	1
Bits-Rial	823812.49	421974.55	£3497458	621516.03	- 22	. 0	1
2147+R140	E23734-44	#21886.3K	EDIOLES	821727.34	16	0	1
R144	833728.61	821749.82	632607.73	821684.38	14	- 0	4
R149	833774.00	621643.52	032507.73	621684.36	13	0	1
R190	823756.67	#21784.23	853687.71	821603.81	- 17	0	-
R151	833613.61	421610.68	833663.50	821663.70	13	0	- 1
R151	ADDEED OF	621543.70	#337762H	#21842.83	14	0	- 1
W192	635774.DB	621843.52	9334D8-17	821500.58	28	٨	1
RIS3	823991.31	622369.76	83467877	822454.27	78	0	1
8194	833960.66	222320-66	#ESWZ.00	822189.07	18	. 0	1
RIN	633909.46	122271.36	X33000.44	932130.45	16	0	4
#196	823698.78	622222.16	#11W09/85	022271.30	18		1
R197	823868.58	622222 54	611M0965	622172.98	78	0	-
R155	833827.77	822172.95	#1577E49	822113.30	18	0	- 1
HIER.	634070.01	622299.62	EMNERO	632384.34	18	0	1
RIES			#34577-61	622152.11			
B 191	834099.38 834034.90	\$22287.53 \$22250.52	834075.91		15	0	- 2
_				622299.62		_	-
R162	634049.42	822236-28	834800.16	#22287.53	15	0	1
M163	E33993.00	622201.66	EMS14.00	012250.01			_
R164	#34007 RE	\$22194.33	#S4S49.AZ	015130.20	75		1
R165	E33961.31	622151.78	£25994.47	62222123	3,6	0	1
R158	835872.14	822651.39	82196476	822190.50	18	0	- 1
R142	633,683:47	822042.45	#34007.E8	EX.181.33	18	0	1
R163+R169	833815.72	\$21 EF 67	EDDEN	WEIGHT AT	21	. 0	1
N179-9171	E33756.44	821 FB 8-15	833812-49	621178:50	18	0	1
8172×8173	823884.92	821823.12	811719.26	821487.65	26	. 0	-1
物でかれびた	833061,78	621407.56	E12W(3:34)	021023:55	36	0	1
8178	E30496,77	f2),600,49	\$\$3,540.47	821680.73	20	0	1
R177	E33517.08	821599.24	\$31.63.TE	621688.A2	29	0	1
RITE	X35440.44	621529.00	EX2408.60	#21908.41	16	0	Υ.
.800	XX3451.04	421624.31	#3591173	\$21600.38	17	0	1
8190	E34218.31	622256.35	\$54305.90	622585.39	18	0	1
R191	E28181.98	822212.72	83421831	822258-36	18	0	1
#192	838140-62	822162.47	834191.76	022212.3#	16	0	1
用482	E34099,34	622113.33	E34440:62	822162.67	18	-0-	1
RIM	E34077.01	622152.66	#54051.51	022100.94	13	-0	- 1
P.184	STADE 1.51	E22100.94	E34871.90	622094.18	13	0	- a
Kita.	£34071.00	02208 s. 18	834007.30	822115.02	14	0	- 1
Mies .	634309.65	\$22180.68	134312.66	833167.A4	10	0	
RIFE	834221.54	62238 à 63	£34273.34	622136.83	39	0	
RIAT	834190.59	822037.73	83423176	622086.A5	- 9	0	- 1
R153+R159	834004.93	#21315-03	834955.24	821600.22	96	0	1
R190-R191	823921,12	921727,74	\$34004.0E	621816.03	19	0	1
#192-R (92	633876.32	621460.75	812610.69	621727.58	29	0	1
R194+R195	833825,79	621600.86	613867.51	621631.AB	20	0	- 1
R395+R292	833784.01	621323.35	#13826.17	821650.58	20	0	,
E 197	634364.00	622040.04	E3440E11	82210471	17	0	1
Rtss	834323.77	822010.66	83436436	622060.94	78		- 1
R199	834291.93	421961.17	E34323.00	622010.A8	-38	0	1
R200	634239.47	#21914.12	834210.00	821983.18	14	0	1
#100	834239,47	821914.13	E34327.69	021840.33	18		1

			7							Val	nicle count	for each	road										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	13	9	6	7	10	50	50	100	100	180	150	150	150	200	200	150	250	300	250	150	150	100	100
50	19	12		10	14	-50	50	150	150	150	150	150	150	200	200	150	200	200	150	100	100	100	50
100	50	50	50	50	50	100	250	450	500	450	400	400	400	450	400	300	400	450	300	200	200	150	130
100	50	50	25	50	50	100	200	400	450	400	350	350	350	150	350	250	150	350	250	200	150	150	100
21	12	7:	4	5	3	22	160	72	73	70	69	119	118	120	139	115	169	220	166	112	109	58	57
29	16	10	-7 -	7	12	11	63	150	150	150	150	150	100	150	100	100	100	150	100	100	100	100	71
14	- 6	5	4	.4.	5	15	50	50	50	50	50	50	90	50	50	-21	50	- 23	19	13	10	10	1 2
14	8	5	4	4	5	15	50	50	50	50	50	50	50	50	50	2.5	50	23	19	13	10	10	1 7
14		- 5	4	- 4	- 5	15	50	50	50	50	50	50	50	50	50	- 31	50	23	.19	13	10	10	1 7
14	8	- 3	- 4	-4	5	14	50	50	50	50	50	50	50	50	50	23	50	24	19	13	11	10	
14	- 8	- 5	4	A	- 3	14	50	50	50	50	50	50	50	50	50	23	50	24	19	13	- 11	10	- 3
14	. 8	5	4	.4.	5	15	50	50	50	50	50	50	50	50	50	50	50	50	24	D.	14	13	10
100	100	50	50	50	50	100	200	250	200	200	200	200	200	200	200	200	200	150	150	150	100	100	100
100	100	50	50	50	50	100	200	250	250	200	200	250	250	250	250	300	300	300	250	200	200	150	150
100	100	50	50	50	30	100	200	250	200	200	200	200	200	200	200	200	200	200	150	150	100	100	100
450	350	300	250	700	250	400	1100	800	800	800	800	800	100	750	700	700	700	650	550	450	-400	400	300
500	400	350	300	250	250	450	1050	1300	1100	1050	950	950	1000	950	900	950	900	900	750	650	550	300	400
450	350	300	250	200	250	400	900	1100	950	900	850	850	900	650	800	BS0	550	850	700	600	500	500	900
23	19	15.	14	10	12	22	50	50	50	50	50	50	50	50	50	50	100	50	50	50	50	50	50
100	50	50	50	50	50	100	200	250	200	200	150	150	150	150	150	150	150	150	100	100	100	100	50
150	100	100	100	50	50	150	300	350	360	300	300	300	300	300	300	350	350	350	300	250	200	200	150
200	150	100	100	100	100	150	350	450	480	350	350	350	400	350	35G	400	400	350	300	250	250	700	150
200	190	150	100	100	100	200	400	500	450	450	450	450	500	500	500	550	600	600	500	400	350	150	250
150	100	100	100	50	100	150	300	400	350	300	300	300	350	300	300	350	350	350	300	250	200	300	130
150	100	100	100	50	100	150	300	400	350	300	300	300	350	350	350	350	400	350	300	250	250	200	150
300	250	200	150	150	150	250	600	750	650	600	600	600	650	650	650	700	700	700	550	500	450	400	300
750	200	150	150	100	100	200	450	600	500	500	450	500	550	500	500	550	550	550	450	400	350	350	230
400	150	300	200	200	200	350	850	1050	950	900	900	900	1090	1050	1050	1150	1250	1150	950	850	750	700	550
350	300	250	200	150	200	350	750	958	900	800	800	900	950	900	1000	1050	1150	1100	900	800	700	650	450
450	350	250	250	200	250	400	850	1100	1000	950	900	950	1050	1050	1050	1100	1200	1100	950	800	700	700	550
450	390	300	250	200	250	450	900	1150	1000	950	950	950	1050	1000	1000	1090	1100	1100	900	750	650	650	500
300	250	200	150	150	150	300	650	800	700	650	600	600	600	600	580	600	500	550	450	400	350	350	250
250	200	150	150	100	100	200	500	600	550	500	500	500	550	550	550	600	650	600	500	458	350	350	250
300	750	200	150	150	150	250	600	750	650	600	600	600	600	600	550	600	600	550	450	400	350	350	250
300	250	200	150	150	150	250	600	750	650	600	600	650	700	700	700	750	800	800	650	550	500	450	150
150	150	100	100	100	100	150	350	450	350	350	300	350	350	350	300	350	150	350	300	250	200	200	150
12	9	8	7	5	6	11	50	-50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	20
50	24	19	17	13	14	50	50	100	50	50	50	50	90	50	50	50	50	50	50	50	50	50	50
24	20	16	19	11	12	72	50	50	50	50	50	50	50	50	50	50	50	50	50	24	21	20	16
50	21	16	34	12	13	12	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	- 50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	90	50	50	50	50	50	50	50
100	50	50	50	50	50	100	150	200	200	200	200	200	200	200	200	200	250	200	200	150	150	150	100
19	16	12	11	8	11.	17	50	50	50	50	50	50	50	50	50	50	50	50	50	22	19	18	14
100	50	50	50	50	50	100	150	200	200	150	150	150	150	150	150	150	150	150	100	100	100	100	50
64	62	59	58	57	58	63	150	200	200	250	150	200	200	200	200	290	200	200	200	150	150	150	119
71	68	64	62	29	33	60	150	150	150	150	150	200	200	200	200	250	250	250	200	200	150	150	119
36	79	25	22	17	19	32	100	100	100		73	71	73	70	70	68	65	150	64	64	51	64	25
60	59	57	55	- 55	35	39	173	200	172	171	119	117	117	116	114	314	112	112		58	57	51	55
		44																	100				
100	100		338	- 31	35	100	150	200	150	100	100	100	100	100	100	100	100	100	100	100	100	100	71
. 6	7	5	A	A	4	7	17	21	17	14	12	11	11	9	7	3	4	4.		3	3.	2	1
16	-13	11	- 3	7	3	14	50	50	90	50	50	50	50	22	19	18	15	15.	13	- 11	10	9	- 6
20	17	14	- 11	8	10	19	- 50	50	50	50	50	50	- 50	50	- 50	21	20	19	17	- 13	- 11	11	9
50	25	20	17	15	16	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	-50	90
50	25	20	17	15	16	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50

Road Type (caline 4) Height #22006 (3) #2179 42 #2177 42 #2177 45 #2178 47 #2180 32 #2180 34 #22007 37 #22008 37 #22008 37 #22008 37 #22008 37 #22008 37 #22008 37 #22008 37 #22008 37

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210.0	9510'0	1510'0	4910'0	\$2100	20200	0.0185	LETOO	\$610'0	Z610'0	2020.0	16100	0.0200	0.0211	0.0220	1120.0	0.0242	012010	80200	6,0217	£220.0	0.0212	7150.0	315
510.0	2910.0	5910.0	9510.0	9510/0	62100	h3f0.0	7210.0	2510'0	5210.0	0,0160	8E10.0	15100	0.0145	£510'0	89100	0610.0	£510'0	0.0154	ZST0'0	6210.0	0.0154	95T0'0	153
\$10.0	0410.0	9E10.0	1510.0	SSTOO	87.000	E310.0	9510'0	55100	0.0150	t9t0:0	0.0139	05100	0.0144	PS10.0	29100	6840.0	\$510.0	05100	8610.0	SETO D	09100	0.0155	601
510'0	09100	DETO'0	1210.0	5510.0	82100	E910.0	95100	\$5100	0.0150	1910.0	65100	0.0150	9910.0	P\$100	89100	681070	9510.0	09100	86100	8510.0	0.0160	55100	691
100	FS10'0	0510.0	£910'0	0510.0	16190	6710.0	69100	6910'0	99t0.0	9510.0	£5100	59100	6510'0	1710.0	£810.0	T050.0	5910.0	05100	05100	0.0150	00120	9410.0	\$91
0.00	7910,0	9610'0	0.0223	6810.0	0.0204	£610.0	5610'0	9810.0 9910.0	het0.0	1610.0	0.0183	56100	2610.0	8810.0	16100	0.0260	1550.0	8750.0	098070	9410.0	9/20/0	1050.0	192
10:0	29100	0910°C	79100			E610.0	82100	1910.0	V810.0		64100	COTRY	1810.0	£6100	0.020.0	8050.0	92100	EETOO	1150.0	1720 0	0.0207	9610'0	
100	80100	0.0115	0.0121	0810.0	0.0130	6010.0	00130	62100	0.0132	0.0138	0.0200	0.0208	0.0148	0.0224	0.0146	0.0141	0.0137	00575	6210.0	0.0342	1650.0	0.0215	951
100	00100	2110.0	6510.0	0910.0	98100	E710.0	0.0172	6910.0	0.0160	EC10.0	P5100	E910.0	6510.0	8710.0	06100	1410.0	£910.0	1910D	\$910.0	1910.0	13100	1910.0	551
100	9910.0	2010.0	0910.0	19100	ENTOD	1/10.0	0.0163	29100	ZSI0'0	9910'0	SM100	8210.0	25100	£9100	7710.0	\$610.0	2510 O	45100	ZS100	4510.0	45100	7210.0	151
0100	5910'0	ZM0.0	95100	19100	0.0183	E410.0	E9100	5910.0	6510.0	8910.0	49100	6210.0	\$510.0	19100	8/100	96100	8510 O	85100	85100	8ST0'0	8510.0	8510.0	851
8100	99100	9910'0	2210.0	8410.0	0.0204	0610.0	£810.0	6510.0	\$710.0	\$810.0	E9100	5/100	6910'0	92100	8810.0	8020.0	9410.0	8/100	\$410.0	5410.0	\$710.0	94100	921
8100	9910.0	9910'C	\$810.0 -	0.0184	11700	EETO,0	E810.0	3810.0	2810.0	2610.0	27100	5810/0	6/10/0	7810.0	66100	0.0215	2510.0	92100	0.0184	2510.0	1810.0	9510.0	181
0.023	\$520.0	5170 C	9 0555	0.0230	0.0262	0.0242	0.0228	11/20.0	7550.0	0.0243	96200	9EZ010	0.0236	9620.0	00234	6450.0	1229.0	0.0214	0.0233	0.0240	0.0220	0.0234	922
910'0	Z#10'0	1210.0	1910'0	0.0172	7610.0	0.0185	9/100	5810.0	8/10.0	£810.0	7910.0	COTES	ZZ10:0	0610'0	16100	2150.0	\$810°0	THIOD	6810.0	0.0182	\$810.0	1810.0	181
610.0	1120'0	91200	Z120'0	0.0201	17720.0	8020.0	70700	60203	0.0200	11150.0	98100	96100	0610'0	2020.0	00201	9150.0	1619.0	16100	0/0188	0610.0	\$610.0	Z610.0	161
9100	5510'0	ÞETD'C	P210.0	6910'0	P510'0	060.0	9910'0	0/10/0	p910.0	89.tb.0	99100	0.0160	\$510.0	7910.0	06100	0050.0	1910.0	09100	09100	Z910'0	19100	19100	791
8100	09100	9510,0	Z810.0	\$810'0	01700	8610.0	M810.0	06100	5810.0	6610.0	84100	26100	Z810.0	£6100	10200	0.0219	8910.0	20200	91200	0.0227	51200	0.0204	561
0.000	5610.0	66TO'U	9610.0	\$6100	Q.0217	6610.0	P8100	\$810.0	1810.0	8610.0	ESTO'O	92700	8910.0	8210.0	SHLOO	4150.0	CL10.0	62100	9/100	0.0181	0.0172	82100	821
0.021	8020.0	7020.0	Z020.0	0.0214	86,700	8150.0	E110.0	0.0218	MIZO.O	71150.0	9020'0	0.0210	0.0207	TTZ0'0	0.0214	££50.0	8610 0	86100	4610.0	0.0301	0.0203	7610.0	961
1700	1050.0	9,020.0	0.0203	91100	0.0236	0.0219	£1100	8120.0	4150.0	9110.0	9020'0	0.0208	4050.0	8070'0	8050.0	0.0322	\$610.0	6610'0	861070	0.0302	1610.0	7610.0	461
0.021	7050.0	0.020.0	0.0203	0.0216	0.0236	0.0219	D0214	8170.0	0.0215	0.0216	9020'0	0.0209	5020.0	9020'0	0.0209	0.0221	2610.0	16100	0.0205	6810.0	86100	96100	661
0.021	1020,0	0.0207	0.0203	0.0214	0.0235	0.0219	8020.0	££20.0	0.0214	7150.0	10000	0.0210	0.0207	7020.0	00210	0.0223	8610.0	56100	90200	0.0190	8610.0	£6100	002
1700	8050.0	7050.0	E020.0	0.0214	SEZO'0	6,0219	6.0212	0.0218	0.0215	7150.0	1020.0	0.0210	0.0207	£020'0	00270	\$£20.0	6610.0	0.0203	6.0203	2020.0	5610'0	E610.0	261
570.0	9520/0	6550.0	0.0340	1520.0	24200	2520.0	120.0	6920'0	5/20.0	\$450.0	64200	0.0278	5850.0	0850.0	1920 0	2550.0	72503.0	65200	0.0362	\$520.0	65200	0.0262	152
0.022	0.0212	0.0212	0.0210	0.0222	10.0247	0.0226	0.0223	1520.0	8,550.0	0.0230	0.0219	E250.0	0.0220	0.0224	0.0223	0.0232	0.0204	0.0204	0.0203	0.0207	7010,0	0.0203	900
0.022	6610.0	0.0214	56t0 0	9020.0	0.0211	0.0215	0.0205	0.0213	5050.0	8050.0	7610.0	0.0203	8610.0	6610'0	9070'0	6,0223	0.0204	00220	0.0155	0.0148	1210.0	0.0200	081
0.030	2150.0	OZEO'O	9820.0	10E0.0	SEEOD	6060.0	E6Z0'0	£1/E0.0	2250.0	raed.o	8950.0	0.0369	0.0384	IBEO.0	SEEOO	NZEO.O	SEED.O.	1550.0	\$SED'O	5520.0	9250.0	HAEO.O	158
0.033	1550.0	PIZG.C	0.0212	0.0220	今7000	6.0224	\$150.0	0.0226	ESSO.0	2550.0	1120.0	0.0215	91200	ETZO-0	7150.0	P.ESO.0	6050.0	0.0202	0.0221	9220'0	0.0210	5610.0	212
0.022	0,0214	0.0223	0.0218	0.0222	30.50.0	6550.0	8150.0	0.0225	1550.0	0.0224	60200	0.0214	0.0211	1120.0	91200	0.0236	0.0204	66100	0.0214	8120.0	E050.0	6150.0	908
0.024	51000	0EZ0,0	0.0211	0.0223	05700	0.0227	0.0220	0.0230	0.0220	85,00.0	6120.0	0.0218	0 0310	0.0212	51200	0.0232	8610.0	80200	0.0227	6ES0.0	7150.0	7910.0	100
0.013	0.0227	6170'0	0.0214	0.0226	8970'0	0.0229	0.0222	52200	0,0224	0.0222	60200	0.0215	0.0210	0.0211	51700	0.0231	6610.0	0.0208	0.0226	8250.0	7150.0	7610.0	706
0.032	0.0230	0.0231	0.0223	0.0223	15700	0.0229	0.0223	1520.0	8650.0	8550.0	0.0212	0.0217	5100'0	91200	61200	6,0243	0.0207	0.0212	0.0231	1920.0	61200	10200	100
0.023	0.0224	0,0255	0.0219	0.0238	0.0262	0.0246	0.0235	6EZ0'0	1750.0	0.0262	0.0222	0.0220	0.0271	0.0224	8550.0	2620.0 3620.0	0.0209	90200	0520.0	0.0260	0,0210	\$610°0	513
970.0	6250.0	6920,0	0.0243	8620.0	12200	2520.0	0.0239	6/200	M/20.0	£950.0	90600	9920.0	£1(0,0	0.0304	52200	2620.0	9620.0	98200	8/200	1620.0	0,0262 0,0254	MOEG.0	762
8200	6920.0		0.0262		0.0302	6,0279	99200	10000	9000'0	IIED.0	STEGO	7150.0	91100	75E0.0	1650.0	£150.0	8750.0	90200	0.0281	6820'0		E750.0	-
2200	2850.0	0.0282	0.0258	0.0273	6150.0	6750.0	9450.0	0.0323	0.0332	0.0339	OSEO O	0.0349	P9100	ETEO.0	5250.0	C160.0	\$550.0	61500	0.0334	1000.0	94500	9150.0	LEE
E50.0	1570'0	0.0261	#20.0 #20.0	0.0243	08700	1420.0	92.000 E9200	05200	1970'0	820.0	1970'0	00200	11700	£2£00	0.0260	BSZO.0	82200	1/100	1910.0	1010.0	0910.0	Z820'0	157
0.0074	5920'0	1350.0	Z#20.0	Z9Z0'0	£5700	8420.0	E9200	1570'0	1520.0	£20.0	85700	55200	/S20.0	9570'0	15700	0620.0	60.0249	Z\$Z0'D	6910.0	1970.0	7650.0	9920'0	752
8000	0100,0	\$100.0	Z900'0	0800.0	\$5000	E600.0	06000	26000	16000	5010.0	96000	50100	1010 0	E1100	01100	8110.0	0110.0	11100	11100	60100	60100	01100	601
0.020	0.0200	2810.0	5610.0	0.0210	0 0500	0.0224	90200	0.0215	0.0210	0.0214	26100	0.0204	0.0204	01200	12200	0.0233	2610.0	66100	86100	0.0198	7010.0	76100	761
0.020	00200	9810.0	2600.0	0.0210	0.0240	\$520.0	90200	STZ0'0	0,0210	\$150.0	26100	0.0204	90000	0.0210	1550.0	EESO.0	2610.0	66100	8610.0	8610.0	7910.0	7610.0	261
1200	£610,0	7810.C	7610.0	6050.0	5EZ0'0	0.0222	0.0210	0.0220	0.0214	9150.0	0.0203	0.0209	9020'0	0.0214	52200	2820.0	\$610.0	96100	0.0189	8810.0	8810,0	5610.0	1 661
5000	Z500'0	5900°C	8500.0	#S00'0	65000	1900 0	290070	6900.0	8300.0	0400.0	P/000	52000	0.0085	P800'0	99000	6,000.0	Z900 0	0.0083	0,0083	5300.0	0.0082	78000	750
500'0	Z500'0	5500.0	8500.0	15000	65000	1900.0	Z900'0	6900'0	8900'0	0700.0	4700.0	52000	5800.0	4800.0	98000	£600.0	Z800°0	£800.0	E800.0	6,000.0	Z800'0	Z800'0	786
500'0	£500'0	5500'0	8500.0	#S00'0	6500'0	1900.0	Z900'0	6900'0	8900.0	0100.0	P/.00'0	52000	\$800.0	4800.0	98000	5600.0	7800'0	0.0083	£800.0	£800.0	0.0082	Z800.0	790
500'0	£500'0	5500'0	8500.0	\$500°0	6500'0	1900.0	Z900'0	6900'0	8900'0	0100.0	6,0074	52000	580010	4800.0	9800'0	£600'0	2800.0	0.0083	£800.0	6,000.0	£800.0	Z800.0	780
500'0	£500'0	5900'0	RS00.0	1/500'0	65000	1900.0	£900'0	6900'0	8900.0	0100.0	4100.0	52000	\$800.0	0.0084	9900'0	£600.0	2800'0	£800'0	0,0083	0.0083	Z800.0	Z800'0	290
0000	4500'0	5500.0	8500.0	P\$00'0	65000	T900'0	2900'0	6900'0	8900.0	0400.0	¥4000	52000	\$800.0	1/800.0	99000	6600.0	\$800.0	0.0083	0.0083	0.0083	0,0082	0.0082	280
500'0	Z500'0	5900'0	8500.0	\$500°0	65000	1900'0	7,900.0	6900'0	8900'0	0700.0	8400.0	5/00'0	0.0085	4800.0	9800'0	£600'0	0,0082	E800'0	6,0083	0.0063	2800'0	0.0082	780
500'0	£500'0	5500'0	8500.0	\$5000	65000	1900.0	79000	6900'0	8900.0	0700.0	\$100.0	52,000	2800.0	4800.0	9800'0	£600.0	0.0082	£800'0	6.0083	6800.0	Z800'0	0.0082	780
500 a	8500'0	9500'0	NS00.0	9500'0	19000	5900'0	99000	£100.0	14000	£400'0	6400.0	67,00.0	0.0091	\$600'0	10100	8600.0	0.0083	2800.0	0.0082	0.0083	£800.0	0.0082	£80
500'0	8500.0	99000	8500.0	95000	19000	5900 0	5900'0	£400.0	1700.0	£400.0	6100.0	64000	160000	\$6000	10100	8600.0	£800.0	0.0082	0.0082	0.0063	£800.0	0.0082	- 680
500'0	8500'0	9900'0	8500.0	9500'0	6,000.0	5900.0	\$9000	£100,0	1700.0	£400'0	6200'0	62000	1600 0	\$6000	Totoo	8600.0	0.0083	2800.0	G,0082	0.0083	E800.0	5800.0	180
500.0	8800.0	9500'0	8200.0	9500'0	89000	5900.0	\$900.0	£700.0	1700.0	£100.0	6100.0	64,000.0	16000	\$600.0	totoo	8600.0	£800.0	1800.0	5800.0	5800.0	\$800.0	Z800.0	580
500'0	8500'0	99000	8500.0	9500'0	£900'0	2900.0	\$900'0	6,0073	1700.0	£400'0	6200'0	67.00.0	1600'0	\$6000	10100	8600.0	E803.0	0.0082	Z80010	0.0083	6800.0	0.0082	690
500'0	P\$800	9900'0	8500.0	99000	19000	99000	\$900.0	6,000.3	1400.0	£100.0	6100.0	6200.0	1600'0	\$600.0	10100	8600.0	6,800.0	0.0082	0.0082	6,0063	£800.0	0.0082	880
500'0	8500.0	9900'0	8500.0	9500'0	1900'0	2900.0	\$9000	£700.0	1/00.0	E100.0	6700.0	6200.0	16000	\$600'0	1010'0	8600.0	6800.0	5800.0	S800.0	£800.0	£800,0	Z800.0	£80
120.0	9110.0	TIZO.C	9170.0	2150.0	62200	0.0219	61100	0.0220	0.0220	0.0222	91700	0.0219	81100	6120.0	0.0219	1110.0	0.0214	0.0214	0.0215	2150.0	2150.0	2150.0	517
810.0	7710.0	BY10.0	6/10.0	6210/0	7610.0	5510.0	BZ10/0	6710.0	NY10.0	2810.0	0710.0	0.0100	5710.0	0.0150	ratoro	5050.0	8710.0	82100	8710.0	8710.0	8/10/0	8710.0	BZT
0.018	11100	8210.0	6710.0	6410/0	76100	2810.0	82100	6210.0	8710.0	\$810.0	0710.0	0.0180	0.0172	00100	28100	0.0202	82100	82100	8/10/0	8710.0	82100	8710.0	841
0.019	9910'0	6810.0	0.0194	2610.0	0.0212	6610.0	P610'0	9610'0	0.0194	8610.0	8810.0	0.0192	0610.0	9610'0	96100	0.0211	5810 0	28100	8810.0	8810.0	7810.0	7810.0	981
610:0	9810'0	9810.0	\$610.0 0.0194	2610.0	0.0212	6610.0	96100 96100	9610'0	\$610.0 \$610.0	8610.0	9810'0 8810'0	26100	0610'0	9610'0	9610'0 9610'0	0.0211	\$810°0	1810.0	0.0188	8810.0	7810.0 7810.0	7810.0	981
810.0	2810.0	0010.0	0610.0	8810.0	11200	5610.0	68100	2610.0	0610.0	8610.0	2810.0	06100	9910'0	96100	16100	6020.0	1810 0	08100	1810.0	1810.0	1810.0	0810.0	981
8100	£810.0	0610.0	0610.0	8810.0	11500	2610.0	68100	2610.0	0.0190	8910.0	S810.0	00100	\$810.0	0610.0	16100	6050.0	TRIO.0	08100	1810.0	1810.0	1810.0	0810.0	641
p100	Z#10'0	9510.0	9E10.0	SETO,0	13:00	2610.0	66100	1510.0	0,0137	8610.0	19100	00100	0.0140	9E10.0	2E100	9610.0	7E10.0	09100	42100	0.0128	82100	0610.0	EET
P10'0	50,0142	9510.0	6610.0	SETUTO	20100	0.0136	EETGO	19100	0.0137	EA10.0	10100	0.0140	0.10.0	6E100	CETOO	9E10.0	7£10.0	00100	00157	0.0128	82100	7ETOO	251
0.014	Z#10.0	95100	6610.0	SETO'0	0.0142	9610.0	0.0133	19100	\$510°0	0.0143	Into o	00100	0+10-0	0'0128	75100	9610.0	7E10.0	00100	42100	8210.0	82100	7E10.0	EEI
0.020	5610'0	9610.0	6610.0	0.0200	0.0234	0.0207	5610.0	5020'0	2020.0	0.0205	26100	0.0200	2610.0	7910.0	86100	2150.0	2810.0	98100	8810'0	\$810.0	7810.0	5810.0	181
0.020	5610.0	9610.0	6610.0	0/0200	0.0224	0.0207	6610'0	0.0205	2020.0	2020.0	26100	0.0200	0,0192	7910.0	86100	2150.0	5810.0	98100	8810.0	\$810.0	7810.0	58100	481
0 0 3 0	\$610'0	96100	6610'0	0.0200	0.0224	0.0207	66100	50200	0.0202	5020.0	26100	0.0200	2610.0	26100	86100	0.0215	5810.0	98100	881070	0.0187	C810.0	5810.0	781
510'0	##10°0	2010.0	05100	£\$10'0	1/100	8210.0	E510'0	£510'0	5510'0	0.0162	69100	Z5100	\$5100	0910'0	9910'0	\$10.0	8510'0	85100	9510'0	0910'0	0910'0	8510'0	851
(10.0	B310.0	1710.0	0.0165	Z910/0	0.0188	Z/10.0	E910.0	6510.0	9/10.0	2810.0	5710.0	E810.0	2810.0	9810'0	EBITO'O	0.0204	1810.0	1810.0	6/10/0	6510.0	8/10/0	0810.0	661
100	1910.0	Z\$10°C	7510.0	tsto'o	69100	9510'0	05100	\$510.0	ESTO'O	6510.0	59100	55100	2510.0	8510'0	59100	6,610.0	9510'0	95100	6210.0	2510.0	45100	5510'0	951
510'0	1810.0	D.OIBM	B/10'0	28100	0.0202	9810.0	1810.0	0.0201	0.0205	0.0212	6.0213	0'0530	0.0225	0.0228	91200	0.0235	0.0214	0.0214	0.0212	8120.0	5120'0	0.0217	EU
	5510'0	0'0122	4510.0	19100	18100	99100	19100	6910'0	8910.0	5410.0	5910'0	EZTOO	2710.0	7710.0	8710.0	8610.0	1710.0	57,10,0	0/10/0	£410'0	2710.0	1710.0	041
0.016	2210.0	5510.0	72£0.0	1910.0	1810.0	99t0:0	19100	6910.0	8910.0	2510.0	setoro	EZTO'O	2510.0	5510.0	82100	8610.0	1710.0	2/100	0/10/0	£710.0	1710.0	1/10.0	30
910'0		5510'0	Z\$10'0	1910'0	18100	99t0'0	[9100	6910'0	8910.0	5/10.0	\$9100	E/10.0	0.0172	££100	8710.0	8610.0	1710.0	1710.0	0/10/0	£710.0	5710.0	1710.0	02
0.016	2210.0	EZTO'0	0.0170	54100	96100	0.0180	\$4100	16100	£610.0	0.0200	86100	0.0204	80000	0.0212	0.0304	0.0224	6610.0	0.0202	£6100	0.0204	0.0202	0.0200	86
910'0	2210.0	E210 C	0/10/0	S/10/0	96100	0.0180	\$4100	1610.0	E610.0	0,0200	8610/0	10200	807010	0.0212	00204	1,550,0	6610'0	0.0202	46100	0,0204	2020/0	0.0200	861
910'0 910'0 910'0	AT10.0	5710.0			96100	0.0180	5/100	1610.0	E610.0	0.0200	8510.0	0.0204	907070	0.0212	10200	0.0224	6619.0	20200	7610.0	0.0304	0.020.0	0.0200	861
910'0 910'0 810'0 810'0 810'0	\$510.0 \$710.0	£710.0	0.0170	5/10/0																			
910'0 910'0 910'0 810'0 810'0 910'0	P2100 P2100 P2100	0.0146 5710.0 5710.0	0.0152	8510'0	6/100	5910'0	8510'0	19100	0.0165	6,0173	£910'0	1710.0	0.0170	5/100	TTIOO	8610.0	1710.0	0710.0	7510.0	9910'0	E710.0	6910'0	
910'0 910'0 810'0 810'0 810'0	\$510.0 \$710.0	£710.0	0.0170				8510'0 1910'0	02100	6910.0	E510.0	£910'0 9910'0	EZTOU	0.0172	92100	87100	7610.0 8610.0	1710.0	00100	7510.0 6010.0	9910'0	E710.0	4/10.0	
9100 9100 8100 8100 8100 8100 9100	\$2100 \$2100 \$2100 \$5100 \$5100 \$5100	2210.0 2210.0 2010.0 2710.0	0210°0 2510°0 9510°0	8510'0 2910'0 5910'0	62100 19100	5910°0 2910°0 6910°0	1910'0 E910'0	00100	9910'0 6910'0	2710.0	9910'0 0910'0	001X3	0.0163	92100 29100		7610.0 7610.0	£710.0 0.0164	99100	69100 69100	9210°0	£210'0	\$2100 59100	221
9100 9100 8100 8100 8100 8100 9100 9100	9210'0 9210'0 1510'0 5510'0	2210.0 2010.0 20173 20173	0210°0 2510°0 9510°0	2910'0	6/100 28100	2910'0 2910'0	19100	02100	6910.0	5410'0	99100	EZTOU	0.0172	92100	8,1100	7610.0	E710.0	00100	69100	9230'0	£410'0	4/10.0	991 591 161 621

(caline 4)	(m)	(Jucingue)	72	(m) ates	ŀλ	IX	Pair
	0	St.	SEATORES.	AL TRECES	62.658158	10,755500	1108
1	0	92	TO THEFT.	92100000	22.878758	PE Zecces	2306
	8	41	#21875.22	AS. THECE B	42 G367558	BB. FRECCE	£10#
-	0	02.	82.000158 80.000158	76.800.CCE	40,196158 60,196158	BA.BACCE	610R
- 1	9	- 10	421889778	PRINCES	09,788758	29'109019	9250
		91	66388128	C#100000	77.649.54	DO RESTRICT	9256
1	0	2 P T	\$5,483153 \$21684.38	TACSSCER	831884.14 831884.00	TA.CORCER	940R
. 4 .		- 45	BE PTEPER	84-200CC#	90749124	\$8,E88EE8	1100
- 1 -		18	60 216152	PETARCES	82143128	BA-GOARTS	1,158
1	0	B1	65,160158 66,160158	19710000	BC.CCB126	85.5 SBCCB 85.5 TBCCB	810A 810A
- L	0	91	9E /951Z8	AR RESERVE	61.160158	59.8 58CE8	9908
- 4	0	2.0	16.588151	93396556	86.623156	10.788158	1906
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- 1	0	**	SA CHANCA	81349CC8	19.2825158	ER-SCREES	racu
- 1	0	11	SELETTIER	SCHEECES	8218128	BP.BRACCE	£80A
- 4	0	Pi	19.18815.6	18.666448	62.17.120	95,3526.36	tiou
- 4-		n	SA MARYEN	65336006	20/249524	15'295119	1906
- 4	0	T)	48.1602.87	17.700CCE	29 799128	497245118	1904
-	0	71	\$6.878158	PEOPPECS.	HE 2001ES	AC. GOOCES	1906
	0	Pi.	SE SIGIZE	58.0476E8	55.25255 55.25255 55.25255	PE CHOCCO	590s
	0	25	RE CHESTER	88.5005C8	\$51849.8E	07.022.FEB	995%
	0	41	SPRISIES	CALENSCOR	St. C. BETER	NB.C90CCR	1609
- 1	0	to to	02.808.28	APSOSCE	CP'899128	EF 679000	1909
	- 1	23	19.306158	GEROCCE	82.118158	15.32553	8904
,	4	21	12.804158 40.198158	68754668	831656.64 821656.64	08.840008	8809
	01	25	10.001758	cantecca	40,140,158	CO.TSACCO	840%
		43	27.788158	089/5006	45 944128	to certa	990%
•	1	23	21100128	91/009004	27.7283554	08.4725558	260%
	,	41	LE LISIER	80317558 80317558	28 509128	88.885.618	890W
	1	91	E0.528*5#	sc trece		80.855.618	\$904
		91	\$2.628158		834883703	96.75A668	6909
- 10	01-	- 01	00.001158	997275558	92.629128	09.084008	4908
		91	TA. SETTER	ELCHECCS.	00 987756	SA STREETS	\$10k
	- 1	93	AE CORLER	TOTABLES	TARETTAGE TELEBRICA	EL CARCES	690H
- :		10	18.402158 38.502158	65366CC8	951394'46 95161733	TO SARETS	690H
	0	24	ci.ecsiss	AB-TEECEB	P\$ 629169	at.esscca	1409+040
	0	- 02	acoretze.	95'819'55'8	421632.93	18.100018	1908-230
		92	92 869128	40119CC4	10,040156	95-647119	1909-250
4	0	81	14.072158	PARACER	83140112	#6.TCCCC8	1608
-	0	25	TE ACASTER	EASIDACE TESTOACE	#C.+6+126	46.600CC0 82.056CC0	250H+960 540H
	0	81	PR. SECSER	TATERACE SATERACE	ACAMATER SCAMPING	45,056,528 77,850,528 77,850,528	160H+960
	0.	- 11	SE BOSSER	PERSTACE	PATESTER.	19,151468	1013-001
ı.	Û	- 11	45 101 558	581602928	86.862326	IC BISHES	TOTALED
- 6	0	10	85,880558	24.108.6C6	95749728	96 ECC119	\$018+90L
- 1	0	91	40 990000	37,146628	16.FEACEG	CB.Trecca	BOTH
1	0	91	CA TRESSER	40040908	0.01CEE8 0.08EEE8	60,144CCB	TOTAL BOTAL
-	0	D 91	SESTEEM SEE	20212400	22.252.224	95'161929	50LH
	0	44	PE-090228	85 HKHC8	ER 95) 228	HE ETIENES	611.8
1	0	-10-	Ch exossa	47.000ACE		89,536,468	RIFF
- 4	0	61	19'50CZZ#	*6700000	WI SOUTH	87,648,76	EHR
i	0	91	SE PUZZER	\$33000.00	21.252228	32,508513	1308
4	0	91	6221229 82220133	TAMBECER	\$5,175558 87,000358	30.440EEB 30.446EEB	9118
	0	- 85	SA AFFESS	00,740466	46 161554	26,81024.8	91116
		93	T.F. 120022.8	82919028	25/933228	00.760358	008
	0	61	#6 C00129	82636328	LT.TEGESE	88.08FMC8	8118
- 1	0	61	SA 100158	STARRESCO.	28,500158	BE, FESTATES	B1150
· ·		93	46.876558	11,447224	21.374.15	to serrita	1518
4	0	91	Betttttt	87,816008	27.115258	88.181008	8133
4	0	- 11	08.007558	STATECCS.	BY ZZZZZE	81,830008	REES
	0	91	TO SECTION	TT.TERCER	TT 195 III	38.450028	9718
1.1	0	- 11	652174.73	66.810.004	922389.00	04.620668	9519
	0.	61	49 SIZZZE	12,000.00	SESIETTS.	89,694,000	4250
	0	91	NE VESTER	SCASSCCA	\$V # (2.22.8)	16 COSCES	9710
	0	81	46.817558 10.817558	71.846.008	\$0252558 \$0.252558	08.TTCCEB	M128
4	ò	91	\$2,000528	01,454.00	HO.ATTELS	IA RECCCO	1618
- + -	9	91	16.100.528	1204000	821080.70	811433.92	251.9
i	0	91	82:585:28	00168008	26.760558	SA GRACES	1178
- 4	0	51	TO STITZE	TRANSCER BOLESECE	BY SPETTS	90,1845C8 70,695CE8	8138
- 4		- 83	96 55×578	ecasecce	822 (78.06	10.565518	BESE
	0	81	PF-621228	23340022	9531858	10.040029	1218
			TO ETOSER	82333438	4978121878	63.001-008	ECTR
- 1	0	81	\$6.1187SB	95300558	£0,140328	633121,668	961.9

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E S	4	aline 4 input for		2034 03	Width				
Pair	**	Coordin	Coordinate (m)	64	Dischaling	ind	(caline 4)	000	C.T.
B141	613295.35	821847,25	833315558	821881.67	CONTRACTOR STORY			0.0200	0.015
8142	\$11329.88	121153.47	833318.98	621691.54	- 13			0.0139	100
RTAR	833539,75	SPERMENT	113370-17	821534.01	- 18	-		0.0210	0.02
0.544	11.481.00	121534.07	833118.74	621753.15	13			0.0211	0.02
R145+8146	633812.43	\$21,075.50	83100438	823816.03:	- 0		. 4.	9210'0	100
BIST-RISE		-	832821.13	\$7,727,74	118			0.0177	0.01
R140	833728.61	-	033807,73	821684.38	14	0	. 4	9910.0	0.016
8149	833774.08	E1043.52	83380773	621684.36	- 13	0		0.0166	0.618
R150	533736.67	\$21739.20	83386731	8214655.87	111	n		9910'0	0.016
RTST	623613.61	BZTEVE SR	83368250	\$21542.70	11	. 0		99100	0.016
Rtf1	1211693.00	E1643.70	13377528	821642.53	14	0.	14.	9910-0	100
R152	813774.08	22.542.52	833426.17	621609.58	2.0	0		9910'0	0.01
R153	613391.31	84,648,238	834018.77	922414.27	- 18	0		9810'0	10.0
8154	893980.86	\$22339.ed	83389200	\$22,269.87	118			0.0186	100
R156	1033009.05	822771.58	13390046	822320.45	18.	0.		0.0157	0.01
R156	623668.76	81177778	83280845	\$22271.35	108			0,0223	0.02
R157	53366.55	80 Z/2/238	83382727	82217238	- 60			0.0304	0.020
Rtsa	613827.77	822172.96	8327728	\$221435	- 13			0.0200	0.020
RTSS	834075.91	172799.62	13411739	622394.34	11			0.0190	100
6,16.0	82,040,629	12,787.53	83411782	11.222.228	. \$1			0.0194	0.620
R150	\$34134.9C	22 032228	163/0708	822298.62	. 50			0,01194	0.018
RTRZ	E34049.42	822228 28	834068.39	622287.53	. 51			0.0193	0.016
R162	622993.06	822201.46	13403430	822280.41	10.	0		0.0198	0.01
R164	854197,86	622111.33	93404642	822239.28	118	0		0,0184	0.016
RIES	633953.31	822151.70	93389447	\$22705.228	. 93			0.0009	0.02
RIGH	833672.14	822051.38	83396478	622160.50	13	0		0.0175	0.01
R167			134007.08	622109-33	10	0		0.0270	0.07
BILLA-RISS	513613.72	14.2.47	83387638	622056.03	21	0		90,000	100
RETE-RETE		80,0883.05	93391249	121976.51	- 69			0.0025	0.01
Rifte-Bitt	-	821822.33	83377923	\$21367.65	2.0		+	0.0186	0.018
R174-R175	833581.75	\$21077.NE	83368338	421223.55	100	-		0.0200	0.020
Betze	653496.77	621608.49	833565.47	82168073	2.6			0,0200	0.020
R177	813813.08	-	83357368	\$21558.67	316			0,01189	0.01
R178	833440.44	REVIETA	353453.00	#21609.61	18	•	-	67200	20.0
RITE	833451,64	EXTAGA 27	13381132	82100)138	11.			0.0216	0.02
R150	634216.31	-	83433598	822388.33				0.0208	0.02
Rege	8341911.98	-	10312500	82229833			-	0,0169	0.016
R162	834140.62	-	83484.78	62221239	- 16	-	-	0.0198	0.020
6493	634099.34	62111233	#34 M49.62	0.22162.07				0.0208	200
	B10011 01	80.2(1.225 G	83600151	822 10E34				0.0100	100
WHAT .	BA4071 80	87508A 18	STAINING N	892418.03				3000	100
A100	634309.99	\$22.180.NE	93428246	822287.44		0		0.0302	0.02
2186	634231.54	19 940728	83427334	822136.83	91			0.0030	0.02
R187	45.041643	622057.73	03423176	\$22006.45	316	0		0.0215	0.02
R188+6189	834004.88	821810.03	83499834	92108932	18			0.0181	100
M186-N191	633631,13	621/27/34	89,900,60	621815.03	14			0.0212	0.02
R162+R193	-	62169.25		821727.98	26			0,0087	0.015
R154+R198	_	621905.80		\$216E1.49	28			0.0217	0.02
H199+K303	-	8249233E	\$33828.17	821500.00	50			0.0210	0.02
4619	134344.34	SECOND IN	9364001B	622104.71			-	0.0169	100
R196	636322.77	-	12426426	\$22 DHE 94	82	-		0.0168	0.01
18139	234291.93	-	93433100	822010.48		-		0.0224	0.02
M200	834239.17	821816.12	97434976	621M2.38				0.0184	200
6671	Special	-	-	Second Sec				Water	UDA

Hr23	0.0175	69100	0.0182	0.0182	00100	0.0172	0.0172	0.0172	69100	0.0169	0.0173	100164	0.0164	0.0164	26100	0.0191	0.0184	90200	0.0162	E6100	0.0162	98100	0.0178	0.0197	0.0164	90100	20100	0.0187	0.0301	0.0204	0.0191	0.0705	0.0229	0.0232	0.0235	0.000	0.0162	0.0162	29100	31200	0.0234	0.0231	66100	00000	20000	000356	05100	COLOGG	0.0190	0.0185	0.0165
Hr22	0,0147	96100	0.0157	95100	0.0004	0.0155	0.0155	0.0155	0.0155	0.0155	95100	0,0146	0.0342	0.0145	22100	0.0165	0.0163	0.0153	0.0173	0.0184	0.0163	12100	0,000	0.0187	0.0136	O CUMOS	00000	0.0174	06100	96100	97100	0.6202	0.0234	0,0199	0.0193	00000	60,000	92100	62100	0.0200	0.0209	0,0211	00100	0.0188	COURS	00100	00000	D-0.0274	0.0175	0.0154	15100
Hr21	0.0151	0.0208	0.01470	19100	0.0174	0.015/8	30100	3,0158	0.0152	3,0152	3.01555	0.0342	0.0138	0.0142	0.0169	0.0169	3.0162	0.0182	0.0172	0.0184	69100	0.0172	0.0161	0.0186	0.0129	0 /685	0.0036	0.0173	0.0190	0.0395	621010	0.0303	3.0226	0,0199	0.0195	DATE OF	0.0121	1,0121	2,0121	0.0200	0.0264	90054	0.0173	0.0138	0.0000	0.0101	ESTOS	0.0260	0.0075	0.010.0	0.0160
Hr20	0.0164	0.0177	0.0172	0.0172	0.0149	0.0172	0.0172	0.0372	0.0172	0.0172	0.0169	0.0158	0.0156	0.0367	0.0190	0.0184	0.0174	0.0178	0.0171	0.0185	0.0169	0.0176	0.0167	0.0187	00120	0.000	2000	0.0178	0.0193	0.0194	0.0179	0.0300	0.0214	0.0205	OGZIS	10000	0.0146	0.0146	0.0145	0.0200	0.0200	0.0216	0.01SA	0.0199	0.000	0.000	0.0174	0.0232	0.0181	40107	0.0522
Hr19	0,0173	0.0174	0.0183	0,0180	43100	0.0171	0.0171	0.0171	0.0171	0.0171	0.0169	89100	0.0165	0.0170	0,0205	9610/0	0.0184	0.0190	0.0180	0.0188	0.0173	0.0182	0.0172	0.0195	0.0268	00000	00122	0.0186	0.0201	0.6200	0.0187	0.0202	0.0223	0.0207	0.0213	00000	65100	0.0159	0.0159	0.0204	0.0199	0.0222	0.0186	0.0202	00100	0.000	99100	0.0232	0.0187	0.0177	0.6427
Hr18	0.0196	0.6181	0.0203	0,0200	0.6030	0.0195	0.0195	0.0195	00194	0.0194	0.019A	16100	0.0193	0.0194	0.0210	0.023	0.0205	0.0208	0.0158	0.0217	0.0136	0,0006	0.0194	0.0218	0.0158	00018	CELLOO	0.0011	0.0028	0.0219	0.0209	60219	0.0246	0.0234	0.0280	0.0017	0.01	0.0183	0.01355	0.0030	0.0219	0.0247	00000	0.0227	20000	0.0016	00100	0.0245	0.0198	0.0195	0.0100
HH7	0.0162	0.0176	26100	0.0158	0.0169	0.0179	6,0179	60100	0.0178	0.0178	6.0179	0.0177	0.0179	0.0380	0.0227	0.0250	26100	0.0190	0.0186	0.0198	0.0784	0.0189	0.0177	0.0202	87100	0.0110	0.0178	0.0195	0.0212	0.0204	10197	0.0705	0.0227	0.0234	0.0231	0.0100	0.0171	0.0171	0.0171	0.0218	0.0200	0.0231	69100	0.000	00000	0.000	9/10/0	0.0226	0.0192	0.0387	A 0.167
Hrd6	60173	0.0168	0.0155	00183	00100	0/10/0	0.0170	00170	07100	0/10/0	0.0171	89100	07100	0.0173	0.0219	602000	0.0187	0.0133	0.0177	68100	62100	0.0185	0.0170	96100	22100	O. William	0.01192	0.0186	0.0202	96100	0.0185	0.0200	0.0218	0.0205	00204	0.0100	0.0162	0.0162	29100	0.0203	06100	0.0222	0.0183	0.0135	COLLOS	0.0306	9000	60200	0.0184	98100	20100
Hr15	49100	0.0177	0.0197	90193	0.0168	0.0171	0.0171	0.0171	99100	0.0169	0.0170	0,0176	0.0176	6/10/0	0.0224	0.0207	16100	00196	90100	60100	0.0187	86100	0.0178	90208	0.0175	STADO	1000	30100	0.0212	00200	\$6100	6:02:11	0.0234	0.0216	0.0221	0.0107	0.0164	9000	0.0164	0.0213	0.0250	0.0212	16100	60700	0.000	AAAAA	0.0170	0.0219	0.0183	0.0184	ACTOR .
Hr14	00100	6.0173	0.0199	0.0193	0.0169	0.0165	0.0165	0.0165	0.0165	0.0165	0.0164	0.0173	0.0172	0.0174	0.0224	0.0204	0.0189	76100	0.0188	0.0193	0.0785	0.0295	0.0175	0.0208	1/100	0.0100	0.0131	0.0100	0.0210	0.0206	0.0192	5 0232	0.0233	0.0215	0.0222	0.0100	0,0160	09100	0.0160	0.0212	96100	0.0228	26160	0.0208	00000	0.0000	0.0161	0.0213	0.0175	0.0174	A 0474
Hr13	0.0208	0.M71	0.0210	0.000	0.000	0.0175	0.0175	0.0175	0.00755	0.0175	0.0176	6,000	0 mss	0.0183	0,0241	0,0122	0.0201	0.0203	0,0199	0.0200	0.0200	0.0206	0.0186	0,0015	0.0177	O DESTA	0.01197	0.0198	0.0719	0.0210	0,0197	0.0270	0.0237	0.0023	0.0230	0.0000	0.0172	0.01772	0.0172	0.0219	0.0229	0.0232	00200	0.0218	O OTENS	0.0010	0.0077	0.0215	0.0217	0.0192	The second
Hr12	0,0157	0.00.75	0.0202	0.0196	0,000	0.0155	0.0153	0,0158	0.0153	0.0153	0.0152	0.0351	0.0157	0.0164	0.00235	6600'0	0.0386	0.0179	0.0188	0,0387	0.0184	0.0196	0.0173	0.0208	0.0164	00014	STATE	0.0134	90000	0.0262	0.0136	0.02215	0.0229	0.0259	0.0191	0.0013	0,0152	0.0152	0.0152	50200	0.0222	0.0222	0.0185	0000	0.000	0.0147	0.0154	0.0199	0,0205	0.0167	20000
Hr11	0.0205	0.0165	0.0215	0.0210	0.0167	0.0165	0.0165	0.0165	0.0116	91100	0.0165	0.0360	0.0178	0.0184	0.0240	0.0234	00100	0.0179	0.0136	0.0199	0.0194	0.0005	0.018d	0.0217	0.0175	00116	0.0136	0.0197	0.0212	0.0269	0.0198	17291	0.0227	0.0229	D0204	00000	29100	73100	0.0157	0.0210	0.0231	0.0239	G100	0.0217	0.0300	20000	99100	0.0205	0.0210	0.0134	40000
HHO	0.0234	0.0063	9000	0.0214	0.0161	0.0160	0.0360	09100	0.m59	6510.0	0910.0	0.0175	0.0174	0.0179	0.0238	9120/0	96100	0.0156	0.0201	0.0193	0.0195	0.0207	6,000	0.0278	0.0075	O MILE	04.100	0.0190	0.0711	0.0211	0.0190	0.0224	0.0236	0.0217	0.0202	0.000	0.0163	0.0063	0.0163	0.0212	0.0225	0.0224	0.0186	0,000	66700	0,000	0.0244	0.0200	0.0204	0.0175	20,000
Hr09	0.0224	- 00100	0.0233	0.0222	0.0171	0.0168	89100	0.0168	89100	0.0152	20100	Q03E7	0.0190	26100	0.0251	0.0227	0.0207	0.0190	90200	55100	90200	0.0214	0.0189	0.0223	00180	00110	91100	0.0197	0.0216	0.0216	0.0194	6:0234	0.0229	0.0221	90200	0.000	0.0178	82100	8/10/0	0.0215	0.0234	0.0223	20200	24700	dulb/	20000	0.0233	00200	0.0212	96100	A COUNTY I
Hr08	0.0234	0.0144	0.0221	00220	0.0164	0.01811	0.0183	0.0183	0.0183	0.0183	0.013.1	0.0203	0.0202	0.0208	0.0259	0.0238	0.0216	26100	0.0206	0.0203	00200	0.0212	9610'0	0.0221	66100	10000	00176	0.0100	0.0221	0.0215	16100	0.0228	0.0221	0.0228	0.0209	0.0000	0.0100	0.0185	0.0185	0.0216	0.0216	0.0225	56100	0.0210	0.0174	0.0001	0.0221	0.0202	0.0236	0.0211	A ARREST
Hr07	0.0240	0.0154	0.0237	0.0239	0.0000	0.0206	0.0206	0.0206	902010	90200	0.0206	0.0220	0.0200	0.0224	0.0278	0.0254	0.0233	0.0230	0.0230	0.0221	0.0224	0.0233	0.0215	0,0239	11200	24100	54100	16600	0.0236	0.0253	0.0216	20220	0.0239	0.0245	0.0236	15750	0.0210	0.020.0	0.0210	0.0238	0.0247	0.0346	90200	0,0242	0.0194	O CO THE	0.0252	0.0219	0.0248	0.0223	20000
90/H	60/23/0	0.0159	0.0236	0,000	0.0171	0.0165	0.0165	0,411.65	99100	99100	0,0165	0.0188	0.0185	0.0189	0,0217	0.0205	10000	2610.0	0.0198	0.0187	0.0192	0.0199	0.0181	0.0208	0.0174	0.00.00	04.000	0.0187	0.0201	0.6203	0.6187	0.520	0.0215	0.6213	0,0271	0.6014	0.68.75	0,0475	0.0175	30200	0.0233	61,000	0.01/16	0.0217	0,00,00	O COLOR	0.0172	9970.0	8223.0	0.0185	A 6000
Hr05	0.0173	0.0126	90200	00207	90100	0.0165	0.0165	0.0165	0.0165	59100	0.0165	28100	0.0185	0.0186	0.0207	00200	00501	95100	00130	68100	00192	00200	0.0189	00500	97700	00100	90100	0.0145	0.0301	0.0203	00187	50215	0.0217	0.0212	Holfs	0.0100	0.0174	0.0174	92100	0.0211	0.0257	0,0205	06100	16100	70700	0.000	00169	0.0169	0.0265	16100	10100
Hr04	0.0172	0.0113	0.0216	0.0213	00100	69100	66100	8,0169	60100	69100	0,0169	88100	82100	0.0138	0.0200	96100	66100	0.0151	3,0198	06100	60100	36100	0.0181	0.0213	4100	00000	2000	00134	2610.0	0.0204	06100	0.0216	0,0217	00000	GUIES	00170	0.0176	9/10/0	92100	0.0216	00100	00000	96100	0,0200	90700	00000	actes.	0.0172	00100	56100	Apriles 1
Hr03	0.0176	4	0.0220	0.0222	0.0172	0.0169	0.0169	0,0169	99100	0.0199	0,0169	0.0184	H		0.0207	0.0200	-	-	0,0191	0,0187	0.0198	96100	0,0187	0.0015	0.0176	D Grand	0.0129	OUM	0.0302	0,0280	0,0185	0.0217	0.0214	0.0210	0,0072	0.6040	0.0177	0,0077	2,710.0	0.0309	0.0257	0.0222	COLOR	0.0217	0.0211	2000	+	Н	0.0265	4	ŀ
Н	+	+	+	0.0210	+	٠	۰	0.0165	Н	Н	Н	Н	Н	Н	0.0212	-	0.0199	-	-	-	+	2610.0	+	+	0.0000	+	+	+	٠	Н		5.0217	+	+	Digital	+	0.0174	Н	0.0174	Н	+	+	+	0.0209	+	50000	+		Н	0.0187	۲
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Y2	823675.22	621697.57	821878.23	82186138	\$25EF8.77	821586.00	07107232	82187128	821812.08	821889.75	82385C48	921287.94	14,582.91	821821.12	151765.91	521687.58	821813.13	8771178	#31444 66	621603.87	25 525 120	62355128	621512.65	85128328	141300170	40,000,000	821865.61	821841.09	\$21786.67	821657.75	821605.82	821511.11	821886.87	821882.03	621828.25	821766.33	\$21725.47	621453.37	821854.44	821508.87	821634.13	921640,31	821899.24	821575.41	\$21548.43	622414.27	11725223	822256.35	822180.58	472464.14	822287.63	622212.23	822439.AE	822069.94	82202883	\$22360.57	62227135	62320123	8221228	\$22115.02	822037.73	621365.98	82300CAS	821896.55	86.815228	822222.16	82215155	N22284.07	622172.88	822174.73	822278.48	122221.21	822293.72	822178.17	\$22000.7S	122007.87	62136276	82388238	822178.97	\$22120.84	822125.44	822052.07	A51677.94	821277.38
X2	93536724	83360178	833397.24	833506.97	833548.68	833603.43	83368492	83260048	83367384	83387532	833867.51	33299954	80736708	833810.75	83151639	83367013	133498.18	03301420	********	633667.71	83364024	933581.67	83377052	832607.88	033040.03	20100000	133416.65	835467.53	83352363	933574.30	833600.16	83371268	83137008	633427.36	833489,60	93352246	833542.19	933593.07	83388888	83386893	831317.54	133449.54	892513558	83334151	933648.49	53401877	834127.62	83421631	83436568	41100110	834494.39	834161.93	134273.05	834384.38	63640974	831002.96	833308.65	833964.47	834077.01	834097.30	824190159	83424325	83428216	554368-17	633769.11	83386878	833964.75	93269488	833827.77	83364833	833563.51	82362435	633306.00	931398.77	933454.10	833460.81	833481.00	833505.57	801212108	63325339	63310003	82323558	411166.66	STATE OF
۲.	621053.25	821875.22	821880.54	821861.09	621697.80	821899.77	651086.09	82188428	121171.28	821822.35	821311.43	\$21861.13	821650.88	621664.41	821821.12	821785.93	821055.11	21,010,12	201687.03	821644.68	821605.84	821575.52	821545.20	821548.69	20120120		821856.64	621665.51	821561.09	821786.07	821657.76	\$21605.82	821401.44	821646.87	821952.03	821629.25	821786.30	821725.47	821563.37	821594.44	821829.64	821632.03	821640.31	821634.13	821501.72	822454.38	522414.27	82232211	622258.30	892444 41	822378.04	822238.08	22,212,32	622136.63	98 650228	822405.79	11333517	822771.35	822209.75	822131.94	822115.02	822037.75	821993.85	821961.17	822374:18	622311.12	#12222#	822341.72	822284.07	0015778	822215.75	822278.46	822233,03	822232.03	822175.04	822080.70	822007.00	621952.76	822233.78	822178.06	822182.63	622/23/44	*******	Silvery and a
X1	633327.51	833397.24	833451.80	633449.48	83350 C.48.	E33548.00	633663.43	633653.67	N33600.48	633682.38	82.673.23	833875.67	1073867.01	633458.18	61353676	£13536.39	833436.83	23494.10	27167 64	633582.09	633609.34	633640.24	19:189009	833555.79	87700788	010100	E3356.60	633416.50	£3,582,618	833533.63	833574.80	813690.16	28.32513	833370.08	833427.36	633480.60	£13522.48	833543,19	E33562.07	83358.98	27.525.72	833337.92	833449.06	633337.64	613 609 59	8325960.68	#34628,T7	634127.62	E34218.31	634309.00	SET SEE SE	834090.84	B34101.BE	834273.34	634363.46	813548.7E	833633.16	833309.65	30.366.03	834075.90	834097,30	834190.59	£34242.94	834251.93	833768.03	833761,96	87,848,018	833K73.82	833694.84	633653.46	23,493,65	13563.61	833377,80	633377.60	E33598.42	\$13433.02	833460.45	633483.05	E13209.07	E33232.03	193060.01	53,001,03	#12451 GR	White and
Pair	R571	Rett	HOT3	R076	RoTé	R074	M676	8,077	R077	B1578	B-07-9	ROBO	R081	R082	1000	BOK 5	HOB3	HODE	ROBA	ROBA	ROSS	ROSS	RORS.	R086	1000	1	8.088	Ross	Roke	ROSS	ROBE	ROSS	9,000	ROB9	R089	ROSS	Ribes	Ross	8003	RORS	1600-0600	R093+6903	E92+R493	B254	ROSE	0094-R007	5050×W050	1100-R101	MG2+R103	BINA BINA	R107	Ritte	R109	R110	BILL	Rett2	Rtt2	RITA	RICE	RTIG	RHIT	RITE	8168	R120	R121	R122	R123	RYZ4	R128	RIZE	8127	R128	R129	R13G	Rede	R132	R133	RESA	RESS	R126	R137	RESE	2000	-

0/10/0	0.0142	891010	19100	0.0163	62100	0.0172	TATOO	69100	09100	44100	#S10'0	6910.0	19100	1810.0	HETOD	0.0204	OCTO O	92700	8/100	0.0174	0.01772	0/100	0.010
Z10'0	C00743	8M10.0	19100	£9100	FR10.0	0.0172	11100	69100	0.0160	0.0177	65100	0.0163	- gratet	THIOD	16100	0.0204	04100	92100	8/100	6710.0	0.0172	0710.0	GX10.0
4100	Z910'0	2910'0	(910.0	22100	0.0123	6/10:0	04100	69100	19100	0.020.0	0.01299	1910.0	8810 0	DIZUO	0.0217	Z170'0	0.0210	0.0244	99100	MASO.0 -	5777/0	0.0214	90000
1510 a	2520'0	0.020.0	0.0214	ETZUO	92200	MIDEO O	F6100	0.0201	1610.0	8610.0	ESTOR	enton	#810°0	0.0164	swtora	6050.0	ESTO U	95100	95100	#St0 U	7210.0	tstoo	95100
D.0138	C#10'0	15100	0.0160	65100	S2100	ZSLOTE	551000	95T0'0	D.0149	£910'0	0,0142	PSTOO	A4440.0	51700	60200	0.0230	8210.0	95100	951070	9510'0	0.0152	0.0158	9510'0
8056.0	7520.0	8710.0	5810 0	Z810'0	36100	5610.0	96100	Teton	9510.0	6610.0	1810.0	60100	9810'0	05100	50200	0.0205	£619'0	COTES	891010	\$810°0	8810.0	1610.0	£610.0
0.0216	5050/0	9,0504	6,020.0	605010	4120.0	0.0210	0.0204	50200	1020.0	6050.0	0.0201	E120.0	91700	91200	21200	0.0217	1023.0	ETZOD	80200	£120.0	0.0208	E020.0	6610 0
E910.0	9910'0	1910 C	10.018M	00100	23100	PF10'0	ostoo	45100	CM10.0	4510'0	11100	15100	49100	V\$100	6510.0	9610'0	4510.0	3810.0	06100	0.0194	MKTO.O	0.015.0	E4100
ABICO .	6710.0	EZTOD	0.0183	9810.0	60200	161010	E8100	0.0192	Z610'0	102010	0.0188	0.0200	2610.0	20200	66100	0.0221	0.0199	Large	2610.0	002010	26100	0.0202	96100
EBICO	Z510'0	0910.0	6910.0	14100	667300	DATEO.0	69100	9/100	2270'0	1-810.0	ILIOO	92100	1710.0	98100	6/10/0	1610.0	TATO 0	52100	0810/0	6710.0	7810,0	94100	1910 0
21200	\$610.0	9020'0	6540 0	0.0204	82200	0.0213	0.0204	0.0213	0.0211	\$150.0	50700	0.0211	90600	90200	0.0207	9220.0	0.020.0	SHIGO	06100	0.0394	6610.0	EBTO.0	8610.0
51200	2610.0	SKIGC	\$610.0	6810.0	10500	2810.0	5410'0	#R10.0	0.010.0	1150.0	0.0204	0.0213	0.0207	90200	66100	9550.0	9020 0	9650.0	95100	9670'0	0.0228	0.0230	20203
66100	#810.0	SITOC	2810.0	281UO	232.00	1020.0	LSTOO	96TU 0	2610.0	20200	68100	16100	961010	86TU 0	66100	0.0214	6810°0	\$6100	66100	0.0192	7810.0	Z610'B	98300
61100	STT0.0	5110.0	0.013A	96100	39100	72£0.0	05100	15100	8410.0	8510'0	09100	1210.0	05100	19100	0/100	2610.0	1919.0	09100	THION	£910.0	0.0160	2910.0	19100
6100			AE10.0		50100	7210.0	05100		SALO.0	A. P. C. P.	00100		05100		02100		1919 0		19100	5910.0	09100	Z9100	1910.0
	8110,0	5110.0		9610.0				TSTOO		8510.0		12(0.0		19100		5610.0		09700					
E#100	ELTO.0	TITO'C	\$£10.0	99100	89100	Z\$10 0	05100	15100	8410.0	8510.0	00.0140	E210.0	05100	19100	0710.0	2610'0	1910.0	oston	19100	\$9to 0	09100	5910.0	1910 0
0.0210	06100	BALLOC	1/5/10/0	28100	66100	D.OTAL	14100	19100	6,0177	9020'0	96100	0.0202	9610.0	16100	16100	9150.0	7910.0	95100	25100	12200	0.0210	66100	2510'0
Z810 û	99100	7910.0	0.0185	28100	0.0199	ESTO D	5520.0	0.0187	E810.0	0.0192	62100	M10.0	#810 G	9810.0	82100	0.0213	7810.0	12100	15100	0.020.0	7910.0	28100	2810.0
66100	5530.0	ORIO.C	meto p	9610.0	Etzon	1610.0	0.0188	60203	MOS0.0	0.6211	9/10.0	ME(0.0	9810.0	68100	16100	9150.0	2510.0	05100	5220.0	\$5T0.0	9510'0	\$210.0	9510'0
SSIDO	6810.0	PKIO,C	0610.0	0.0191	0.0216	N610.0	06100	6610/0	6610.0	90000	£610.0	0.0202	0,000	0.0204	60200	5220.0	\$610.0	5610.0	06100	ERID D	SGTO'O	ESIGD	2610.0
0.0211	T050.0	8050.0	7610.0	90000	92200	0.0208	0.020.0	0.0215	0.0214	TISD.0	0.0210	6050.0	0.0208	11200	0.0203	.6150.0	8610 0	66100	0.0200	16000	9610.0	66100	657010
1610.0	3810.0	7810.0	1610.0	98100	10200	9810.0	18100	\$6T00	0.0395	0.0202	3610'D	EDGOLD	10000	51700	0.0210	0.0221	0.0202	86100	66100	0.0233.0	0,0200	66100	2020.0
9/10/0	\$9100	2010.C	9910.0	0.0172	15100	0.0181	1710.0	8210.0	5510.0	0.0182	1410.0	R/100	2510.0	8710.0	62700	\$6£0.0	E710.0	22100	2100	1410.0	0.0134	EVIO.0	9510.0
WS10'0	08100	6/10 C	6/10/0	48t00	10200	NSto.o	tstoo	0610'0	0610.0	0.0194	9810.0	Feto.o	7610 O	86100	16100	0.0213	TB10.0	1810.0	82100	\$810.0	9810.0	98100	8850.0
1810.0	54100	2/10.0	8/10/0	2810.0	0.0209	2610.0	9810.0	\$610.0	EGTO 0	1059.0	9810.0	2610.0	7610.0	66100	0.0204	9170.0	DELLA	SELOG	W100	98100	1810.0	ESIGO	1810.0
0.0172	6210.0	6510.0	ESTOD	0.0171	16100	PC10.0	11100	11100	5210.0	0.0182	04100	22,000	57,10.0	18100	12100	5050.0	2710.0	02100	0/100	6,0172	1710.0	12100	1410.0
ELITO	erro.0	5Z10'C	atton	2110.0	IXIOD	#110.0	PI100	12100	0.0120	0.0126	SELLO	0.0124	65300	82100	SILIGO	ESTO.0	8110.0	21100	0.0116	0.0120	SILOO	9110.0	3110.0
10100	TB00,0	SMOQ.C	9600 0	2600'D	50100	OUTOO	cotoo	90100	\$010.0	SOLO.D	Colog	90100	90100	SOTO	FILTRO	TII0.0	ZOTO O	00100	20100	0.0100	Sataro	1010.0	00100
0.0226	0.0233	9EZ0 0	8150.0	0.0221	0.0248	8220.0	0.0232	9970'0	1520 a	6240.0	9970'0	PSZ0.0.	4700.0	7750.0	15000	0.0267	617010	ESCOR	0.0251	1520 0	0.0252	0.0251	6950.0
ISIO'O	2510.0	8110.0	PE TO U	\$\$100	14100	1910'0	85100	19100	£510/0	6,0163	15100	zertoro	19100	593070	THICG	0.0193	09100	19100	E310.0	Z9300	19100	09100	7910 0
1810.0	0.0172	1/10.C	E410.0	66100	0.0200	9810.0	08100	16100	1610.0	6610.0	16100	86100	0.6200	507070	0.0203	0.0219	Z610'0	16100	9610/0	8510/0	1610'0	5610'0	£610.0
19100	69100	6010 C	951010	estoro	5/100	19100	25100	19100	1910.0	1710.0	6510'0	@10°0	59100	PZ10'0	0.0180	9610'0	2910-0	1/100	99100	22100	3910.0	69100	02100
14100	Z510'0	6510 E	2910/0	£9100	MILOD	0.0174	69100	19100	6/10/0	6810/0	0.0180	O O THE	16100	96100	16100	0.0212	ESTOO	SETGO	0.0182	0.0183	S S S S S S S S S S S S S S S S S S S	ESTOO	E810.0
BOTO	05100	9510'0	9510.0	65100	08000	6.0169	0.0165	2710.0	1710.0	£81D.0	6910'0	6/T00	0.0180	68100	8810.0	5020.0	££10.0	1710.0	18100	0.0182	12100	08100	84700
WZ1070	6910'0	E910.0	1410.0	£410'0	group.	\$500 O	0.0174	6210'0	1710.0	\$800	2410.0	12100	42100	62100	zatoo	0.0202	EZ10'0	1/100	99100	2410.0	89100	69100	04100
R910'0	6510'0	9510.0	8510.0	99t00	1310.0	1/10.0	ESTOO	1/10.0	1/10.0	ESID.O	£4100	DOTAL	4810.0	06100	боли	0150.0	0.0182	8/100	2810.0	9/10/0	6.0184	98100	52100
00100	6910'0	29TO T	0.0165	94100	16100	ESTO 0	5910'0	DOUBLE	DELOG	6810.0	0.0165	5/100	2710.0	5210'0	94100	0.0201	22100	29100	0.010.0	9610 0	76100	IRIO.0	52100
6910'0	05100	6410,E	1910.0	0/10/0	0.01299	7710.0	2110.0	94.00.0	5210.0	2810.0	52100	1610.0	1810/0	1610.0	36100	5150.0	SETO'O	sitoo	£8100	S#10'0	Ento.o	E810.0	1810.0
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9/100	9510'0	95100	52100	63100	0.0215	0.0209	0.0202	90200	0.0206	2550.0	407070	0.0221	6110.0	00231	9E200	0,0255	0.020.0	06100	0.0135	0610'0	56100	1610.0	50000
15100	PETO'O	1610,E	0510/0	25100	6/100	9910'0		90100	1910/0	69100				44100	16100	90200		14100	0.0173	0410'0	89100	59100	2410'0
15100	1510.0	8210.0	0.0144	25100	62100	2010.0	95100	29100	B210.0	1710.0	5510'0	0.0160	99TD 0	94100		1050.0	£710.0	12100	ET10.0	0.0170	6,0167	59100	1510.0
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28 27 28 28 28 28 28 28 28 28		4 1	10	=	2	1	1.6	2 5	2	П	2 5	П	0 1	10	10	2 2	10	z	2	10	14	2	2 2	12	13	П	2	2	9	П	=	97	14		2			2	17	53.	10	91	2 2	4	20	2	2	61		10	1	9	2 2	*		Ш	2 1	Т	١	
1.2 1.22346.74 6.22346.74 1.622342.09	6 822546.74 5 622346.62	822421.56	8 822406.53	1 822626.09	6 822429.54	F \$22464.47	1 822441.55	3 822458.02 8 822367.16	5 \$22468.34	4 622432.68	# 822462.AB	8 S255502	023462.07	1 122300.41	8 \$22364.59	4 42254 65	7 822388.31	7 622236.78	62229377	\$ \$22316.75	B ATSTRAN	622578.07	8222228	2 622341.72	1 622276.03	8 N22405.79	022464.38	8 822072.05	9 822128 94	5 622221.21	0 622209.00	8 822264.07	422339.74	6 62233 17	1 622320.45	0 62229 41	1 822006.45	3 622511.22	6 621977.96	82308678	0 422007.07	3 822:04.73	6 82215433 1 62217473	1 622127.03	8 822346.43 8 822362.83	6 622166.92	9 8221133	4 822081.39	\$1.60028 0	821738.42	4 \$21880.22 1 \$21727.45	12188631	82230738 1 82230757	I SEDERRE	0 621163.31	421891.67	62196276	82194339		
XZ 131 8315773 131 833494 141 833494	10 933165.0	41 633455.7	56 8336757	ALTHUR 30	09 834546.1	21 8337129	47 8337924	31 033840.5	16 8328418	30 133896	AC STREET	47 833421.5	0314180	38 833544.6.	48 833587.5	ASSESSED AND ADDRESS OF	91 833861.1	43 833298.0	10 0113064	12 8334896	A41.131.104.5	44 133277.0	01 0116013	46 833873.k.	72 633746.1	A13 833846.7	11 83388654	71 833411.7	07 8332533	17 833834.30	21 833652-4	00 833884.8	17 K13758.A	16 8338331	57 0328604	48 834034.9	67 B34231.2	48 6542212	42 835556	99 533434.5	00 6034367	23 855888.3	25 8334883	24 1335617	4C 033043.6L	65 633713.8	36 035775.4	04 8338721	M 134192	78 834255.1	22 634341.8	28 8334187	50 833-665 50 833-666.5	OR RESERVE	12 1335037	07 9353(88	AT 833481.0	16 9335361		The second second
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21 CON 10	C4 (23)11	04 83342	46. 6335	05 83165	900 8338	- Hight Exten	ROOT 8337.	AGES COM	Water etsen	- Hatt B319	BEETS STORY	ROLL EDDIN	H012 8334	Rett state	Rets 8335	HOTE SAME	REAT 63363	10 8230	11 6533	T EDS.	A 8330	100	6232	7 83350	8 6336	6 6337.	1 83161	1021	1 6331	4 63334	6 63363	7 6138.	8 83378	0 8337	2 62360	9 8334	2 6347	6 6142	# 83308	9 6331	11 83337	5334	E 81372	1034	10 61364	4 8338	4 61375	6157	T SADE	1 6341	10 E34 O	1 833 1	2 603	4 833.6	4 8335	4131	6113	1 633 1		

Hr17 Hr18 1700 1650 900 900 500 740 1474 Hr15 H 1550 3400 1456 1 600 700 700 700 700 750 800 600 | March | Marc | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1500 | 1770
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 <th 100 Road Type (caline 8) Heaght
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Road		Coordi	rate (m)		including	Height	Road Typ
Pair	X1	Y1	X2	¥2	mixton rope)	(m)	(calline 4)
RSAT	B33254.35	821947.25	.885315.56	821691.57	13	0	1
R162	E33329,69	821353.87	\$10315.94	621691.04	13	0	7
R163	\$33129.75	621689.31	#33160.67	#21#34.07	- 13	0	- 1
R164 -	833,160,17	62183A.07	#33,878.74	821783.18	13	0	1
RIES-RINE	823817.49	621976.5%	\$349458	621516.03	- 32	0	1
2147+B140	E23734-66	#21886:3K	SERVICES	821727.34	16	0	-1
R146	833728.61	921749:AZ	612007.73	821694.38	14	- 00	- A
R149-	E33774,00	621643,62	032507.73	021604.30	13	0	1
R110	833755.67	#21784-25	853697.71	821603.81		0.	- 1
R151	833612.61	821610.98	833663.50	821863.70	13	0	4.
R151	WINDOWS WO	821543.70	#3377628	#21842.83.	14	0	- 1
WIR2	\$35774.08	621843.52	\$1180£17	821500.58	- 28		. 1
R193	823991.31	622389.76	634G/8.77	622454.27	78.	0	1
R194	\$33950.66	222530-65	#EXWZ.00	#22189.07	18		1
8100	£33'909.60	122271.36	X33000.66	932130.45	18	0	1
#186	813688.78	622222.16	#11M09/85	01111130	18		- 1
B197	R33866.58	622722.34	6550777	622172.98	98	0	
P155	833827.77	822172.95	#1577E49	\$22113.30	18	0	
HITT	634070.01	622299.62	ESANIERO	617384.34	18.	0	1
RIES	834090.38	622287 53	13417767	622332.11	15	٥	- 1
891	834014 NO	#22250.52	834075.61	822209.62	15	0	- 1
R162	634049.42	822228.28	234800.19	822287.53	15	0	1
#163	E33993.00	62220188	#34534:00	032250.01	- 0.	0	- 1
R164	834007.86	622194-31	#34949AT	025EM:20	15		1
RIES	#33953.31	622353.75	#259/A47	62272123	16	0	- 1
R150	833872.14	822651.39	88191476	822190.52	18	0	1
H167	633,683,47	822042.45	E34007.E8	822189.33	18	0	1
R163+R169	833813.72	821 87 E 47	EDWEN	027050.03	21	. 0	1
R179-9171	E33716.44	821 FR 8 15	8.21812.49	AZINTRAD	18	0	1
R172+R173	833864.92	821823.12	811719.26	821487.65	26	. 0	1
RETAKRETS.	#33061,78	621407.56	£13M3.38	821623.98	16	0	1
804	E33496.77	f21508.49	#11560.47	621680.73	20	0	-
R177	E335(3.09	821599.24	SPAN	621688.A7	29	0	1
RITE	R33440.44	621529.99	EXTRES	621608.61	16	0	7
9179	X23451.04	621629.31	#10411.33	821608.81	12	0	1
9160		621029.31 622286.16	#30511.33 #34375.98	-		0	_
	E34218.31	40,000.00	***	621585.39	18	-	1
R191	E2A181.98	422312.ZZ	#34Z1831	622258-36	-18	0	1
R182	13A140-62	822162.47	834191.76	027212.3#	16	0	1
W-182	#34099.34	622113.33	E34440/62	622162.67	18	-0-	1
R194	E34077.01	622152.66	#54051.51	622180.94	15	0	- 1
R164	SMOKE ST	E22100.94	E3407130	822094.18	13	0	- 1
H184	£34071.00	07208 s. 18	834007.30	822115.02	14	0	- 1
RIES	634369-95	\$22180.68	13131244	833167.44	10	0	, ,
8196	E3#221.54	62236 à 63	EM27134	622136.83	19	0	- 1
RIST	83A190.59	822037.73	83423176	622086.A5	- 9	0	- 1
R155+R157	834004.93	#21315-C3	834965.24	821600.22	16	0	- 1
R190+R191	823921,12	921727,74	834004.08	621814.03	19	0	1
#192+R(8)	633878.32	621460.75	A\$2830.60	621727.50	29	0	1
R194-R195	833825,79	621600.86	613867.51	621631.AB	20	0	4
R195+R292	8337E4.01	#21523.1E	#11816.17	821690.58	20	0	,
R197	634364.00	822040.04	E3440E18	82210431	- 11	0	1
RISE	834323.77	822010.68	SHM436	822060.94	18		- 1
R199	139/20193	421561.17	EJANIZACO	822010:AB	-38	0	- 1
R300	634239.47	#21914.12	834210.06	821983:18	44	0	1

										Vet	nicle count	for each	road										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	13	9	6	7	10	50	50	100	100	180	150	150	150	200	200	150	250	300	250	150	150	100	100
50	19	12		10	14	-50	50	150	150	150	150	150	150	200	200	150	200	100	150	100	100	100	50
100	50	50	50	50	50	100	250	450	500	450	400	400	400	450	400	300	400	450	300	500	200	150	130
100	50	50	25	50	50	100	200	400	450	400	350	350	350	150	350	250	150	350	250	200	150	150	100
21	12	7:	4	5	- 8	. 22	60	72	73	70	69	119	118	120	139	115	169	220	166	111	109	58	57
29	16	10	7	7	12	n	63	150	150	150	150	150	100	150	100	100	100	150	100	100	100	100	71
14	- 6	5	4	.4.	5	15	50	50	50	50	50	-50	90	50	50	29	50	- 23	19	13	10	10	1 2
14	8	5	4	4	5	15	'50	50	50	50	50	50	50	50	50	2.5	50	23	19	13	10	10	7
34		- 5	4	- 4	- 5	15	50	50	50	50	50	50	50	50	50	- 3	50	23	.19	13	16	10	7
14	8	- 5	4	4	3	14	50	50	50	50	50	50	50	50	50	23	- 50	24	19	13	11	10	
14	- 8	- 5	4	A	- 3	14	50	50	50	50	50	50	50	50	50	23	50	24	19	13	- 11	10	- 8
14		5.	4	.4.	5	15	.50	50	50	50	50	50	50	50	50	- 50	50	50	24	D.	14	13	10
100	100	50	50	50	50	100	200	250	200	200	200	200	200	200	200	200	200	156	150	150	100	100	100
100	100	50	50	50	50	100	200	250	250	200	200	250	250	250	250	300	300	300	250	200	200	150	150
100	100	50	50	50	50	100	200	250	200	200	200	200	200	200	200	200	200	200	150	150	100	100	100
450	350	300	250	700	250	400	1100	800	800	800	800	800	100	750	700	700	700	650	550	450	-400	400	300
500	400	350	300	250	250	450	1050	1300	1100	1050	950	950	1000	950	900	950	900	906	750	650	550	300	400
450	350	300	250	200	250	400	900	1100	950	900	850	850	900	650	800	BSO	850	850	700	600	500	500	000
-23	19	15.	14	10	12	22	50	50	50	50	50	50	50	50	50	50	100	30	50	50	50	50	30
100	50	50	50	50	50	100	200	250	200	200	150	150	150	150	150	150	150	150	100	100	100	100	50
150	100	100	100	50	50	150	300	350	360	300	300	300	300	300	300	350	350	356	300	250	200	200	150
200	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	350	300	250	250	700	150
200	150	150	100	100	100	200	400	500	450	450	450	450	500	500	500	550	600	600	500	400	350	150	250
150	100	100	100	50	100	150	300	400	350	300	300	300	350	300	300	350	350	350	300	250	200	200	130
150	100	100	100	50	100	150	300	400	350	300	300	300	350	350	350	350	400	350	300	250	250	200	150
300	250	200	150	150	150	250	600	750	650	600	600	600	650	650	650	700	700	700	550	500	450	400	300
750	700	150	150	100	100	200	450	600	500	500	450	500	550	500	500	550	550	550	450	400	350	350	230
400	150	300	200	200	200	350	H50	1050	950	900	900	900	1090	1050	1050	1150	1250	1150	950	850	750	700	550
350	300	250	200	150	200	350	750	950	900	800	800	900	950	900	1000	1050	1150	1100	900	800	700	650	450
450	350	250	250	200	250	400	850	1100	1000	950	900	950	1050	1050	1050	1100	1200	1100	950	800	700	700	550
450	390	300	250	200	250	450	900	1150	1000	950	950	950	1050	1000	1000	1090	1100	1300	900	750	650	930	500
300	250	200	150	150	150	300	650	800	700	650	600	600	600	600	550	600	600	550	450	400	350	350	250
250	200	150	150	100	100	200	500	600	550	580	500	500	550	550	550	600	650	600	500	458	350	350	250
300	750	200	150	150	150	250	600	750	650	600	600	600	600	600	550	1900	600	550	450	400	350	3500	250
300	250	200	150	150	150	250	600	750	650	600	600	650	700	700	700	750	800	800	650	550	500	490	150
150	150	100	100	100	100	150	350	450	350	350	300	350	350	150	300	350	150	350	300	250	200	200	150
12	9	8	7	- 5	6	-11	50	150	50	50	-50	50	50	50	50	50	50	50	50	50	50	50	20
50	24	19	17	13	14	50	50	100	50	50	50	50	90	50	50	50	50	50	50	50	50	50	50
24	20	16	19	11	12	- 72	50	50	50	50	50	50	50	50	50	50	50	50	50	24	21	20	16
50	21	16	34	12	13	- 12	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	21	16	14	12	13	22	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
103	50	50	50	50	30	100	150	200	200	200	200	200	200	200	200	200	250	200	200	150	150	150	100
19	16	12	35	8	11.	17	50	50	50	50	50	50	50	50	50	50	50	50	50	22	19	18	14
100	50	50	- 50	50	50	100	150	200	200	150	150	150	150	150	150	150	150	150	100	100	100	100	50
64	62	59	58	57	58	- 63	150	70G	200	150	150	200	200	200	200	290	200	200	200	150	150	150	119
71	68	64	62	29	33	60	150	150	150	150	150	200	200	200	200	250	250	250	200	200	150	150	119
36	79	25	22	17	19	32	100	100	100	75	73	73	73	70	70	62	65	65	64	64	51	64	75
60	-59	57	55	55	35	39	173	200	171	171	119	117	117	116	114	314	112	112	1.00	58	57	51	55
100	100	44	38	- 31	35	100	150	200	150	100	100	100	100	100	100	100	100	100	100	100	100	100	71
5	7	5	A	4	4	7	17	21	17	14	12	11	I)	9	7	7	4	4.	4	3	3.	3	1
16	13	11	- 1	2	8	114	50	50	90	50	50	50	50	22	19	18	15	15.	13	11	10	9	- 6
20	17	14	- 11	8	10	19	50	50	50	50	50	50	50	50	50	21	20	19	17	13	11	n	3
50	25	20	17	15	16	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	50	90
50	25	20	17	15	16	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50

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Width	(Including	mixing robel	20	20	20	26	63				=		**	. 72									10	100	100	10	**	*	31	48	91	91	1.6	14	**	**	- 44	13	43	0	,												18	18	18	. 63	18	18	17	91			31	118	44	18	93	18	10	91		16	10	13	. 0	16	16	. 91	1.6	118	18	. 61	118	91	*		- 52	11
2034 Q4	64		82234678	822409.45	622543.00	82254£7E	822316.62	157380.41	200,400,600	#22654.64	822436.04	822626.S4	822455.21	493,464,49	833444 66	873464.07	277 107 44	47544674	822417.88		477.454.07	40,000,00	623463.07	822424 33	\$22380.AS	635164.65	822384 65	875854 84	822308.34	83221678	822203.73	822346.13	\$2231£7E	822125.44	822178.07	8222558	822278.92	622344 72	822296.83	82240578	27 14754		822072.07	200000000000000000000000000000000000000		822175.17	822221.21	00'697778	***********	STATE OF THE	433444	822368.57	822330.45	822250.62	1972115287	A22086.AS	\$22011.22	621969.66	821877.95	922080.76	822007.07	8724744	82236328	622174.73	822422.03	822344.43	822162.85	522149.52	822138.55	822113.33	822086.33	822039.(2	621814.78	#21738.42	82188122	821727.AS	10,488128	821847.78	122007.97	#22038.72	621163.31	821863.31	821801.67	821862.74	821763.88	821812.88	401704.01	121812.67
	(m) are	93547737	833231.06	833434.80	833960.46	83398546	8331125.93	033425.15	4016166	43341347	833973.74	83404615	833827.55	811211587	*********	BYTHREET	911001100	****	17189464		BILLBACK	27,444	43341669	031547752	83354464	47169764	13 627 64	*******	411044 47	RATIOGRAF	63338666	835415.61	83348948	833100.53	833252.06	833.977.80	83356334	63367382	83374811	83384678	41101741		83389478	2000000	40000000	933396.77	833624.35	033003.40	0000000	NAME AND ADDRESS OF	***************************************	91190236	83395646	834034.80	834540.82	83423478	83432121	134394.01	933158.50	633404.10	933274.46	41168411	83377868	83366833	13355271	033649.55	831663.68	83371385	633767.83	835778.48	81187214	833867.20	93410921	834255.10	83406834	034241.81	633139.76	93328678	93346651	83354373	931543.70	633563.70	83231556	83348100	933178.47	83125768	*****	*******
input for	500	822324.11	822330.25	822345.74	622408.45	822543.00	622308.10	822319.62	1000000	27,464.53	B37614.6K	822628.09	822418.61	839464.34	27.454.47	ET1441 AA	PATRICIA NA	833367 48	872463.30		20, 12, 61, 62		RT1664.03	622482.00	82242X38	823356448	413314	A 2714 CA BA	877774.04	823462 83	871118 78	\$7.283.72	822345.13	822119.68	122129.64	822178.07	82225203	822278 48	ST3M172	822376.15	497.464.74		ATTINGE TI	********	2007000	221220	822175.17	17.17.17.1			******	82233.47	822360.57	822320.48	822250.52	\$22.62.57	822081.85	822010.68	671955.43	821977.96	62186233	#25088.31	822 (23.88	82216126	827067.29	82212203	822144.00	622152.80	822148.62	622128.55	822123.04	822113.30	822062,66	621814.78	822039.23	821889.22	821689.28	621889.31	821947.50	\$22008.03	822028.73	621952.62	821834.07	821691.68	821775.07	621783.15	434747.67	821826.73
4	**	633125.78	127171258	833231.06	833434.89	633360.46	E23118.28	633185.93	51354 B 19	etsers re	R31633.67	633973.74	833827.00	******	10 414418	611782 11	41104147	211691.65	#1167£ +&		ETTERT GA	201100	635425.86	613414.00	E13.447.62	277444.64	133488.TP	20,000,00	61361147	#110k2 47	R13308.67	633355.00	REDARDS OF	833073.42	833100.63	E13232.06	E13377.60	E35663.61	635673.62	83378.8.65			811074.00	200000000000000000000000000000000000000	200,000	1000000	833298.77	673074.33		******	*********	KD303.16	E13502.96	833.950.40	634034.90	\$34141 £7	834231.72	834322.77	633097.20	613156.56	410,000	RATE OF THE PARTY OF	613738.86	833734.06	#33438 #3	633586.71	25.649.55	833683.68	833713.66	E33757.83	613734.63	833778.89	833873,29	634155.21	et1887.79	E340963	83311E.37	833139.75	20.255.66	49.099.03	833543,73	633.480.98	77.081.013	833315.00	833184.01	£3178.74	*****	833249.00
Caline	Pair	R003	R1003	R003	R003	R003	R004	N004	Brees	8000	Roof	MEGS	Rotte-Rott	Debod-subbry	Send & Prior	SERVICE STATE	District Bridge	Bitting a state	E SOLO-SECTOR	-	Dernambet	Division in the latest	Edd 2+ Rott3	8012+B013	Ratz-mact	ant3-Ratt	ROLL	Diffe & Gifter	Dark. Dar	Abre	8.624	Rezz	R422	R023	R024	REZE	neze	Regr	8028	B-0.5	Band	1	SM17+RID1	- Carlotte	1	west.	MODE	8000	1	2000	2000	mos.	N042	N943	ROAA	BS45	Note	F847	HOAR	BOAS	mose	BOAT	REKS	R083	A 200 M	FI054	11054	NO84	8.064	R054	BOCK	ROBE	H057	Resa	9000	NONO	1001	ROSZ	RDES	HIN4	#100 W	H054	RORS	ROBG	H007	BOKe	RONG	MOTO

Note Column Col		9510'0	15100	4910.0	S210'0	0.0202	0.0185	ZZ10'0	\$610.0	£6£0.0	2050.0	6610.0	0.0200	0.0211	0.0220	1150.0	0.0242	0.0210	8020.0	5150.0	£520.0	0.0212	7150.0	212
																								851
1																								691
																								591
								49.54.4														4,0,04		
Column C		2010.0						20100			2022			20.00				70.00						192
																								581
																								951
1																								531
																								721
1		71700			23100					2000				4414			3415		45.14.5	2010	2012		100.00	851
10																								921
1																								180
19						77.00																		922
Column C															7.44	1,000								181
Fig. Cont.																								161
10							DELO.O.		0/10/0				09100									2910/0		291
Color Colo																								561
18																								8/1
150		8020'0		Z020'0	0.0214		8120.0			N120.0	4110.0	9070'0		4070'0	1120.0	0.0214	£520.0	8610.0	86100		10000		4610.0	961
1899																								461
Color Colo																								661
18																								002
1989 1989														2040.0										261
Column C																								152
1985 1985																								900
Color		4144	2109.0														2000				2242.2	40.00		081
The column The																								TSI
Color Colo				0.000 0	7020										10000	34400								213
No. Control																							6150.0	900
6703 (1972) (1973) (1973) (1974) (197																								TO
Column C																								700
0.000 0.000			0.0231	0.0223	0.0223		6720.0	0.0333		NC20.0	8220.0	21200	0.0217		91200	61200		0.0207	21200	0.0234	19000	61200	10000	100
1968 1969			0.0225				0.0242			0.0235			0.0220				9650.0							717
SECT CAPTO																								090
1998 1998	92070	65200		E#20.0	0.0241	5/200		1220.0	6420'0		7950.0	9060.0		£160.0	P0E0.0	0.0284		7.659.0	9820.0	0.0278	1650.0	0,0262	80£0.0	767
Column C	8200	6920'0	E150.0	0.0262	0.0273	0.0302	6750.0	99200	10000	9060.0	LIED.O	STEGO	7150.0	0.0314	7550.0	2620'0	6150.0	8750.0	10.0304	0.0281	6820 0	94200	6750.0	LO
NEW 1870	0'053	9850.0	0.0282	0.0258	0.0280	6150.0	£620.0	94500	0.0323	0.0332	0.0339	05000	0.0349	19ED 0	ELEO'O	52.60.0	Q.0337	\$2E0.0	61500	0.0334	100.00	0.0303	9150.0	200
100 100	E50.0	1520'0	0,0241	0.0234	0.0243	0.0280	0.024I	0.0243	05200	1920'0	8550.0	10000	0.0246	11700	1970'0	- 0920'0	8520.0	8223.0	1/100	1910'0	6,0163	0910'0	Z820.0	157
1800 1800	0.024	0.0245	P#20.0	Z#20.0	2520.0	6250.0	8450.0	89200	15200	1520.0	£250.0	6520.0	5520.0	7250.0	9570'0	0.0254	0.0250	6453.0	0.0247	0.0249	1950.0	0.0247	9920.0	757
1800 1800	800'0	0100,0	\$100.0	Z800°0	0800.0	\$50000	£600'0	06000	26000	1600'0	5010.0	96000	50100	10100	E1100	01100	8110.0	0110.0	11100	11100	60100	60100	01100	601
0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000	0.020	0.020.0	earo,c	5610'0	0.0210	0.0240	0.0224	902010	51700	0.0210	0.0214	1610.0	0.0204	0.0204	01200	12200	0.0233	5610.0	66100	861070	86100	7210.0	Z6100	761
The color The	0.020	0.020.0	6810.0	5600.0	0.0210	0.0240	0.0224			0.0210		26100		0.0204	0.0210	1550.0	6.0233	2619.0	66100	8610'0	8610.0	£610.0	7610.0	761
1,500 1,50	0.021	£610'0	7810.C	76t0.0	6050.0	68.200	0.0222	00210		0.0214	9110.0	0.0203	0.0209	9000'0	\$120°0	52200		5610'0	\$6100	0.0189	8810.0	8810/0	Z610.0	161
Section Sect	0.005	£500'0	5900°C	8500.0	#S00'0	65000	1900 0	29000	6900'0	8900.0	0400.0	PL00'0	54000	0.0085	P800 0	99000	£600'0	2800 0	0.0083	0.0083	6.0003	0.0082	0.0082	780
1,000 1,00	0.005	Z500'0	5500.0	8500.0	15000	6500'0	1900'0	29000	6900'0	8900'0	0700.0	4/00.0	52000	2800.0	4800.0	99000	£600.0	0.0082	5800.0	£800.0	6.800.0	2800.0	Z800'0	780
1,000 1,00	500'0	£500'0	5500.0	850010	1500'0	6500'0	1900.0	Z900'0	6900'0	8900.0	0100.0	6400.0	52000	5800.0	4800.0	98000	£600.0	7800'0	0.0083	£800.0	£800.0	0.0083	Z800.0	790
1998 1998	500.0	£500'0	5500'0	8500'0	\$500°0	6500'0	1900.0	Z900'0	6900'0	8900.0	0500.0	6,0074	52000	5800 0	4800.0	98000	£600.0	\$800.0	88000	6800.0	6,000.0	£800.0	Z800.0	780
1,500 1,50	0.005	£500'0	\$500.0	8500'0	t/S00'0	65000	1900'0		6900'0	8900.0	0500.0	4100.0	5200'0	\$800.0	0.0084	9900'0	£600'0	2800.0	£800'0	0.0083	6,0083	Z800.0	0.0082	290
\$500 \$5000 \$	0'002	4500'0	5500.0	8500.0	15000	65000	T900'0	0,0062	6900'0	8900.0	0400.0	¥4000	54000	\$800.0	1/800.0	99000	6600.0	\$800.0	0.0083	6.0083	0.0083	0,0082	0.0082	280
9000 90	500'0	£500'0	5900'0	8500'0	15000	6500'0	T900'0	79000	6900'0	8900'0	0700,0	8400.0	5/00'0	0.0085	4800.0	9800'0	£600'0		£800'0	6,0083	0.0063	2800'0	0.0082	780
9000 9000 9000 9000 9000 9000 9000 900	S00'0	£500'0	5500'0	8500.0	\$500.0	65000	1900'0	79000	6900'0	8900.0				2800.0	4800.0	9800'0	£600.0	2800.0	£8000	6.800.0	6800.0	2800'0	0.0082	780
1800 1800	SOC O	8500'0	9500'0	R200.0	9500'0	13000	5900'0	99000	£700.0	1/00/0	6,0073	6100.0	64,000	160000	5600'0	totoo	8600.0	6800.0	78000	0.0082	0.0083	£800.0	0.0082	580
1800 1800	0.005	#\$00'0	9906'0	850070	95000	19000	5900'0	\$900'0	£400.0	1700.0	£400'0	6100.0	64000	160000	\$600'0	10100	8600.0	6800.0	0.0082	0.0082	0.0063	£800.0	0.0082	£90
Section Sect	500'0	8500'0	9900'0	8500'0	9500'0	6,000.0	6,0065	990010	\$200'0	1700.0	£400'0	6400.0	62000	16000	\$6000	Tetee	8600'0	0.0083	2800.0	Z800'0	0.0083	E800.0	2800.0	£80
1800 1800	500.0	8500'0	9500'0	8500.0	9500'0	89000	5900'0	9900'0	£700.0	1700.0	£100.0	6100.0	64000	16000	\$600'0	10100	8600.0	£800.0	1800.0	0.0082	5800.0	\$800.0	Z800.0	590
1800 1800																			G 0082				0.0082	E90
1800 1800	500'0	B200.0	9900'0	8500.0	99000	19000	6,0065	99000	6.0073	1400'0	£400'0	64000	64000	1600'0	\$600.0	10100	8600.0	6803.0	0.0082	0.0082	0.0083	£800.0	Z800'0	£80
1870 1870		8500'0		8500.0	9500'0		5900'0	\$9000	£100.0		£100.0	6100,0	62000	16000	\$600'0	10100	8600.0	0.0083			6,0063	£800'0	Z800'0	£80
\$\frac{1}{100}\$ \frac{1}{100}\$ \frac	0.021	9110.0			2150.0	0.0223	0.0219	61100				91700		81000			1110.0	0.0214	0.0214	0.0215		5120'0	2150.0	STI
10 10 10 10 10 10 10 10	eteo	LL100	BZT0°C	6/10/0	62100	46100	5810.0	B7.10.0	6/10/0	N710.0	\$810'0	0/10/0	0.0100	2710.0	09100	retoro	2050.0	8/10.0	8/100	8/10/0	8710.0	8/10/0	87.10.0	821
\$\frac{6100}{6100}\$\$\frac{6100}{	8100	44100	8210.0	6410.0	6410'0	C6100	0.0182	82100	62100	8410.0	\$810.0	04100	0.0180	0.0172	0.0150	0.0182	0.0202	8410.0	82100	84100	8410.0	8/10/0	8710.0	841
Section Sect																								981
STOP								16100											1810.0				7810.0	981
STOP OFFICE STOP OFFICE OFFICE STOP S	6100	9810'0	PALO.0	1610.0	2610/0	21200	6610.0	P610'0	96100	0.0194	8610.0	88100	26100	0610'0	96100	96100	0.0211	0.0185	1810.0	0.0188	8810.0	7810.0	V810.0	981
Fig.		5810.0			8810.0					0.0190				1810.0										641
Part																								641
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\$\\ \begin{array}{cccccccccccccccccccccccccccccccccccc				4440.0																				EEL
\$\ \text{100}\ \text{200}\ \te	744.0.	343.00	3.07.5	7700.0		2440.0	2000	4474.0		20.00	2000		40.44.6	20,000			2200	0.010.0	30.00	2010.0		2010	30.00	- 181
\$\frac{1}{100}\$ \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \text{pick} \qquad \qq \qu																								481
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1600 \$1000 \$		30,000		40,410,41						Approx. 41					30,007,00.00					440.00.00	30,000,000		Part of the	02
00500 00505 00504 00103 00505																								06
1800 \$\(\)\)\[100 \) \(\)\]\[100 \\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	0.010	5510.0	5510.0	Z510 0	1910'0	tetoo	9910'0	[9100	6910'0	8910.0		\$910'0	ELTOD	5710.0	12100	8710.0	8610.0	1710.0	2710.0	0/10/0	£710.0	1710.0	1710.0	02
0700 07070 0											0.0200													86
0000 0000 0000 0000 0000 0000 0000 0000 0000		1/100	5710,0	0.0170				\$4100	1610.0	E610.0	0,0200	8610/0	10700	0.0208		10200	\$550.0		0.0202	2610'0	0,0204	2020,0	0.0200	86
00114 00113 00109 0010 0010 0010 0010 0010 00	8100			0.0170	5/10/0	96100	0.0180	0.0175	1610.0	E610.0	0.0200	8510.0		90'00'0	\$120.0	10200		66ta.0	20200	7610.0		0.0203	0.0200	861
9100 45100 45100 69100 59100 69100 69100 69100 69100 69100 69100 69100 99100 14100 69100 99100 14100 69100 99100 14100 69100 69100 69100 69100 69100 69100		15100	9410,0	5220.0		6/100	5910'0	8510'0	19100	5910'0	6,0173	2910'0	1/100	0.0170	5/100	77.10.0	8610.0	1710.0	0710.0	7510.0	9910'0	ET10.0	69100	691
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	9100				\$910.0		6910.0	E910'0		9910'0		09100		£910 0	Z910'0	14100	0610.0	9910.0		5910.0			59100	991
\$100 \(\frac{1}{2}\)100 \(EZTO'0	6910.0	8/10/0	66100	C810.0	94100	06100	6810.0	\$610.0	06100	56100	Z610 0	6610.0	16100	2150.0	0610.0	16100	0.0198	5810.0	£610'0	6810.0	16
2100 02100 12100 #9100 22100 %f00 08100 12100 18100 18100 18100 18100 SSDO 64100 E8100 06100 98100 6000 98100 22100 22100 22100 22100 22100 32100 32100 32100	810'0	KEIMO																						6/

P unites)	(m)	Beibulani)	Y2	ZX (ut) atte	Coordin	IX	Pair Pair
+	0	(MOOT DOLESS)	\$2.67875.	AL TRECES	62,688158	16,75000	1108
1	0	92	SEATHARK AT	ASTRECES.	\$2.878758	52.14EEE8	2306
1	0	- 02	821860:58 821860:58	AS THECE &	42.005158 62.005158	99'19CCC8	610M
	0	- 11	80.088158	76.808.00.8	60,186156	84.644.000	6109
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	8	91	851886.99 821886.99	C#100004	921886.09 77 649158	DO ENSUES	9206
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4		- 45	82.128728	\$9300CC4	95799124	78,E88E18	1200
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· L · ·	0	91	9E 196158	PERSECT	81.399128	197878.678	9908
1	0	92	16.55215H	80290CC8	25.623.56	10.Taatda	1906
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k	0	***	ES CARACE	83349EE8	11.222158	ERSCYLLA	1909
1	0	P1.	SECTITIES SECTIONS	STREETES STREETES	\$2.577.23 \$2.577.23	87,2454,58 87,5454,58	ENDR
4	0	D Pi	SA MAPES	F8.555558	20/209524	95 245 CT9	1908
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7 0.01S6 0.0134 0.0180	0.0186 0.017	0.0199 0.0158		0.0188	0.0136 0.0188	Н	Н	Н	0.0206 0.0201 0.0296	0.0206 0.0205 0.0201 0.0136	0.6230 0.0206 0.0206 0.0201 0.0396	0,0199 0,0198 0.0230 0.0206 0.0265 0.0201 0.0236	acrose across crass crass cases cases acros across	0.0191 0.0198 0.0198 0.0230 0.0206 0.0206 0.0201 0.0196	0.0191 0.0191 0.0198 0.0198 0.0198 0.0206 0.0206 0.0204 0.0204
0.0198 0.0217	0.0195	0.0200 0.0193		0,0187	Н	0.0156	0.0156	0.0195 0.0193 0.0193	0.0203 0.0195 0.0193 0.01993	0.0221 0.0203 0.0195 0.0193 0.0193	0.01E7 0.0221 0.0203 0.0195 0.0193 0.0199	0.0187 0.0187 0.0221 0.0209 0.0195 0.0193 0.0193	80150 0.0189 0.0187 0.0201 0.0205 0.0193 0.0193	0,0187 0,0180 0,0187 0,0271 0,0201 0,0195 0,0193 0,0193	DO157 0,0187 0,0187 0,0187 0,0187 0,0221 0,0203 0,0195 0,0195 0,0195
0.018A 0.0196	0.0187	-	-1	0.0184	+	0.0194	0.0195 0.0194	0.0206 0.0195 0.0194	0.0205 0.0206 0.0195 0.0194	0.0224 0.0205 0.0205 0.0195 0.0194	0.0192 0.0224 0.0205 0.0206 0.0195 0.0194	0.0192 0.0192 0.0224 0.0205 0.0206 0.0195 0.0194	0.0197 0.0192 0.0192 0.0124 0.0105 0.0195 0.0195 0.0194	0.0198 0.0197 0.0192 0.0124 0.0205 0.0206 0.0195 0.0194	0.0192 0.0198 0.0197 0.0192 0.0132 0.0224 0.0205 0.0205 0.0195 0.0194
5 0.0389 0.000s 0.0383	00198 00188	0.0206 0.0295	1	0.0198	0.0005 0.0196	+	0.0205	0.0207	00214 00207 00205	00217 00214 00207 00205	0.0233 0.0237 0.0234 0.0207 0.0305	0.0159 0.0213 0.0217 0.0214 0.0207 0.0305	00136 00300 0.0159 0.0233 0.0212 0.0207 0.0205	0.0198 0.0198 0.0200 0.0199 0.0233 0.0237 0.0214 0.0207 0.0205	0.0198 0.0198 0.0200 0.0199 0.0233 0.0237 0.0214 0.0207 0.0205
0.0202 0.0218	90208	H	1	0.0008	+	0.0217	0.0218 0.0217	90223 60216 00217	00221 00223 00218 00217	04299 04221 04223 04276 04277	0.0208 0.0219 0.0221 0.0221 0.0217	0.0207 0.0208 0.0319 0.0221 0.0223 0.0216 0.0277	GUT13 BO207 GLUDS GLUT9 BO221 GG273 GLT12 GG277	0.0015 GUD13 DOOOT DODGE 0.0019 DODZ1 DODZ2 GUD15 DOZ77	00207 0.0015 0.0013 0.0000 0.0008 0.0021 0.0021 0.0021
0.0178 0.0188	0.0175	17100 77100		0.0164	Н	0.0175	0.0175 0.0175	0.0180 0.0175 0.0175	0.0199 0.0180 0.0175 0.0176	0.0211 0.0199 0.0180 0.0175 0.0175	0.0211 0.0199 0.0180 0.0175 0.0175	80176 64174 0.0211 0.0199 0.0180 0.0175 0.0175	9.0177 0.0176 0.0174 0.0211 0.0199 0.0180 0.0175 0.0175	0.0176 0.0177 0.0176 0.0174 0.0211 0.0199 0.0180 0.0175 0.0175	0.0175 0.0176 0.0177 0.0176 0.0174 0.0211 0.0199 0.0180 0.0175 0.0175
0.0248 0.02EF	8970'0	+		0.0289	Н	2820.0	0.0398 0.03MG	0.0301 0.0398 0.03%C	0.0276 0.0301 0.0398 0.03%C	0.0252 0.0276 0.0301 0.0398 0.028C	G.CC70 0.0752 0.0276 0.0301 0.0288 0.0236	0.0272 0.0270 0.0752 0.0276 0.0301 0.0258 0.0396	0.0273 0.0272 0.0270 0.0792 0.0276 0.0301 0.0398 0.028C	0.0273 0.0273 0.0272 0.0392 0.0376 0.0301 0.0388 0.038C	0.0203 0.0273 0.0272 0.0270 0.0792 0.0276 0.0301 0.0398 0.0396
1 0.0119 0.0118 0.0107	00115 00111	0,0114 0,0112	1	0.0111	0.0115 0.0111	+	0.0015 0.0115	0.0115 0.0115	00118 0.0KIS 0.0115	0.0177 0.0127 0.0118 0.0115 0.0115	00177 00121 00118 00115 00115	0.0110 0.0177 0.0121 0.0118 0.0115 0.0115	00110 00108 0,0110 0,0177 0,0121 0,0118 0,0115 0,0115	0.0007 0.0010 0.00108 0.0010 0.00177 0.00121 0.00118 0.00115 0.0015	0.0113 0.0107 0.0110 0.0108 0.0110 0.0177 0.0121 0.0118 0.0115 0.0115
00000 00000	1000	+	1	000100	+	COUNTRY	CONTRACT	COLUMN COLUMN COLUMN	notes court cones cones	noise contra dellas noise	OANUT OANUT DOISE DOISE OANUT OANUT	OANUT OANUT DOISE DOISE OANUT OANUT	ODIES CONTRO CON	COLUMN CO	UDIA UDIES U
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0.0204	Н	0.0210 0.0206	Н	0.0202	Н	Н	0.0209	0.0211 0.0209	0.0216 0.0211 0.0209	0.0233 0.0215 0.0216 0.0211 0.0209	0.0233 0.0215 0.0216 0.0211 0.0209	0.0203 0.0213 0.0215 0.0216 0.0211 0.0209	0.0204 0.0209 0.0203 0.0213 0.0215 0.0216 0.0211 0.0209	0,0200 0,0200 0,0200 0,0203 0,0213 0,0215 0,0216 0,0211 0,0209	0,0202 0,0200 0,0204 0,0209 0,0203 0,0213 0,0215 0,0216 0,0211 0,0209
00200 00500	1	1	+	0.0185	1	00193	00193	00193	00193	0,0216 B0194 0,0194 0,0190 0,0190	0.0127 0.0216 0.0194 0.0194 0.0190 0.0199	0.0187 0.0187 0.01216 0.0194 0.0194 0.0190 0.0199	0.0150 0.0157 0.0116 0.0194 0.0190 0.0190 0.0190	0,0136 00190 00187 0,0137 0,0216 0.0194 0,0194 0,0190	0000 0000 0000 0000 0000 0000 0000 0000 0000
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0.0234 0.0234	+	0.0023 0.00215	+	0.0259	+	0.00239	0.00239	0.0217 0.0229	0.0228 0.0221 0.0217 0.0229	0.0245 0.0224 0.0221 0.0217 0.0219	0.0345 0.0228 0.0223 0.0245 0.0229	04213 04245 04224 04221 04217 04219	daye again of the action actio	0.0210 0.0210 0.0213 0.0213 0.0245 0.0221 0.0217 0.0219	0.0212 0.0210 0.0210 0.0213 0.0213 0.0245 0.0228 0.0221 0.0217 0.0219
M 8-0223 0-0230 0-0213	0.0221 0.0204	0.0230 0.0222	-	0.0191	0.0264 0.0191	Н	0.0204	0.0204	0.0204	0.0209 0.0205 0.0202 0.0284	1 0.0236 0.0209 0.0205 0.0204	1 0.0236 0.0209 0.0205 0.0204	Q.0165 0.0163 0.0211 0.0236 0.0209 0.0205 0.0202 0.0204	6,0172 Q.0165 Q.0161 Q.0171 Q.0136 Q.0209 Q.0205 Q.0202 Q.0204	D. D
0.0159 0.0217	0.0204 0.0193	0.0208 0.0199	Н	0.0195	Н	Н	Н	0.0200 0.0200	0.0204 0.0202 0.0200 n.0205	0.0231 0.0204 0.0202 0.0200 n.0205	0.0231 0.0204 0.0202 0.0200 n.0205	0.0166 0.0201 0.0201 0.0204 0.0202 0.0200 0.0205	9.00168 0.00166 0.0003 0.00231 0.0204 0.0202 0.00200 0.0205	0.0221 0.0168 0.0166 0.0203 0.0231 0.0204 0.0202 0.0200 0.0205	9.00168 0.00166 0.0003 0.00231 0.0204 0.0202 0.00200 0.0205
0.0199 0.0217	0.0197	+	1	0.0211	+	0.0219	0.0212 0.0219	0.0214 0.0212 0.0219	0.0210 0.0214 0.0212 0.0219	0.0239 0.0210 0.0214 0.0212 0.0219	0.0214 0.0239 0.0210 0.0214 0.0212 0.0219	0.0214 0.0214 0.0219 0.0210 0.0212 0.0219	0.0171 0.0169 0.0214 0.0219 0.0210 0.0214 0.0212 0.0219	0.0240 0.0171 0.0169 0.0214 0.0219 0.0210 0.0214 0.0212 0.0219	0.0228 0.0340 0.0171 0.0169 0.0214 0.0229 0.0210 0.0214 0.0212 0.0219
2 0.0171 0.0183 0.0159	20000 00000	0.0172 0.0160	+	0,0052	00000 00000	+	00000	0.0063 0.00167	00178 00163 00167	0.0185 0.0178 0.0163 0.0163	0.0210 0.0155 0.0178 0.0153 0.0157	0.6175 0.0210 0.0185 0.0178 0.0165 0.0157	0.0176 0.0174 0.0175 0.0210 0.0185 0.0176 0.0165 0.0167	0.0177 0.0176 0.0174 0.0175 0.0210 0.0185 0.0176 0.0165 0.0165	0.0176 0.0174 0.0175 0.0210 0.0185 0.0176 0.0165 0.0167
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3 0.0238 0.0230 0.0204	0.0203	0.0219 0.0212	Н	0.0205	0.0210 0.0205	Н	0.0210	0.0212 0.0210	0.0215 0.0212 0.0210	0.0216 0.0215 0.0212 0.0210	0.0238 0.0216 0.0215 0.0212 0.0210	0.0206 0.0238 0.0216 0.0215 0.0212 0.0210	Q0216 Q0211 Q,0206 Q,0218 Q,0216 Q,0215 Q,0210	0.0209 0.0216 0.0211 0.0206 0.0218 0.0216 0.0215 0.0212 0.0210	0.0203 0.0209 0.0216 0.0211 0.0206 0.0238 0.0216 0.0215 0.0212 0.0210
0.0200 0.0219	00200		-	0,0222	+	0.0231	0.0235 0.0231	0.0224 0.0275 0.0231	0.0216 0.0224 0.0275 0.0231	0.0347 0.0216 0.0234 0.0235 0.0231	0.0747 0.0216 0.0234 0.0235 0.0231	1 0.0257 0.0233 0.0347 0.0216 0.0224 0.0275 0.0231	0.0169 0.0257 0.023 0.0347 0.0216 0.0224 0.0275 0.0231	0.0257 d.0169 0.0257 0.0233 0.0347 0.0216 0.0224 0.0215 0.0231	0.0169 0.0257 0.023 0.0347 0.0216 0.0224 0.0275 0.0231
0.0231 0.0247			4	0.0222	+	67000	0.0234 0.0229	0.0223 0.0224 0.0229	0.0225 0.0223 0.0224 0.0229	0.0346 0.0225 0.0223 0.0224 0.0259	0.0219 0.0346 0.0225 0.0223 0.0224 0.0229	0,0205 0,0219 0,0346 0,0225 0,0223 0,0224 0,0229	0.0207 0.0205 0.0219 0.0246 0.0225 0.0221 0.0224 0.0229	6,0222 0,0207 0,0205 0,0219 0,0246 0,0225 0,023 0,0224 0,029	0.0217 6.0222 0.0207 0.0205 0.0219 0.0346 0.0225 0.0221 0.0224 0.0229
0.0205	16100	1	4	0.0185	1	1	0.0186 0.0179	90005 00186 001ED	0.0195 0.0202 0.0186 0.0189	0.0200 0.0195 0.0202 0.0186 0.0189	0.01% 0.0208 0.0195 0.002 0.0186 0.0170	0.0190 0.0186 0.0205 0.0195 0.0200 0.0186 0.0186	0.0195 0.0196 0.0195 0.0195 0.0195 0.0186 0.0180	GANG GALOS GALOS GANKS GACOS GALOS GALOS GALOS GALOS	0.0201 0.01M3 0.0155 0.0150 0.0205 0.0205 0.0155 0.0156 0.0150
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0.0209 0.0216		1	+	0.0197	1	+	+	0.0207 0.0202 0.0206	0.0223 0.0207 0.0205 0.0206	0.0224. 0.0223 0.0207 0.0202 0.0206.	0.0210 0.0224 0.0221 0.0207 0.0202 0.0206	0.0210 0.0224 0.0229 0.0207 0.0202 0.0206	0.0206 0.0204 0.0224 0.0221 0.0207 0.0206	0.0204 0.0205 0.0204 0.0214 0.0221 0.0207 0.0205 0.0206	D07205 0.0204 0.0205 D07204 0.0210 0.02214 D07221 0.0207 0.0207 D07056
9 00176 00130 00156	+	0.0377 0.0161	+	0.0154	0.0166 0.0154	1	1	1	0.0273 0.0244 0.0346	0.0252 0.0221 0.0238 0.0244 0.0346	0.0252 0.0221 0.0238 0.0244 0.0346	0.0172 0.0252 0.0221 0.0238 0.0244 0.0346	dotte 0.0169 0.0172 0.0252 0.0221 0.0218 0.0344 0.0166	0.0169 0.0169 0.0172 0.0522 0.0221 0.0284 0.0166	0.0345 0.0349 0.0349 0.0177 0.0252 0.0221 0.0248 0.0346
200 0050 0050 0050	000219 00000	Outro during	+	0.0000	1	1	1	00200 00200 00200	00200 00200 00200	00200 00200 00200	0.020 0.020 0.020 0.020 0.020 0.020	0.020 0.020 0.020 0.020 0.020 0.020	GUIN GOING GOING GOING GOING GOING GOING GOING	0.0167 0.0172 0.0166 0.0179 0.0279 0.0270 0.0270 0.0270	0.0017.7 (0.000) 0.0010.0 (0.0010) 0.0010.0 (0.0
t	+	+	+	0.0167	+	+	+	0.0205 0.0204 0.0204 0.0106 0.0175 0.001M	0.0196 0.0175 0.0184	00033 00031 00036 00125 0003M	00033 00031 00036 00125 0003M	0000 0000 0000 0000 0000 0000 0000 0000	00100 00100 00100 00100 00100 00100 00100 00100 00100 00100	0.01459 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.01459 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150 0.0150
Sound Course	2000	t	+	0.000	+	COURS	0.000 0.000m	ACTUAL CONTRACT CONTRACT	ADDIT TOTAL TOTAL OCUM	0.022 0.031 0.032 0.032 0.0334	Other Design apply Apply Design and a	OCIET OFFICE OCCUPY OCCUPY OCCUPY OCCUPY	ACTION CONTRACT CONTR	COURT ACTION COLORS COURS COLORS COLORS COLORS	CASES CALLES CALLES CALLES CALLES COLLEGE CALLES CA
ł	H	0,0294	-	NOTES.	1	1	0.00284	CORES CORES	William Course Course	GOLD MAIN DAMES COMES	W0003 000011 000100 000103 000100	0,0185 VOCES 0,0011 VALSO 0,0162 U.0189	MUSS 00155 00155 00055 00051 00055 00155 00155	WORLD GOLDS GOLDS WOLES WOLES GOLD GOLDS GOLDS	NEGOT CONTROL OFFICE

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404	Y2	822336.25	\$22346.7 E	823409.45	622843.00	82254£7E	822316.62	873474 44	822496.58	822614.65	822626.09	822526.54	822455.21	\$22464.A7	822441.65	\$22454.02	822367.55	\$2286634	822432.88	822462.AS	122456.07	822556.02	622462.07	4224251	\$22380.48	622354.59	622354.65	822274.91	622396.31	82222878	822293.72	822346.13	\$2234£.78.	822125.44	822178.07	822252.03	822278.92	822341.72	822376.93	82240579	822421.11	822464.38	622072.07	H22126.94	822178.17	822221.21	822269.00	822264.07	\$22308.61	622330.74	422339.17	82236157	822320.45	842250.02	NZZ DBE AS	622011.22	82130758	821877.85	822086.76	822007.07	822067.62	822474.73	82236328	822174.73	822144.43	822162.85	82214882	822138.55	82211333	82208(3)	\$22039.CE	621614.78	821738.42	82188122	#21727.AS	10,488128	821847.78	122007.97	#2200B72	621163.31	821863.31	821881.67	821862.76	821763.88	8218128	\$21796.91	121802.07
r 2034	X2	935177.37	833231.06	833434.80	833969.46	83196546	633465693	********	93367378	18228228	13397371	834046.15	831627.55	833772297	833752.11	833840.51	83386358	83384185	13319664	833883.54	933846.51	83342248	633416.03	033447.02	93354454	833587.56	133587.54	633633.17	833861.17	833209807	633316.00	935485561	93348985	833100.53	133232.06	833377.80	833563.54	633673.62	833744,11	83384676	833917.83	833980E8	8331111.75	83125139	833394.77	833624.35	833883.40	833664.88	833763.76	#337/18.45	833833,16	9239029	83395046	634034.90	83423476	63432121	834384.01	833156.58	633434.10	9933274.46	633438.70	63368633	93373698	83346833	033649.55	83168168	83371386	633767.83	83577848	83387214	833867.20	93410921	834255.10	83405834	131341.81	833139.74	93328674	93346651	83354373	133543.70	633563.70	832315.56	833481.00	933176.47	93325369	833254.16	93332666
Coordina	**	822324.11	822330.25	822345.74	822408.49	822543.00	622308.10	201100	85125228	822496.58	132614.05	832628.09	822419.61	822455.21	132494.47	822441.00	10 865228	822297.16	822463,30	822432.88	822462.40	822567.47	822556.02	522482.05	822425.38	822350.48	522318.11	\$22354.80	822374.91	822192.93	822239.78	\$22293.72	822345.13	822119.68	1231215.44	822178.07	82225203	822278.46	823341.72	822376.15	822405.79	822431.11	822085.71	40745738	822129.94	822175.17	122221.21	82228300	822284.50	822311.12	522318,98	11.365228	822369.57	972220.48	62246267	822084.65	822010.68	621955.43	821977.96	821642.33	822004.80	822080.21	1000000	82218328	82212203	822444.60	622152.80	822148.62	8221228.85	422123.04	822113.30	822062.66	621814.78	822039.23	821859.22	821080.28	621889.31	821947.50	\$22008.03	822028.73	\$21952.62	821834.07	821491.68	821775,07	821783.15	821757.87	821826.73
7	X1	633125.78	12717128	833231.08	833434.89	633960.46	2011878	E1147&14	633596.26	83.873.85	131533,67	633973.71	633527.00	833627.55	833732.97	633782.11	533661.17	613693.59	833978.15	633696,64	613883.64	823387.36	835423.89	633416,00	613.647.62	£33544.64	133488,77	832587.56	613633.17	825082.67	833209.07	633355.00	19:087519	833073.42	833100,63	633232.06	613377.64	832503.51	833673.82	613764.65	£13848.76	833917,83	833076,99	633121.79	\$13253.39	833598.77	833524.35	613653.40	£13694.68	R35761.98	833763, 91	813(3)316	E13902.04	833950.40	KMAN KZ	£34231.72	834322.77	833097.20	823156.55	813101.67	833274.00	833434.18	202120	833736.08	633586.71	25.943513	833683.68	833713.66	633757 63	613734.63	833778.69	833873,20	634155,21	et3887.29	834058.34	833118.37	633139.75	20.255.65	633460.69	833543,73	633460.98	77.091013	833315.00	833154.01	633176,74	£13168.60	E33249.00
Calline	Pair	R003	R103	R003	11003	R003	8004	8000	Roce	F-00.6	H005	REGS	RS16+R307	P006+R007	R006-R007	R096+R007	R318+R409	ROOM-ROOM	R010+R011	RELIGNATION.	RECE-8001	RD12+R013	R013+R013	R012+R013	RDC2+RDC3	RD12+R013	Rol4+Rols	R016-H017	ROLE-BOLZ	Rote	8621	RGEZ	R422	R023	R024	R625	neze	R027	R028	820H	Rese	RODT	F052×R201	RESS	R034	ROSS	N036	R437	Rate	R029	8,040	ROAT	N942	NOW D	BS46	Ross	F104.7	BS48	8049	NONO	ROST	R652	man.	A SA	8664	19084	NO84	*00*	R054	ROSS	ROBG	R057	Ress	9100	NONO	1001	ROSZ	RDES	HDEA	#100 W	H054	RORS	ROBB	160H	ROSS	RONG	More

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e (m)	YZ	621687.07	621875.23	821800.54	82388128	\$21B90.77	921584.99	82182232	82188436	82187128	*******	27 1000 70		*************************	11111111	# 10 10 10 10 E	**********	20,100,10	********		********	SECTION ST	1000000	821646.35	621512.65	624533.68	821546.45	821508.35	821854.64	821865.51	821841.09	\$21786.57	82148976	8318/A 83		111111111111111111111111111111111111111	/ Supple 2	92/862.03	62182828	821766.33	821728.47	821453.37	821554.44	821508.87	821634.13	15,689,24	82159924	829576.41	\$21548.43	822414.27	822332.11	N2225635	822180.58	822098.55	822308.38	SECTION OF	2777777	822438.48	#2 dans 24	# 22 W. C. P. A. P.	822360.57	622271.35	62220123	8221228	822115.02	822037.73	621965.98	82758CAS	92189K SS	862228	82222216	822158.50	N22254.07	622172.55	822174.73	822278.48	622221.21	822265.72	822578.17	622546 7 K	45100454	1000000	20100000	62386230	822178.07	822120.84	122129.44	822072.07	8218178	\$21347.58
iate (m)	ANTERTAN	83369175	833397.14	633491.50	83350697	833548.6E	833603,43	833684.92	931553.57	832600.48	********	1319(0.54	11000			11616.10	1010000	2200012				32545.8	The same	41164167	833728.62	11340311	633646.83	83369649	833368.50	633416.50	835487.53	83352363	855874.80	3116/416		1071.1500	9313/609	033417.30	833489.60	9335EZ46	833542.19	833563,07	03300119	83366693	83333734	133441354	69'619'60	83134151	933648.49	83401877	834127.62	83421631	834309:08	834407,44	933991.76	DAGGE JV	034161.00	1072770	024204.20 034404.24	03000074	832902.98	03330046	833994.47	834077.01	834097.30	834190.09	83424325	83428216	834369.17	633769.11	83386878	833964.78	833694.68	833827.77	83364833	833563.51	63362436	6333866	031358.77	913414	*******	03248021	********	93390937	93121208	93321339	833106.63	82323558	83316688	833796.88
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1 1	X1	833397.24	833451.80	833281.64	633449.48	E33501.44	E33548.00	633663.43	53356657	623352.57		811084.38	******		0.1444.00	STACAGE TO		*********	*******	20.000	Distance of	BA3387.34	644446.44	ETTERS DA	613681.67	833645 75	833603.88	COSCIE AN	833354.34	633566.60	633436.50	613.687.63	833633.63	STATES BA	STAGNA 16	B. (0.00) 50	48.000.00	633370.00	833427.39	633480.60	£13522.48	833543.19	133562.07	633598.96	223259.78	833337.92	833449.06	633337.64	85'8 69'STR	832565.5E	\$34028.T7	634127.62	EMPREST	834309.00	633917,63	S12991 95	234199.04	BANDA M	20000	63439349	633848.70	833833.16	633303.65	613994.00	834074.90	834097,30	634190.59	634242.94	834251.93	833768.03	833761.96	87.848.018	E33673.82	833694.84	633653.40	ETSABB.65	E35563.61	833377.80	633377.60	619 509 473	******	2010000	#17.481.00	633493.05	£13291.01	#3222.02	833069.91	53,000,03	e13121.68	E35274.6E
Road	Page 1	R472	ROTA	B574	R575	RoT6	F-07-6	NG76	BG77	11011	MOTO	mere mere	British	and a	2000	0000	200	2000	1000	Britis .	1	Page 1	Dies.	BASE	ROBS	8086	RCSS	8687	ROBA	8,088	Ross	Rokk	ROSS	8448	9946	ness.	nes.	488W	R089	ROSS	Ribes	Ross	# C09 9	RORS	R090+8091	ROV2+R003	R092+R093	B-094	ROSE	R099-R1937	R090+N099	R100-R101	R102+6103	R104+R104	N 106	1010	ANIE	R109	0110		MITTE	Rtt3	ATTA	Rits	RTES	RHIT	RITE	RTES	R120	R121	R122	R-C23	R124	8428	RYZE	8127	R128	R126	R13G	Best	2000	N I	a series	M134	Reta	R126	R137	RESE	Retail	R140

54100	Z910'0	\$310,0 8810,0	7910'0 (910'0	£9100	F510.0	5710.0	27700	69100	0.010.0	2610.0	65100 68100	0.0163	0.0168	0.0214	0.0217	¥650.0	0.6210	92100	99100	6710.0	52200	0.0170	90000
05100	2520.0	0.020.0	0.0214	STEWO	92200	MOCO O	F6T00	0.0201	1610.0	8610.0	COTES	enton	48100	0.0154	sutoro	8050.0	ESTO 0	95100	25100	#510 U	.4510'U	15100	9510 0
0.0138	C#10.0	1510.0	0.0160	£51070	≤100	ZSLOT	5510'0	95T0'0	DOTAS	£910'0	0,0142	ESTOO	A4440.0	51700	60200	0.0230	8210.0	95100	951070	9510'0	0.0152	0.0158	9510'0
8050.0	TT10.0	8/10,0	5810 0	4810'0	36700	5610.0	96100	Tetton	9510.0	6,0193	1810.0	60100	9810'0	05100	50200	0.0205	£619.0	CETTOO	8810.0	\$810.0	8870.0	1610.0	6610.0
0.0216	5050/0	9,0204	6,020.0	6050.0	4120.0	0.0210	0.0204	50200	1020.0	6050.0	0.0201	E120.0	917000	91200	21200	0.0217	1023.0	Etzoo	grzon	6720.0	0.0208	E020.0	6610.0
ERIDO	9910'0	2010 C	M810.0	0.010.0	23100	PH10'0	ostoo	45100	2010.0	£510°0	11100	15100	Z9100	V\$100	6510.0	96100	45100	98100	06100	0.0154	ARIO.0	0510.0	E4100
4916.0	EZIOO	EZTOD	0.0183	9810/0	0.0203	10101	E8100	0.0192	Z610'0	1073501	3810.0	0.0200	76100	20200	99100	0.0221	66TU 0	Largo	2810.0	0020.0	0.0192	0.0202	9610'0
ESICO	Z510'0	0910'0	6910.0	T/100	COURS	D.0174	69100	9/100	2210'0	term'o	ILLOO	0.0174	1710.0	98100	6/100	1610.0	14100	52100	0810/0	6710.0	7810,0	92100	1910.0
51200	P6100	9020'0	6540 Q	0.0204	822010	6.0213	0.0204	0.0213	0.0211	\$150.0	5020'0	0.0211	90600	90200	0.0203	9220.0	0.0203	SHICK	06100	0.0394	6610.0	EBIO'O	8610.0
5150.0	2610'0	SRTGC	1610.0	68100	0.0201	2810.0	54100	M810.0	osto a	1150.0	0.0204	0.0213	0.0207	0.0206	66100	0.0226	90200	9650.0	95100	9670'0	MSS0.0	0'0530	0.0202
6610 Q	1810.0	2.0185	0.0145	2810.0	232.00	0.0201	LSTOO	96TU 0	0.0195	0.02002	6810.0	16100	961010	86TU 0	66100	0.0218	6810.0	\$6100	66100	0.0192	7810.0	Z610'B	98300
6110.0	Stt0'0	5110.0	NETO D	96100	3910.0	72.0.0	05100	T\$100	84£0.0	8510.0	09100	1220.0	ostero	19100	0/100	2610.0	1910.0	09100	TOTOR	£910.0	0.0160	79100	19100
6110.0	81100	STTO'C	NETO'D	99100	S0100	7210.0	05100	TSTOO	84£0.0	8510.0	0.0140	15100	estero	19100	02700	5610.0	1919.0	00700	00163	5910.0	0910'0	79100	1910.0
61100	ELTO.O	Lito.c	0.013A	90100	3910.0	LSTO 0	DSTOO	1510'0	89100	8510.0	0.0140	E510.0	05100	1910'0	0710.0	2610'0	1910.0	OSTO 0	tetoro	£910'0	09100	2910.0	19100
01100	067070	BATOC	1910'0	2810/0	56100	D.O.A.I.	14100	19100	0.0177	9020'0	96100	0.0202	9610 0	16100	16100	6120.0	16100	95100	25100	12200	0.0210	66100	2510'0
Z810 0	99100	£910°C	0.0185	28100	0.0199	ESTO D	8120.0	0.0187	E810.0	0.0192	62100	0.03 NK	M810.0	9810.0	88100	0.0213	Z810'0	£5100	15100	0.0204	7910,0	7810.0	0.0182
66100	5530.0	ORIO.C	BETO'D	96100	E1200	M20.0	0.0188	60203	M050.0	0.6211	92100	M240.0	9810'0	68100	16100	9150.0	2510'0	05100	ZS10.0	85T0'0	9510'0	1510.0	9510.0
Salara.	£810'0	PKID,C	0610.0	16100	grasse	N610.0	06100	66100	6610.0	5020'0	£510'0	0.0202	0,000	0.0204	60200	\$220'D	5610 0	56100	06100	ERIDO	SETO'O	ESIGO	2610.0
0.0211	T050.0	8050.0	7e10.0	0.0205	92200	0.0208	0.020.0	0.0215	0.0214	V150.0	0.0210	0.0209	1805010	11200	0.0203	.6150.0	8610.0	66100	0.0200	0.0197	9910.0	66100	657070
16100	3810.0	7810 C	0.0184	98100	107.00	6810.0	18100	0 OT 00	0.0195	0.0202	3610 D	EDGOLO	10000	51700	0.0210	0.0221	0.0202	86100	66100	0.0550	0.0200	66100	2020.0
92100	\$9100	2,016S	9910.0	0.0172	1510.0	0.0181	1510.0	8710.0	5510.0	0.0182	1710.0	17,10.0	5510.0	8710.0	62700	\$6£0.0	E710.0	\$7,10.0	2100	1710.0	\$210 a	EVIOLO	6410.0
W810'0	08100	6/10 C	6/10 0	\$810°0	107.0	NSLO.0	0.0183	0610'0	0610.0	16100	9810/0	B610.0	9610 O	8610'0	1610.0	0.0213	V819.0	1810.0	82100	\$810.0	8810.0	9810.0	8850.0
1810.0	54100	SAIDE	8710.0	2810.0	0.0209	20195	9810.0	\$610.0	EGTO 0	1059.0	9810.0	0.0135	7610.0	66100	0.0204	9170.0	DELLO	28100	4100	9ব্যয় ত	1810.0	ESIGO	1810.0
2710.0	6510.0	6510'0	E910 0	14100	\$610D	P(10.0	11120	11100	2710.0	Z81D'O	04100	77,000	57,10.0	18100	12100	5050.0	22100	OZTGO	0/100	5510.0	1710,0	1/100	1710.0
ELTOO	erro.o	5Z10'C	at to 0	2110.0	EXTOR	#LL0.0	PI100	12100	0.0120	0.0126	SELOO	0.0124	6,0123	8210.0	Strag	ESTO.0	8110.0	21100	91100	0.0120	51100	3110.0	9110.0
10100	7.BO0,0	SMOOLC	9600'0	2600 B	50100	OULTO	cotoo	9010/0	4010.0	9010'0	colog	SULTO,O	90100	SOTO	PILLO	Z110.0	2010.0	00100	20100	0.0100	Satao	0.0104	0.0100
92200	0.0233	9550.0	0.0218	1550.0	0.024	0.0228	22200	9970'0	1520.0	6250.0	9970'0	E5120.0	A1100.0	7750.0	HSCOR	0.0267	617010	0.0251	0.0251	15000	0.0252	1220.0	6540.0
ISIGO	2510.0	8110.0	RETOIL	\$\$100	14100	1910 0	8210.0	19100	7210.0	£910'0	0.0151	Z9100	1910 0	0.0165	THICG	£610.0	0910.0	19100	E910.0	29100	19100	09100	1910.0
1810.0	5510.0	1/tto.c	E410.0	61100	0.0200	9810.0	0610.0	16100	1610.0	6610.0	16000	ento o	0.6200	0.0205	0.0203	0.0219	2610.0	1810.0	9610.0	8510.0	1610.0	2610.0	£610.0
1910.0	69100	6010 C	9510.0	esturo	6/100	1910.0	25100	19100	1910.0	17,10.0	6510'0	回10.0	59100	PZ10:0	0.01310	9610.0	7910.0	1/100	99100	2710.0	3910.0	69100	0.0170
14100	7210.0	00129	2910/0	49100	MIO 0	PATTO.0	6910.0	18100	6710.0	6810.0	0810.0	0.0166	1610.0	9610.0	1610.0	5150.0	ERIO O	SELOO	2810.0	0.0183	SACOR	ESTOO	ESCO.O.
89100	0510.0	9510'0	9510.0	65100	080.0.0	WA10.0	0.0165	£1100	ITIO.0	£81D.0	6910'0	RZTO O	0.0180	68100	8810.0	5020.0	1710.0	1710.0	18100	0.0182	LZ10'0	0810.0	0.0178
N2100	6910/0	6910.0	1510.0	£210/0	00000	£220.0	60174	62100	5510.0	\$800.0	5710.0	17.10.0	2710.0	6210.0	SELGO	0.0202	E740.0	1/100	99100	5110.0	89100	69100	0.0170
R910'0	65100	9210.0	0.0158	99t00	1310.0	1/10.0	E910'0	1/10.0	1/10.0	ESID.O	E710.0	1810.0	4810.0	06100	extoo	0150.0	5810.0	8/100	2810.0	9710.0	PHIO.0.	98100	52100
00100	6910'0	2010.0	0.0165	92100	1610.0	£810.0	5910'0	TRITO	INIO G	6810.0	59100	27.00	57,10,0	5210'0	92100	0.0201	2210.0	71100	0410.0	9610.0	76100	IRIO.0	5210.0
69100	05100	6510.E	1410.0	0510.0	0.03299	77.10.0	5510.0	94100	5,710'0	2810.0	5740.0	1610.0	1810/0	1610.0	36100	5150.0	SHT0.0	sitoo	2810.0	SETO'0	10,00	E810.0	4810.0
5/10/0	1510'0	95t0'C	69t0.0	621070	0.0205	0.0193	6810.0	06100	8,210,0	0.0204	\$310.0	7910.0	6610 O	0.0209	0.0220	0,0233	8810.0	PS10'0	5810.0	\$810.0	EA10.0	7810.0	£810.0
92100	9510'0	9510.0	52100	68100	0.0215	0.0209	0.0202	90200	0.0206	0,0222	20700	0.0221	6110.0	0.0231	8E200	0.0255	0.0200	06100	2810.0	0.0190	56100	1610.0	9050.0
15100	PETO'O	TETO,E	0510/0	25100	EL100	9910'0	9510'0	9100	1910.0	69100	75100	DOTAL	99ID'0	2/10/0	16100	9020.0	\$7.10.0	14100	60173	0/10/0	89100	59100	0.0172
15100	1610.0	TETO'C	99100	\$510°0	9/10/0	E210.0	95100	0.0162	M210.0	1710.0	5510'0 6#10'0	99100	0°0100	9210'0	98100	1050.0	ETTO.0	02100	FTIOD	0520.0	2910'0 2910'0	5910.0	0.0171
6510.0	SVIO.0	EMOC	991010	95100	87100	\$910.0	25100	95100	1510.0	5910.0	00100	2510.0	7810.0	45100	8310.0	8810.0	2510.0	02100	95100	95100	5510.0	95100	PS10'0
95100	2010.0	0,010,0	#510 G	25100	#2100	1910 0	95300	95100	7510.0	1910.0	1910.0	75100	£910'0	95100	89100	8810.0	£\$10°0	22100	95100	95100	25100	95100	ESTOO
95100	Z\$100	0510.0	B210.0	Z\$100	8/100	\$310.0	95100	00120	\$20.0 \$20.0	1910.0	TOTOO	25100	\$410.0	SSTOO	19100	8810.0	£510.0	25100	95100	9510'0	12100	95100	1210.0
RSIGO	50100	9vto'c	B210.0	25100	£100	5910.0	95100	45100	2510.0	19100	19100	25100	Z910 0	\$510°0	19100	8510.0	25100	25100	95100	9570'0	75100	95100	2510 D
R5100	29100	SALOE	8510 0	25100	#100	5910.0	95100	45100	Z/10/0	1910.0	THIGO	25100	Z910/0	\$510.0	89100	8510.0	2510.0	tstoo	95100	95100	CS10.0	95100	E210.0
BSICO.	29100	99100	8510.0	25100	64100	5910.0	95100	45100	Sero.o	19100	19100	ZSTOO	7610.0	55100	89100	8510,0	2510.0	12100	95100	95100	£510'0	95100	£510'0
20100	6110.0	2010.C	6210.0	29100	49100	0.0155	45100	05100	0.0146	9510'0	85100	7510.0	69100	65100	69100	0610.0	6510.0	19100	8510.D	8210.0	6210.0	95100	\\ \text{\rm 2210.0}
HP1DO	71100	THO.C	ESTO O	69100	MIOD	0510.0	£9100	25100	KALO.O.	6510'0	19100	5510.0	15100	29100	65100	2610.0	0910.0	19100	25100	9510.0	9100	19100	1910'0
49100	£9100	SAIGC	#\$10°0	99100	COLER	6,0173	39100	8/100	2210 0	1610.0	18100	2010.0	1510.0	50200	0.0203	9150.0	2610.0	06100	66100	0.0204	2610.0	R6100	1910.0
Z910'0	25,10,0	8540,0	8510.0	69100	COLET	7770.0	14100	TRITO	E810.0	\$610°0	COURT	66100	6610'0	21200	10200	0.0217	6610.0	06100	86100	0.0202	E010.0	86100	1610.0
H9160	1810,0	\$610.0	E910-0	09100	49100	Z910 0	0.0155	00163	0910.0	8510.0	19100	2510.0	este o	60100	TETOU	1410.0	9419.0	81100	0.0104	16000	51100	ottoo	0.0127
19100	SETUTO	9E10.C	1510.0	09100	08100	16210.0	95100	22100	54100	16100	19100	OUTOD	26100	90700	7610.0	0.0220	2610'0	65100	25100	19100	19100	5/100	2500
H4Z3	Hr22	Hr21	Hr20	614H	SINH	ZPH	PHI	SINH	THAT	HU3	HUS	HH	HAO	601H	BONH	TOTH	904H	Hros	Hroa	Hr03	ZOJH	104H	90ºH
		1 1000	1/1/1/1	Dial.	0.010	4 141	me ett	31,44	F PAD	61417	5,510	6.6-(1)	N Park	שיייעע	00761	- PA-17	1 20-11	1 20°F7	L LOSH	L COMP	DAN P	1 20017	A PART

4	0	840	FE-marca	98446968	\$2101432	\$3.0CCM58	9654
4	0.	9.0	\$1.5821E	SODIETE	CLTIBICS	41 6CZ9ES	9500
7 -	9	10	89-010528	OPELERCE	27.200128	ERRESTER	STILL
1	0	- 16	88.000558	DC ROCKCE	REGIOZZE	TTASCACE	1010
	0	10	REZYDA TY	81.008.6C8	48 (0032)	BE PREPER	Z#LW
Ψ.	a a	96	99 S094Z9	17,918164	80.632.54	10.141628	7508+9816
	.0	12	34 164173	12,140ccs	821605.58	en asacco	951819510
+	0	16	30.707754	SAACHECE	82409938	SE-ATRECA	CAN HI-CONE
4	0	\$6	#24B46.01	82900918	45.157150	\$2.3 £92£8	141840919
4	n	81	RZ4886 22	ACRIDACE.	10919128	\$2410PT 58	5918+9918
4	0.	- 40	Ch dispara	STIMES	EL. SCORES	NO OFFICE	1518
1	0	10	622138.83	+C.C.CEACH	ES SECTES	PRINTERED	981W
	0	- 6	39 252 223	#5121216	82.188.558	SO ROCKES	9910
¥		- 43	EG 2175X8	00,740408	81.840558	00, FTBA68	1918
	0	Di -	BY ABOUND	9310159	16 223 224	16.120128	1916
	0	14	BELLOOPEE	PATROACE	80,51,1208	10,110460	46178
74.	0	DA.	TESTASAIT	43434042	EC S H- ECG	82409428	ESLN
4	- 8	8.0	NE STEER	85,157456	LB 2 83 228	ESTRIPES.	SHIRE
	0	- 40	ST WEEKE	*C.BTSACS	EE E LEEZE	88.767548	1818
- 1	0.	- 6	AL AMERICA	BESTERES	achettte.	BIFFERE	6,819.
	0	40	#E-009169	SELLBECE	12'920128	BB.F ZACCO	#45.W
1.0	0	91	19 909121	93341650	951629.50	STREET OF	8118
- ¥		10	LF THREETER	#925SEC#	*2.646158	60719279	10.8
	0	02	62,080,73	74.000ccs	891608.48	11.844CC0	611.8
4	0	99	BECCUSCH	*CCFFCCF	86.519326	81.748558	F41-8+9-418
- 4	0	30	59 280 CH	92351828	10.003333	16769519	1718-1715
- 4	0	- Dr	SEA PROPERTY.	SPETIFICS	\$5.688.28	SA SCTEER	1219-0318
	0	12	60.00055#	SCAUSCES.	IN WEGSTER	ET.CTRCCE	00138+0018
1.61	0	9)	EE WESTER	88.790AC8	197290228	TA-ZAMECO	1919
- * -	0	- 10	BERBETSER	SCHREES	85780558	\$1.578628	9910
4	ů.	99	SZ POZEZA	ZY PHÁCES	05 191338	10'CSACCO	\$9536
4	0	49	BE WEERE	INCHORES	ECAMPLES.	88,700A68	P93.96
- 4	0	99	25.005228	00710958	98162528	STSSET OF	CHAR
4	0	91	TW /BEEER	93401039	62.912226	Exchass at	25126
- 1	0.	- 51	29 462229	16'6,0000	TO WHERE	DA PCOVER	1919
- 1	0	13	sertette	TYLESES	ER.TRETER	NE GHOPES	- DAYA
- 1	0	10	#E35246.34	00/216458	835388 85	10 BYONES	637.0
1	0	91	BE ENTER	SYPHETES	802 C) 258	AT TERETS	9518
1	0	- 10	96 21123	TCATACES.	#C.5322228	922668.06	7819
-	0	- 91	AC PUTER	2240ECE8	SP. ECCCCO	92.69600	931M
-	0	21	SY DECEST	92300046	80 145558	99 608119	3318
1	n.	91	19 SUCCES	OCTRACTS	SA HATTAN	STIRRE OF	9918
1	0.	- 11	42 MACEZN	TTRIBACE	#5.000 E28	CC.FWGGG	1518
	0	10			-	_	2318
			621400.58	T1-BURGER	GE AMENGE	80.477.00s	
		- 11	ERTHILE	STATISTICS.	25,543,58	25 C691128	1916
	0	10	STERRIZE	04248024	96 019126	19719219	1916
			18.000 tS8	FC.TOOCES	15,001150	to.actcco.	OSTH
4	0	n.	AE MODITE	L'ATORCES	854643.87	#D.A.\TCC#	6918
- 4		- to	#216843K	CT.TOBGE&	26,637,956	PRACTICA	AFLE
- 1	0	te	A C IZZZEZE	CALIGRACES	20,888258	SA ACTORS	parsi-tack
- 1	0	- 11	co ereice	44 FORFER	06.850158	88.5186c0	BATRACATE
1.5	0	- 0	84.687168	PERMIT	TOALBILL	75,034660	PRIM .
	. 0	D.	TOACETER	VEGRECER	FE-REATES	at geitig	DISE
	0	15	PETERIZE	BESIETES	STORY	40,412320	2996
	0	fearst politim	49.1001SB	SERVICORS	82,140,158	023205.25	1999
(F-94EA1)	(0.0)	Buignipui)	72	XS	- 14	1X	nie.q

Road			nate (m)	-	producting	Height (m)	Road Type (calline 4)
Pair	X1 833126,78	Y1	#23-07.37	¥2 82000-25	mixing room	(m)	(canno 4)
RIGI	833177.37		#DD104	627.545.75	20	0	1
Rúd3			#13414H0		29	0	1
							1
.003	833434.00		#33900.49 #33905.46		29	0	1
RIGI							. 1
RIDA		#22306.10			39	0	-1
F1004		822316.62	83342518	022286.61	38	0.0	- A
M004	833425,10	622396:41	032510.26	022421.58	19	. 0	1
RIDE	833616.28	£22,421.55	851671.75	822496.58		100	1
ROOS	833671.75	822.49 ÷ 58	£33933.47	822414.65	16	. 0	4.
H008	633933.67	022014.00	#33973.71	822424.0¥	19	0	1
WEGS	632973.71		E3404E15	622620.54	18		1
005+Ras7	833527.00	622410 61	633627.55	622455.21	14	0	1
dos-8407	833627.65	822455.21	811712.67	872494.A7	18	0	1
							1
604-R607	633732-07	822494,47	81079244	922441.65	14	- 0	
404-9407	833762,11	622441,65	\$13,840.61	822456.02	34		1
003-R105	E23664 17		\$25 EB 2.59	622497.15	13	- 0	1
dole-Reput	\$33693.50	822397.15	ELIMANA	822456.38	13	0	
010×H011	833V78.40	672463.30		83Z452.88	(1	0	- 1
010+#011	632,819.64	822432:88	832883,54	822462.45	12	. 0	- 3
#1#R=18	\$33@81.54	822A5 E 49	813842.51	822458-02	12	0	- 1
\$12+6813	633387.26	822567-47	833423.59	822556.02	16	0	1
012-R013	833423.00	\$22668.02	835419/06	022462.07	10	000	1
012+R612	833416.08	622402.07	823447A2		10		1
817+R813			£054464		10	0	-
012+H013	833447.62 833544.64	822390.48	811367.56	822354.50	16	0	1
					16		1
014-1015	6334EE 77		#12M17.6#			0	1
\$14-R\$17	833587,56	\$22354:III		622374-91	15	. 0	1
015+9917	103611-17		41364147		15	0	1
Rist	8330k2.67	822192.93	311219.07	822239.71	18	. 0	1
M621	#30/209-01	6222219:76	813395.00	022293.72	36	. 0	1
R102	E38355,80	£22291.72	\$35400.61	6225A0.13	38	0	1
R1122	EDDAEG 61	#22340 tJ	22549.44	622218.75	16	0	1
PH423	W33072.42	422113.68	EXPRISES.	822129.45	14	0	7
H024	633100.63	617179.44	#13232:04	SITITS.O7	74	. 0	1 4
R825	8222228	622176.ST	\$13377.50	621432.03	74	0	1
Rujs	E33377.80		83350334	822278.92	18	0	1
M027	633503.91	922278-46	RMMINE	022341.72	13	0	1
M028	813675.82		849768-11		13	0	1
R129	833766.03	£22374.16	\$\$154E76	622405.73	- 15	- 00	- 1
Reso	\$33848.76	E22405.79	EE1917.E3	\$22431.11	18	0	- d.
H621	633917.63	972431.14	#30946/68	822454.1E	14	0	- 1
017/4101	89.910CE9	\$2200.0.71	BTO COLUMN	#EE072.07	18	0	3
REST	833121.79		#ED252.16	622120.94	78	0	- 1
WAY'S	633251.39	822120.94	#2539E77	622175.17	- 0	0	1
Rúss	633394.77	#22175.47	833524.35	#22221.21	- 10	0	- 1
M034	823524.35	1000131	632062.40	622289.00	10	0	1
9627	623653.40	62229-9.00	A12694.86	622284.07	15	0	-
						0	1
RESIR	833664.68	622284.56	613762.79	622339.51	96		
RUSE	A337E4.68	622311.12	#23795.AC	82232674	- 12	0	1
H040	833789.11	622316.09	#35003.18	0.22.125.11	18	0	1
R042	823833.10	822 235 17	\$53,912.94	022360.5T	16	0	- 1
R142	8338E8	#22380.57	94-2090/18	822120.A5	18	0	- 1
Risks .	633050.46	222120.4E	E34E14.00	#27250.52	48	0	1
8044	E34034.90	\$22250.62	#3454 042	012162.07	18.	0	- 1
2545	824145 62	\$12 M LAT	83423376	822581.45	19	0.	-
RISAR	E2A231.72	622084.65	634323.21		1,0	0	1
	839322.77	\$27010.KB	EMBARI	821999.48	16	0	1
RUNT HOSE		621010.68 621165.43		821999.A8	12	0	1
	#33097.20						
R549	X33155-56		83343430		18		,
RISS	E20101.47		83327446		71	-0	-1
RUST	633274.50		RELADE 70		- 18	. 0	- 1
R061	633434,10	822080:21	83386673	822174.73	98	0	1
R053	133,784.85	\$22120.44	#\$3738.5Q	622193-24	58	. 0	1
R955	\$33756.FE	622165.28	\$1500E33	AZZ17AJD	16	0	1
RIGS4	432419.43	622967.29	SHAME?	822122.03	18	0	
9054			#3364#A5		18	0	1
ROSA	823649.55		#136F26#	622152.80	18		1
RIGH4	E330E3.68		811713.66		18	0	- 1
RODA	633713.85		832757.83		16	0	1
DOSA .	633713.85	822140.82 822128.66	83375783	#22128.05 #22113.30	16	0	1
11927							
Ross	823786,53		811072.14	622051.39	39		- 1
RIBS	83377E.49	622113.86	831M7.20	822639.12	16	0	7
HIGHT.	833873.20	\$32642.68	134119.21	\$21\$14.TT	16	0	1
ROSE	834159.21	12161478	W34250.10	821708.42	18	0	- 3
9.039	833867.29	422039-21	63485E34	621690 22	-37	0	1
Auso	83405E34	#21380.7Z	234261Æ1	821727.A5	48	0	1
8061	833115.37	821680.26	8221976	821609.31	16	0	1
		\$21889.31	613216.78	021947.79	50	0	-
R082	623339.76						1
Rob2	833294.88	621947.56	6134(0.51	822607-91	96	0	1
ROSA	A33460.49	#22568 k)	#31543.73	82200M.72	18	0	7
H004	823541.73	63293E72	#33861.70	#21985.51	15	0	- 1
R064	823480.98	\$21952.82	932543.70	821962.31	18	0	- 1
Brief.	833160,17	#21834.GT	\$1539.556	821691.67	16	0	1
M066	\$33316.96	221391.6E	833491.00	821652.75	16	. 0	1
ROBT.	833184.01	\$2177 b.07	032 178 AT		19	0	1
MORE.	823175.74	621782.16	853293AB	821613.88	18	0	1
RIGHT.		621787.67	813251,68			0	- 4
			E13210.16		13	0	1
Refo							

										Val	iela count	for each r	nad										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr05	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	He16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
1250	500	550	400	450	650	1650	4900	5500	4650	4700	1950	3600	3500	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1.750	800-	550	400	450	650	1650	4900	5500	4650	4200	3950	36210	3600	3800	4000	4.750	4800	4900	4150	2750	2600	2550	1750
1250	800	550	400	450	650	1650	4900	9500	4f50	4200	3950	3800	3600	3800	4000	4350	4800	4900	4150	2750	2600	2550	1750
1250	1900	550	400	450	650	1650	4900	5500	4650	4200	3950	3800	3600	1800	4000	4350	4800	4900	4150	1750	2500	7550	3750
1250	800	550	400	450	650	1650	4900	5500	4650	4200	1950	3600	3E00	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1100	700	500	350	400	600	1500	4350	5150	4200	3950	3750	3500	3650	3900 3900	4250	4700	5350 5350	5500	4750 4750	3100	3000	2950	2000
1100	700	500	350 350	400	600	1500	4350	9150	4200	3950	3750	3500	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3650	1900	4200	4700	5350	5500	4750	1100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	- 5350	5500	4750	3100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	5350	5500	4750	3100	2950	2950	7000
1190	.700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3690	1900	4200	4700	5350	5500	4750	3100	2950	2950	2000
17	10	6	4	4	7		60	69	71	32	73	100	100	100	200	62	70	67	64	59	58	31	25
17	10	6	4.	- 4	7	. 18	60	69	71	72	73	100	100	100	100	68	70	67	- 64	59	- 58	- 31	- 25
- 17	10	- 6	4	4	7	18	60	69	71	72	73	100	100	100	100	- 65	70	67	64	.59	58	31	- 25
17 63	10	13	4	10	16	18	50 73	69 150	71	72 150	73 150	100	100	100	100	100	70	57 100	100	59 100	58 74	72	37
62	22	В	Б.	10	16	62	73	150	150	150	150	150	150	150	150	100	100	100	100	100	74	72	37
100	72	30	-21	24	38	100	200	350	400	350	350	350	350	150	350	250	100	350	750	150	150	150	100
100	72	31	. 21	24.	38	100	200	350	400	350	350	350	350	150	350	250	300	350	250	150	150	150	100
100	72	31	21	24	38	100	200	350	400	350	350	350	350	350	350	250	300	350	250	150	150	150	100
7	- 1	2	1	1	2	7	- 12	25	27	24	23	25	26	30	29	23	32	35	27	20	16	14	11
7	- 1	2	1	1	1	7	12	.25	27	24	23	25	76	30	29	23	32	- 35	27	30	36	14	11
7	1	2	1	1	2	7	12	25 25	27	24	23	25	26	30	29	33	32	35	27	20	16	14	11
7	3	7	1	1	3	7	12	25	27	24	23	25	26	30	29	23	32	35 35	27	20	16	14	11
66	v	16	12	13	20	- GR	100	200	200	150	150	150	150	150	150	100	100	150	100	100	100	100	72
66	26	16	- 11	12	20	67	100	200	200	150	150	150	150	150	150	100	100	100	100	100	100	100	-65
66	26	16	11	12	20	67	100	200	250	150	150	150	150	150	150	100	100	100	100	100	100	100	45
-50	50	16	- 11	13	19	-50	100	200	290	200	150	150	150	150	100	50	100	50	50	50	50	50	21
50	50	50	14	16	24	50	100	250	250	250	200	200	300	200	500	190	200	200	150	100	100	100	50
50	50	17	12	14	20	50	100	200	200	200	200	200	200	250 250	250	200	250	250	200	150	100	100	100
50	23	17	11	11	17	50	100	200	290	200	200	250	250	300	300	250	400	450 450	350	250	200	200	150
50	22	12	3	11	16	90	100	150	200	200	200	200	250	100	300	250	150	400	300	250	200	150	150
50	50	18	12	15	21	50	100	200	250	250	250	300	300	350	400	300	450	500	400	300	250	200	150
50	50	17	12	1.4	20	:50	100	250	250	250	250	250	250	300	300	250	350	350	300	200	150	190	100
100	50	50	72	25	50	100	200	350	400	350	350	350	350	450	400	350	450	500	400	250	250	790	150
50	23	15	10	11	16	50	100	150	200	200	200	200	200	750	250	200	300	350	250	200	150	150	100
50	15	9	6	. 8	10	50	50	150	150	100	100	100	100	100	100	100	100	100	100	50	50	50	50
50 15	50	24	17	19	50	50	150 50	300 100	350 100	300	100	350 100	350 100	100	100 100	300	450 150	500 150	100	100	250 50	200	150
106	105	51	54	54	- 55	108	320	450	450	378	371	421	419	469	404	519	619	618	463	150	308	258	205
200	150	100	100	100	150	200	550	800	750	700	650	750	750	850	900	950	1150	1200	900	650	550	500	350
200	150	100	1.00	100	150	200	550	850	800	700	700	750	750	850	950	1000	1200	1200	950	650	550	500	150
300	250	200	200	200	256	400	900	1400	1350	1150	1050	1100	1090	1100	1150	1150	1300	1300	1000	706	600	250	400
350	300	250	250	250	250	450	1050	1650	1550	1150	1250	1300	1300	1400	1450	1450	1700	1700	1300	900	750	700	500
300	250	200	200	200	200	350	890	1950	1250	1100	1000	1050	1000	1050	1100	1100	1250	1200	950	£50	550	500	350
300 200	250 150	200 150	200 150	200 150	150	350	900 650	1000	1250 950	1100	750	1050 750	750	1100	1100 800	1150	950	1300	700	700 500	400	550	250
200	150	150	150	100	150	250	550	900	850	700	650	650	650	650	650	650	750	700	550	400	350	300	200
700	150	150	150	150	150	250	700	1050	1000	850	750	800	750	800	300	800	900	850	650	450	400	350	230
250	200	200	150	150	200	350	900	1250	1150	1000	950	1000	1000	1050	1100	1150	1350	1350	1050	700	600	550	480
150	150	100	100	100	1.00	200	450	500	700	600	550	600	600	650	70G	700	850	850	650	450	400	3090	230
200	150	150	150	100	150	250	550	900	850	750 500	700 500	750 550	700	750	300	#50 650	950 750	950 750	750	500	350	400	300
150 200	150	100	150	100	150	250	400 600	900	850	750	700	750	700	600 800	800	IISO	950	950	750	400 500	450	490	300
200	150	100	100	100	150	250	550	300	750	650	650	700	650	700	750	800	900	900	700	500	400	350	250
650	500	450	450	400	500	850	2000	3100	2900	2450	2200	2250	2150	2250	2250	2200	2500	2350	1,800	1250	1050	950	790
550	450	400	400	350	450	700	1700	2650	2900	2950	1850	1900	1750	1800	1750	1700	1900	1750	1350	950	800	700	500
650	500	450	450	450	500	800	1950	3000	2050	2450	2300	2450	Z350	2550	2650	2700	3150	3100	2400	1650	1400	1300	900
550	450	350	350	350	400	700	1650	2500	2350	2050	1850	1950	1900	2000	2050	2100	2450	2350	1,800	1250	1100	950	780
350 400	300	250 300	250 250	250 250	300	450	1100	1700	1600	1890	1250	1350	1500	1700	1750	1500	1750 2150	2100	1650	1150	950	700	500 600
400	300	300	250	250	300	550	1250	1950	1850	1600	1500	1600	1550	1700	1750	1800	2150	2100	1650	1150	950	900	500
450	150	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650
4503	350	300	300	300	350	550	1350	7050	1950	1650	1550	1650	1600	1750	1300	1250	2200	2150	1650	1,150	1000	900	630
450	150	300	300	300	350	550	1350	2050	1950	1650	1950	1650	1600	1750	1800	1950	2200	2150	1650	1150	1000	300	650
450	350	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	23,50	1/650	1150	1000	900	650
450	150	300	300	100	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650 650
500	400	300	350	150	400	650	1500	2050	1950	1900	1750	1850	1750	1850	1900	1890 1950	2200 2250	2150	1700	1150	1000	900	650
250	200	150	150	150	200	300	750	1200	1100	950	900	950	950	1000	1050	1050	1250	1250	950	650	550	500	150
350	250	250	250	250	250	450	1100	1650	1550	1300	1200	1250	1200	1250	1250	1250	1400	1350	1050	700	600	550	460
300	250	200	700	200	250	400	950	1500	1400	1200	1050	1100	1050	1100	1100	1300	1200	1150	900	600	550	500	150
200	150	150	150	150	150	250	600	950	900	800	750	800	800	900	950	1,000	1200	1200	900	650	550	500	150
200	150	150	150	150	150	250	600	900	850	750	700	800	750	850	900	900	1100	1100	8.50	600	500	450	500
50	50	14 50	9 18	20	16 50	100	100	150 300	350	300	150 300	300	150	150	300	250	100	350	100	300	150	50	100
50	20	13	10	10	15	50	100	150	150	150	150	200	200	200	200	290	150	300	200	150	150	100	100
50	21	13	3	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	50
50	21	13	- 4	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	400	50	50	50
50	- 21	13	3	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	30
50	50	17	12	14	.20	50	100	200	250	200	200	200	150	200	150	150	150	156	150	100	50	50	50
-50	50	21	15	17	24	- 50	100	250	250	250	250	250	250	30G	300	250	350	400	300	200	200	250	100
1500	1200	1000	1000	950	1150	1900	4450	4750 4750	4750 4750	4750 4750	4750	4750 4750	4750 4750	4750 4750	4750 4750	4750 4750	4750	4750 4750	4750 4500	1150	2850 2650	2600 2400	1800
1350 950	1100 750	950 650	900	600	1050 700	1750	2850	4750	4100	4750 3600	4700 3400	3600	3550	3900	4050	4750	4750 4750	4750	4500 3800	2650	2650	2050	1700
400	300	250	250	250	300	500	1200	1800	1700	1450	1350	1400	1.850	1450	1450	1500	1700	1650	1750	300	750	700	500
						- Sale			2.00		1100	2.00			2.30				2.30			- 34	-10

Pair	X1	Y1	rate (m)	¥2	proclusting	Height (m)	Road Type (calline 4)
REF	B393E7.91		82339724		mixing room!	0	formin 4)
8972	E33597.24	821875.22		821697 AT	20	0	1
			#39307.24		- 17	0	1
- HIDTA	X33251.04		#33451A0		70		1
			#17444.00		76	0	
RU78	E33501,4E	44109100	********	021002.00	18	0	
		421097.00	\$2160241 61200241	821699.37			1
R076	833548.66				16		
M074	R33693.43	621685/99	83369492	621622.32	14	. 0	1
R877	E33564.57	521684.14	#51562.57	821654.38		100	1
R077			833605.68		12	0	4.
H077	A33.600.48		¥33973.44	#21812.0F	17	0	1
MOTA	\$358£1.3E	621822:35	853875.52	821560.F5	16		7
R679	833673.29	623391.43	833597.51	821651.48	16	0	
Riddo	\$33675.67	821661-18	833999.54	821457.98	16	. 0	1
M081	633667.01		932993.08		30	- 0	1
M082	833A58.18	621884.41	813510.76		34		- 1
RRB2	82351G.75	627821.12	611508.16	621785.93	-	- 0	
HOEZ:	833516.79	821785:33	E11570.13	821667.55	14	0	- 1
						0	
HOET	633424.63		#33.416.1B		18		1
MOE2	\$13,499.18	621813.12	83352436	821772.29	14.	. 0	- 3
H192	\$33524.38	821772.26	813519.61	821652.62	34	0	
MONA	633567.54	821687.02	83156240		15	0	1
M094	813682-0)	\$21644.05	052007.71	021603.07	13	000	- 1
Rost	833009.34	\$21605.64	81354024	021675.52	14		1
H193	\$33640,24	623578.52	£13691.67	621645.20	12	0	
moss	\$33.681.67	821545.20	833729.52		14	0	- 1
HORE.	633,060,70		#32003.89		12	0	1
ROPE.	823 6C3 8E	821583.58	533646.83		12	. 0	1
			#3364F16		12	0	1
					17		
MUSE	833254-24		833345.50				· · ·
M1966	#33365.50	621650-04	833416.50		12		4
8.52.6	E23416.50		£\$3497.£3		17	-6-	4
RIBS	E334E7.63	821841.09	£33,533.43		17	10	
FORE	8355142		E33574:E0		17	- 1	
more.	\$33,074.00	621697.75	832600,18	821605.82	17	1.00	
Ross	823666.16	621505 62	613712.68	621511.11	. 32		4
RIBS	E33256.85	821501.44	E33370-00	821685.B7	18		
F1089	633 370.08	221046.87		821652.03	16	1.7	4
			83341949		16	- 1	4
Ritas	833459.60	621829.25	853522.46	621786.30	18	- 10	4
mons .	833522.46		E11343.19	021780.30		0	
		821786.32	E13343/19	821725 A7	16		- 4
HOSE	83354119				16	3.	
HOER		121633.37	111515.05		16		4
	823599.99	621594.64	41369251		16		4
FICKOVE DY1	833264.78	821629.64	823337.54	821634.10	97	0	- 1
R692+8991	633337.92	#21632.93	833449.56	8216A9.31	30	0	1
N092-R093	833449.50	921640.21	632512.09	021599.24	30	0	1
2004	633337.84		855341.61	821678.41	10	0	1
Riss	833604.59	421501 TZ	613598.49		42	0	- 1
RS95+R397	623080.55	622 AS A 38	#3402E77	822414.27	10	0	1
100 A - 11 00W	634028.77.	822414.27	E34117.E2	822302.11	18	0	1
#100+R101					18	0	
	834127.62		8342(8.7)				- 1
R192+R101	834216.31	#22258-35	SERVENES	822190.58	18	0	- 1
	634309.95		BBIQUTAG		48	0	1
R106	£33917.63	\$22431.11	E52891.74	012109.38	18.	0	- 1
B127	1223111.55	622370.04	834/00/23	822287.53	- 0	0	. 1
R108	H24090.84	622784.06	8349134	822212.22	36	0	- 1
Rise	839181.08	82221E 22			47	. 0	1
WHE	K14273.34	422134.63	63436436		12	0	1
2157	E24363.46		834400.74		- 18	0	1
B117	ED646.78	622A05.79		822.000.57	18	-0-	1
RH11			ST/865/80		18		1
							- 1
R114	613,909,65	822271.56	855W14.47		18	0	1
RIS	\$33994.08		#34@17.01		18	. 0	1
RITE			\$34W730		18	0	1
RHIT			EXCHAIN		18	0	
RITE			834245.29		- 19	0	- 1
RUY	824242.94	621993.85	654282.16	021951.A5	- 12		1
R120	E34281.93	821981.17	634359.17		78	0	1
P121	623768.03	22227 E. 66	833789.46		16	0	- 4
R(22	613761.08	812351.12	\$33668.78		18.	0	1
R122	822656,78		512954.75		- 18	- 0	- 1
R134	833671.82	622341.72	825ma.66	822284 DZ	16	0	-
REZS	#33671.92 #33694.80	\$2738 4.07	#33#17.77	822172.05	18	0	1
R128	833093.40	822269.00	#33M633	822174.73	- 12	0	- 1
	823455-65		61750251	BEEDBAS	-16	0	- 1
R127	833503.61	22127 E-66	SENERAL S	822221.25	- 68	0	1
#128	633377.60	822232.03	#10255.00	022203.72	18	0	1
		622232.63	A153+8.77	620175.17	18	- 0	1
#128	623377,80		613434.10	622000.76	36	0	1
R128 R120 R120		422175 D4		622007.07	18	0	- 1
R128 R128 R120 R121	833396.42	822175.04 822085.70	#11444 FF		18		1
R128 R120 R120 R121 R132	822394.42 833421.62	#22080.7V	#23415.51	White or			
R128 R120 R120 R131 R132 R133	833396.42 833433.62 833460.45	82208070 832007.88	#33481.00			0	
R128 R120 R120 R121 R132 R133 R124	833396.42 833431.02 833480.45 823481.00	#22080.70 #32007.00 \$21952.76	933481.00 932506.97	821982,08	- 18	0	- 1
R128 R129 R120 R121 R132 R133 R134 R128	833396.42 833433.62 833460.45 823481.00 823205.67	82208070 82200708 82195278 82222978	#33481.00 #32606.97 #13232.66	821982,08 822178.01	78	0	1
#128 #129 #120 #121 #132 #133 #124 #125 #126	833396.42 833431.02 833480.45 823481.00	622080.70 632007.00 521952.76 622239.78 822178.06	#33481.00 #32506.97 #13232.56 #33252.36	821882.08 822178.01 822120.04	- 18	0	1
R128 R129 R120 R121 R132 R133 R134 R128	833396.42 833433.62 833460.45 823481.00 823205.67	622080.70 632007.00 521952.76 622239.78 822178.06	#33481.00 #32606.97 #13232.66	821882.08 822178.01 822120.04	78	0	- 1
#128 #129 #120 #121 #132 #133 #124 #125 #126	833396.42 833431.92 833460.45 823481.00 833205.07 6332232.03	622068.70 632007.00 821952.76 622239.78 822178.08 622182.63	#33481.00 #32506.97 #13232.56 #33252.36	821882.08 822178.01 822120.04	18 18 18	0	1
R128 R120 R120 R121 R132 R133 R124 R128 R136 R137	833396.42 833423.62 833460.45 833481.00 833205.67 833202.03 833202.03	#22080.79 #32007.09 #321052.76 #22239.76 #22178.08 #32182.63 #32129.64	#33481.00 #32506.07 #13202.66 #33202.04 #33400.63	821982,08 822178.01 822120.08 922120.48 822072.01	78 78 78 78	0	1

			_							Vat	icle count	for each r	pad					_			_		
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hros	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
450	350	300	300	300	350	550	1300	7.000	1900	1650	1500	1500	1500	1650	1650	1700	1950	1900	1450	:1000	850	800	550
200	150	150 150	150	150	150	250	750	900 1100	850 1050	750	700	750	750 800	900	850	ESO	1000	1000	500	558	450	400	390
250 250	200	150	150	150	150	300	700	1050	1000	900 #50	800	850	800	900	900	950 950	950	1050	700	500	500	350 450	300
150	150	100	100	100	100	200	450	750	700	600	550	550	550	550	550	600	650	650	500	150	300	250	200
150	100	100	100	100	100	200	450	700	650	550	500	550	500	550	550	600	650	650	500	350	300	750	200
150	100	100	100	100	100	200	450	700	650	550	500	550 550	500	550	550	500	650	650	500	150	300	250	200
300	100 250	200	200	200	250	400	950	1450	1490	1200	1100	1150	1100	\$50 1150	550 1200	1200	1400	1350	3050	350 750	300 600	250 350	460
300	250	200	200	200	250	4/30	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	250	400
300	250	200	200	200	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	350	400
150	150	100	100	100	100	200	500	.750	700	600	550	550	500	550	550	550	600	600	450	300	250	250	150
250 150	200 100	150	150	150	100	300	750 450	1150	1300 650	950	850 500	900 550	550	900 600	900	950	1050 750	1050	550	550 400	450 350	300	300 200
250	200	200	200	200	200	350	800	1250	1200	1050	950	1000	1000	1050	1100	1150	1300	1300	1000	700	600	550	400
200	700	150	150	150	150	300	650	1000	1000	850	750	-800	750	800	950	150	950	950	700	500	-400	400	250
200	200	150	150	150	150	300	650	1000	1000	350	750	800	750	BOC	850	850	950	950	700	500	400	400	150
200	200 50	150	150 50	150 50	150 50	300 100	650 250	1000	1000	850 350	750 300	800	750 300	100	850 300	850 300	950	950	700 250	500 450	400 150	400	150
100	50	50	50	50	50	100	250	600	400	350	300	300	300	100	300	300	300	300	250	150	150	150	100
100	50	50	50	50	50	100	250	400	400	350	300	300	300	300	300	300E	300	300	250	150	150	150	100
200	200	150	150	150	150	300	650	1000	950	850	750	800	750	850	850	eso	1000	950	750	500	450	400	300
200	150	150 150	150	150	150	300 250	650	1000	950	MSO BIGO	750 750	800 750	750 750	#50 800	900	#50 800	900	950	750 650	900 450	450	350	250
200	150	150	150	150	150	250	650	1000	950	800	750	750	750	800	800	800	900	900	650	450	400	350	150
250	150	150	150	150	150	250	650	1000	950	800	750	750	750	600	800	800	900	900	650	450	400	350	250
100	50	50	50	50	50	100	250	400	400	350	300	300	300	300	300	300	350	350	250	200	150	150	100
100	100	100	100	100	100	100	250	500	500	350 450	300 400	300 400	400	300 400	300 400	300 400	400	450	250	200	200	150 190	100
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	2850	3150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	890	600	400	400	650	3400	2950	3600	3600	3200	3100	2950	2890	3150	3250	3250	3600	\$600	3200	2650	2500	2,900	1960
1200	850 850	600	400	400	650	1400	2950 2950	3600	3600	3200	3100	2950 2950	2850	3150 3150	3250 3250	3250 3250	3600	3600 3600	3200	2450 2450	2500 2500	2600 2600	1950
1200	890	600	400	400	650	1400	2950	3600	3670	3200	3100	2950	2890	3150	3250	3250	3600	3600	3200	7450	2500	2600	1950
1200	850	500	400	400	650	2.400	2950	3600	3600	3200	3100	2950	2850	3150	3250	3250	3600	3900	3200	2450	2500	7600	1950
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2990	2950	1150	3250	3250	3600	3800	3200	2450	2500	2600	1950
850	600	400	300	300	450	1000	2100 2100	2850	2750	2400	2400	2350	2300 ·	2650	2750 2750	2800 2800	3450 3450	3600	2900	2200	2250	2350	1750
850	800	400	300	100	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3800	2900	2200	2250	2350	1750
850	500	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	2.500	2650	2750	2800	3450	3800	2900	1700	2250	2350	1750
850	600	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	Z300	2650	2750	2800	3450	3800	2900	2200	2250	2350	1750
850	800	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	2300	2650 2650	2750	2900 2900	3450	3800	2900	2200	2250	2350	1750
850	600	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	1100	2250	2350	1750
350	250	250	250	250	250	450	1050	1600	1500	1250	1100	1200	1100	1150	1150	1150	1300	1200	950	650	.550	500	150
250	200	150	150	150	20G	350	750	1150	1150	950	900	900	850	90G	900	950	1000	1000	750	550	450 450	400	300
250 50	200 50	50	150 50	150	200 50	350	750 200	1150 300	1150 300	950 250	900 200	900	200	200	200	950 200	1000 750	250	150	550 100	100	100	300 50
100	100	100	50	50	100	150	350	500	500	450	400	400	350	400	400	400	400	-400	300	200	200	150	100
57	19	- 11	7	7	14	57	64	150	150	150	150	150	150	150	150	70	150	150	121	68	63	62	58
100	-56	73	34	20 40	100	150	300	900 600	300 650	300 550	250 500	250 550	250 500	550	250 550	350	250 500	500	250 450	200 250	150 250	150 250	150
1.00	100	22	16	16	26	100	150	250	300	250	250	300	300	300	300	250	350	350	250	200	200	150	100
71	27	16	11	11	19	72	100	200	200	290	20G	250	250	250	25G	290	50G	300	200	150	150	150	100
50	50	24	17	20	50	50	150	300	300	300	250	250	250	300	250	200	300	300	250	150	150	100	100
50	50	20	14	16	50	50	100	250	300	200	200	200	150 200	200	200	150	200	200	100	100	100	100	50
50	50	21	15	16	24	50	100	250	250	250	200	200	200	200	150	100	150	100	100	50	50	50	50
103	50	50	20	- 21	50	100	150	850	350	300	250	250	250	250	200	150	150	150	150	100	100	50	50
50	50	23	17	18	58	9)	150	300	300	250	250	200	200	200	200	150	150	150	100	100	50 200	50	50
50	22	12	10	12	17	50	100	150	200 150	280 150	200 150	150	250 100	150	300 100	250 100	100	100	100	30	200	200 50	30
200	100	50	50	50	100	200	450	850	950	850	750	750	700	800	750	550	700	750	550	400	350	300	250
200	100	56	50	50	50	200	400	750	850	750	700	700	650	750	700	550	700	750	600	400	350	300	230
200	100	50	50	50 50	50	200	400 350	700	850	750 700	700 650	700 650	700 650	750	700 650	550 500	650	750	550	400	350 350	300	250 250
200	100	50	50	50	50	200	350	750	800	750	700	700	700	1000	750	600	800	850	700	500	400	350	300
200	100	50	50	50	100	250	450	900	950	E50	800	800	200	850	900	650	800	850	700	500	400	350	.180
250	150	100	50	50	100	250	500	950	1050	950	900	900	850	950	900	700	900	950	750	500	450	400	300
100	13	50	50	50	30	100	200	100	100 450	100	400	400	400	150 500	150 450	350	500	350	150	300	250	100	300
50	50	22	15	17	.50	30	150	250	300	250	250	250	250	300	300	200	300	350	250	200	150	150	100
50	50	20	34	16	23	50	100	250	250	200	200	200	200	200	500	150	150	150	100	100	50	50	50
50	50	20	14	16	23	50	100	250	250	250	200	200	200	200	200	150	200	290	150	100	100	100	50
50	50 23	15	15	16	16	50	150	250 150	300	250	250	300 200	300 200	350 250	350 250	300	250	450 300	350 250	250 150	700 150	200 100	150
50	50	18	. 14	15	- 21	- 50	100	700	250	250	250	250	250	500	300	250	350	400	300	200	200	250	150
150	100	100	100	100	100	200	400	650	600	500	450	500	450	500	500	500	600	.550	450	500	250	250	150
200 300	190 250	200	206	100 200	150 250	400	550 900	1400	1300	700 1050	950	950	900	900	700 850	700 850	900	800 800	650	400 458	350 350	300	250 250
290	150	150	150	150	150	250	550	250	800	700	700	250	700	500	800	BSO.	1000	1000	750	950 950	450	400	100
200	100	50	50	50	100	200	350	750	600	750	700	700	700	500	750	500	600	850	700	500	400	350	500
200	100	100	50	50	100	200	400	800	960	850	800	850	H50	950	950	750	1000	1100	900	600	500	450	350
- 6	6	3	1	1	3	7	13	50	50	50	50	50	50	50 50	50	50 50	50 50	50	50	22	26	19	13
8	4	3	1	- 2	3	9	17	50	50	50	50	50	50	50	50	50	50	50	50	21	17	16	13
1	4	3	1	-2	3	9	17	50	- 50	50	50	50	- 50	50	50	50	50	.50	50	21	17	16.	18
100	50	50	24	50	50	100	200	400	450	400	400	450	450	550	550	400	500	650	500	350	300	250	200
100	50	50	- 50	50	50	100	200	450	450	450	450	500	500	600	600	500	650	750	600	400	350	300	250

Road		Coordi	nate (m)	-	Width	Height	Road Typ
Pair	X1	Y1	X2	¥2	(including	(m)	(caline 4)
Rist	B30294.35	521947.25	885315.56	821631.57	13	0	1
B162	H33329.89	621853.67	ED315.94	821891.04	13	0	7
RIAS	HXX129.75	421489.31	#33465.67	#21#34.07	- 13	0	1
TIME	XXX160.17	621834.07	#33.978.74	821783.18.	13	0	- 1
PLES-RIAL	H2381Z.49	621976.58	\$34\$P458	621516.03	-32	0	1
2117+2180	E33734.44	#21806:3K	\$2100112	821727.34	18	0	-1
R148	833728-61	921749:AZ	632607.73	821684.38	14	- 0	- 4
R149	833774.00	621643.62	032807.73	821684.38	13	0	1
R150	833755.67	#21784.Z3	853687.71	821603.81	- 0	0	1
R151	\$33612.61	421410.98	833663.50	821643.70	13	0	- 4
R151	WINDERS OF	621543.70	¥3377628	#21842.83	14	0	1
W192	835774.08	621443.52	\$1587£17	821500.58	28	٥	- 1
R193	823991.31	622300.76	83467877	622454.27	78	0	1
R194	\$33950.66	222320-65	RESWIZED	\$22189.07	18		1
8198	£337009.40	1427271.31	X33900.66	932130.45	16	0	4
#186	833464.78	622222.16	#11M09/85	022277.30	18		1
B197	E23666.58	622222.14	62380777	622172.98	78	0	-
R153	833827.77	822172.95	#1577B.44	\$22113.30	18	0	-
Kitt	634070.01	622299.62	EMNIXED	622384.34	18	0	1
RIES	834090.38	\$2228FA3	#345776T	622332.11	16	0	- 3
RIGIT	E34034.00	#22250.52	834075.91	622209.62	15	0	1
R162	634049.42	822236.28	EMB/039	822287.53	15	0	1
					- 10	_	
#163	E30 990.00	622201.68	E34534.00	010354.01		0	1
R164	834007.86	622194:33	#34/94%AZ	025EM:20	75		1
R165	E23951.31	622151.78	£25994.47	622221.23	3,6	0	1
R158	835872.14	822651.39	8219647.6	822196.50	18	0	- 1
RHZ	633,683.47	822042.45	#34007.E8	82218E33	18	0	1
R163+R169	833815.72	121275-07	EDIFER	SETSSDAY.	21	. 0	. 1
#171=R171	E33756.44	821898-35	833812-49	821Y78:50	18	0	1
R172+R173	833864.92	821823.12	811719.26	821407-65	26	. 0	-1
物でかれびき	#33061,7E	621407.56	£12M(3:34)	821,623.58	38	0	1
804	E38496,77	f2),600,49	\$33560.47	621680.73	20	-0-	1
R177	E33547'08	821599.24	\$31.63.TE	62168E.42	29	0	1
RITE	X35440.44	621525.00	EX2408.60	#21908.41	16	0	· T
.003	\$23451.04	421424.31	#3541173	821400:38	12	0	7
8190	E34218.31	622286.35	\$54X75.90	622585.39	18	0	1
R191	E24181.98	822212.72	83421831	822258-36	18	0	1
R182	K3A140-62	822162.47	834191.76	022212.38	16	0	1
W-182	E34099,34	622113.33	E34440/62	022162.07	18	-0-	1
R134	E3A077.01	522132.66	#\$48E1.51	622180.94	15	- 0	- 1
R184	STATIST	822100.94	83487134	\$22094.18	13	0	· · · · · · ·
Kina.	#34071.00	07208 s. 18	E34007.30	822115.02	14	0	1
H165	834369-95	\$22180.68	E3439246	822267.44	- 10	0	
8.94	E24221.54	622364 63	EM27134	622136.83	19	0	
RIAT	834190.59	822037.71	8362D176	622086.A5	- 91	0	- 1
R189+R199	824004.93	#21815-03	834H5534	82100.22	96	0	1
R190-R191	B33921,12	921727,74	E34004.08	021816.03	39	0	1
#192+R (92	633876.32	621660.75	#45KH0.65	621727.50	29	0	1
R394-R 195	833825,79	621600.86	823B751	621631.AB	20	0	4
RISS+RINI	A337E1.01	621523.18	#200517	\$21450.58	20	0	- 1
RIST	634364.00	622040.04	E3440E11	82210471	17	0	1
RISE	834323.77	822010.66	8343M436	822060.94	18		- 4
R199	839291.93	421961.17	E34323.00	622015.AB	-38	0	- 1
R100	834239.47	#21914.12	834210.06	821983.18	-14	0	1
	834239,47	821914.13	E34327.65	021540.33	18.	0	- 1

										Vet	ricle count	for each	road	-				-			_		
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	16	10	7	8	12	50	50	100	150	150	150	150	200	750	250	200	100	350	250	200	150	150	100
50	22	14	10	11	17	-5D	100	200	290	200	150	200	200	200	200	150	250	250	200	150	100	100	100
150	50	50	50	50	50	150	250	550	600	500	500	450	450	500	450	350	450	A50	350	250	200	- 200	130
100	50	50	50	50	30	100	250	450	500	450	400	400	400	450	400	300	400	400	300	200	200	150	130
24	13	- 8	. 5	7	10	25	63	100	150	124	122	123	322	174	172	117	222	. 224	168	113	11.1	110	. 58
-57	18	12	ä	9	13	58	65	150	150	150	150	150	150	150	150	100	200	200	100	100	100	100	100
17	- 9	5	4	4	7	-18	50	50	50	50	50	-50	90	50	50	50	50	- 50	22	16	13	12	9
17	9	5	- 4	4	2	118	50	50	50	50	. 50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	5	4	.4	7	- 10	50	50	50	50	50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	- 3	4	4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	25	16	13	12	10
17	9	- 5	4	- 4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	23	16	13	12	10
. 17	9	- 5	4	. 4.	7	18	50	50	50	50	50	50.	50	50	50.	50	50	50	50	.20	17	14	- 11
100	100	100	50	50	'50'	100	250	300	250	250	200	200	250	200	200	200	200	200	150	150	156	100	100
100	100	100	50	50	50	100	250	300	250	250	250	250	300	50G	300	350	350	350	300	250	200	200	150
100	100	50	50	50	50	100	250	300	250	250	200	200	250	200	200	250	250	200	200	150	150	150	100
500	400	350	300	250	250	450	100	800	800	100	800	800	100	800	900	800	800	750	650	550	450	450	350
600	500	400	300	250	300	550	1200	1500	1300	1,200	1100	1100	1150	1100	1050	1050	1050	1000	950	750	650	600	450
500	400	350	300	250	250	450	1000	1300	1100	1050	950	1000	1050	950	950	1000	1000	950	800	700	600	980	450
50	23	18	15	12	15	24	50	50	50	50	50	50	50	50	50	100	100	100	50	50	50	50	50
100	100	50	50	50	50	100	200	250	250	200	200	200	200	150	150	150	150	150	150	100	100	100	- 50
150	150	100	100	50	100	150	350	400	350	350	350	350	400	350	350	400	400	406	350	300	256	250	200
500	150	150	100	100	100	200	400	550	450	450	400	400	450	400	400	450	450	450	350	300	250	750	200
750	200	150	150	100	100	200	450	600	550	500	500	550	600	600	600	650	700	700	550	500	450	400	100
150	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	400	300	300	250	250	700
150	150	100	100	100	100	150	350	450	400	350	350	350	400	400	400	400	450	490	350	300	250	250	200
300	250	200	200	150	150	300	650	850	750	700	650	700	750	750	750	800	850	800	650	530	500	450	350
250	700	150	150	100	150	250	550	650	600	550	550	550	600	600	500	650	650	650	550	450	400	350	300
500	150	300	300	200	200	450	950	1200	1050	1050	1050	1100	1200	1200	1250	1350	1450	1350	1150	1000	850	800	600
150	350	300	250	200	200	400	900	1100	1050	950	950	1000	1150	1100	1150	1250	1300	1250	1050	900	750	750	550
500	400	350	250	250	250	450	1006	1300	1150	1100	1050	1100	1200	1200	1200	1300	1350	1350	1100	950	800	100	600
590	490	350	300	250	250	450	1050	1350	1200	1100	1050	1100	1200	1150	1150	1290	1300	1200	1050	900	750	750	550
350	300	250	200	150	200	300	750	900	800	700	650	700	700	650	650	650	650	650	500	450	400	350	300
250	200	200	150	100	150	250	550	700	600	680	550	600	650	650	-650	700	700	100	600	500	450	400	500
350	250	200	200	150	150	300	700	850	750	700	650	650	700	650	650	750°	650	650	550	#50	400	400	300
350	250	200	200	150	150	300	650	850	750	700	700	750	H00	600	900	900	950	900	750	650	550	950	460
200	150	150	100	100	100	200	400	500	450	400	400	400	400	400	400	400	400	400	300	100	250	250	200
15	12	9	ä	7	8	14	50	-50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	24
50	50	22	19	16	18	50	50	100	100	50	50	50	90	50	50	50	50	50	50	50	50	50	50
50	23	19	16	13	15	24	50	50	50	90	50	50	50	50	50	50	50	50	50	50	24	22	17
50	50	19	16	13	15	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	56	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
103	100	50	50		30					200		200		250		250							100
	19	15		50		20	200	250	200	50	200	50	250	50	250	50	50	250	200	200	22	150	17
22			12		12		50					200		200		150							50
1.00	100	50	- 50	50	50	100	200	250	200	200	200		200		150		150	150	150	100	100	100	
68	63	61	59	\$8	59	64	200	200	200	290	200	200	200	200	200	250	250	250	200	206	150	150	122
100	70	66	64	16	63	12	150	200	200	200	200	200	200	200	250	250	300	250	750	700	200	700	122
42	35	29	24	22	.13	38	100	100	100	100	100	100	100	73	73	70	68	.68	66	66	62	62	31
64	60	58	57	55	56	63	200	200	200	2/00	172	172	171	119	13.7	116	115	114	111	111	58	- 58	57
100	100	70	40	- 33	38	100	150	200	150	150	150	100	150	100	100	100	150	100	100	100	100	100	74
10	7	5	-5.	4	- 4	B.	18	24.	20	17	14	13	12	11	6	3	5	5.	- 4	- 4	3.	1	3
19	15	12	10	8	3	16.	50	50	50	50	:50	50	50	:50	22	23	18	18.	13	13	11.	-0	9
22	18	15	- 13	10	12	- 21	50	50	50	50	50	50	- 50	50	- 50	50	.23	20	18	15	13	12	10
50	50	23	20	1.6	19	50	50	106	100	50	50	50	50	50	50	50	50	50	50	50	50	-50	50
50	50	23	.20	16	19	50	50	100	100	50	50	50	50	50	50	50	50	50	50	30	50	50	50

	(caline 4)	+						-	-																	-		-	I	-	I		Į.				1									-				-	-								+					T.							-							1.4						
	Height		0	0	0		a	0	0				a				9		0	0	a	0	0	6		0	0	0			0	0 0								0	0		a	a	0	0	0	. 0	0	0						0	0		a	0					a	0	0	0	. 0	0	0				0	0	0	0	0					0
	(Including	nazing zonel	20	20	- 32	2.0	- 10	10					**			**			11	17	23	10	10	10	- 10	10	**	12										43		17	14		91	31	- 10		118	83	14						11	- 18	17	16	21	18	91			18	- 16	16	10	16	69	**			91	95	. 91	118	15	18	18	2 :				11
901	V.2	822306258	82234678	822409.45	822543.00	82284£7E	\$22316.62	822288.41	822421.55	20 400 770		813434 K4	#22466.2Y	493,464,49	833454 66	87245A.02	872387.55	675566 14	822432.88	822462.AS	822456.02	822556.02	623462.07	82242539	822380.48	622354.69	822304 ED	822374.91	822398.31	2000000	27755555	64934673	BALANCE OF		*********	E 10 214 61	835 tet 73	822296.83	82240579	822424.11	872464 38	822072.07	#22126.94	822178.17	822221.21	822269.00	822264.07	\$22304.61	822320.74	422339.17	82236857	#22340.45	822167.67	RZZDBEAS	622011.22	821367.68	821977.95	822086.76	\$22007.07	822067.62	822474.73	62247474	822422.03	822344.43	822162.89	522149.92	822128.55	422115.33	822206(3)	822039-12	621814.78	821738.42	624727.44	821889.31	823847.78	122000287	#2200H72	624163.31	821863.31	821891.67	92196276	STATES BY	44120601	\$21882.87
2	ate (m)	83347737	833231.08	833434.80	833969.46	83198546	8331164.93	033425.15	02391620	0210/210	100000	31707	833677.55	81121267	*********	831840.51	411661144		13329664	83388354	833846.51	83342248	833418.03	033447.02	93354454	833587.55	833587.56	033633.17	93309437	100000000	object of	83346648	2000000	2001000	41141144	*********	41181183	83374811	83384678	833917.83	83398668	83311178	83325239	833394.77	133584.35	833843.40	833664.88	833741.79	83374E45	933833.16	92396296	03295040	834546.67	834ZM28	83432121	134384.01	833158.58	633434.10	833274.46	833438.70	83364833	83373688	13366671	033649.55	8315613.68	83371235	63371783	835778.45	83347214	833867.20	3941021	834255.10	174341.61	83383878	93325678	93346651	83354373	933563.70	833563.70	831315.56	03348100	********	931253.00	933326558
-	Coordinate	622724.11	822330.25	822345.74	621408.45	822543.00	622308.10	822315.62	522386.41	522421.55	100000000000000000000000000000000000000	ATTACAL DE	822419.61	27,464.51	27.454.47	822441.65	E77398.31	835367 48	822463.30	822432.88	822462.40	822567.47	832556.03	522482.07	8E3ZYZZ8	822350.48	522318.11	522354.80	1677778	20,000	1000000	B100000	200 140 24	2011111		20034304	A11278 68	BITIMETE	822376.15	822405.79	823431.11	822055.71	\$22,672.07	822129.94	822175.17	622221.21	822289.00	822284.50	822311.12	522316,96	11.500225	ATTA 50 48	STITIS AT	62216267	822084.65	823010.68	821955.43	821977.96	821842.33	822004.80	822080.21	27216136	827067.29	82212203	822144.40	622152.80	822149.62	622122.55	422/23.04	822112.50	822062,66	621014.78	824886 23	821080.29	621889.31	821947.50	822008.03	822028.73	\$21952.62	821834.07	89148176	#21778/07	447762.19	821826.73
4	**	633125.78	127771258	833231.08	833434.89	833960.46	E33118.28	833185.93	633424.19	273000		841071.74	833527.00	******	10 414418	633782 11	AUSBAL 17	#11691 68	831678.15	613696.64	ESSESS SA	613387.36	633423.89	613416.00	E33447.62	233544.64	133488,77	833587.56	613633317	200000	103266101	611488.64	********		B.20.00.00	211117 60	235463.64	635673.62	833768.65	E13545.76	835617.83	833076.99	833121.78	833263.39	833398.77	833524.35	613653.40	ELDESA GR	835761.98	833763,11	613633.16	#12002.W	E34034.90	EM 140 S7	£34231.72	834322.77	833097.20	633156.66	613101.67	833274.00	533434.10	811774 00	#33438 #3	633586.71	25.649.55	833683.68	833713.66	833757.63	613734.53	833778.49	833673,20	634 199.21	ENGORA NA	#3311E.37	633139.75	813298-86	49.094.03	833543,73	633460.98	77.091073	833315.00	632154.01	#13175,74 #1466,66	E25249.00
Caline	Road	R003	R003	F003	R003	R003	R004	N100.4	#00#	8000	2000	BOOK	Posts+R007	Debogs Doby?	Short- Prot	R006+R007	PERSONAL PROCES	Britis Hotel	Roto-Rot1	FEGT G. HIGHT	RECU-RECT	RO12+R013	R013+R013	RD12+R013	R012+R013	RD12+RD13	Hote-Rots	8016-H017	Mark and A	No.	200	Hank A	Tares.	2000	The same	Barre	1000	8628	9758	Read	R031	6032×R301	8633	B034	ROSS	N:036	R437	RESE	R029	8,040	ROAT	1000	ROAD	Blas	Ross	FIS47	HSH	8549	moto	Rost	R052	1000	8000	H654	11037	H084	H054	R054	ROSS	NORE	#1057	8050	ROKO	8661	ROSZ	RDES	NOI-4	#100 W	H094	RORS	AMA	1001	ROSS	More

Pair	X1	Coordin Y1	x2	Y2	(including	Height (m)	Road Type (caline 4)
BID1	8353E7.93			821875.22	_mixing_rone)_	0	(camio 4)
RU72	833597.24		83359724 83359175		29	0	4
ROT3	8334E1.50		839397.24		- 01	0	1
R074	833261.64	821790:34	833451.60	821860.54	20	0	
R875		621961.09	633506.97		16	0	1
RU76	\$33501.4E	#21897.80	813568.46	821699.77	16	0	1
R076	633548.66	821899.77	821603.43		16	0	4.
R074	832603.43	821688-99	83368492		16	0	1
R677	833564.57	621884.14	833563.57	821884.36	37	0	- 1
R077	\$33553.57	821084.3%	E33600.68	821871.38	17	0	- 1
HOT?	633000.48	821971.28	931973.64		17	0	-
ROTE	#33667.38		833875.32		16	0	
R079	833673.29	623831.43	633867.51	821651.AB	16	0	1
R060	833675.67	821661.18	833999.54		16	0	1
R091	833867.01				20	0	4
R082		821650.86	933943.08		14	0	4
	833458.18	\$21864.41	813510.76	021821.12			1
Rtaz	823510.75		833518.39		- 194	0	4
ROES .	833526.39	821785.93	#33576.13 #33496.18	821667.58	18	0	
	833424.83	821665.11			18	0	1
R083	\$33496.1E	821813.12	833524.36	821772.28	14	0	- 3
B183	\$33524.3E	821772.29	813559.51	821652.62	14	0	
R094	\$33567.54	821687.02			13	0	1
R094	833.582.69	821644.85	833607.71	821003.87	13	0	
Ross :	833009.34	821605.64	83364024		14	0	1
RIBS	E33640.24	82) 57 8-52	813691.67	821545.20	14	0	- 1
R065	\$336E1.67	821545.20	821720.62		18	0	- 1
HOSE.	833500,70	821649.89	#33963.88	821163.58	17	0	. 1
Rote.	#33003.88	621533.58	811646.83	021545.45	12		1
R1887	833646.49		EDISIEAS		33	0	1
Ross	833254.24		#22245.50		17	1	- 4
ROBE	833304.50	821854.64	833416.50		17	-	-
Ross		521905.51			17		1
ROSS	8334E7.63	821BA1.09	833533-63		17	10	-
Ross		621786.07			17	10	-
FORB.	833574.80				17	- 1	-
	SEPTEMBER .		833600.16				
Rota	833600.16		633712.66		37	6	
		821501.44			16		
8089	633370.06		812427.26		16	113	4
RORP	833477,36		833490,60		16	0	4
Ritas	\$334E0.60	821929.25	83352246	821786.30	18	10	194
ROBS	833522.46	821786.32	E13545.19	821725.AT	16	0	
HOEK	833543.19	821725.67	9315(2.07	821655.37	16	1	
RORR	832062.07	821653:37	\$3350E25	021504.44	16	0	4
6199	833596.99	621594.64	613699.51	821508.87	16	6	4
R050+R091	833259.78	821629.64	823337.84	621634.13	97	0	- 1
R997+R993	#33337.92	#21632.93	£13449.56	821640.31	20	0	- 4
			#32512.09		20	0	- 1
R094	833337.84	821634.13	833341.61	821576.41	- 16	0	- 1
R195	833609.59	421501.FZ	833548.49	821548.43	97	0	- 1
R095+R097			E3402E77	822414.27	18	0	1
R008-R000	834028.77	822414.27	934127.62	822332.11	18	0	-
R100+R101		822332.11		822258.38	18	0	- 4
R192+R193	83421631	822258.35		822190.58	-18	0	1
			834309.95 834407.46				
R104+R105	834300.95	822180.58			18	0	1
R106	B33917.B3	822431.11	833991.74		18	0	1
8127	833991.68	\$22270.04	894892.33	822287.53		0	1
R108	824090.84	622288.06	634181.96		36	0	1
Riss	ESATE1.98	822212.22	834275.08		- 17	0 -	1
Ritte			#3436436		17	0	7
R111	834363.46	822009.86	834400,74	822028.83	- 18	0	1
R112	833848.76	822 AD 5.79	611992.95	622380-5T	19	0	1
Rtto			233909:65		18	0	- 1
R114	#33,909.65	822271.35	833994A7		18	0	1
R115		\$22200.75	834977.01		18.	0	1.
RISE			E34097.10		16	0	1
RHIT	634097.30	822115.02	E34110.89		18	0	. 7
RITE		622037.73	834243.28		- 19	0	1
RIII	#34242.94	621993.65	#14TF2.18	071951.45	19	0	1
R120		#21961.17	E34359.17	221205 PA	18	0	1
R121		822376.15			18	0	1
R122	833764.03	822376.46	833769.11		18	0	1
						0	1
R123	#33848.78	\$22222.16	£33954.75		18		
R124	833671.82	6223A1.72	STIENASE	877784.07	16	0	7
R125	833694.86	822254.07	822827.77	822172.05	18	0	1
R126	833053.40	822299.00	832688.33	822174.73	12	0	- 4
R127	633469.65	822315.75	633502.51	822278.AB	-38	0	1
	12.£0065K	82227 E-66	833524.36	822221.21	18	0	1
R128	833377.80	822222.03	833355.00	822293.72	18	0	- 1
R129	833377,80	822732.63	833318.77		18	0	1
		822175.04	813434.10	8220HD:78	n .	0	4
R129	833396.42		#13410.51	822007.97	16	0	7.
R129 R120	833596.42 833431.92	#22080.70			16	0	- 1
R120 R130 R131	A33431.92			821952.78			
R129 R130 R131 R132 R133	833431.92 833460.45	833007.05	¥334§1.00	821952.76 821883.08			- 4
R129 R130 R131 R132 R133 R134	833451.92 833460.45 833461.00	823607.95 821982.76	933491.00 833506.97	821887.08	16	0	1
R129 R130 R133 R132 R133 R134 R135	833431,92 823460.45 823481,00 823269.67	823007.95 821962.76 822239.78	#33481.00 #32506.97 #13232.66	821883.08 822178.01	16	0	-1
R129 R120 R123 R122 R122 R124 R125 R126	\$33481.92 \$33480.45 \$33481.00 \$33259.07 \$332322.03	823607.95 821962.76 822239.78 822178.06	#33461.00 #33606.97 #33232.64 #33233.39	621563.00 622178.01 822129.94	16	0	1
R129 R120 R123 R122 R123 R124 R125 R126 R127	833481.92 833480.45 833481.00 833289.07 8332323.03 833080.91	823607.66 821982.76 822239.78 822178.06 822182.63	#33481.00 #33506.97 #33232.06 #33253.39 #33100.03	621863.08 622178.01 622120.04 622120.44	16 78 18 18	0 0 0	1
R129 R120 R123 R122 R122 R124 R125 R126	\$33481.92 \$33480.45 \$33481.00 \$33259.07 \$332322.03	823007.05 821062.76 822239.78 822178.06 822182.63 822182.63	#33461.00 #33606.97 #33232.64 #33233.39	821882.08 822178.01 822120.04 822129.44 822672.07	16	0	1

					_						NO = 40	0 (=0/147)											
Hr00	11.01	Hr02	Hr03	Hr04	Hr05	1 1100	1 11.00	1 11.00	11.00	Hr10	NO _X x 10	0 (g/VMT) Hr12	Hr13	Hr14	Hr15		Hr17	11.40	11.10	11.60	1 11.01	11.00	
66.2174	Hr01	66.4357	66.6422	66.6783	67.0088	Hr06	Hr07	Hr08	Hr09	66.4470	69.0095	66.5037	66.9487	61.9885	65.4018	Hr16	61.3237	Hr18 60.9801	Hr19 58.6614	Hr20 67.5878	Hr21	Hr22	Hr23
59.6986	59.4632	59.4049	59.8408	50.5603	59.7567	59.8383	69.0608	53.7639	61.5715	57.3065	60.4423	58.5555	57.2600	52 2973	56 9931	55.1758	50.9317	48.4488	49.5369	57.9159	71.8476	66.0789	55.7887
62.8030	62.4036	62.7767	63.1293	63.3470	62.9188	63.1943	71.1925	55.9972	65.6670	61.3516	64.4859	62.8337	62.1167	58,0928	61.0247	59.2716	56.9287	56,6632	56,6309	64.3655	77.0990	71.7868	62.0314
63.2049	62.9218	63.2561	62.9184	63.5326	63.4866	GL:6475	71.4927	56.1911	65.0853	61.4515	643639	62,3660	61.5903	56.9377	59.8875	57.7524	55.8816	54.6439	54.3606	63.4372	77.3533	71.5468	59.8594
59.1368 61.6141	62 3005	58.7785 61.5912	59.4809 62.4517	59:3525 62:4324	62 1385	59.7621 62.2970	67.9307 71.5880	56,4298	63.9019	57.5451 59.8245	63.4783	58.9189 61.5028	57.4702	56.1661	56.7134	54.4328 59.2773	51.9595 55.6704	51.2236	54.9245	59.9000 65.2904	74.0927	68.7612 72.7599	56.4314
6L6141	62.3005	61.5912	62.4517	62.4324	62.1385	62.2970	71.5880	56.4298	63.9019	59.8245	63.4783	61.5028	61.7507	56.1661	60.8358	59.2773	55.6704	54.9955	54.9245	65.2904	79.7244	72.7599	60.9343
61.6141	62.3005	61.5912	62.4517	62.4324	62.1385	62.2970	71.5H80	56.4298	63.9019	59.8245	63.4783	61.502H	61.7507	56.1661	60.8358	59.2771	55.6704	54.9955	54.9245	65.2904	79.7244	72.7599	60.9343
59.6724	59.7863	59.7521	59.8972	60.3802	60.1690	60.3228	68.6984	53.5837	62.7212	58.3852	61.7260	60.0962	59.6754	55.2870	58.7364	56.8635	55.5690	54.7524	54.3590	63.9848	78.3229	72.0046	59.8010
59.6724	59.7863	59.7521	59.8972	60.3802	60.1690	60.3228	68.6984	53.5837	62.7212	58.3852	61.7260	60.0962	59.6754	55.2870	58.7364	56.8635	55.5690	54.7524	54.3590	63.9848	78.3229	72.0646	59.8010
59.6724 66.5529	59.7863 66.0399	59.7521 66.2801	59.897Z 66.6229	66.6914	67.1973	67.1207	68,6984 76,1591	53.5837 62.2776	62.7212 68.9122	58.3852 64.5064	61.7260 68.0198	65.4350	59.6754 65.7121	55.2870 59.6780	58.7364 64.0798	56,8635 62,6691	55.5690 58.4092	54.7524 57.6178	54.3590 57.6068	63.9848	78.3229 80.9083	72.0046 74.0383	59.8010 63.7005
57.4055	57.8687	57,4730	57.9026	58.0291	57.8142	58.1239	66.0559	49.5605	59.3714	56.5552	60.0129	58.9028	58.3902	54.7392	57.6215	55.7657	54.7071	55.7874	54.9337	64.8103	79.1770	73.0745	59.7970
65.8806	65,9891	66.0189	66.3598	66.3925	65.8930	66.3369	75,0648	58.1680	68.1680	63.4896	67.3830	64.7530	65,5351	59.0830	62.7188	60.7568	57.5184	57.4105	56,6929	67,3488	81.8970	74.6267	62.7008
59.8718	60.2274	59.9763	60.2280	60.3679	60.2277	60.7124	68.0763	52.6985	61.9015	59.2518	62.4642	61.1147	60.5721	57.0362	59.7416	57.8868	56.6338	57.7980	56,9079	66.2660	80.0708	74.3990	61.8051
85.1290	85.5718	84.8062	85.0954 85.0954	85.5761	85.1270	85.7498 85.7498	96.3152	81.7545	94.5164	87.5338	91.2947	88.6416 88.6416	88.6761	82.6119	85.4525 85.4525	83.2160 83.2160	79.8536	79.5044	79.3089	87.6438	102.6151	95.3178	81.7898
85.1290 85.1290	85.5718 85.5718	84.8062 84.8062	85.0954	85.5761 85.5761	85.1270 85.1270	85.7498	96.3152	81.7545 81.7545	94.5164	87.5338 87.5338	91.2947	88.6416	88.6761 88.6761	82.6119 82.6119	85.4525	83.2160	79.8536	79.5044	79.3089	87.6438 87.6438	102.6151	95.3178 95.3178	81.7898 81.7898
48.2901	48.8006	48.6146	49.1546	49.9162	49.5741	49.0558	\$1.8600	45.6886	52.0153	50.0399	50.8115	51.6118	47.4578	48.0112	19.6656	47.6528	45.8149	44.5878	46.5795	49.3818	59.5016	58.1833	49.4312
48.2901	48.8006	48.6146	49.1546	49.9162	49.5741	49.0558	51,8600	45.6886	52.0153	50.0399	S0.H115	51.6118	47.4578	48.0112	49.6656	47.6528	45.8149	44.5878	46.5795	49.3818	59.5016	58:1833	49.4312
48.2961	48.8006	48.6146	49.1546	49.9162	49.5741	49.0558	51.8600	45.6886	52.0153	50.0399	50.8115	51.6118	47.4578	48.0112	49.6656	47.6528	45.8149	44.5878	46.5795	49.3818	59.5016	58.1833	49.4312
86.0133 86.0133	85,6158 85,6158	85.3827 85.3827	86.0573 86.0573	86.1974 86.1974	85.9241 85.9241	86.3188 86.3188	96.8174	81.7579	92.8300	88,4817 88,4817	92.8050 92.8050	90.5311	91.5774	85.7368 85.7368	87.9476 87.9476	86,1974 86,1974	86.8185 86.8185	86.7090	85,2852 85,2852	94.3724	109.3025	101.9249	86.4441 86.4441
88.4146	88.7170	88.4032	88.7522	88.9010	89.2061	89.5990	98.6868	85.8829	95.3634	91.4912	95.3767	92.9913	93.6973	88.2593	90.1133	88.4008	86.7489	88.4629	85.0581	95.3532	109.7021	100.3455	88.2430
88.4146	88.7170	88.4032	88:7572	88.9030	89.2061	89.5990	98.6868	85.8829	95.3634	91.4912	95.3767	92.9913	93.6973	88.2593	90.1133	88.4008	86.7489	88.4629	85.0581	95.3532	109.7021	100.3455	B8.2430
88.4146	88.7170	88.4032	88.7522	88.9030	89.2061	89.5990	98.6868	85.8829	95.3634	91.4912	95.3767	92.9913	93.6973	88.2593	90.1133	88,4008	86.7489	88.4629	85,0581	95.3532	109,7021	100.3455	88.2430
86.9918 86.9918	86.4842 86.4842	87.1006 87.1006	85.9585 85.9585	87.1345 87.1345	87.3249 87.3249	87.3754 87.3754	94.7771	79.3080	91.2749	84.7625 84.7625	88.4403 88.4403	85.5976 85.5976	86.0519 86.0519	80.2407	81.8902	79.4698	77.6224	78.4860 78.4860	77.1970	86.9210	101.5429	95.4722	81.5709
105.0802	104.8571	104.9910	104.4312	104.7471	104.7149	105.1832	107,7038	103.8887	107.5038	106.3521	107.1419	105.4772	105,4700	103.5578	104.1314	104.3909	103.4288		101.8552	104.1301	101.5429	106.1606	103.4518
21.4580	21.2699	21.1384	21.1648	21.2386	21.4483	21.8938	29,9360	31.6511	30.6114	29.8559	29.0555	26.3883	22.7448	25.2796	21.5898	24.0647	23,5708	20.8576	17.4882	18.6792	21.4066	21.7445	18.5468
21.4580	21.2699	21.1384	21.1648	21.2386	21.4483	21.8938	29.9360	31.6511	30.6114	29.8559	29.0555	26.3883	22.7448	25.2796	21.5898	24.0647	23.5708	20.8576	17.4882	18.6792	21.4066	21.7445	18.5468
21.4580	21.2699	21.1384	21.1648 21.1648	21.2386	21.4483	21.8938	29.9360	31.6511	30.6114	29.8559	29.0555	26.3883	72.7448 72.7448	25.2796 25.2796	21.5898	24.0647	23.5708	20.8576	17.4882	18.6792	21.4066	21,7445	18.5468
21.4580	21.2699	21.1384	21.1648	21.2386	21.4483	21.8938	29.9360	31.6511	30.6114	29.8559	29.0555	26.3883	22.7448	25.2796	21.5898	74.0647	23.5708	20.8576	17.4882	18.6792	21.4066	21.7445	18.5468
21.4580	21.2699	21.1384	21.1648	21.2386	21.4483	21.8938	29.9360	31.6511	30.6114	29.8559	29.0555	26.3883	22.7448	25.2796	21.5898	24.0647	23.5708	20.8576	17.4882	18.6792	21.4066	21.7445	18.5468
21.4580	21.2699	21.1384	21.1649	21.2386	21.4483	21.8938	29.9360	31.6511	30.6114	29.8559	29.0555	26.3883	22.7448	25.2796	21.5898	24,0647	23.5708	20.8576	17.4882	18.6792	21.4066	21.7445	18.5468
21.2262	21.0403	20.9497	21.0772	21.2679	21.2503	21.5308	24.5514	24.9314	23.5704	24.0157	24.0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943	20.7921	16,6096	18.2952	21.1966	21.1650	18.3647
21.2262	21.0403	20.9497	21.0772	21.2679	21.2503	21.5308 21.5308	24.5514	24.9314	23.5704	24.0157	24.0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943	20.7921	16,6096	18.2952	21.1966	21.1650	18.3647
21.2262	21.0403	20.9497	21.0772	21.2679	21.7503	21.5308	24.5514	24.9114	23.5704	24.0157	24.0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943	20.7921	16.6096	18.7952	21.1966	21.1650	18.3647
21.2262	21.0403	20.9497	21.0772	21.2679	21:2503	21.5308	24.5514	24.9114	23.5704	24.0157	24.0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943	20.7921	16,6096	18.2952	21.1966	21.1650	18.3647
21.2262	21.0403	20.9497	2L0772	21.2679	21.2503	21.5308	24,5514	24.9514	23.5704	24.0157	24,0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943	20.7921	16,6096	18.2952	21.1966	21.1650	18.3647
21.2262	21.0403	20.9497	21.0772	21.2679	21.2503 21.2503	21.530R 21.5308	24.5514 24.5514	24.9114	23.5704	24.0157	24.0208	22.6724	20.0578	22.4200	19.0297	21.7335	22.6943 22.6943	20.7921	16.6096 16.6096	18.2952 18.2952	21.1966	21.1650	18.3647 18.3647
65.7626	65.5285	65.0507	65.4972	66.3541	65.6654	66.3185	81.0775	62.6759	75.9199	69.7704	72.8911	73.4003	68.1926	65.6528	71.9493	69.0301	66.8052	62.8235	63.9070	71.1455	90.1624	81.8145	67.1787
64.5416	64.0258	66.1463	67.0349	56.5505	63.6588	65.7195	78.9799	59.9044	72.3267	68.9794	72.2178	72.2612	57.8308	64.8048	71.0522	68.6934	64.9097	61.2988	62.4767	70.6809	88.4079	81.9053	68.1643
64.5416	64.0258	66.1463	67.0349	66.5505	63.6588	65.7195	78.9799	59.9044	72.3267	68.9794	72.2178	72.2612	67.8306	64.8048	71.0522	68.6934	64.9097	61.2988	62.4767	70.6809	88.4079	81.9053	68.1643
54.2152	54.0196 113.0085	53.8471	54.7276 113.7144	55.1049 114.0539	55.1680 114.1704	115.0342	58.6721 119.8302	46.6848 114.6757	55.5822	52.5555 116.7629	\$1.7877 138.0245	51.1271 116.5845	43.0059 116.1976	42.0702	42.6421 115.7928	38.1645 116.4147	33.8607 114.4619	29.1131 115.1960	32.6400	36.7230 115.0025	50.8669 120.7159	50.0675	36.8813 114.6007
113.7586 77.8298	88.6725	76.3041	56.7812	57.0803	82.8860	75.9435	92.0399	79.4855	117.6921 89.3889	84,2530	86.0844	84.2649	83.4512	77.3432	83.7117	78.6266	74.0384	69.5868	70.2054	78.9300	98.8190	91.9441	79.7086
102.3635	101.9616	104.4382	107.3202	104.5748	97.7063	100 1433	110.2492	109.9799	119.2951	110.5860	109.7191	104.3035	102.1327	95.0525	99.3007	87.9272	81.8153	78.5082	79.6873	87.9913	103.5924	93.9933	83.7930
89.9090	89:5426	97.2671	90.6874	95.5662	89.6451	98.4651	105.5415	953085	110.3982	101.5468	100.5549	101:5259	94,5152	89.2927	97.2479	86.9726	81.7176	76.6356	77,4991	85.2404	105.5009	95.5590	84.7716
89.5253 83.4997	95,5142 91,4848	87.9050 85.7727	89.0451 81.4965	89,4713 81,8910	94.2704	90.3298	107.5616	89.5016	100.4693 94.3178	91,0849 88,6325	95.5296	89.2049 87.4308	87.2045 84.1786	78.0824 76.6559	85.9420 83.8824	80.7304 78.4294	71.7603 72.6104	67.5100	69.6883 70.5967	81.8109	100.1525 99.2654	90.8595	80.4203
72.5432	72.7363	75,0828	74.0545	76.1903	71.2999	72.6955	85.6163	86.0510 68.0003	BO.4451	76.6261	80.7737	80.0737	78.2494	73.6224	80.7716	77.1620	73.9948	70.3949	72.2947	81.4918	100.2763	89.5984	76.6506
75.1428	70.9458	75.5339	82.4227	76.8697	72.5269	75.6431	83.9982	65.1010	75.7987	72.2675	77.0127	76.5293	73.8493	69.1734	76.0040	74.9957	70.3834	66.2057	67.8140	77.7921	97.3018	90.6258	29.7457
74.6204	71.5497	75.0332	80,4217	78.2463	77,2161	75.2689	84,0856	66.0757	76.7586	74.0483	77.1001	76.8769	74,9064	70.5638	77.1943	76.8855	71.1986	67.7752	69.1861	79.8567	97.9888	89.0251	76.8327
71.4376 72.3558	70.1919	73.8889	79.4911 76.0283	77.1555	76.0969	74.0787	83.2304	64.6013	75.6290 75.6112	72.9473 72.2288	76.3180 76.0011	75.5642 75.6549	73.8711	69.5885	75.8324 75.4954	75.3591 73.8349	69.5415 68.4222	66.3213 66.3078	67.2072	77.4919	96.5313 94.8181	90.4566 89.1265	77.4159 76.5512
73.2495	73.8741	70.3973	74.1910	72.4327	71.5064	73,8946	83.5203	66.5709	78.0819	72.8265	76.8808	75.7769	73.0956	69.2809	74.9257	74.5326	68.8220	65.2040	67.9609	77.6972	96.6653	88.5806	78.3973
105.4289	107.1034	111.7484	106.7994	108,0306	107.8963	107.8620	119.1369	109.4368	115.9948	107,7106	109.8818	108.0745	106,6432	93,5219	101.6088	93,1346	84.2252	80.4592	81,8363	90.6132	107.0793	96.3169	88.7522
67.3207	66.9876	68.5679	64.7383	51.4559	70.5414	66.0436	75.2832	59.0521	69.8479	65.9135	70.2934	68.7247	55.4457	62,9880	67.8990	67.0466	62.0874	59.2905	60.0512	71.0491	87.2045	80.8331	68.9505
74.6712	72.2043 89.9307	72.8839	73.3866 90.3468	73.3271	73.1999	74.3283	85.2435	74.0394	86.2874 97.6288	81.4015 89.9353	93.0293	81.5540 89.3836	79.0283 88.9255	77.2377 80.8270	80.4085 86.6339	79.3514 84.2788	74.6959 76.1014	71.3590	71.1764	77.9774 81.1576	93.4526	85.0773 87.6289	74.8475 80.6875
90.2034 71.1750	71.0872	72.9862	73.6285	73.1248	73.0133	72,1768	80.8032	65.7788	77.1296	72.5994	75.9632	74.9162	72.9516	69.1644	74.4212	74.8868	68.8783	65.8428	67.4536	74.3529	89.1157	82.8791	72.7469
71.4961	72.9414	71.9464	73.5012	73.7924	72.7715	72.7252	80.8834	66.3892	75.8954	73.2248	75.4473	75.2593	73.3349	69.6860	74.5018	75.4275	69.3755	66.2849	67.8556	74.5341	89.3449	83.3013	73.6625
73.4406	73.1803	72.6244	74.1246	74.4288	73.4450	73.1973	81,4493	67.2077	76.4735	73.9722	76.8486	75.6955	73.7816	70.2303	75.0572	75.9503	69.8800	68.3679	68.2224	76.6962	#9.6683	83.7361	73.4938
71.5106	70.9157	71.9699	71.7548	70.9042	71.8103	72.1016	80,5578	67.5132	76.9566	74.3564	75.9564	75.0098	73.0710	71.1352	74.6633	75.7604	69.6332	68.3679	68.2224	76.6962	89.6683	83.7361	73.4938
72.7265	72 9153 81 7291	72.8976 91.9512	72.5725 85.8187	71.8846 86.2220	73.9040 86.2884	72,8117	96.7523	73.7938	78.0576 89.5173	75.3872 85.6277	78.6041 91.8420	77.5781	75,4126	71.8726	76.9855	76.1347	71.6718	99.7341	96.5114	76,7769	89.5437 130.9425	119.6518	100.6876
89.2111	90.3550	89.7685	91.0419	92.5672	90.6132	109.2744	101.5607	83.4420	102.7035	92.2833	94.8606	90.7865	87.5811	82.NZ88	83.5180	72.9489	72.7175	73.6335	72.4186	79.0711	96.5633	91.0481	72.6327
56.2058	55.8924	55.4414	55.3293	53.2234	58.8182	57.4989	68.6852	47,4370	61.1717	58.7691	61.9946	63.3772	58.1111	57.5372	62.1021	58.7144	58.9986	58.7532	58.4969	65.9883	85.5161	81.1079	61.0521
95.1737	93.3060	93,1844	96.7065	93,7995	96.3284	94,1655	102.2929	88.5752	101.9535	96,4878	100,9005	100.4954	102.4540	97.4068	100.1941	103.0085	100.5098	102.6108	98.1500	111.7163	126,9490	119.6201	101.3163
91.7849 80.4851	94.4709 80.3515	91.6911 78.3000	94.2639 84.7284	96.9107 #2.3045	91.7232	94.0613 81.6615	91.1494	75.0025	99.8401 86.3234	90.4194 82.0040	91.H825 86.2996	86.2535 84.5754	82.4527 82.6586	74.0480	73.6880	60.3867 82.1859	59.4011 78.4072	57.2654 77.6611	57.9405 77.1337	66.1021 85.5850	104.9717	95,7948	62.9033 81.2092
79.1379	82.7882	79.7455	79.0131	76.5553	78.9787	80.7886	89.6862	71.1381	84.0254	81,7283	86.1142	85,4680	83.6656	83.2612	86.9047	85.9126	78.4072 85.7018	86.3416	85.2888	94.6557	112.6033	102.7655	86.4245
76.5238	76.0597	78.5921	78.5516	76.5446	75.8084	76.0182	85,4767	65.2450	78.2880	75.7301	80.2752	80.0662	78.7668	77,9230	81.5846	80.5736	80.8168	81.5506	80.8668	89.7693	107.9859	101.3097	83.9967
64.7049	64.4836	63.8803	65.0928	64.6278	65,2041	f5.3449	76.0431	56.8576	69.7907	67.3436	70.3507	71.9982	69.2017	68.2119	71.7615	69.8360	69.8399	71.8311	69.2856	80.6250	96.0138	89.2539	73.0462
63.6192	63.4843 66.0252	63.1541	63.3246 66.0690	54.1079 56.8469	63.6670	63.9629	75.0525	55.5780 61.0114	68.7692 72.1342	66.4914	70.6912	69.1918 70.0175	58.1896 58.8486	64.3499	70.7152 69.7257	68.9165	68.7888 65.9137	70.8425 65.6905	68.2368	74.8313	95.5370	88.6057 83.6688	71.8676
50.3477	50.3487	50.6108	50.6651	50.5844	50.8687	50.3553	78.1196 54.5070	49.0146	55.9913	53.6202	53.7678	54.1518	48.2125	47.3805	48.5631	45.5077	42.5538	40.0608	41.9568	43.3636	54.4365	52,4644	42.8335
80.3113	81.6900	82.6496	83.5894	83.6068	81.6461	80.1690	90.2595	77.5837	8IL0577	81.2730	84.4657	80.9048	78.9609	71.7814	75.1066	67.9646	65.6788	63.8885	64.4487	72.6976	88.0777	79.7284	67.3704
66.0125	67,4722	69.3323	70.9017	69.8575	67.8527	65.5618	76,4056	60.7755	70,6577	66.9079	69.8786	69.0146	65.8268	62.4964	66.9825	65.2598	62.NS32	60.2089	60.1526	66.3474	83.0928	77,4211	63.6074
72.3862	84.5355	94.5041	81.9462	78.9157	92.9358	82.9080	83,6690	61.4343	77.2680	71.5956	76.6701	78.3356	76.1958	74,2414	78.0318	74.4730	73.6272	73,4074	74,9066	86.2219	103.5197	99.8059	84.0962
64.5815	72.8976 64.5269	85.5764 75.2462	35.0030	35.2241	86.2884 75.8663	79.0583 61.5459	80.8335 72.9366	59.5583 49.9135	75,6385 64,1078	69.9855	73.8192 64.4992	75.8085	73,4096 54,7322	71.4436 60.8760	75.3938 65.3905	71,9590 66,6126	72.1432 63.4332	72.3388 64.8780	73.0657 65.4086	82.2653 74.9580	94.1374	98.5501	81.5613 71.8198
64.5815	64.5269	75.2462	32.5306	12.7397	75.8663	61.5459	72.9366	49.9135	54.1078	60.0747	64.4992	66.7710	64.7322	60.8760	65.3905	66.6128	63.4332	64.8780	65.4086	74.9580	94.1374	90.1210	71.8198
60.9886	60.4137	61.7027	59.3704	51,4591	61.8624	61.8177	71.3688	50.6123	63,4465	60.7088	65.3625	65,4984	54.3497	61.7552	65,4972	65.2887	64.6852	67.3163	64.8443	76.7424	94.6671	87,7900	70.0229
91.6774	92.6886	92.3501	92.6409	92.5768	95.0566	94.0229	103.7599	83.7291	96.7198	29.2047	90.8388	86.1907	82.1862	74.5604	75.4433	65,4952	64.3654	62.5219	62.1002	70.7895	8E.8531	84.0907	68.2593

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Road		Coordin	Coordinate (m)		flert ding	Meight	Road Type		Н
Pair	X1	۲.	X2	Y2	mixing zone)	(m)	(caline 4)	Hr00	
B141	633295.35	821547,25	83331555	823891.87	13	. 0		89,3564	-
R142	833339.89	821853.87	833315.93	\$2189134	- 43	0		89.5789	
R143	833129.75	821889.31	832169.17	621834.07	- 18	0		94.9572	in.
H144	633165.17	621634.07	43347874	621753.15	13	0		94.3526	
R145+R146	633812.49	821976.50	83100438	827816.03		a		85,7216	**
R147+R148	E3377EM	621688.36	832921.13	82172778	4.6			762156	
R149	833728.61	821748.53	833807.73	12168438	14	0		70,7037	
RIAS	633774.08	621643.62	633807.73	82168436	13	9		70.7037	_
R156	533736.67	624759.23	93366771	827805.87	. 11	ó	,	70,7037	_
RtSt	633613.61	821619.98	833683.50	\$21543.75	12	0		70,7037	9
R151	111693.50	121543.70	133776.28	121547.53	14	0	1	70.7037	
R152	833774.08	821643.62	833828.17	821509.55	20	0		70,7037	
R153	633991.31	822369.76	834018.77	\$22414.27	16	0		71,6190	-
R154	873950-86	\$22339.66	33299200	822368.67	- 11	9		71.2542	
R155	833909.68	822271.08	133910.46	822330.45	- 18	0		71.1912	77
R156	633868.78	6222223	83190855	\$22271.35	18	9		90,2271	ω,
B157	82388.53	RZ22228	833827.77	82237228	- 68	0		92,4038	~
RTSB	613827.77	822172.96	83277268	\$221539	118	9		88.1035	~
Ress	834075.91	872395.62	134112.90	822384.34	15	0	1	67.6074	9
R160	82.040ACB	522.287.63	834117.62	822232.11	- 10	0	+	74.4212	
RISE	634034.90	822259.53	8370768	\$22.25W.62	. 53	a		68,4065	-
R162	E34049.42	822238.25	83409638	622287.53	18	0		74,8914	1
H163	633993.96	822201.68	83403430	822260.01	14	0		71.2311	-
H154	834107.86	62218133	53404842	82223928	- 14			72.4200	-
8165	613953.31	822151.70	83399447	822201.23	. 91			73.5391	1
R166	623872.14	F	83396475	622160.53	- 61	0		62.5783	1
R167	133805.67	522042.45	834007,86	622189.33	18	0		89.6809	~
R168+R165	57.519572	521975,47	83387636	822050.03.	21	0		37.4086	
R478+R474	633738.44	821883.35	82381249	821976.53	- 69			49.0049	7
R172+R173	E23666.92	82182232	83377938	821867.65	20	9	. 4	74,5584	
H174-H175	833581.78	821677.50	SCERPEES	621823.55	. 91	0		77.0498	-
RETE	633498.77	621608.49	833565.47	82158673	26	0		713149	
R177	613513.09	821899.38	831/2108	\$21568.67	2.0			78.8550	
R178	833440.44	821529.90	933413.00	821608.61	. 91	0	1	77.5310	"
R179	833451.64	121526.21	133111.52	621609.38	- 11	0		83.1404	-
R180	634218.31	\$22256.35	834315.96	8222588 33	- 13	0		80.6447	~
RIBE	E341811.9E	62271222	10312100	822256.35	- 41			79.1251	
R182	834140.62	822162.67	834181.78	6222223	- 11	0		76.6754	"
8183	834099.34	822113.33	834149,62	822162.07	18	0		82.0607	-
R184	634877.01	74 F	834064.51	822109.94	0		-	85,7254	~
H184	E34151.51	H5 254 525	834974.50	822504.18				83,7254	"
Will be	2011/04/20	20000	0710000	2000000				907/534	"
BIRE	KIATIN SA	APTICAL AT	MATTER	872136.83				05 MC 50	1"
8187	234190.62	822037.73	83421176	\$2208E.45	21			83.6944	1
R188+R189	834004.88		83408834	821580.22		0		76.9606	1
R150-N191	633831.13	821727.74	834004.98	821816.03	**			813400	1
R182+R183	£13 £12 £12	821669.75	83191688	821727.98	2.0			65,7183	1
RIS4+RISS	87.24.EES	821505.80	833867.51	\$21681.45	2.0			98.5991	6
R194-R202	10,197618	821523.38	933828.17	821500.58	30	0		96.9553	5
H197	E3334.36	522060,54	83440018	822104.71	- 44	0		86.0391	"
R198	634322.77	822019.68	83436436	9.22.00E B.C.	. 18			77,8264	-
R199	E34281.93	421961.17	83432300	822010.48	18	0		87.9501	900
R200	834239.17	821914.13	834289.06	621963.58	**	0		84.8553	~
1 200	E34238.17	521914.13	834317,63	621548.33	14.			84.8233	_

	Hr23	56.8380	70.5377	63.8441	54,7070	50.6497	85,5043	85,5043	80.3784	80.3784	76.1844	63.2524	62.9321	63.7129	75.2885	75.2346	74.8152	67 1660	73.2881	67.2859	0698 999	58.6077	71.3322	53.7367	81.9834	35.3648	40.0008	15, 7730	76.5187	68.5179	84.5466	77.3488	80,4058	80.5159	82.6678	53.4670	53.4670	53.4670	8479 60	90 1813	73.9552	78.6025	65.7655	11.5677	5508 10	85.5043	84 1660	81.5150	81.5150
	Hr22	69 2127	86.2040	829958	72.0658	+	0650501	-	H	105.0590		80.8475	803336	82,7740	96.2691	93.8910	90.7793	BO ATOS	87.4704	82.5968	82.1338	84.1400	84.0625	66.1302	91 9319	48.7189	56.3806	91 2920	87.4740	81.4017	96,0941	87.8853	100 1943	97.0535	93.9809	73.4551	73.4551	73.4551	90,4130	1	+	95.0374	67.5307	107.6762	101.5278	105.0432	92,9552	929284	92,9254
	+	72 5045	-	90.0047	74,1255	68,0878	1	-	108 3333	108.3333	9	84.5591		Н		+	1	23 74 EA	٠	٠	58.9856		90 2854	4	101.6364	+	28.2047	67.6939	94.0476	87 3412	-	H	100.08979	₽	105.2779	75.3956	75.3956	75.3956	+	+	+	102,2859	70,4627	11,2883	105.2886	2465	103.9545	Н	100.6082
Н	H	56.8409	73.6310	72.4471	55.8818	52.3265	89,6666	9999		89,6666		65.7530		+	1	+	80,6035	t	۰	t.	71.0455	Н	-	+	+	35,8784	47.0271	82.8622	t	70,9952	Н	+	80.0330	t	84.9725	57.0619	6190'25	57.0619	T	1	1	39.9746	64,9475	102.6820	94.7999	78.0286	+	Н	83.0520
	611	51 9088	67.1529	64.0681	50.3302	44 9310	77.3523	+	H	75.2219	Н	56.7177		+	+	1	+	50 E102	t	t	60.7027	62.8321	66.1382	+	+	32,5993	43,7145	73.8631	t	62-3051	79,3927	+	74.0112	71.7851	72.2741	49,7132	+	49.2332	+	t	٠	72.6382	54.8053	Н	+	96.E522	82 5211	Н	73.3616
	Hr18	48.5783	66.3259	64.5678	48,3066	42.3860	79.1251	79,1251	77,2122	77.2122	72,9698	55.2666	56.5775	57.0789	78.4656	76,9063	70.5443	60.8346	67.5913	62,0594	61.2709	64,1830	65.3223	48,0989	73.8604	29.6878	41,6845	74.0692	713650	62,5860	81,6745	70.1491	76.3959	73.4136	70.0944	48.0171	48.0171	48.0171	010000	0002.78	65.9122	72.5667	51,0501	96,6075	88.6885	58.2023	81 2364	73.1430	73,1430
	Hr17	59.8460	Н	66.8539	50.6460	45.6597	77.6333	77,6333	76.1321	76.1321	73.8692	56.7157		60.0340	+	78.4514	71.3290	E3 00E3	t	1911	61.1014	54.7762	95.00.29	51.7852	76.9040	33.3721	44.7381	77.4683	72.9531	64.6055	81.8189	72.5429	77 6323	74.6987	69.7533	49.9911	49.9911	49.9911	C7 0.877	86.1938	67.4830	73.0744	55.0813	96.0666	+	59.3750	84.4627	Н	75.15/8
	Hrd6	54.4987	72,1030	68.1552	51.1082	47.0155	79.6410	79.6910	74.3216	74.3216	73.4555	60.2219		+	+	81 8945	74.2358	65 765A	H	66.7348	65.6911	67.1007	70.4276	54.3107	85.1813	35,6173	60.3024	79.7911	75.3778	68.8571	83.6989	78 3256	76 405.5	77.0452	72.7343	53.8231	53.8231	53.6231	60 3700	99 5415	+		58.3837	97.3304	91.7886	72.7K36	77.7794	78.9535	78.9535
	Hr15	59 0502	-	79.2300	64.8222	57.2570	74.5099	74.5099	74.5099	74.5099		64,4700		66.0977	1	1	78.6911	+	1	70.2743	68.9746	68,1137	6627.27	+	X7.3674	18.2876	49,0054	81 2231	76,5009	71.9562	84.3508	80.3875	51,7852 81 3693	77.4668	25,6895	61,3267	613267	513267	73 3670	90.4711	1	79.7334	62.3642	97.2496	92.2150	10.9701	78.8706	Н	80.5254
	Hr14	71.8740	H	78.5798	64.9864	57.5748	72.0208	-		71.1610	68.7840	60.9364	62.3412	62.5342	+	85.6092	77.3512	65.2561	H	66.6641	64.3725	1060.29	68.4868	+		+	47.0738	77.1944	71.4199	68.9263	6268 64	3736	76.733	71.7486	9905'54	50.1404	60.1404	1001404	TA TARK	RC 3401	69.5580	74.0975	58.5864	94.7589	90.1495	71.439E	75.2033	Н	74,0874
	+	79,2498		85.8798	59,7212	63.1553	+	-	-	73.6971	71.7568	56,6732	66.3184	68.7735	+	+	9636	٠	+		59.9307	72.0495	72.8188	-		+	47.8841	83 3022	75.1067	74.6475	83.8264	82.4391	52,0403	79.8236	30.4600	9905'99	9905.99	9905.99	30 5400	30. FRO	73.7377	1	66.6621	97.2579	85.3583	71.7530	54.4844 81 8848	81 3780	31.3780
g/VMT)	+	62 5302		89.5325	Н	69.7846	+	-	H	75.1712	Н	69,7408	-	+	_	+	+	74 5107	۲	H	72.1054	71.5766	-	+		+	53.5279	N2 8865	76.1852	75.2416	83,2729	Н	184.1587 63.1541	78.8258	82.8414	72,7132	72,7132	72.7132	1	+	1	82.1325	68.2293	99.1895	94.5864	71.6379	64.6529	81.1461	81,1461
NO _x x 100 (g/VMT	+	88,5127	Н	94,2090	80.5298	73.7301	+	H	H	73.9374	73.2390	71.2889		+	d	992122	23 0440	+	H	۰	74.1412	Н	76,4514	1	+	+	27.6275	84 6692	76.9039	77.9923	BA 2578	E8.7443	20.8483	79.0350	83.4734	78.0742	78.0742	78.0742	05.00.00	91 8132	77.A767	33.2665	68.5045	02.0781	KK.6822	85.2397	84 3812	84.1569	84.1569
-	+	60.8109	H	92,4795	78,1190	72 7822	t	-	-	70.2697	8507.69	72,0957		1	-	-	89.1591	t	٠	-	20.9068	-	73.5555	+	90.7328	+	27.32.76	81.9879	73.1451	75.3263	Н	82 1603	75, 4171	74.6277	80.5232	76,6976	+	76.6976	00.0150	87 5078	74.5244	79.3322	64,3679	96.1128	+	81.5359	16C 1934	80.3174	80,3174
П	Hr09	61 6539		99.6237	Н	+	72 3881	72.3881	-	12.89.27	72 3881	76.7424	-	+	-	+	95.9769	+	H	+	76.4167	76.6265	Н	1	7601	+	24.32.75	16.1641	75.7521			+	79 7176	77.7288	85.6009	88.2075		88.2075	+	+	+	Н	68.1583	98.6690	91.6000	6,5695	1,0959	Н	88.6909
	Hr08	52 2530	91.0358	86.5249	70.8822	65.7655	58.4054	58.4054		58.8898	58.4054	62,6209		+	+	98.6655	823284	+	t		55.4466	54.5786	58.4161	+	90.4638	31.0999	10.5332	76 5874	928099	71.4689	73,7438	77.3439	750557	67.1580	73.8682	71.5878	71.5878	71.5878	12.63.27	NO 1814	+	73,2566	58.6349	88.1567	93.4162	71.895.3	80.1082	76.1909	76.19G9
	+	63.8980	304,2244	103.7235	33.5847	28.1567	81.5393	31.5393	11.5393	\$1,5393	\$1.5393	54.7350	84.8805	160078	14.3381	15 5844	9562 00	27 1448	82.1044	H	64.0899	82,7782	K1131	72.3394	105.1857	14,4148	23,9317	32 3866	82.9478	88.0939	88.6613	34,7931	M.2050	87.11.74	33.3537	95,9046	95.9046	35.9046	OC BOKE	+	-	32.9553	74.6018	03.2065	97.8674	31.3696	57.5364 36.6414	94.2261	34,2261
П	Hr06	60:1399	Н	94,7446	9605'48	78,3071	69,3337	69,3337	71, 3359	71.3359	69,3337	72,4523	72.8062	72.7750	91,0188	93.0874	88.6117	76.2570	+	H	72,1637	77,8831	74,1564	63,1875	+		49.0361	77.1341	71.7144	79.1506	Н	83.6042	87 9489	77.8137	82:2395	9551.98	96.1556	96.1556	01.0/010	SK 31K1	9500.87	83.6347	68783	99,2012	98.2319	73.5882	91,0129	85.2742	85.2742
Н	Hr05	58.6673		96,6094	81.1861	82 3635	78.9993	78.9993	18 9993	78.9993	78 9993	73.1798	71.8923	72.5131	+	+	+	75,4307	H	-	72.1379	72.8126	73.8436	61.8992	+	+	49.7763	76.4396	71.9196	79,4633	77.7312	83.4951	23,630	80.5836	89 9160	16.2884	86.2884	86.2884	40.00390	86.1659	77.9746	83.4455	65.5393	97.8356	92.3716	73.5325	96.6522	Н	2068 98
П	+	53 7142	Н	94.7353	100.7928	56.2220	73.4725	73.4725	73.4725	73,4725	Н	73.0663		+	+	88.0560	99166	73 7363	t	H	H	73.4150	72,7084		9120	+	49 8811	75 9834	-	-	78.5920	83.4494	28 9366	₽	86.4802	1667.28	1	82.2991	2005	27 5840	78.5738	Н	69.2816	10	91.8452	73.4725	93 5340	86.7538	86.7538
	Hr03	56.2448	H	Н	65,4924	921706	73.1148	73,1148	73.1148	Н	Н	71.0190	Н	4	85,1348	+	+	75.0564	H	٠			-	Н	4	+	48 3727	+	H		77,7454	83.1153	72 11.69	₽	86.0232	Н	+	+	90.3350	٠	+	Н	-	101.4314	91.1961	65.492M	96.1728	83.9160	83.9160
П	7	57,7137		93.3150	Н	+	65.1773			65 1773	Н	71.0502		7	\neg	_	-	74 2463	+-	-	_		\neg	-		37.4402	-	+	۰		П	\neg	58 5773	_	Г	82.8923	+	82.8923	+	+	+		Н	н	7	+	87.7759	++	84.1070
П	-	55,2968	-	Н	Н	77.1498 3	+	+	H	68.6453	Н	72.0459		-	-	+	_	74 6757	+	٠	-	Н		60.9250	9662.68	36.7315		+	H		Н	\rightarrow	72 8076	+	83.5731	Н	+	+	OC COME	٠	+	Н	-	Н	+	+	87.8592 8	-	81.1856
П	+	89.3564	$\overline{}$	94.3526	Н	762156	+	1	$\overline{}$			71.6190		7	7	7	-1	74.4713	Т		71.2311			62.5783			49,0049	+	1	78.8550	П	\rightarrow	791761		82.0607	П	_	+	OC BECCO	٠				т	7	_	87.9501	П	84.8553

R002 R004 R004 R004 R005 R005 R005 R005 R005	833177.37 833231.06 833434.80 833966.46 833116.28	822330.25 822345.76 822408.45	833231.00 837414.80		mixing zone) 28 29	(m) 0	(caline 4)
R603 R603 R603 R604 R604 R605 R605 R605 R605 R605 R605	833221.06 833434.80 833966.45 833116.28	822345.76 822408.45	837414.80				1
R603 R603 R604 R604 R604 R605 R605 R605 R605 R605	833434.80 833960.46 833118.28	822408.45					_
R001 R104 R004 R004 R005 R005 R005 R005 R005	833966.45 833116.28				20	0	- 1
R104 R004 R004 R005 R005 R005 R005 R005	833116,28		933900,46	822643,00	20	0	1
R004 R004 R005 R005 R005 R005 R005			\$33995,46		20	0	
R004 R005 R005 R005 R005 R008+R607		822308.10	41741221		-19	0	. 1
R005 R005 R005 R005 R005	833188.93		833415.15		19	0	4.
R005 R005 R005 R008+R007	833425:15	832386.41	833518.28		39	0	1
R005 R005 R008+R007	833616.28	\$22421.55	813673.75		19	0	1
R005 R005+R007	\$23671.75	822494.5E	E1191347	822414.65	10	0	4.
R005-R007	633933.67	822614.88	W33973.71		19	0	1
	833973.71		834546.10		-10	0	1
	833527,80	622410.61	633/637.55	822455.21	14	0	. 4
R004-R007	833627.55	822A55.21	833732-97		18	0	1
R005+R007	833732.07	822494.47	833782.11		14	0	1
H004-R007	833762.11	822441.65	813840.51 833693.59	822456.02 822197.15	12	0	1
R003+R005 R003+R009	833693.50	822397.15	E33841.E4	822456.38	13	0	- 1
R010+R011	833978.15	822463.30	832004.64	822452.88	12	0	1
R010-R011	#33#94.64	622432.88	933993.54	822462.AD	12	0	1
R010+R011	833883.54	822A52.40	833849.51	822456.02	12	0	- 1
R\$12+R\$13	833387.26	822567.47	#33423.50		10	0	1
R012-R013	833423.69	822658.02	832416.08	822482.07	10	0	1
R012+R013	833416.08	822482.07	833447.62		10	0	1
MIN2+R013	833447.62	822425.39	#13544.64	627190-A1	10	0	1
R\$12+R\$13	833544.64	********	833517.56	. oregonists.	10	0	1
		822318.11			14	0	1
R014-R017		822354.88		022374.91	15	0	1
RB16*RB17			E33641.17		15	0	1
ROID	833082.67		833209.07		16	0	1
R021	833209.07		833355.00		16	0	1
R622	833355.00				18	0	1
R022	#334E0.61	822340.13	833419-65		18	0	1
PI023	833073.42	8221T9.68			19	0	7
M624		822129.64			14	- 0	- 1
R025	833232.06	Acc in bone	633377.60	EMP.114(4)	14	0	1
8128	823377.80				18	0	1
8027	633503.51		811073.82		-13	0	1
8020	832673.82		833768.11		13	0	1
R829	833766.63	822374.15	833843.76	821405.79	13	0	- 4
RISSO	\$33848.76	822405.79	E13917.E3	822431.11	18	0	- 1
H031	633917.63	822431.11	932990.58		14	0	1
H037+R301	833076.99	622000.71	933121.79	822072.07	10	0	7
8833	833121.79	622072.07	£13252.36		18	0	1
R034	833253.39	822120.94	83339E77	822175.17	18	0	1
REST	#33396.77	822176.17	833524.35	822221.21	18	0	- 4
R036	633524.35	822221.21	#32913.40	822269.00	18	0	- 1
R637	633653.40	822269.00	833694.86	822284.07	19	0	- 1
RESE	633694.68	822284.56	833763.79	622339.61	78.	0	4
RUST	833761.98	822311.12	E23788.45	822329.76	14	0	1
R040	833789.11	822318.08	832833.16	R22335.11	18	0	1
R041	833833.10	822335.57	833802.94	822160.57	18	0	- 4
R342	823902.96	822360.57	833965,46	822320.A5	-18	0	1
R043	813950.46	822320.6B	834014.90		12	0	1
R044	B34024.90	822250.62	834140.62	N12162.67	18	0	1
RIMS	834140.62	822182.67	834211.76	822086.45	39	0	- 1
RSAS	834211.72	822086-65	834323.21	822011.22	18	0	1
ROAT	854322.77	#22910.EE	834384.01	821939.68	- 18	0	1
H048	#33097.20		833,150,54		17	0	3
R549	833156.50		833434.10		16	0	1
R155	830101.47	821942.33	E13274.46		21	0	1
RUST	833274.56		211416.70	822067.62	16	0	1
R051	833434.10	822080.21	83364873	822174.73	16	0	1
R053		\$22123,44			18	0	1
R953	833736.68	#2219.1.2S			16	0	1
R054	833438.83	822967.29	#3251671		16	0	7
PI054	833584.71		833649.55		78	0	- 1
ROSA	83364R.55	622144.43	413613.61		16	0	1
R254	6336E1.68		813713.65		- 16	0	1
ROSA	623713.85		633757.83		16	0	1
R054	633767.83	832128:66	833778.49		16	0	1
R053	#337##.53	\$22123.04	833872,14	821651.30	19	0	1
R256	833778.49	#22113.30	8118h7.20	822039.12	16	0	7
WOST	#33973.20	822052.66	834119,21	821B1478	16	0	1
Rose	634159,21	821614.78	834250.10	821738.42	16	0	- 4
RUSS	633867.29	622031.23	65485E34	821680:22	-97	0	- 1
R065	83A068.34	821380.22	834241.51	821727.AS	16	0	1
R061	£3314£37	821890.28	833139.76	821889.31	16	0	1
R082	633139.76	821889.31	839294.78		16	0	1
RINS	833296.88	821947.56	833410,51	16 200129	16	0	1
ROSE	833450.49	#2250E.03	#11543.73	822038.72	13	0	7.
FI064	833543.73	832038.72	¥33.642.70	821983.31	15	0	- 1
R064	633489.98	821962-82	833543.70	8,21962.31	15	0	1
ROSS	833166.17	823834.07	613315.56		36	0	1
R066	833316.56	321301.68	#33461.00	821952.78	16	0	1
R087	833164.01	821778.07	83317847	021703.00	10	0	- 1
Attes	833178.74	621783.16	833253,69		- 18	0	
R(65	123164,10	821757.87 821820.73	813/260.16		13	0	1

r					_		_				NO ₂ x 10	0 (a/VMT)											
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
2.7462	2.7414	2.7123	2.7141	2.7490	2.7482	2.7886	4.5162	4.6506	3.8774	1.5835	3.4776	3.0937	3.1808	3.2012	3.5664	1.8182	3.5955	3.6708	3.1078	2.7554	2.5448	2.6312	2.7806
2.7462	2.7414	2,7123	2.7141	2.7490	2.7482	2.7886	4.5162	4.6506 4.6506	3.8774	1.5835	3.4776	3.0937	3,1808	3.2012	3.5664	1.8182	3.5955	3.6708	3.1078	2.7554	2.5448	2.6312	2.7806
2.7462	2.7414	2.7123	2.7141	2.7490	2.7482	2.7886	4.5162	4.6506	3.8774	1.5835	3.4776	3.0937	3,1808	3.2012	3.5664	3.8182	3.5955	3.6708	1.1078	2.7554	2.5448	2.6312	2.7806
2.7452	2.7414	2.7123	2.7141	2.7490	2.7482	2.7886	4.5162	4.6506	3.8774	1.5835	3.4776	3.0937	3.1808	3.2012	3.5664	18182	3.5955	3.6708	3.1078	2.7554	2,5448	2.6312	2.7806
2.7359	2.7248	2.7193	2.7325	2.7268	2.7196	2.7592	3,9895	4.2672	3.5161	1.3075	3.2744	2.9895	3.1059	3,1628	3.5774	3,9095	3.9830	4.0242	3,3441	2.6449	2.4591	2.5774	2.6542
2.7359	2.7248	2.7193	2.7325	2.7268	2.7196	2.7592	3,9895	4.2672 4.2672	3.5161	1.3075	3.2744	2.9895	3,1059	3.1628	3.5774	3.9095	3.9830	4.0242	3,3441	2.6449	2.4591	2.5774	2.6542
2.7232	2.7052	2.7238	2.7389	2.7379	2.7268	2.7650	3.9892	4.2682	3.5156	1.3071	3.2726	2.9870	3.1026	3.1598	3.5739	3.9061	3.9740	4.0199	3.3398	2.6394	2.4534	2.5715	2.6552
2.7232	2.7052	2.7238	2.7389	2.7379	2.7268	2.7650	3.9892	4.2682	3.5156	1.3071	3.2726	2.9870	3.1026	3.1598	3.5739	3.9061	3.9740	4.0199	3.3398	2.6394	2.4534	2.5715	2.6552
2.7232	2.7052	2.7238	2.7389	2.7379	2.7268	2.7650	3,9892	4.2682	3.5156	1.3071	3.2726	2.9870	3,1026	3,1598	3.5739	3.9061	3.9740	4.0199	5,3398	2.6394	2.4534	2.5715	2.6552
3.2790	2.7052	2.7238 4.1671	2.7389	2.7379 1.0998	2.7268 3.7724	2.7650 3.1834	3.9892	4.2682 2.7068	3.5156	1 3071	3.2726	2.5870 3.6761	3.1026	3.1598	3.5739 2.5493	1.9061	3.9740 1.7338	1.0632	3.3398 1.2307	2.6394	2.4534	2.5715 1.9518	2.6552 1.7821
3.2780	2.9460	4.1671	1.0933	1.0998	3.7724	3.1834	1.5803	2.7068	3.6183	1.3195	3.3513	3.6761	3.2042	2.4373	2.5493	1.4298	1.7338	1.0632	1.2307	1.3469	2.0847	1.9518	1.7821
3.2780	2:9460	4.1671	1.0933	1.0998	3.7724	3.1834	3.5801	2.7068	3.6183	1.3195	3.3513	3.6761	3.2042	2.4873	2.5493	1.4298	1.7338	1.0632	1.2307	1.3469	2.0847	1.9518	1.7821
3.2790	2.9460	4.1671 2.3897	1.0933	1.0998	3.7724 2.1649	3.1834	3.5803 2.8304	2,7068	3.6183 2.5237	1.3195 1.3087	3.3513 2.4245	3.6761 2.2621	3.2042 1.8398	2.4373 1.7298	2.5493	1.4298	1,7338	1.0632 1.1431	1.1403	1.3469	2.0847	1.9518 2.3516	1.7821
2.1420	2.6291	2.3897	1.0933	1.0998	2.1649	2.1254	2.8304	2.0458	2.5237	2.3087	2.4245	2.2621	1.8198	1.7298	2.1411	1.5003	1.7348	1.1431	1.1403	1.3626	2.4188	2,3516	1.5403
4.4984	4.4620	3.9383	2.7108	4.7988	5.7116	4.5071	5.3841	4.5503	5.1549	4.8506	5.3041	5.0357	4.9161	4.3475	5.1084	4.5630	4.3599	4.1707	3.9337	4.7221	5.5346	5,0432	4.9908
4.4984	4.4620	3.9383	2.7108	4,7988	5.7116	4.5071	5.3843	4.5503	5.1549	4.8506	5.3041	5.0357	4.9161	4.3475	5.1084	4,5630	4.3599	4.1707	3.9337	4.7221	5.5346	5,0432	4.9908
4.4984 11.4928	4.4620	3.9383 1.3946	2.7108	4,7988	5.7116	4.5071 11.5273	5.3841 15.6059	9.7476	5.1549 12.8818	4.8506	5.3041	12.2035	4.9161 15.7472	4.3475	5.1084	4.5630 11.8077	4.3599	4.1707	3.9337	4.7221	5.5346 23.5114	5.0432 18.4249	4.9908 14.1592
11.4928	13.2568	13946	1.8271	1.8336	1.8340	11.5273	15.6059	9.7476	12.8818	10.8813	13.0422	17.7035	15.7472	11.6783	12.1712	11.8077	13.2549	15.1997	12.9495	20.2840	23.5114	18.4249	14.1592
11.4928	13.2568	1.3946	1.8271	1.8336	1.8340	11.5273	15.6059	9.7476	12.8818	10.8813	13.0422	12.7035	15.7472	11.6783	12.1712	11.8077	13.2549	15.1997	12.9495	20.2840	23.5114	18.4249	14.1592
11.4928 11.4928	13.2568	1.3946	1.8271	1.8336	1.8340	11.5273	15.6059	9.7476	12.8818 12.8818	10.8813	13.0422	12.2035	15.7472	11.6783	12.1712	11.8077	13.2549	15.1997	12.9495	20.2840	23.5114	18.4249 18.4249	14.1592
5.4601	5.5646	6.0298	7.438R	7.0271	6.9012	5.7815	9.2137	4.9218	6.1777	6.3062	7.1657	6.7759	7.5558	6.1418	7.0187	6.7299	7.0718	6.8934	6.4628	8.6372	10.8930	9.9276	7.1555
5.5116	5.7087	6.0298	4.8880	4.6469	6.9012	5.3810	8.6738	4.6551	5.8917	5,7413	6.2477	5.8849	6.1701	5,2893	5.8611	4.8934	5.4150	5.0523	4.4827	6.5613	7.9404	6.5175	5.5561
5.5116	5.7087	6.0298	4.8880	4.6469	6.9012	5.3810	8.6738	4.6551	5.8917	5,7413	6.2477	5.8849	6,1701	5.2893	5.8631	4.8934	5.4150	5.0523	4,4827	6.5613	7.9404	6,5175	5.5561
13.5910	13,8360	12.6270	14.4766	15.1713	12.7439	12.9283	15,4881	12.4101	14.1005	12.6643	14.2399	13.1447	15.0635	12.0358	13.7658	14,6170	12.6295	12.3327	11.9210	15.9639 15.8576	19.7101 18.4258	14.3106 15.1396	15.0994
16.6585	15.1412	15.4431	17.3214	16.5309	16.3808	16.5746	18.0797	15.3546	17.0773	15.7963	17.0703	16.0173	17.4949	14.6572	16.0461	16.8192	14.9922	14.7300	14.0475	17.3181	19.8654	16.7755	16.6700
16.6585	15.1412	16.4431	17.3214	16.5309	16.3808	16.6746	18.0797	15.3546	17.0773	15.7963	17.0703	16.0173	17.4949	14.6572	16.0461	16.8192	14.9922	14.7300	14.6475	17.3181	19.8654	16,7755	16.0700
15.2487	13.4580	15.3813	15,2468	15.5237	14.0910	14.8252	17.8181	15.2254	16.6275	15.2596	16.4119	15.4734	17.2570	14.1108	15.5165	15.7321	14.7837	14.8660	13.7019	16.9620	19.5583	15.9488	14.5369
15.7619	13.9945	14.2536	13.1344	15.5237	14.8678	15.2646	17.3990	14.9476	16.7461	15.3383	16.4375	15.1255	17.0829 16.8330	14.0468	15.4706 15.6423	15.9510	14.9530	14.5006	13.3441	17.0295	19.1650	16.0613	14.7995
16.7649	16.4142	16.9511	17.6051	16.8876	16.0116	16.8359	19.7432	18.5898	19.1112	17.2185	18.1489	16.1901	18.2421	14.8127	16.3949	17.7095	15.8506	14.8167	13.9680	17.4382	18.7409	15.5182	15.2954
16.3278	15.8842	15,7318	16.0173	16-5612	16.9976	16.2749	18,4841	17.0757	18.5906	17.3379	18.3139	17.1937	18,5395	16.2939	17.0300	17.3656	16 1684	15,6945	14.5888	17.4194	20.2653	16.4850	15-6082
13.3862	10.9012	13.3476	15.7415 7.4388	14.5273	12.6782	13.4098	15.0191	12.7961	14.6039	13.1745	14.1412	13.4721	15.0912	12.6438	13.9894	14.2713	13.4403	13.5607	12.7344	15.8125 16.7167	18.7979	15.3807	13.4927
11.6760	11.6652	12.1503	11.7913	10.2734	11.5702	11.5751	15.8149	13.0277	13.9522	11.9197	13.7218	13.1157	14.7056	11.7345	13.4993	13.9428	12 9236	12.7641	11.3599	15.1045	17.5713	13.7568	13.0511
10.9059	13.1141	8.5566	10.2447	10.2734	7.4642	11.8366	16,9810	15.2675	15.4746	13.4844	14.5305	12.6277	15.7082	11.9934	13.6776	15.0614	13.1817	12.7699	12,2755	16.1264	17.9383	14.5952	14 1402
15:0724	14.5513	11.2759	11.2385	10.9122	10.8450	11.3073	14.3874	11.8486	13.2873	12.1020	13.5701	17.5806	14.2537	11.6910	13.1100	13.2560	12.6726	12.5582	11.6039	14.9138	16.8771	13.8594	13.0145
12.0347	12.0429	12.0837	12.1726	12.2938 11.1721	12.0771	12.1225	14,3694	11.6132	13.1633	11.8534	13.1596	12.185Z 11.7902	13.7826	11.4904	12.9675 12.6678	13.0766 12.8180	12.4576 12.2565	12.3365	11.3693	14.3694	16.8192	13.8062	12.5914
13.5874	13,4437	13.3554	13.1000	13.2127	13.1504	13.3366	16.2639	14.0317	15.2407	13.9385	15,0304	14.2167	15.6891	12.9551	14.9800	14.9187	13.4325	13.1878	12.5248	15.3760	18.0827	14.8911	14.0502
12.5176	12.3462	12.3803	12.5044	12.3633	12.5618	12.4612	14.9999	12.8431	14.4444	12.8332	14.2170	13.1663	14.8641	12.2423	13.7333	11-8231	13.2169	13.1355	12.1342	15.1063	17.1491	14.1797	13.4184
16.6707	16.5519	15.5607	16.6992	16.5715	16.5638	16.6945	19.8237	16.9528	18.8714	16.2857	17.6982	15.9385	17.9069	14.1847	15.5647	15.4073	14.1888	13.7985	12.7656	15.9975	18.4929	15.1947	14,2025
16.8988	16,8101	16.8876	16.7946	16.9233	16.9421	18.9600	20.1462	17.1115	19.1610 22.1751	16.2193	17.5524 20.8767	15.5466	17.3366 20.7075	13.4966	14,7415	14.7961	13,0774	12.2878	11,4662	14.2262	16.4322 18.4947	13.5491	12.8000
19.5044	19 6422	19.5953	19.9375	19.6999	19.8657	19.7796	23.0119	21.5817	21.9076	19.2663	20.1301	18.0672	19.9971	15.5085	17.9748	18-1090	15.4741	13.8029	13.4081	16.1513	17.8846	14.4254	15.5359
19.9144	18.8785	19.2815	19.3868	19.1740	19.5231	19,2477	23,7272	22.3284	22.6796	19.5377	20.8158	18.6721	20.6541	15.1711	18.5474	18.6176	15.5604	13.9644	13.5996	16.5663	18.6217	14.7799	15.8259
19.9843	19.2518	19,2858	19.3734 22.4991	19.3096	19.6119	19.4331	23,1951 25,4264	21.7831	22.1491	19.0355 21.6036	20.2911	18.1498	20,1762	15.6585 18.1740	18,4787 21,1060	18.5364 21.4789	15,3527	13.6390	13.3118	16,3100	17.9250 21.0073	14,4775	15.5757
19.5788	19.4921	19.5795	19.9032	19.6668	19.7084	19.7551	22,9628	21.5781	21.8751	18-7864	20.1381	18.0053	19.9678	15.5197	17.8985	18.4179	15.2971	13.5815	13-1824	16.0539	17.7260	14.2724	15.3309
19.9043	16.3657	16.5937	17.4302	17.7583	17.4935	19.8136	22.5648	21.1646	21.4942	19.0452	20.3136	18.2570	20.2768	15.9204	18.2362	18.4236	15.4133	13.8089	13.7852	16.3253	18.2135	14.8975	15.8813
20.1009	18.9950	19.0858	19,4255	19.2042	19.3935	20,2003	23,2765	21.9475	22.2599	19.2922	20.5017	18.4048	20.2951	15.9619	18.1906	18.6766	15,5941	13.9551	13.6040	16.5111	18.0368	14.6875	15.8100
20.1042 14.5668	18.8729	19.1736	19.2805	19,4138	19.3053	20.2220	17.5727	21.4994 17.0055	21.7970 17.2048	19.3070	20.5821	18.4388 14.4854	20.3545	16.0122	18.2773	18 3251 15.6115	15.6507	13.9582	13.6201	16.5634 15.3678	18.0820 17.4891	14.7501	15.6417
14.5895	14.5254	14.5651	14.5385	14.5882	14,5518	14.6313	17.2713	16.3885	16.5952	14.2943	15.7444	14.2797	16.2258	12.7653	14.7931	15.1967	13.5644	12.8768	12.0568	15.4250	17.5259	14.1487	14.1512
15.5307	15.5326	15,5424	15.4891	15.5209	15.5755	15,5883	18:5715	17.5492	18.3490	15.5497	16.8654	15.0856	17.0706	13,5261	15.3251	15,4325	13,7831	12.7396	11,7402	14.1993	15.8372	12.6179	12.8952
16.7187	16.7462	16.7859 16.5023	16.7535 16.6561	16.7722 16.6736	16.8120	16.3085	19.6433	18.4749 19.0665	19.0233 18.1811	16.3155	17.7640	15.9954	18.2856 17.7149	14.5192	16.6133	17.3650 16.8247	14.9557	13.6743	12.8961	15.6653	17.4340 18.0943	13.9679	14.9188
17.8913	17.2561	17.2865	17.3122	17.3871	17.4056	17.8458	20.3333	19.8380	19.5231	16.8005	18.2433	16.4044	18.8614	14.9176	17.3115	17.7977	15.5490	14.5955	13.8254	16.9944	19.0344	15.2982	15.8253
17.8913	17.2561	17.2865	17.3122	17.3871	17.4056	17.8458	20.3333	19.8380	19.5231	16.8005	18.2433	16.4044	18.8614	14.9176	17.3115	17,7977	15.5490	14.5955	13.8254	16,9944	19.0344	15.2982	15.8253
18.3401	18.3160	18.2484	18.3537	18.4341	18.3582	18.3907	20.8266	19.8939	20.1118	17.7731	19.2382	17.7782	20.3976	16.3343	19.1812	20.4354	17.6271	16.5066	15.8450	19.2891	21.3268	17.0223	18.2000
18.3401 18.3461	18.3160	18.2484 18.2484	18.3537	18.4341	18.3582	18.3907 18.3907	20.8266	19.8939	20.111M 20.1118	17.7731	19.2382	17,7782	20.3976	16.3343	19.1812	20.4354	17.6271	16.5066 16.5066	15.8450 15.8450	19.2891	21.3268	17.0223	18.2000
18.3401	18.3160	18.2484	18.3537	18.4341	18.3582	18.3907	20.8266	19.8939	20.1118	17,7731	19,2382	17.7782	20,3976	16.3343	19.1812	20,4354	17.6271	16.5066	15.8450	19.2891	21.3268	17.0223	18.2000
18.3401	18.3160	18.2484	18.3537	18.4341	18.3582	18.3907	20.8266	19.8939	20.1118	17,7731	19.2382	17.7782	20.3976	16.3343	19.1812	20.4354	17.6271	16.5066	15.8450	19.2891	21.3268	17.0223	18.2000
18.3401	18.3160	18.2484	18.3537	18.4341	18.3582	18.3907	20.8266	19.8939	20.1118	17.7731	19.2382	17,7782	20.3976	16.3343	19.1812	20.4354	17.6271	16.5066	15.8450	19.2891	21.3268	17.0223	18-2000
16.9382 20.8843	16.9247	16.9174	16.8874 20.8535	16.9797 20.9290	17.0190 21.0133	16.9858	19.3164	18.0486 23.0178	18.3214 21.6889	16.0119	17.0890 21.2334	15.3342 19.2558	17.4699 22.3051	13.6830	15.8261 21.0728	16.0551 22.3129	14.0240	13.2352	12.4632	15.7225 20.4200	17.7541 22.1279	14.3418	14.5114
13.7853	12.8101	12.9201	13.1524	13.1133	13.1553	13.7855	15.7565	16.3228	14.3956	12.9626	13.7119	12.5198	13.7084	11.0762	13.8063	14.4077	11.8768	9.6059	10.0884	11.6953	12.5039	10.0498	12.3598
19.1529	18.1557	18.1356	18:3775	18.3883	18.5368	19.2105	21.7233	21.0470	20.2503	17.6294	18.9322	16.8857	19.2451	14.8792	17.2902	17.6928	14.7613	13.5739	13.3508	16.7253	18.6541	14.9679	15.7271
16.1475	16.2059	16.1325	16.0694	16.3408 19.9645	16.1868	16.2167	18.3336	19.1147	16.6331 20.6966	15.2837 18.6566	16.0736	16.6736	16.1241 21.7564	12.9589 16.8418	16.2265 20.6900	17.0631 22.0162	13,5088	10.8994	11,6129	13,4305	14.0896 22.1811	17.1018	14.2261
23.0940	22.0706	22.2239	20.0146	20.5251	20.1097	22,7615	22.6184	22.1182	22.8946	22.4186	20.5079	22.5050	22.9221	22.2026	22.8097	22.9233	22.2226	22:3724	22.1775	22.9108	23.6401	23.0737	22.1549
12.8771	12:4674	12.6238	12.5034	13.3134	13.3169	12.7239	15.1333	13.1922	14.2743	13.1950	14.6495	13.7680	15.3005	12.4482	14.2439	14.5696	13.3935	13.0080	11.9226	15.1340	17.7450	14.2439	14.0039
13.4662	11 3376	13.5652	11.5465	13.6397	12.0989	12.9607	15,9896	12.9494	14.3419	13.0124	14.3457	13.2434	15.1561	12,3228	13.7844	14.2275	12,9396	13.0233	11.9723	15.5017	18.1219	14.9920	14.1999
12.7095	10.4595	12,2509	13.1087	12,0583	11.5685	12,2061	15,4599	12.3175	13.7698 13.7698	12.2855	14.0701	12.8037	14.6605	11.6671	13.4653	13.6929	12.3284	12.3222	11.7534	15.3710	18.0543	14.8418	14.3246
12.7095	10.4595	12.2509	13.1087	12.0583	11.5685	12.7061	15.4599	123175	13.7698	12.2855	14.0701	12.8037	14.6605	11.6671	13.4653	13.6929	12.3284	12.3222	11.7534	15.3710	18.0543	14.8418	14.3246
14.5851	13.2493	13.9766	14.3368	13.6796	13.0767	14.7470	16,2157	13.7894	15.3721	14.0701	15.5627	14.5201	15.7800	13.0566	14.2993	14.8039	13.3891	12.6076	11,9040	15.0116	17.6695	14.6397	14.1546
13.7886	13.5731	13.2693	14.0847	13.5721	12.6056	13.7182	16.2322	13.2117	14.8840	13.5730	14.9839	13.7615	15.1563	12.7033	14.2345	13.9479	13,0797	12.6339	11.8124	14.9935	17.7673	14.3232	13.5334
9.7648 9.6786	9.7426	9.7146	9.7083	9.7293	9.7606	9.7830	13.2317	10.4592	12.600N 12.5495	10.9745	12.3327	11.0716	12.9223 12.8798	10.0712	10.8539	10.7130	10.2960	10.7318	9.6767	11.5568	13.2558	10.7381	9.1763
7.2563	7.2785	7.2365	7.2322	7.2643	7.2733	7.2937	8.8500	7.0513	8.6199	7,3037	8.2569	7.6403	8.9640	7.3544	7.9698	7.9168	8,7702	9.6220	7.5489	10.1392	12.3333	10.0202	7.9781
12.6813	12.6056	12.6285	12.5525	12.6395	12.6515	12.5899	14.8994	12.1636	14.3944	12.3843	13.7150	12.4436	14.1986	11.4330	12.1764	12.1815	11.8308	12.1210	10.7688	13.8717	16.3131	13.4821	11.8552

Road			nate (m)		(including	Height	Road Type
Pair	X1	Y1	X2	Y2	mixing rope)	(m)	(caline 4)
Rd71	8333E7.91	521859.25	533397.24	821875.22	18	0	1
RU72	833597.24	\$2187 b.ZZ	833501.75	821697-07	20	0	4
R073	8334E1.50	621980.54	833397.24	821875.22	- 0	0	1
R074	833261.64		833451.60	821860.54	20	0	
R875					16	0	1
		621961,09		821683,08			
RU76	\$33501.48	921897.80	83356846	821699.77	16	0	1
R076	633548.66	821899.77	823603.43	821866.99	16	0	4.
9074	832602.43	821689.59	83368492	821822.32	14	0	1
R677	833564.57	821884.14	833563.57	821884.36	32	0	
							1
R077	\$336E1.57		E33600.48	821871.28	17	0	
HOT2	633000.48	821971.28	931973.84	821812.08	17	0	- 1
ROTE	833662.38	621822.35	833875.32	821660.76	16	0	1
B279	833673.29	621811.43	633867.51	821651.48	16	0	
R060					16	0	1
	833674,67	221661.12	811999.54	821557.98			
R091	833.667.01	821650.86	932013.08	821852.08	20	0	4
R082	833458.18	821884.41	813510.76	821821.12	16	0	1 1
Rta2	823510.75	621821.12	833518.39	8217B5.93	14	0	
ROSE	\$33526.39	821785.93	E33570.13	821657.58	14	0	1.
ROES						0	1
	833424.63	821665.11	833496.18	821813.12	18		1
R083	833496.18	821913,12	933524.36	821772.25	14		
B193	833524.38	821772.29	813569.51	821652.62	14	0	
R094	\$33567.54	821687.02	233512.60	821644.65	13	0	1
R094	833582.69	821644.85	833607.71	821003.87	13	0	1
Ross	833009.34		833640.24	021575.52	14	0	1
RISES		82) 57 8-52	813691.67	821545.20	14	0	4
R065	\$33681.67	821545.20	823720.62	821512.85	18	0	- 1
HOSE.	833580,70			021102.58	17	0	1
ROPE.		621533.58	811646.81	021545.45	17	. 0	1
R087		\$2154E-43			- 33	0	1
#198 ·		821811.68			12	. 4	- 4
ROBE.	433305.50		833416.50	821865.51	12		4
Rtbs	833416.50	521985.51	533487,63	821641.08	97	-9	- 4
ROSS		821BA1.09	833553-63	821788.07	17	10	4
Ross		821786.07					_
					1T		
HOER.	833574.80	821657.75	933600.16	821605.82	17	d	
Ross	833696.16	621605.8Z	533712.05	821511.11	57	6	
8299	833256-85		\$13,370.00	821646.87	16		
Ross		821846.87	832427.26	821852.03	16	-	1
RORP				821829.25	14	. 0	4
Ritas .	833480.60	821929.25	83352246	821786.30	36	10	- 4
RISES	833522.46	821784.32	E11545.19	821725.AT	16	. 0	- 4
HOEK	833543.19		833562.07	821653.37	16	1	
		621653.37	W3350E25				4
RORR				021504.44	16		
6093		621594.44	613699.51	821508.87	16	6	4
050+R091	833259.78	821629.64	833337.54	621634.13	97	0	- 1
197-R993	#33337.92	821632.93	£13449.56	821640.31	20	0	- 4
092-H093				821509.24	20	0	
							1
R094		\$21634.13	833341.61	821576.41	16	0	1
R095	833609.59	621501.FZ	833548.49	821548.43	97	0	4
095+R097	433980.58	#22454.38	E3402E77	822414.27	18	0	1 -
098-R009	834028.77	822414.27	934127.62	822302.11	18	0	1
100-R101			83421831		18	0	- 4
		822332.11		822258.38			
192+R103	83A216.31	822258.35	E34309.95	822190.58	-18	0	1
1104+R105	834300.95	822180.SE	834407.46	822098.55	18	0	1
R106	833917.83	822431.11	833991.74	022309.39	18		1
8107	833991.55	822270.04	834890.33	822287.53	- 10	0	- 4
R108	834090.84		834181.98	822212.22	36	0	1
R169	ESATE1.SE	822212.22	834275.08	\$22156.AB	17	0 -	- 1
RITE	834173.34	822134.83	#3436436	922060.84	17	0	- 1
R111	834363.46	822009.86	834400.74	822628.83	- 16	0	1
R112	833846.76	822 AD 5.79	£11992.95	822380.57	19	0	1
Atti		822334.17			18	0	1
R114	R33309.65	822271.35	833994A7	822301.23	18	0	1
R115	#339\$4.06	\$22200.75	834977.01	822132.08	18	0	1.
RUE	834076.99	822131.84	834097.30	822115.02	18	0	1
RHIT	834097.30	822115.02	E34110.89	822007.73	18	0	
Ritta		622037.73			- tr	0	1
RIII	83424Z.94		834292.16	021961.A5	-19	0	1
R120	R3A281.93			821895.00	- 18	0	1
R121	833768.03		#33780.11	822316.98	16	0	4
R122	633761.98	822311.12	833818.78	922222.16	18	0	1
R123	831848.78	\$22222 16	833954.75	822150.50	18	0	- 1
R124	833671.92	622341.72	STIMASE	822284.02	16	0	9
R125	833094.80	822254.07	822827.77	822172.05	10	0	1
R126	#33093.40	822269.00	833988.33	822174.73	12	0	- 9
R127	633489.65	822315.75	633502.51	822278.AE	-98	0	1
R128	12.500 EX	82227 B.46	#33574.35	822221,21	18	0	-1
R129	833377.80	822222.03	833315.00	822293.72	18	0	1
	833377,80	822732.63	833318.77	822175.17	18	0	1
R120	833596.42	822175.04	813434.10	822000.78	18	0	4
R120	833431.92		#13410.51	822007.97	16	0	- 7
R131	R33460.45				16	0	-
R131			¥334\$1.00	821952.78		_	
R131 R132 R133		821982.76	832506.97	821567.08	16	0	1
R133 R132 R133 R134	823481.00		413732.64	822178.01	78	0	1
R131 R132 R133		822239.78	griffithe.				
R133 R132 R133 R134 R135	823481.00			822120.94	18	0	1
R133 R132 R133 R134 R135 R136	833481.00 833259.67 833232.03	822178.06	#11211.39	822120.04		0	1
R131 R132 R133 R134 R135 R136 R137	833269.87 833232.93 833232.93 833080.91	822178 06 822182.63	#33253.30 #33100.63	822129.44	18	0	1
R131 R132 R133 R134 R135 R136 R137 R138	833209.67 833232.03 833232.03 833080.91 833100.63	822178 06 822182.63 822129.64	#33253.30 #33100.83 #33121.79	822129,44 822672,07	18	0	1
R131 R132 R133 R134 R135 R136 R131	833481.00 833205.07 633232.03 833080.81 833100.53 833121.68	822178 06 822182.63	#33252.30 #33100.#3 #33121.79 #3315#.56	822129.44 822672.07 621877.98	18	0	1

					_						NO ₂ x 10	O (a/VMT)											
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Bort	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
12.3567	12.3847	12.4325	12.4494	12.3866	12.4983	12,4606	14.3443	11.5737	13.7160	11.9810	13.1141	11.8753	13.5959	11.0235	11.8197	11.6749	11.3003	11.6817	10.3914	13.6273	15.9771	13.2489	11.6568
10.8514	10.8057	10.7710	10.8577	11.0294	10.7497	10.7602	12.6313	10.3979	11.3954	10.0363	11.0657	10.0021	11,2495	8.8840	10.0798	10.0444	9.2293	8.8206	8.2799	10.9312	12.7706	10.4282	9.7310
11.2263	11.0753	11.2218	11.2623 11.2908	11.4217	11.1212	11.2057 11.4538	12.8316	9.9987	12.0233	10.7197	11.8056	10.9120	12.1484 12.0385	9.8259	10.8353	10.6731	9.9689	10.7582 10.1498	9.9630	12.5340	14.4801	12.3172	11.2346
10.3218	10.3430	10.7259	10.3530	10.2954	10.4791	10.4112	11.9470	9.3833	10.8867	9,7708	10.7540	9.8037	10.9049	8.8439	9.5529	9.2820	9.0499	9.2357	8.3759	11.2007	13:3340	11.1092	9,4818
11.5304	11.7832	11.5615	11.7570	11.7395	11.5874	11.6647	13.5650	11.3035	12.2269	10.860)	12.0242	10.8782	12.5647	9.9004	11.0387	10.9867	10.2687	10.4622	9.5404	13.0392	15.4026	12.5719	10.9896
11.5304	11.7832	11.5615	11.7570	11.7395	11.5874	11.6647	13.5650	11.3035	12.2269	10.8603	12.0242	10.8782	12,5647	9.9004	11.0387	10.9867	10.2687	10.4622	9.5404	13.0392	15.4026	12.5719	10.9896
11.5304	11.7882	11.5615	11.7570	11.7395	11.5874	11.6647	13.5650	11.3035	12.2269	10.8601	12.0242	10.8782	12.5647	9.9004	11.0387	10.9867	10.2687	10.4622	9.5404	13.0392	15.4026	12.5719	10.9896
10.5572	10.6212	10.5959	10.5895	10.6845	10.5991	10.5473	12.2904	9.7662	11.3464	10.0838	11.1739	10.1888	11.6033	9.3998	10.1380	9.9525	9.8861	10.2099	9.1977	12.4562 12.4562	14.8406	12.2472	10.4624
10.5572	10.6212	10.5959	10.5895	10.6845	10.5991	10.6473	12.2904	9.7662	11.3464	10.0838	11.1739	10.1888	11.6033	9.3998	10.1380	9.9525	9.8861	10.2099	9.1977	12.4562	14.8406	12.2472	10.4624
13.1711	12.9829	13.0351	13.1078	- 13.1170	13.2567	13.2032	15.1468	13.0854	13.8471	12.3539	13.5057	12.1823	13,7933	11.0334	12 1213	12.0814	11.1289	11.2360	10.4004	13.5738	15.8871	13.1436	11.9090
9.6333	9.8118	9.6805	9.7396	9.7372	9.6414	9.7578	11,2278	8.4499	10.2446	9.3334	10.4434	9.6427	10.9946	9.0444	9.5725	9.3459	9.5236	10.3217	9.1536	12.5484	15.0309	12.4914	10.2455
10.3384	10.4832	12.3549	12.4131	12.3973	12.1618	12.3278 10.4888	14.2334	10.5878	13.0158	10.1097	12.8019	10.1157	13.3274	10.3964	11.2833	11.0797	10.5160	10.9559	9.8263	13.4974	16.1187	13.1214	11.3549
15.0022	15.1746	10.3951	10.4013	10.4018	10.3297	15.0590	17.4113	9.2179	16.9995	14.9497	16.5381	15.1999	11.5744 17.2160	9.7182	10.2176	9.9537	10.0488	10.8569	9.7222	17.2633	19.9477	12.9875	10.8385
15.0022	15.1746	14.9343	14.9505	15.0275	14.8136	15.0590	17.4113	13.6557	16.9995	14.9497	16.5381	15.1999	17.2160	14.2692	14.9256	14.7012	14.3274	14.9708	13.8307	17.2633	19.9477	16.8511	14.8342
15.0022	15.1746	14.9343	14.9505	15.0275	14.8736	15,0590	17.4113	13.6557	16.9995	14.9497	16.5381	15.1999	17.2160	14.2692	14.9256	14,7012	14.3274	14.9708	13.8307	17.2633	19.9477	16.8511	14.8342
6.5882	6.7962	6.8584	6.9287	7.0539	6.8763	6.7470	7.2713	6.5880	7.4718	6.9196	7.3177	7.0546	7.2190	6.6701	6.9272	6.5855	6.4803	6.6424	6.3138	7.3212	3.5986	7,7742	6.8057
6.5882	6.7962	6.8584 6.8584	6.9287	7.0539	6.8763	6.7470	7.2713	6.5880	7.471H 7.4718	6.9196	7.3177	7.0546	7.2190 7.2190	6.6701 6.6701	6.9272	6.5855	6.4803	6.6424	6.3138	7.3212	3.5985 3.5985	7,7742	6.8057
15.0811	14.9285	14.9000	15.0089	14.9964	14.9090	15.0176	17.3667	13.3073	16.6013	14.9366	16.6629	15.3642	17,6232	14.6348	14.9890	14.7562	15.1578	16.2948	14.7501	18.7295	21.8010	18.5952	15.5093
15.0811	14.9285	14.9000	15.0089	14.9964	14.9090	15.0176	17.3667	13.3073	16.6013	14.9366	16.6629	15.3642	17.6232	14.6348	14.9890	14.7562	15.1578	16.2948	14.7501	18.7295	21.8010	18.5952	15.5093
15,9310	16.0420	15.9964	16.0230	16.0165	16.0562	16,1689	18.1668	14,6908	17.5619	16.0699	17.6376	16.3859	18.3153	15.5839	15.8460	15.5629	15.5633	16.8610	15.1048	19.0618	22.0443	18:5820	16.1228
15.9340	16.0420	15.9964	16.0230	16.0165	16.0562	16.1689	18.1668	14.6908	17.5619	16.0699	17.6376	16.3859	18.3153	15.5839	15.8460 15.8460	15.5629	15.5633	16.8610	15.1048	19.0618	22.0443	18.5820	16.1228
15.9380	15.2331	15.3964	16.0230 15.0689	16,0165	16.0562	15.3437	17.1114	13.1937	17.5619 16.4858	14.5453	16.0477	14.6930	18.3153 16.5578	15.5839 13.8004	14.0285	15.5629	15.5633	16.6610	13.1667	16.8177	22.0443 19.7048	17.0171	14.2038
15.3495	15.2331	15.3980	15.0689	15.2990	15.3333	15.3437	17.1114	13.1937	16.485H	14.5453	16.0477	14.6930	16.5578	13.8004	14.0285	13.5656	13.5581	14.5437	13.1667	16.8122	19.704R	17.0171	14.2038
21.7394	21,6880	21.7244	21.5357	21.5568	21.5421	21.6441	22.2582	21.2491	22.3543	21.9070	22.4352	21.9256	22.4580	21.7080	21.8004	21.6728	21.5163	21.9206	21,2120	22.1990	23.0111	22.1360	21.5047
2.4959	2.4716	2.4690	2.4742	2.4558	2.4952	2.5189	4.0261	4.1959	4.0832	3.8191	3.2429	2.9724	2.5945	2.7193	2.5550	2.3919	2.3575	2.0744	1.6925	1,7709	1.7587	1,8398	1.6432
2.4959	2.4716	2,4690	2.4742	2.4558	2.4952	2.5189	4.0261	4.1959	4.0832	3.8191 3.8191	3.2429	2.9724	2.5945	2.7193	2.5550	2.3919	2.3575	2.0744	1.6925	1.7709	1.7587	1.8398	1.6432
2.4959	2.4716	2.4690	2.4742	2.4558	2.4952	2.5189	4.0261	4.1959	4.0832	1.8191	3.2429	2.9724	2.5945	2.7193	2.5550	2.3919	2.3575	2.0744	1.6925	1.7709	1.7587	1,8398	1.6432
2.4959	2.4716	2.4690	2.4742	2.4558	2.4952	2.5189	4.0251	4.1959	4.0832	1.8191	3.2429	2.9724	2,5945	2.7193	2.5550	2.3919	2.3575	2.0744	1.6925	1.7709	1.7587	1.8398	1.6432
2.4959	2.4716	2.4690	2.4742	2.4558	2.4952	2.5189	4.0261	4.1950	4.0832	1.8191	3.2429	2.9724	2.5945	2.7193	2.5550	2.3919	2.3575	2.0744	1.6925	1.7709	1.7587	1.8398	1.6412
2,4959	2,4716	2.4690	2,4742	2.4558 2.4656	2.4952	2.5189	4,0251 3,0832	4.1959	4.0832	1.8191	3.2429	2.9724	2.5945	2,7193	2.5550	2.3919	2.3575	2.0744	1.6925	1,7709	1.7587	1.8398	1.6432
2.4468 2.4468	2.4250	2.4394	2.4395	2.4656	2.4540	2.4727	3.0832	3.1262	2.9630	2.8823	2.5394	2.4437	2.1913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1,7564 1,7564	1.6149
2.4458	2.4250	2.4394	2.4395	2.4656	2.4540	2.4727	3.0832	3.1762	2.9630	2.8823	2.5394	2.4437	2.1913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1.7564	1.6149
2.4458	2.4250	2,4394	2.4395	2.4656	2,4540	2.4727	3.0832	3.1262	2.9630	2.8823	2.5394	2.4437	2.2913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1.7564	1.6149
2.4468	2.4250	2.4394	2,4395	2,4656	2.4540	2.4727	3.0832	3.1262	2.9630	2.8823	2.5394	2.4437	2.1913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1.7564	1.6149
2.4468	2.4250	2.4394	2.4395	2.4656	2.4540	2.4727	3.0832	3.1262	2.9630	2.8823	2.5394	2.4437	2.1913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1,7564	1.6149
2.4458	2.4250	2,4394	2.4395	2.4656	2.4540	2.4727	3.0832	3.1262	2.9630	2.8823	2.5394	2.4437	2.1913	2.3173	2.1737	2.1039	2.2297	2.0580	1.5703	1.7004	1.7230	1,7564	1.5149
9,4721	9.5548	9.3763	9.4337	9,5935	9.4124	9.4695	12.0154	9.4610	11.1916	9,7100	10.9435	10.1894	11,3218	9.3385	10.8669	10.7487	10.6401	10.2269	9.3775	11.9069	14.1703	11.2627	10.2487
9.2187	9,0352	9.7612	9,9096	9.7905	8.7712	9.3337	11.6699	9.1522	10.7437	9.7733	10.8670	10.1256	11.4211	9.1989	10.7168	10.7642	10.4285	10.0075	9.2080	11.8455	14.0586	11.3186	10.6557
9.2187	9.0352	9.7612	9.9096	9.7905	8.7712	9.3337	11.6699	9.1522	10.7437	9.7733	10.8670	10.1256	11.4211	9.1989	10.7188	10.7642	10.4285	10.0075	9.2080	11.8455	14.0586	11.3186	10.6557
5.8637 23.8862	5.8379 23.5953	5.8159	5.9299	5.9619	5.9685	5.7900	25.0031	4.7611 24.1965	6.2958 24.8092	5.3079 24.5072	5.5836 25.0260	4.9049 24.5452	4.8857	3.8603 24.1250	3.9290	3.4012	3.2973	24.2925	2.5544	5-3627 24.4822	4.3166 25.5463	3.8140 24.5321	\$.1430 23.8487
12.7093	16.4867	11.0068	6.6371	6.6563	14.2274	12.1248	16.3052	15.0375	16.5244	14.6994	15.5799	14.2489	16,3802	13.3325	15.0013	14.5079	13.5898	12.8327	11.6055	14.7212	17.8307	14.7297	14.2489
21.1743	21.0470	21.4026	22.4207	21.0902	19.3820	20.7805	22.1302	23.8030	25.0617	21.9679	22.5691	20.1343	22.1427	18.3291	19.8969	17.8181	16 1998	15.4599	14.7716	17.7715	19.3678	15.6858	16.0923
16.8917	16.9039	19,4412	17.2067	18.4434	16.5980	19.2657	20.4336	19.3238	21.9222	19.1606	19.4756	18.7532	19.5149	16.3631	18.7276	17.2382	15,7881	14.7662	13.8590	16,7988	19.7948	15.8923	16.1839
16.6454	18.6513	15.8279	16.8847	16.9456	17.7542	16.8005	21,4145	18.4836	20.2046 18.2444	17.0680	18,7764	15.4255	17.8971 16.8843	13.7751	16.1809 15.3724	15.4682	13.0951	12.0133	11.6285	15,7673	18.4423	14.7688	14,7332
11.3046	11.5597	11.8317	11,9926	12.1910	10.7642	11.1577	13.6949	11.1255	13.0401	11.6986	13.2084	12.2538	14.2572	11.5565	13.4278	13.4656	12.8797	12.4355	11.6333	14.8205	17.6434	13.8698	13.6394
32.1178	10.6655	12.1499	14.1710	12.6705	11.2562	12.0361	13.5049	10.7651	12.2378	11.0389	12.7085	11.8412	13.3942	10.8008	12.5489	13.1029	12.3762	11.7173	10.9194	14.1672	17.2056	14.1178	14.1215
11.9736	10.8405	12,0200	13.6188	12.9950	12.2410	11,9344	13,5023	10.9113	12.4279	11.5144	12.6473	11.9629	13.6548	11.1446	12.9232	13.6011	12.5109	12.0974	11.3009	14.7899	17.4255	13.8330	13.1594
11.1014	10.4361	11.6541	13.3503	12.6835	10.7341	11.5871	13.2121	10.5402	12.0919	10.9948	12.4176	11.4978	13.3608	10.6833	12.4891	13.1261	12.0867	11.6067	10.7050	11.8943	16.7940	14.1875	13.2095
11.4074	11.7723	10.7771	11.9471	11.4288	10.7410	11.3811	13.3203	10.8904	12.6065	11.1826	12.5740	11.5848	13.0920	10.7899	12.1648	12,7994	11.7778	11,3465	10.7546	14.1369	16.8656	13.4692	12.0041
22.0052	22.5571	24.4376	22.9219	22.2921	22.5173	22,6475	25,5210	24.4026	24.9634	22.0655	23,2363	21.5651	23.8012	18.3884	20.9755	19,6831	17,0886	16.1081	15,5413	18.6570	20.7192	16.5957	17,7769
11.0375	10.8486	11.9235	9.2238	8.4118	11.9297	10.5802	12.1177	9.8766	11.5479	10.2253	11.7191	10.6217	11.9837	9.9139	11.3867	12.0065	10.9810	10.5602	9.7414	13:2362	15.3862	12.7566	11.9226
18,7095	12.6548	12.9613	18.2760	12.8386	12.8219	18.1839	20.3576	18 4774	19.9629	17.6719	18.9465	17.2987	15.2293	13.4239	14.3984	14.9651	13.8219 15.2581	13.3127	14.0262	16.7089	17,1379	14.1200	13.5425
12.2438	12.2540	12.8545	12.8951	12.5386	12.6277	12.4316	14.0866	11.7678	13.5712	12.3590	13.5403	17.7052	13.9933	11.9068	13.2676	14.0304	12.7187	17.2620	11.7375	14.2548	16.2554	13.6889	13.1166
12.3335	12:8077	12.4291	12.9755	12.9188	12.7007	12.5860	14.1265	11.9484	13.4353	12.5623	13.7009	12.8217	14.0905	12.0688	13.2932	14.2059	12.8675	12.3761	11.8486	14.2999	16.3515	13.8413	13.3978
12.8964	12.8553	12.5998	13.124H	13.0737	12.8635	12.6967	14.2750	12.1114	13.5704	12.7480	13,7839	12.9286	14,1719	12.2027	13.4329	14.3164	12.9722	12.7870	11.9410	14,7407	16.4137	13.9524	13.3101
12.3204	12.1099	12.4908	12.3707	12.0263	12.2317	12.3074	13.9773	12.0194	13.4659	12.6157	13.5096	13.2352	13:9750	12.2361	13.3127	14,2665	13.2796	12.7870	11.9410	14,7407	16.4137	13.9524	13.3101
13.5540	12.1917	14.4525	13.0505	13.0867	13.0943	12.6501	15.5520	10.1948	14.3192	12.4927	14.7601	14.1136	17.2308	13.8111	14 1990	14.8250	15.6158	17.8730	15.2805	21.9224	26.3985	21.4396	16.8294
14.6087	15.1518	15.3966	15.9174	15.9779	15.0495	14.2925	16.9356	11.9395	16.7938	13.8124	15.2299	13.3795	15.0750	11.9405	11.9083	10.4019	10.7046	11.5676	10.0422	13.2840	15.7625	13.2618	10.6372
6.5637	6.5028	6.4126	6.3165	5.8053	7.0328	6.7343	8.4876	5.5619	7.4392	6.6538	7.6165	7.2084	8.0393	6.6365	7.3950	7.1076	7.8402	9.3250	6.9988	9.7090	12:2692	10.1825	7.6913
16.5147	16.1096	16.0848	16.7631	16.1054	16.6951	15.2120	18.1145	14.4627	18.0306	16.2880	17.9849	17.1656	19.6433	16.6708	17.0049	17.9537	17.5615	19.2223	16.9940	22.4396	26.0107	22.5417	17,7590
15.1249	15.2822	14.6832	15.7063 14.9202	15.7309	14.5821	15.0895	17.7610	12.0411	16.7349	13.6611	14.8759	13.9537	14.2533 15.6878	10.6585	10.4656	14.6771	8.5816 13.9038	14,0325	7.7064	10.2498	12.2665 19.1886	10.7397	8.4837 14.1924
12.9519	13.7772	13.0608	12.8525	12.2816	12.8684	13.2048	14.9906	11.4812	14.1308	13.1405	14.5872	13.5972	15.1685	13.3188	13.7943	14.1512	14.2987	15,4580	13.7099	17.7250	21.0093	17.3412	14.3698
11.8045	11,7150	12.2868	12.1732	11,7084	11.5821	11,6019	13.4758	9,7770	12.4188	11.3974	12.8795	12.0547	13.7450	11.8437	12.3589	12.6199	12.9950	14.1639	12.5388	16,4060	19.7846	16.7105	13,4514
9.6703	9.6244	9.4935	9.7156	9.5646	9.6893	9.7156	11.6606	8.1775	10.7134	9.7362	11.0200	10.4734	11.9773	10.1061	10.6498	10.4261	11.0253	12.4017	10.6276	14.7716	17.6165	14.6061	11.6246
9.2822	9.2575	9.1892	9.1692	9.3056	9.1973	9.2587	11.2840	7.7547 9.7192	10.3358	9.3410	10.6191	9.8460	11.6128	9.4728	10.2266	9.9667	10.6450	12.0472	9.9720	14.6185	17.3716	14.2982 12.9608	11.4724
7.3003	7.4346	7.5781	7.5116	7.4126	7.2473	6.8739	7.8355	7.1908	8.3007	7.3537	7.6860	7.2267	7.2615	6.1279	6.3561	5.9349	5.6791	5.6231	5.0881	5.9047	5.9407	5.8923	5.2669
14.7647	15.4919	16.1504	16.7899	16.2951	15.3544	14.3413	16.6674	14.1774	16.2978	13.9599	15.2787	13.5221	15.1121	11.7474	12.4994	11.3806	11.0034	11.0832	10.0565	13.2718	15.2665	12.2010	10.5708
11.0512	11.6503	12.5518	13.1611	12.5395	11.5847	10.5883	12.5850	10.3616	11.7231	10.5062	11.4941	10.6076	11.6767	9.6169	10.6340	10.6786	10.3670	10.1581	9.1528	11.4270	13.7158	11.2761	10.1340
11.0947	16.5888	19.1512	19.8706	18.6553	17.5681	13.8257	13,4549	3.6168	12.0241	11.1600	12.1873	11.7107	13.3673	11.2593	11.8492	11.1737	11.3798	12.2367	11,3048	16.4183	19.1437	16.9328	13.6078
9,2302	9.2250	13.0487	1.8271	1.8336	13.0943	11.4898 8.4195	10.6910	7.7717 6.5456	9.2986	7.9435	9.3645	9.1683	10.7067	9.7594 8.3402	9.0747	9.8143	9.5430	10.7664	9.5125	14.0915	17.7254	15.3620	12.1950
9.2302	9.2250	11.7245	1.7143	1.7207	11.7641	8.4195	10.6910	6.5456	9.2986	7.9435	9.3645	9.1683	10.7067	8.3402	9.0747	9.5181	9.5430	10.7664	9.5125	18.2297	16.8117	14.5867	10.9629
8.3960	8.2694	8.5771	7.9722	8.4132	8.5014	8,4835	10.2860	6.6722	9.1380	8.0820	9.5721	8.8772	10.6121	8.5675	9.1480	9.3162	9.8368	11.2094	9.4247	13.7450	17.0094	13.9448	10.5473
16.2602	15.9624	15.7068	16.0711	15,8893	16.7350	16.1863	18.5890	13.9245	17.2817	14.6941	15.6677	13.6471	14.8521	11.3822	11.3978	9.4447	9.6309	9.8155	8.5701	11.4408	13.9335	11.7111	9.8904

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Road		1 1	Coordinate (m)		Width	Height	Road Type		П
Pair	X1		X2	Y2	mixing room	(m)	(called 4)	Hroo	F
B141	613295.36		935316.58		0			14,7698	14.4
NA.	*********	041833.0V	032315.90	10100100	-		-	8.0653	100
W. 14.0				#21 FET 114				669331	16.40
RTASellias	-				.0	0		13 0615	121
R147+R148			833921.13		919	a		10,9693	11.15
R149	833728.61	821748.53	833807.73	821684.38	14	0		9.7549	9.31
RIAS	833774.08	621643.62	633807.73	821664.38	13	0		9,7549	9.31
RTSG	533736.67	821759.23	83366771	827855.87	. 11	0		9,7549	9.31
RtST	e25613.61	_	633683.50	821543.73	12	0		9.7549	9.31
Atst	833693.50	1171543.70	133776.28	821647.53	14	0	1.1	9.7549	9.31
R152	833774.08	621643.62	833-828-17	821509.58	20	0		9,7549	931
R163	633991.31	822369.76	834018.77	\$22414.27	16	0		10.3995	10.6
R154	823950.86	822339.86	33299200	822368.87	11	0		10.3306	10.68
R155	833909.68	822271.38	133310.46	822320.AS	118	0		103334	10.7
R156	633848.78	62222210	83390825	\$22271.35	118	0		14,6625	14.14
R157	823 MAR 56	RZ22228	833827.77	85231228	. 83	0		15,1511	14.76
RTSB	E13827.77	822172.05	83377268	\$221533	2	0		14.8987	14.95
Reds	834075.91	822399.62	134112.00		15	0		10.7141	10.96
R180	82.040,608				10	0		12.5299	12.43
RIES	83413A.90	822259.52	83407591	922294.6Z	1.5	a		10.8998	10.8
R162	534549.42			822287.53	18	0		12,6350	12.56
H163	6325953.86				14	0		11.8770	32.00
R154	834707.86				16			11,7738	11.75
8918	613953,31		83399447	\$22,201,53	. 93			13,2109	13.09
R166	23372.14	822051.30	83396475	622160.53	19	0		9,9668	9.63
R167	133005.47	822042.45		6225189.33	18	0		18.0383	38.06
R168+R165	833613.72	521975,47	83387636	822050.03	21	0		4.1796	4.13
R470+R474	ED738.44	821883.35	57716110	1121978.53	83	- 6		6,2348	6.22
R172+R173	823681.92				20	0		123353	12.1
H174-R175		821677.50	83368338	421523.65	16	0		13.1319	13.1
RITE	633498.77		833565.47	821686.73	2.6	ė		12,2769	12.2
R177	633513.09		83157168		2.6	•		13.6094	13.6
R178	833440.44	821529.90			16	0	1	14.2564	14.1
R179	833451.64	121526.21	26,118448	82,000128	44	0.		15.2638	15.1
R180	634218.31	\$22256.35	834315.86	822386.33	- 13	. 0		13.0183	13.1
RIBE	E34181.9E	82271222	10315169		1.6	a		13.3629	10.2
R182	824140.62				- 18	0		11.7994	11.8
R183	834099.34	122113.33	834149.62	822162.07	18	0		13,2307	13.74
R184	634877.01	_	834061.51	822109.94	13			13.0632	12.66
R184	121203121				2	0		13.0632	12.60
R184	834071.99				14	0	-	13.0632	12.60
K105	834309.95					0		12.6742	12.57
8186	634231.54							14.2891	14.4)
18187			834221.78	823006.45	2	a		14.2119	14.54
R188-6189			83405834			0		12,3354	11.6
R100-N191			034004.90			0		13.1202	13.80
R192+R193	633875.52				216	0		10.3961	10.15
R194+R195					20	0		18,6035	17.6
R194-R303	-	-	933-828-17	821503.58	30	0		18,7738	19.17
H197	134344.34	-			- 13	0		15.7622	11.45
R196	634322.77				16	0		12.7078	10.80
R199	E34281.93			822010.48	10	0		15,4956	15.69
K100	834238.17	821814.13		623963.58	11	0		14.1447	130
WING	*******								

	Hr23	3,7801	6.7357	10.6565	10,3176	6,2382	5.4068	13.0610	13.0610	13.0610	11.9352	11.9352	11.0142	8.4611	0.2778	6.330/	13 22 28	11.4842	12.6330	10.4970	12.0922	10.5049	10 5211	10.7017	12,2087	7,5580	15.5447	3.8421	3.8776	12.8860	13,7183	11,3365	15.7507	14.2232	13 2492	12.7680	13.9889	6.0251	6,0251	6.0251	13,0633	16.2125	11,4277	12.6095	10.6310	20.0064	21.6380	13.0610	14 4734	19.47.34	13.1605
	Hr22	11.1664	9.7317	12,6021	123597	7,9571	6.7366	17.1823	17.1823	17,1823	17.1823	17.1823	14.9735	10.5266	10.3353	13 7760	13 7977	13,8152	13.9950	12,7040	13.9939	12.6856	12.3345	13.0775	13.5772	8,0750	16.1193	4.341/	1/6990	14.9603	14.9012	12,7325	17.5530	15.0395	16,6930	15,4889	14.7177	8,3456	8.3456	8.3456	15.4076	17 9967	13.0130	15.0095	9.2441	20.4160	19.0466	17.1752	14 9468	14 3400	14 3306
	Hr21	13,6060	11.2994	14,6937	14,4015	9.1718	7.3568	19,4553	19,4553	19,4558	19.4553	19,4553	18,6696	12,4106	17.3448	16.0310	1613/4	16.2282	16:8496	15,6261	17,2680	15,6297	15.3548	16,0959	16.2804	E 9304	200195	2,0336	15,4341	17.8667	17,6393	152571	20.4598	18.2718	19 0738	19.7484	19.0696	9,5333	9.5533	9.5533	18.7083	20.8524	15 3842	18.1982		+	20.7478	20.9300	10 1464	13,3404	
	Hr20	10.9124	9.1442	1	1	7.3041	6.3893	15.9959	15.9959	15,9959	15.9959	15.9959	15,3968	9.9625	9.9919	10.5407	13 9858	13.9015	14.4304	12,8547	14.2908	12:7240	Н	+	14,1978	7.797.1	17.2915	3.9/12	+	۰	15.2461	Н	Н	16.1098	16, 1968	15.3569	15.4122	7.6077	7.6077	+	+	18.1854	13.3287	15.2595	11.5443	20.9216	19.1370	13.0003	16 5031	10.2222	
	Hr19	7,7325	Н	+	9.1789	5.4712	4.4576	11.1922	11.1922	11.1922	10.7497	10.7497	10.1553	7,0430	0.11050	11 2130	11 1950	10.5564	10.3649	9,0913	10.6272	9,0653	8:9905	9,4108	10.6121	6,8290	13.6136	33/37	9.3518	12.0561	12,2089	9.9282	14.3570	12.5168	11 6070	10.6977	10.9588	5.3513	5,3513	5,3513	11.4996	14 9917	9.5206	11.0279	75551	18.6820	17.0215	9,0111	14 1874	14.10/4	
	Hr18	8.8256	7,7785	10.8419	10.4042	6.2941	5.0700	13.2083	13.2063	13,2083	12.7838		11,8443	80118	8.1560	0.6343	12 6010	11.7671	11.5387	10.2984	11,7684	10,3256	10.1635	10,8161	11,7102	7,5349	14.76.19	3.2082	10 8408	19.2078	H	Н	н	+	13 6092	t	11,6893	6.3184	6.3184	+	+	15 9444	10.8499	12.3942	7.5559	19.3924	17,6119	15.4574	+	+	
	Hr17	3.4867	7.8137	1	+	6.3540	5.4669	11.6676	11.6676	11.6676	11.3765	11.3765	10.9375	7,7385	1.8/0/	0.1040	12 1581	11 2157	11.1276	9.9619	11.3772	9.9921	Н	-	11.6416	8.0376	14.6420	9,1/34	t	t	t	Н	15.2075	13.4441	13 1588	12.0678	10.8445	6.3065	6.306.5	+	+	15,6183	10.5649	11.7338	7.9430	18.8584	30.2201	10212	14 8514	14.0244	
	Hrife	8.1327	Н	1	10 3021	S.7418	4 9422	11.3243	11 3243	11.3243	\dashv		10.1066	7,8688	1,7556	12 0513	13 1615	11,7194	31.5566	10.4393	11.5692	10.4383		+	1	7.9866	16.7490	4.0922	1.	✝	۰	Н	Н	14.6287	+	+	10.8673	62716	62716	+	+	15 8010	10.8342	12.4207	8.4672	+	+	23 5744	+	+	
	Hr15	10,4786	8.6847	12,6970	12.3215	8,0886	6.7104	10.1467	10.1467	10.1467	10.1467	10.1467	10.0827	8,4679	8,9409	13 6013	130011	12 0340	11.1035	10,6971	11,5941	10.9568	10.9422	10,3117	12,3637	8.7423	16.7822	4.5341	11 1034	13,4498	13,4346	11.8245	15.3940	14,6222	13 0226	11.7576	11.1918	7.5205	7.5205	7.5205	12.8732	15,9340	10.8558	12.3787	9.0372	18,6895	17.7986	9,4409	13 8005	14-08000	
	Hr14	10.4841	7.8954	13.0830	123530	8.3033	6.9252	9.8773	3.8773	9.8773	9.7017	9.7017	9.2160	7.8431	0.0000	13 55.67	114316	11.9833	۰	10.0866	10.5264	10.1602	Н	+	114561	8.5123	14.9708	3.6040	104674	125770	12.2045	Н	Н	+	11 6099	٠	11.6937	7.4498	7.4498	7.4498	11.7742	14.6528	10.2356	113153	3.1695	17.9725	17.2836	17577	+	1	
	Hr13	13,9800	8.9795	16.1010	15.7076	11.0872	9.5281	12,0305	12.0305	12.0305	12.0305	12.0305	11.5699	10.5181	10.3046	10,0001	16.4162	15.1868	13.7452	13.4166	13.1972	13.2166	12,7585	12,8885	13.8712	9.0476	19.1529	4.6233	13 7307	15.5709	14.3802	13.8903	16,7115	16.5772	14 8518	14.4820	14.5991	10.3236	10.3236	10.3236	14.8 833	16.9573	12.8554	14.5951	11.4079	9615.61	16.7439	11.5682	16,7303	13.6333	
(g/VMT)	Hr12	12,6845	8.4806	14.9297	14,4502	10,1914	8.9281	10.0917	10.0917	10,0917	10 0917	10.0917	6,7879	9,2686	93391	253335	14 7156	13,6138	11.1238	11,6534	11.3700	11.6394	11.2514	10,8389	12.6954	9.2494	17.0728	4,4104	+	٠	12.8324	12.2766	14.8473	14.5580	13,0430	11,6504	12.8222	9.5608	9.5608	9.5608	12.4312	15.4249	11.5781	12.6531	9,6803	18.7254	17.9627	9.3277	14.0153	14,0133	*****
NO2 x 100 (g/VMT)	Hr11	14.8326	8.8837	17.2607	16,4550	12.1760	10.6175	10.6694	10.6694	10,6694	10.6694	10.6694	10.5099	10,4068	10.5180	16 0505	16.3760	15.1303	12.3970	12.9775	12,3893	13.0637	12.5500	12,0815	13,7103	25883	18.9076	0,9520	128700	14.7685	13.6628	13.6365	15,7796	16.0305	12 6667	12.6031	13.8632	11.6145	11.6145	11.6145	13.8845	16,7397	12.4317	13.7766	10.5092	19 9662	16.5450	15,0360	146176	TH'OT'LD	
	Hr10	13.6895	Н	4	15.4709	10.9417	96186	9.3207	9.3207	9.3207	9.3207	9.3207	+	+	+	10.0073	+	t	10.8648	11.6494	10.8563	11.6857	Н	+	1	+	27.5060	60/7.6	1	۰	1	Н	Н	14.5711	+	٠	Н	10.6483	10.6483	+	+	14 8214	11.1658	12,2796	9.0385	17.8404	15.5841	13.2754	+	24.07.42	
	Hr09	16.7242	8.5665	18,7249	17.9074	13,7368	12 2463	10.3634	10.3634	10,3634	10.4800	10.4800	10.3634	11.6692	11 2003	11.37043	19 3067	16.6417	12.0139	13.8647	12.1713	13.7491	13.2572	12 8120	13.9218	10,5525	05666	4,5391	1	٠	13.4027	14.3857	15,3905	16.3978	10 7843	12.2581	14.2412	14.0172	14.0172	14 0172	13.6437	15,6801	12.7809	14,1723	10,2119	18,7757	17,4976	14.8774	16 4164	10,4104	40.44.00
	Hr08	13.1301	6.8779	15.6426	14.6253	9.6988	8.8284	7.5755	7.5755	7.5755	7.6579	7.6579	7.5755	8.9350	6.9083	147659	15 5019	13.4034	۰	11.4523	10.0860	11.4792	Н	\dashv	7	+	19:0151	4.0739	10 0991	13.1745	11.9408	Н	Н	+	100163	+	12.0239	9.8194	98194	+	+	13.9895		12.0630	8.5030	16,4119	18.5747	11.6882	14 4037	14.4037	20.000
	Hr07	18,2624	8.9473	18.9053	18.7128	14,7755	13.4938	11.8234	11.8234	11.8234	11.6234	11.8234	11.8234	12.8146	12.6590	101111	19.525.4	17.3826	12.5651	15.0959	13.3989	15.0031	14.4483	13.8953	15.1563	11.4017	71.4999	3.0702	14 6286	16.1196	14.5133	15.5540	15.4468	17.7172	14 7200	13.8716	15.5891	15.3443	15.3443	15.3443	14.8981	16.9578	34.1144	15.7246	11.4227	19.3042	18.5913	15.6101	12.12.77	27.36.75	20,000
	Hr06	14,6535	8.0202	16.5440	16.5065	12,5484	11, 3248	9.3444	9.3444	9,3444	9.7861	9.7861	9,3444	10,5336	10.0144	14 7300	15,1813	14.8897	10,6173	12,9595	11.1161	12.6569	12.0239	11,7296	13.2701	10,0119	18.1501	4,1295	12 1840	13.1749	12.2693	13.5535	IA.3923	15.2876	14 2342	12.0456	13,2921	13.1006	13.1006	13,1006	13.0559	14 5483	12,3359	13.6311	10.0688	18,6462	19.1572	10.2830	16 1140	10.1143	Tree aces
	Hr05	15.8658	73117	17,2906	17.1795	11.9683	12 2281	11.4857	11,4857	11.4857	11.4857	11.4857	11,4857	10.6276	10.5576	130501	14.4750	14 95 19	11,9297	12.8140	10.7782	12.5438	12.0250	11.7453	13.1538	9.8017	18.1194	63700	12 2810	13.1772	12.2732	13.6704	14.1343	15,7107	10 3393	13.2198	15.6532	13,0943	13.0943	13.0943	12.6141	148792	11.9618	13.6615	10.2788	18.4369	17.4472	10.2792	18 1647	7607707	
	Hr04	14,4933	5.7399	16.4482	16.4679	16.3018	13.0867	10.2734	10.2734	10.2734	10.2734	10.2734	10.2734	10.6728	10.6399	102301	14.4751	15.0827	9.2482	12.0778	11.181.11	12,4129	11.8656	11.9925	12.8008	9.8177	18.3048	4,0451	12 0030	13.0169	12.3948	13.4119	14.3968	15,2487	11 4761	14.6457	15.1713	12.2210	12 22 10	12,2210	13.2925	15,3132	12.1535	14.2796	11.4158	19.1392	17.3757	10.2734	17 0703	27.37.02	240000
	Hr03	11,4472	6.1708	165467	16,6394	8,5611	14.4534	10.2447	10.2447	10,2447	10.2447	10.2447	10,2447	10,1855	10.3161	13.8700	14 3748	14.8821	11,8851	12,7142	10.5708	12.4547	11,7349	11.4932	12.9114	9.7694	18.01.36	4,3130	13 1568	13.1108	12 3099	13,5378	14.2110	15.2161	10 3447	12.5678	14.7334	12.3490	173490	12.3490	12.5540	14.8251	13.2915	13,7195	10.8288	19.2060	17.2245	8.5611	18 1331	10,1541	44 0000
	Hr02	11,9257	7.2544	16.3356	16,1294	14,4525	13,0487	8.5566	8.5566	8.5556	8.5556	8.5566	99558	10,1917	10 3000	13 00.00	14 7850	14 9176	11.8572	12,4206	10.8708	12,4457	12.1297	11,819#	12.8507	9.7632	17.9353	0.2454	12 1580	13.0802	12 2593	13.6538	14.1392	15.2281	0 1053	12,6327	14,4668	12,4576	12.4576	12.4576	13,0851	14 1824	12.5588	13.3079	10,1145	18 2031	15.5896	E3566	16,0061	4	200000
	Hr01		_	ℸ	-	12.1917	11 1833	93104	93104	93104	9.3104	9.3104	93104	10.6019	10.0934	+	14.7635	14.9560	10.9637	12,4352		12.5659		н	_	9.6569	18.0631	4,1339	1.	۰	t	Н	Н	1	10.2468	11.8830	Н	-	7	-+	+	14.8495	-	Н	Н	17.6766	19.1721	11,4508	+	130301	
	Hr00	14,7698	Н	7	16.5622	13.0615	10.9693	9.7549	9,7549	9.7549	9.7549	9.7549	9,7549	10.3995	10.3300	14 6636	14.1631	14.8987	10.7141	12.5299	10.8998	12,6350	11.8770	11,7738	13,2109	9,9656	18.0383	9,1790	13 2353	13 13 19	12,2769	13.6094	14.2564	15.2638	13 3639	11,7994	13,2307	13.0632	13.0632	13.0632	12.6742	142119	123354	13.1202	10.3961	18.6035	18.7728	15.7622	15.4956	23,4230	

Pair Reps Reps Reps	X1	Y1	nate (m)	¥2	proluting	Height (m)	Road Type (calline 4)
RIG3 RIG3	R23124.78	52224.11		820 Do 25	mixing rotal	0	1
R003		#22334.25			29	0	1
	633231.00		#33414#0	#22406.45	26	0	1
H003	823434.00	822408-45			- 76	0	- 1
8603	RESSEC AN		#13995.46		29	0	-
MINA	PROCESS PLAN	WANTED TO			19		1
RIDA	833118.28		\$25.0252			0	1
F1004	133411.03		635425/16		38	040	- 4
R004	833425,10	622396:41	037516.26	022421.5B	19		1
RIDE	833616.28	£22,421.55	£\$3673.75	622496.58		10 - 10	1
R003	833671.75	822490.EE	83395347	822414.65	10		4.
H008	633933.67	022014.00	#30973.71	#22424.0¥	19	0	- 1
WEES	632973.71	622825.09	E3404E14	812520.54	18		7
005+B307	833527.00	622410.61	633/637.55	622455.21	34	0	- 1
dos-8407	833627.65	222455-21	813732.67	422494.A7	18		1
606×8.007	633732.07	827494.47	83379244	022441.05	14	0	4
B06+8607				022456.02	34	-	1
	833762,11	622441,65	813840.01				1
003-R105	E33664 17		625H3259	622497.15	13	- 0	- 1
dolensor	\$33693.60	822397.15	EISENIE	822456.38	13	0	
	632976.40		#32900.A4	832432.8E	CI.	0	1
010+#011	632,819.94	\$22432:88	832883,54	832462.45	12	. 0	- 3
01>R611	\$33681.54	822A5 E 49	833849.51	822458-02	12	0	- 1
\$12+R\$13	633387.26	822597-47	833423.59	822559.02	16	0	1
1012-R013	833423.00	\$22668.02	835416/A	012462.07	10	000	- 1
	833416.08	622402.07	#23447A2	022425.39	10		1
B17+6813	E33467.63	622425.36	405444	627.000 AB	10	0	-
012+H013	833544.64	Service State	811367.54	#22354.50	10	0	1
	633468.77		#32847.69		14	0	1
\$14-R\$17	833587,56		SEMALE 17	622374-91	15		1
B15+9E17	103611-17		4236K147		15	0	1
Rose	#330k2.67	822192.91	811219.07		18	. 0	-1
M01	#30309.01	6222218.76		022293.72	16	. 0	1
R102	#38355,60	£22291.72	#15410.61	62E5A0.13	38	0	4
R1122	EXPRES B4	#22340.KJ	2254944	622218.35	16	0	1
F1423	N1071-41		CLOWER		18	0	T
H624	623100.63	632179.44	#13232 o4	#22178.07	14	. 0	- 1
R825	833252 06	AND CLASSES	\$23377.50	621432.03	14	0	1
Ruže	E33377.80		8338G34		14 -	0	-
	633503.91			022241.72	13		1
M027			333473.82			0	1
8624	813675.82		810708-11		13	0	1
R129	833766.03	£22374.16	#\$164E76	622405.73	15	0	- 1
R050	\$33848.76	E22405.79	#EX917.E3	\$22431.11	18	0	- a.
H621	833917.63		#32946.68	812 854 AR	14	0	- 1
4421444	89.810CLB	822000.71	BRITING.	\$22072.07	10	0	
8633	830121.79	622072.07	#EDECL19	622120.94	78	0	- 1
MOD'S	633281.79	822120.94	#2529E77	622175.17	- 0	0	- 1
Rúss	633396.77	#22175.17	833524.35	#22221.21	10	0	- 1
M034	823524.35	1000131	632013.40	622280.00	78	0	-
9627	813653.40	62229 9.00	852694.66		- 15	0	-
				622284.07			
RESIR	823664.68	822284.56	613762.79	622329.51	98	0	4
RUSE	A337E4.99	622311.13	#23765.AC		- 12	0	7
H040	833789.11	622318.08	#33/03/19	822205.11	18	0	1
R041	823,833.14	822335.57	833,802,96	622360.5T	18		- 4
R142	#339E#	#22380.57	94-229235	622125.A5	18	0	- 1
R061	633050.46	922120 At	EMERAGO.	922250.52	48	0	1
8044	E24034.00	\$22250.62	#34540.62	012162.07	18.	0	- 1
8548	824145 SZ	SIZMEAT.	83420376	822581.45	19	0	- 1
RISAE	E2A214.72	622084.65	834303.21	622E1122	16	0	1
	839322.77	822096.85 822010.88	EMPART		16	0	1
RUNT ROSE				821959.48			
	XXX097.20		#354\$4.5W		12	0	,
9543	K33115-66		81343410		18		,
RISS	E33101.47	821942.33	82127446	622007-01	71	0	-1
RIST	633274.50	922504.60	BELGIE 74	922007 62	18	. 0	- 4
R062	633434,10	822080:21	\$15A66.13	822174.73	58	0	1
R053	833786.86	622120.44	#\$1738.64	622103.28	58	. 0	1.
R965	833716.FE	622165.28	81500E21	822174.75	16	0	1
FIQ54	633/419-63	622967.29	SMARKET C		18	0	
2054	633586.71	822122.03	#3354#A5	SEP144.40	18	0	1
ROSA	823649.55		\$1761368		-18		1
ROSA	E330E3.68		#21713.66		- 18	0	- 1
RODA	633712.85		#33757#3		16	0	4
R084	633767,63	822129:56	833775783	622 (28.00	16	0	1
							1
Ross	823786,53	522123.04	821872.14	622051.39	19		1
RIBS	83377 E.49	622113.56	831M7.20	822039.12	10	0	7
HOST.	833873.20		134111.21	821814.78	16	0	1
ROSE	834159.21	921814.78	#34210.10	821708.42	18	0	- 3
Biddy	833867.29	422039-21	63685E34	821690 22	-37	0	- 7
Auso	\$340KE-34	821380.72	234261.E1	821727.AS	148	0	- 1
8061	813116.37	821680.76	82211976	821589.31	16	0	- 1
2007	823159.76	821889.51	A15216.78	021947.75	10	0	1
	823294.88	621947.56	613410.51	822607-91	36	0	1
RINZ	A33460.49	#2250A-R3	#11543.73	82200M.T2	18	0	- 1
ROSA	823541.71	63293E72	#33841.70	#21985.5±	15	0	- 5
ROSA .	823480.98	\$21952.82	833543.70	821962.31	- 18	0	- 1
RUNA	200 000	821834.07	613315.56	821601.61	16	0	- 1
ROSA TOSA	833160.17			201500 22	18	. 0	- 4
ROSA ROSA	\$3316.96 \$33316.96	221391.6E	833491.00	82160512 1			
RODA RODA Bright	£33314.96			821952.75		0	1
ROSA ROSA ROSA ROSA ROSA ROSA	833316.96 833164.01	\$2177 B 07	032 (78.47	021763.88	18	0	
RODA RODA RIDE ROSA	£33314.96	821778.07 621782.16		821613.88 821613.88			

										Vali	iela count	for each r	nad										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr05	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	He16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
1250	500	550	400	450	650	1650	4900	5500	4650	4700	1950	3600	3500	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1.750	800-	550	400	450	650	1650	4900	5500	4650	4200	3950	36210	3600	3800	4000	4.750	4800	4900	4150	2750	2600	2550	1750
1250	800	550	400	450	650	1650	4900	9500	4f50	4200	3950	3800	3600	3800	4000	4350	4800	4900	4150	2750	2600	2550	1750
1250	1900	550	400	450	650	1650	4900	5500	4650	4200	3950	3800	3600	1800	4000	4350	4800	4900	4150	1750	2500	7550	3750
1250	800	550	400	450	650	1650	4900	5500	4650	4200	1950	3600	3E00	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1100	700	500	350	400	600	1500	4350	5150	4200	3950	3750	3500	3650	3900 3900	4250	4700	5350 5350	5500	4750 4750	3100	3000	2950	2000
1100	700	500	350 350	400	600	1500	4350	9150	4200	3950	3750	3500	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3650	1900	4200	4700	5350	5500	4750	1100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	- 5350	5500	4750	3100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	5350	5500	4750	3100	2950	2950	7000
1190	.700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3690	1900	4200	4700	5350	5500	4750	3100	2950	2950	2000
17	10	6	4	4	7		60	69	71	32	73	100	100	100	200	62	70	67	64	59	58	31	25
17	10	6	4.	- 4	7	. 18	60	69	71	72	73	100	100	100	100	68	70	67	- 64	59	- 58	- 31	- 25
- 17	10	- 6	4	4	7	18	60	69	71	72	73	100	100	100	100	- 65	70	67	64	.59	58	31	- 25
17 63	10	13	4	10	16	18	50 73	69 150	71	72 150	73 150	100	100	100	100	100	70	57 100	100	59 100	58 74	72	37
62	22	В	Б.	10	16	62	73	150	150	150	150	150	150	150	150	100	100	100	100	100	74	72	37
100	72	30	-21	24	38	100	200	350	400	350	350	350	350	150	350	250	100	350	750	150	150	150	100
100	72	31	. 21	24.	38	100	200	350	400	350	350	350	350	150	350	250	300	350	250	150	150	150	100
100	72	31	21	24	38	100	200	350	400	350	350	350	350	350	350	250	300	350	250	150	150	150	100
7	- 1	2	1	1	2	7	- 12	25	27	24	23	25	26	30	29	23	32	35	27	20	16	14	11
7	- 1	2	1	1	1	7	12	.25	27	24	23	25	76	30	29	23	32	- 35	27	30	36	14	11
7	1	2	1	1	2	7	12	25 25	27	24	23	25	26	30	29	33	32	35	27	20	16	14	11
7	3	7	1	1	3	7	12	25	27	24	23	25	26	30	29	23	32	35 35	27	20	16	14	11
66	v	16	12	13	20	- GR	100	200	200	150	150	150	150	150	150	100	100	150	100	100	100	100	72
66	26	16	- 11	12	20	67	100	200	200	150	150	150	150	150	150	100	100	100	100	100	100	100	-65
66	26	16	11	12	20	67	100	200	250	150	150	150	150	150	150	100	100	100	100	100	100	100	45
-50	50	16	- 11	13	19	-50	100	200	290	200	150	150	150	150	100	50	100	50	50	50	50	50	21
50	50	50	14	16	24	50	100	250	250	250	200	200	300	200	500	190	200	200	150	100	100	100	50
50	50	17	12	14	20	50	100	200	200	200	200	200	200	250 250	250	200	250	250	200	150	100	100	100
50	23	17	11	11	17	50	100	200	290	200	200	250	250	300	300	250	400	450 450	350	250	200	200	150
50	22	12	3	11	16	90	100	150	200	200	200	200	250	100	300	250	150	400	300	250	200	150	150
50	50	18	12	15	21	50	100	200	250	250	250	300	300	350	400	300	450	500	400	300	250	200	150
50	50	17	12	1.4	20	:50	100	250	250	250	250	250	250	300	300	250	350	350	300	200	150	190	100
100	50	50	72	25	50	100	200	350	400	350	350	350	350	450	400	350	450	500	400	250	250	790	150
50	23	15	10	11	16	50	100	150	200	200	200	200	200	750	250	200	300	350	250	200	150	150	100
50	15	9	6	. 8	10	50	50	150	150	100	100	100	100	100	100	100	100	100	100	50	50	50	50
50 15	50	24	17	19	50	50	150 50	300 100	350 100	300	100	350 100	350 100	100	100 100	300	450 150	500 150	100	100	250 50	200	150
106	105	51	54	54	- 55	108	320	450	450	378	371	421	419	469	404	519	619	618	463	150	308	258	205
200	150	100	100	100	150	200	550	800	750	700	650	750	750	850	900	950	1150	1200	900	650	550	500	350
200	150	100	1.00	100	150	200	550	850	800	700	700	750	750	850	950	1000	1200	1200	950	650	550	500	150
300	250	200	200	200	256	400	900	1400	1350	1150	1050	1100	1090	1100	1150	1150	1300	1300	1000	706	600	250	400
350	300	250	250	250	250	450	1050	1650	1550	1150	1250	1300	1300	1400	1450	1450	1700	1700	1300	900	750	700	500
300	250	200	200	200	200	350	890	1950	1250	1100	1000	1050	1000	1050	1100	1100	1250	1200	950	£50	550	500	350
300 200	250 150	200 150	200 150	200 150	150	350	900 650	1000	1250 950	1100	750	1050 750	750	1100	1100 800	1150	950	1300	700	700 500	400	550	250
200	150	150	150	100	150	250	550	900	850	700	650	650	650	650	650	650	750	700	550	400	350	300	200
700	150	150	150	150	150	250	700	1050	1000	850	750	800	750	800	300	800	900	850	650	450	400	350	230
250	200	200	150	150	200	350	900	1250	1150	1000	950	1000	1000	1050	1100	1150	1350	1350	1050	700	600	550	480
150	150	100	100	100	1.00	200	450	500	700	600	550	600	600	650	70G	700	850	850	650	450	400	3090	230
200	150	150	150	100	150	250	550	900	850	750 500	700 500	750 550	700	750	300	#50 650	950 750	950 750	750	500	350	400	300
150 200	150	100	150	100	150	250	400 600	900	850	750	700	750	700	600 800	800	IISO	950	950	750	400 500	450	490	300
200	150	100	100	100	150	250	550	300	750	650	650	700	650	700	750	800	900	900	700	500	400	350	250
650	500	450	450	400	500	850	2000	3100	2900	2450	2200	2250	2150	2250	2250	2200	2500	2350	1,800	1250	1050	950	790
550	450	400	400	350	450	700	1700	2650	2900	2950	1850	1900	1750	1800	1750	1700	1900	1750	1350	950	800	700	500
650	500	450	450	450	500	800	1950	3000	2050	2450	2300	2450	Z350	2550	2650	2700	3150	3100	2400	1650	1400	1300	900
550	450	350	350	350	400	700	1650	2500	2350	2050	1850	1950	1900	2000	2050	2100	2450	2350	1,800	1250	1100	950	780
350 400	300	250 300	250 250	250 250	300	450	1100	1700	1600	1890	1250	1350	1500	1700	1750	1500	1750 2150	2100	1650	1150	950	700	500 600
400	300	300	250	250	300	550	1250	1950	1850	1600	1500	1600	1550	1700	1750	1800	2150	2100	1650	1150	950	900	500
450	150	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650
4523	350	300	300	300	350	550	1350	7050	1950	1650	1550	1650	1600	1750	1300	1250	2200	2150	1650	1350	1000	900	630
450	150	300	300	300	350	550	1350	2050	1950	1650	1950	1650	1600	1750	1800	1950	2200	2150	1650	1150	1000	300	650
450	350	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	23,50	1/650	1150	1000	900	650
450	150	300	300	100	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650 650
500	400	300	350	150	400	650	1500	2050	1950	1900	1750	1850	1750	1850	1900	1890 1950	2200 2250	2150	1700	1150	1000	900	650
250	200	150	150	150	200	300	750	1200	1100	950	900	950	950	1000	1050	1050	1250	1250	950	650	550	500	150
350	250	250	250	250	250	450	1100	1650	1550	1300	1200	1250	1200	1250	1250	1250	1400	1350	1050	700	600	550	460
300	250	200	700	200	250	400	950	1500	1400	1200	1050	1100	1050	1100	1100	1300	1200	1150	900	600	550	500	150
200	150	150	150	150	150	250	600	950	900	800	750	800	800	900	950	1,000	1200	1200	900	650	550	500	150
200	150	150	150	150	150	250	600	900	850	750	700	800	750	850	900	900	1100	1100	8.50	600	500	450	500
50	50	14 50	9 18	20	16 50	100	100	150 300	350	300	150 300	300	150	150	300	250	100	350	100	300	150	50	100
50	20	13	10	10	15	50	100	150	150	150	150	200	200	200	200	290	150	300	200	150	150	100	100
50	21	13	3	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	50
50	21	13	- 4	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	400	50	50	50
50	- 21	13	3	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	30
50	50	17	12	14	.20	50	100	200	250	200	200	200	150	200	150	150	150	156	150	100	50	50	50
-50	50	21	15	17	24	- 50	100	250	250	250	250	250	250	30G	300	250	350	400	300	200	200	250	100
1500	1200	1000	1000	950	1150	1900	4450	4750 4750	4750 4750	4750 4750	4750	4750 4750	4750 4750	4750 4750	4750 4750	4750 4750	4750	4750 4750	4750 4500	1150	2850 2650	2600 2400	1800
1350 950	1100 750	950 650	900	600	1050 700	1750	2850	4750	4100	4750 3600	4700 3400	3600	3550	3900	4050	4750	4750 4750	4750	4500 3800	2650	2650	2050	1700
400	300	250	250	250	300	500	1200	1800	1700	1450	1350	1400	1.850	1450	1450	1500	1700	1650	1750	300	750	700	500
						- Sale			2.00		1100	2.00			2.30				2.30			- 34	-10

Road	X1	Y1	X2	¥2	pincluding	Height (m)	Road Type (calline 4)
8021	B10.527.91	121059.25		621675.22	mixton rocal	0	1
RUT2	E33597.24		\$255174		29	0	1
R073	XXX4E1.50		#3930T.24		13	0	1
WOTA .	X33251.04		#2341100		70	0	- 4
8876	B23449.42	621761.09	\$1356E57	621583.08	76	0	- 1
RU78	133501.48	821897.60	EDISHEAS.	821699.77	18	0	1
R076	633546.66		612402.41		16	- C4C-	- 4
R074	R13403.43	621685.99	03309492		16		1.
R#77	E33564.57	521884.14	A\$1562.57	821684.36	12	100	
8077	833561.57	621084.30	833995.68	821871.28	17	0	4.
H077	833,600,48	621971.29	¥32073.64	#21812.0¥	17	0	- 1
MOTE	\$350£1.3E		853875.52		16		1
R679	833673.29	623831.43	833597.51	821651.48	16	0	- 1
Ross	833675.67	221661.18	833999.54	821457.98	16		1
R091	833/667.01	921000.86	932913.08	821652.08	34	- 0	- 4
M082	833A58.18	621884.41	813510.76		34		- 1
RRB2	E23516.75	621821.12	615508.16	621785.93	14	- 0	*
R062	833526.39	821785/83	811570.13	821467.55	18	0	
HOET	633424.63	621668.11	#33.416.18	821812.73	18	0	- 1
F062	813,489.18	621813.12	83352436	821772:29	14.		
H193	833524.38	821772.29	8335951	821652.62	74	0	7
#109 k	633567.56	821687.02	83354249	#21644.85	15	0	1
M094	813682.03	\$2164A.05	05200771	021603.07	13	0	- 1
Ross	833009.34	\$21644.65 \$21605.64	81354024	021675.52	14		1
RIBS .	E33640,24	623578-52	613691.67	821645.20	19	0	. 4
RIQSS	833681.67		833729.52		14	0	1
HORE.	613,080.70		#32093.83		12	. 0	1
R086	823663.88	821583.58	\$33646.83		12		1
R197	H33648,49	\$2354E-43	#13 EFE 49		13	0	1
R098	833254.24		833245.50		12	4	4
8000	#33365-50	621650:04			12		- 4
8498	833416.50		555497.53	821641 DS	17	- 6-	1
RIDS	E334E7.63	821841.0V	£33,513.63		17	10	1
FORE	100 50 1 42		E11574.E0		17	- 1	
moen.	833.074.00		833600.18		17	- 1	1
RAFE	823666.16		613712.68		- 32	. 6	-
Raby	E33256-85		£33370.00		18		
Ross	633370.06		833417.26		16	1.76	1
4085		621682.03	******	A21632.03	14	-	1
Altas	833455.60	621829.25	853522.46	821786.30	- 18	- 10	- 4
mons	833522.46	621786.32	E23343.10	821725.A7	16	9	4
HOLY.	833522.40 833541.10		932942.07		16	- 1	- 1
			832505.09		10		-
HORK		\$21633.37 \$23594.44	633599.05				1
ROPS Rédovados	823596.99				16		
Limbban Limbban	833264.78	421629.64	823317.54		97	0	- 1
R692+8991	633317.92	#21632.93	833449.56 633813.09	821640.31	30	0	1
H092-FIGHT	833449.50	921640.31			30	0	
2094	633357,84	62162A-55	853341.61	621676.41	14		1
R095	833604,59	621501.TZ	E13545-49		42	0	4
RS95+RS97	\$33080.58		#3492E77		w	0	3
1108 K - 11 00W	£34028.77.	022414.27	E34417.E7	0.22.202.41	18	0	1
#100+R101		822332.11	STAZIEJ!		18	0	- 1
R192+R103	834216.31	#22258-35	SERVINES.	822190.58	18	0	1
R194+R199	634309.95	222180.5E	B34407.64		48	0	1
R106	E33917.63	\$22431.11	610991.74	012109.38	18.	0	1
B187	133511.55	622370.04	83489039	822287.63	.0	0	1
R108	H2A090.84	622784.06	63419136		16	0	1
Rise	E394184.08		634272.05		- 17	0	1
WHE		472134.63			12	0	3
8111	K24363.46		834400.74		18	. 0	,
R112	E20646.78	622AD5.79	811992.96		19	0	1
Atti	633635'46	922335-17	317818/00		48	. 0	- 4
R114	813,909,65	822271.38	\$55994.A7		- 10	0	1
RIIS		\$22200.TS			18		1
RITE		622131.84			18	0	1
RHIT	£34097.30	822118.02			18	0	
RITE	834190.09	802037.73	834245:29		- 19	0	3
RUE	E24242.94	621993.85 821981.17	654212.16	821951.45	39		1
R120					- 18	0	- 1
R121		72227 E. (E			16	0	- 4
R(22	613761.08	412351.12	\$53,668.78		18.	0	1
R122	822056,78	6227222.16	512954.75		18	- 0	4
R124	833871.82	622341.72	825m4.66		19	0	7
M.144	813 CH+.80	\$2738 4.07	#33#27.77	822172.05	18	0	4
8125	833093.40	\$22.2FF.00	RE2WIE 7.3	822174.73	12	0	- 4
R126		422315.75	9275F2.51	BEEDBAS	-38	0	- 1
R126 R127	833455.65	#21274-46	SENERALS.	822221.25	- 13	0	1
R126	833455-55 833503-61	CALL STATE		022203.72	18	0	1
R126 R127		822232.03	#10255 <i>88</i>				1
R126 R127 R127	\$33502.61				18	0	
R125 R126 R127 R128 R128	833503.61 833377.60	822232.03	#10255.00	620175.17	38	0	- 1
R125 R126 R127 R128 R128 R120	8333903.61 833377.60 833377,80	822222.03 822232.03	#10255.00 #10256.77	620175.17			
R126 R127 R128 R128 R120 R120 R131	833377.60 833377.60 833377.60 833396.42 833431.62	822232:03 822232:03 82217:5:04	810255/89 610268/77 610414/16 820419/51	6220075.17 6220076 622007.07	98	0	- 1
R126 R126 R127 R128 R128 R120 R120	833377.80 833377.80 833377.80 833396.42 833433.62 833480.45	\$22772.03 \$27732.03 \$2217.5.04 \$2208.070 \$31007.88	810355.00 655396.77 655414.16	822(80).76 822(80).76 822(877.97 821962.74	98	0	1
R125 R120 R127 R128 R128 R120 R131 R132 R133	833377.60 833377.60 833377.60 833396.42 833431.62	822232.63 822232.63 82217.5.94 822989.70	#10355.00 #10356.77 #13414.16 #13415.51 #33481.00	6220075.17 6220076 622007.07)# 18	0 0	1
R125 R126 R127 R128 R128 R120 R130 R131 R132 R133 R133 R134	833 577,80 833 577,80 833 577,80 833 596,42 833 433 42 833 480,45 833 480,45 833 480,45	822272.03 622732.03 62217.5.04 62208.0.70 832007.86 921952.76 622239.78	#10316,00 #10316,77 #13414.16 #13419.51 #33401.00 #33506.07 #13232.66	822175.17 822680.78 822687.97 821962.78 821982.08 822178.03	98 18 28 28	0 0 0	1 1 1
R125 R126 R127 R128 R128 R120 R120 R132 R132 R133 R133 R134 R135	\$33503.61 633377.80 633377.80 633377.80 633431.62 633460.45 633481.00 633209.07 633232.03	822232.03 622232.03 62217-6.04 622060.70 632007.00 821962.76 622239.78 822176.08	#10215.09 #1329#E.77 #13414.16 #13415.51 #33401.00 #3350#.37 #13212.54 #13212.54	622175.17 622000.76 622007.07 621962.14 621962.08 622176.01 622176.01	38 38 38 38 38	0 0 0 0	1 3 3 1
R128 R128 R127 R128 R128 R120 R131 R131 R133 R134 R138 R138 R138	\$33503.61 633377.80 623377.80 623377.80 633377.80 633418.62 633481.00 633208.67 633232.03 633080.01	822732.03 822732.03 822776.04 82207.60 82209.70 821962.70 82239.78 822176.08 822182.63	#10215.09 #1329#.77 #13414.16 #23419.51 #33411.00 #33506.07 #13212.56 #23212.36 #13500.43	822175.17 822580.76 822387.97 821952.78 821962.78 821582.08 822178.07 822120.98 822120.98	78 78 78 78 78 78	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1
R125 R126 R127 R128 R128 R120 R120 R132 R132 R133 R133 R134 R135	\$33503.61 633377.80 633377.80 633377.80 633431.62 633460.45 633481.00 633209.07 633232.03	822732.03 822732.03 822776.04 822080.70 832007.08 821082.76 82239.78 822178.08 822182.63 822182.63	#10215.09 #1329#E.77 #13414.16 #13415.51 #33401.00 #3350#.37 #13212.54 #13212.54	622975.17 622980.78 622997.97 821962.16 621982.08 622178.07 822129.98 613129.48 622672.07	38 38 38 38 38	0 0 0 0	1 1 1 1

Mary											Vet	icle count	for each r	nad										
Second Column	Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr0s	Hr07	Hr08	Hr09		COLUMN TO PAYOR			Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
Section Sect						350			2000	1900	1650	1500		1500					1900	1450	1000	850	800	550
Column C																								
Column C																								
15																								
10																								
100	150			100				450		650		500		500		550		650	650	500	250	300		
Section Column	150	100	100	100	100	100	200	450	700	650	590	500	590	500	550	550	600	650	650	500	350	300	250	300
Section Sect																								
100 100														_										
150						250															750			
100																								
Column C																								
20	250	200	200	200	200	200	350	100	1250	3200	1090	950	1000	1000	1050	1100	1150	1300	1300	1000	700	600	550	400
Section Sect																								
100 100												750												
100																								
100				50																				
Dec 100					50										300							156		
																							400	
Page 190				150	150	150					#SO												400	
							750				800													150
100 600				1.00			150			500		400			400						200			
1906 600 600 600 600 600 600 600 700																								
1,000 1,00																								
Page 196			500	400	400		2.400											3600						
							1400												3600	3200				
Fig. 190																								
190																								
Second S																	2800							
Post			400	300							2400	2400		2300	2650				3800		2200		2350	
Section 180			7400									-						24.4	-					
1909 200																								
100 100																								
Section Sect																								
190 190																								
St. 100			50		100	150	350			450				400			400	-400					100	
100 75 75 75 75 75 75 75																								
100 36 222 16 16 26 300 150 250 300 200 200 30																								
The color The											750						750							
Second Color Seco	71			11						200		20G										150	150	100
59	50	50		17		50																		
50 50 21 15 16 24 20 100 120 250 250 220 200 200 200 120 130 130 130 130 130 150																								
100 50 50 20 21 50 100 150	50			1.6		50					250													
59 93 23 17 18 59 93 150 300 250 250 220 200 200 200 200 150 150 150 30 250 222 34 10 12 17 93 150 30 250 200 200 100 150 150 150 50 56 153 30 56 153 150 150 150 150 250 150 30 56 56 160 200 200 150 150 56 56 160 200 430 850 750									250	250														50
Second S																								
59 20 132 8 9 15 50 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 150 50 50 150 200 150 50 </td <td>50</td> <td>22</td> <td>14</td> <td>10</td> <td></td> <td>17</td> <td>.50</td> <td>100</td> <td>150</td> <td>200</td> <td>200</td> <td>200</td> <td>250</td> <td>250</td> <td>300</td> <td>300</td> <td>250</td> <td>400</td> <td>450</td> <td>350</td> <td>250</td> <td>200</td> <td>700</td> <td>150</td>	50	22	14	10		17	.50	100	150	200	200	200	250	250	300	300	250	400	450	350	250	200	700	150
200 100 50 50 50 50 50 50																								50
200											850		750				550	700			400			250
200 100 30 50 50 50 50 200 350 700 800 770 800 850 850 700 800 850 750 800 350																								
200 100 50 50 50 50 50 50																								
2590 1500 1500 5																								
239 150 150 50 50 100 250 500 990 150 150 990 990 850 990	200		50	50	50			450	900	950	E50	800	800		850		650	800	850	700	500	400	390	380
100 50 50 50 50 50 50 50				50					950	1050	950	900										450	4110	300
59 90 72 13 17 59 90 120 13 17 59 90 120 130 140 250 280 290 200 200 200 200 100 150 <																								
59 50 30 34 16 23 90 100 250 250 200 200 200 200 200 200 150 150 150 100 100 50 50 50 30 34 16 23 90 100 100 200 200 200 200 150 150 150 16 25 50 150 150 250 200 200 200 150 150 150 150 150 223 150 150 250 250 250 220 230 300 300 150 250<	100																			14,046				100
59 50 30 14 16 23 59 100 200																								
59 23 15 30 12 16 50 100 159 200 300 250 350 200 200 150 300 200 200 150 300 300 200 200 150 300 300 200 450 300 300 250 450 300 300 500																								
59 23 15 20 12 16 90 200 159 200 200 200 200 200 200 200 200 200 200 200 250		50	22	15	16	25				300	250			300			300			350			200	
150 100 100 100 100 100 100 200 400 690 600 590 600 590 600 500						16																		
200 150 150 100 100 100 150 250 550 850 830 700 1050 950 950 950 900 800 800 800 600 400 850 850 150 150 150 150 150 150 150 150 150 1																								
500 250 200 200 200 230 400 400 400 1400 1800 390 390 390 390 900 850 850 900 850 650 450 35																								
2000 150 150 150 150 150 150 250 550 850 880 700 700 700 750 800 800 800 850 1000 1800 750 800 400 350 300 200 1000 50 50 50 100 200 400 800 800 800 800 800 800 800 800 8																								
2000 100 50 50 50 50 100 200 350 750 800 750 700 700 700 700 800 750 800 850 700 500 400 350 1400 200 150 150 150 150 150 150 150 150 150 1	290		150	150	150	150	250	550	850	800	700	700	250	700	500	800	850	1000	1000	790	550	450	400	300
f 6 5 3 2 4 8 44 50	200	100	50	50	50	100	200	350	750	800	750	700	700	700	500	750	500	800	850	700	500	400	350	500
6 4 3 1 4 3 7 13 50 50 50 50 50 50 50 50 50 50 50 50 50																								
B 4 3 1 2 3 9 17 50			_																					
18 4 3 3 2 3 9 17 50 50 50 50 50 50 50 50 120 200 400 450 400 450 450 550 550 550 600 650 500 500 350 350 350 350 350 350 350 3	6		3	1	1	3					50													
100 50 50 24 50 50 100 200 400 450 400 450 450 550 550 400 600 650 500 150 300 250 240	1	- 4	3	1	2	3	9														21			13
	100	50			50		100																	
	100	50	-50	50	50		100	200	450		450	450	500		600		500	650	750	600	400	350		

Road		Coordi	nate (m)		WHAT	Height	Road Typ
Pair	X1	Y1	X2	¥2	pincluding mixing room	(m)	(caline 4)
Rist	B30294.35	521947.25	885315.56	821631.57	13	0	1
B162	K33329.89	621853.67	ED315.94	621691.04	13	0	7
R143	833129.75	621089.31	#33465.67	#21#34.07	- 13	0	- 1
TIME	XX3160.07	62183A.07	#33.078.74	821783,18	13	0	1
PUSTRIAL	H3581Z.49	621976.58	£3457458	621516.03	- 32	0	1
2187+2180	E33734-44	821100-38	\$2130112	821727.34	18	0	-1
R148	833728.61	921749:AZ	632607.73	821694.38	14	- 0	- 4
R149	833774.00	621643.62	032807.73	821684.38	13	0	1.
R150	833756.67	#21786-23	853687.71	821603.81	- 0	0	- 1
R151	833612.61	821610.98	813663.50	821863.70	13	0	4.
R151	WINGER W	021543.70	#337762H	#21842.83.	14	0	- 1
WIR2	835774.08	621643.52	#138J#17	821500:58	20		7
R193	833991.31	622300.76	63467877	622454.27	78.	0	1
R194	\$33950.66	222320-65	#EXWIZ.CO	\$22189.07	18		1
8100	£33'909.60	\$22,271.36	X33000.66	932120.45	18	0	4
#186	813688.78	622222.16	#11M(9/65	022271.30	18		- 1
8197	E23666.58	622222.54	62360777	621172.96	98		- 1
R153	833827.77	822172.95	815772.44	\$22113.30	18	0	
KIRK	634070.01	622299.62	E3ATEX#0	622384.34	18	0	- 1
Rico	834090.38	\$2228F 53	E34527-62	6III332.11	15		- 1
891	834014 NO	#22250.52	834075.91	821209.62	15	0	- 1
R162	634049.42	822238.28	234000.19	822287.53	15	0	1
#163	E33993.00	622201.88	834634.00	032250.01	- 0.	. 0	- 1
R164	834007.86	622194-31	#34/SANAT	A22230 24	15		1
R165	E33957.31	622353.70	£259/4.47	62222125	16	0	- 1
R150	835872.14	822651.39	82196475	822190.52	18	0	1
H167	633,683,47	822042.45	E34007.E8	822189.33	18	0	1
R163+R169	833813.72	\$21 87 E 47	SENSTEM.	022050.03	21		1
R170-R171	E33716.44	821 FR 8 15	#21812.49	621978.50	18	0	1
8172+8173	833864.92	821822.12	833719.26	821687.65	26	. 0	1
RUI de RUIS.	#33061,78	621407.56	£13M(3.34)	621623.58	100	0	1
804	E33496.77	f21508.45	£1150.47	621680.73	20	0	-
B177	E33513.09	821599.24	2252744	621698.A2	- 29	0	1
RITE	R35440.44	621525.90	EXTRIBATE	#21608.41	16	0	T
9119	K23451.04	621626.31	#3251133	821600.38	17		- 1
R190	834218.31	622296.35	\$34375.90	622385.39	18	0	- 1
R191	E38181.98	8223°1.72	#34Z1831	822258-36	18	0	1
R182	63A140.62	822162.67	834191.76	022212.30	16	0	4
#183 ·	834099.34	622113.31	834140.62	822162.07	18	0	1
R194	E34077.01	622152.06	#548E1.51	622180.94	15	0	- 1
P184	STATIST .	E22100.84	834E77.94	\$22094.18	13	0	- 1
Kina .	634071.00	07708 s. to	#34007.30	822115.02	14	0	1
RIES	834309.95	\$22180.55	E34302.60	822287.A4	19	. 0	1
RIFE	E34231.54	62206 A 63	6M27134	620136.83	39	0	- 1
R187	834190.59	822037.73	836ZD176	622086.A5	9	0	- 1
R188+R199	634004.93	#21315-C3	#34WE 34	821600.22	45	0	- 1
R190-R191	B23 92 1,12	921727.74	E34004.08	021010.03	19	0	- 1
#192+R (92	633876.32	621460.75	#45WH045	621727.58	29		-
R194-R195	833825.79	621600.56	813887.51	621631.A8	20	0	-
R595+R292	8337E4.04	621523.38	#2180 17	821450.58	20	0	1
RIST	634364.00	\$27000.94	E3440018	62710471	17	0	1
Rtss	834323.77	822010.66	8343434	622060.94	78		1
R199	83A291.93	821961.17	BIANCIO	622910-A8	-18	0	1
R199	834239.47	#21914.12	834210.00	021983.18	-14	0	1
R300	834239.47	\$21914.13	#34290.00	021840.33	18	0	1

											ricle count												
1400	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	16	10	7	8	12	50	50	100	150	150	150	150	200	750	250	200	100	350	250	208	150	150	100
50	22	14	10	11	17	50	100	200	290	200	150	200	200	200	500	150	250	250	200	150	100	100	100
150	50	50	50	50	50	150	250	550	600	500	500	450	450	500	450	350	450	A50	350	250	200	- 200	130
100	50	50	50	50	30	100	250	450	500	450	400	400	400	450	400	300	400	400	300	200	200	150	130
24	13	8	5	7	10	. 25	63	100	150	124	122	123	322	174	172	117	222	. 224	168	113	111	110	:58
57	18	12	- B	- 9	13	58	65	150	150	150	150	150	150	150	150	100	200	200	100	100	100	100	100
17	-9	5	4	4	7	18	50	50	50	50	50	50	90	50	50	50	50	- 50	22	16	13	12	9
17	9	5	4	4	2	118	'50	50	50	50	50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	5	4	.4	7	- 10	50	50	50	50	50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	- 3	4	4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	25	16	13	12	10
17	9	- 5	4	- 4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	23	16	13	12	10
17	9	5	4	.4.	7	18	50	50	50	50	50	50	50	50	50.	50	50	50	50	.20	17	- 14	11
100	100	100	50	50	50	100	250	300	250	250	200	200	250	200	200	200	200	200	150	150	150	100	100
100	100	100	- 50	50	50	100	250	300	250	250	250	250	300	500	30C	350	350	350	300	250	200	700	150
100	100	50	50	50	50	100	250	300	250	250	200	200	250	200	200	250	250	200	200	150	150	150	100
500	400	350	300	250	250	450	100	800	800	100	800	300	800	800	900	800	800	750	650	550	450	450	350
600	500	400	300	250	300	550	1200	1500	1300	1200	1100	1100	1150	1400	1050	1050	1050	1000	850	756	650	600	450
500	400	350	300	250	250	450	1000	1900	1100	1050	950	1000	1050	950	950	1000	1000	950	800	700	600	350	450
50	23	18	300	12	13	24	50	50	50	50	50	50	50	50	50	100	100	100	50	50	50	50	50
100	100	50	50	50	50		200	250	250	200	200	200	200	150	150	150	150	150	150	100	100	100	50
						100																	
150	150	100	100	50	100	150	350	400	350	350	350	350	400	350	350	400	400	406	350	300	250	250	200
200	150	150	100	100	100	200	400	550	450	450	400	400	450	400	AOC	450	450	450	350	300	250	750	200
250	700	150	150	100	100	200	450	900	550	500	500	550	600	600	600	650	700	700	550	900	450	400	300
150	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	400	300	300	250	750	200
150	150	100	100	100	100	150	350	450	480	350	350	350	400	400	400	400	450	496	350	300	250	250	200
300	250	200	200	150	150	300	650	850	750	700	650	700	750	750	750	800	850	800	650	530	500	450	330
250	200	150	150	100	150	250	550	650	600	550	550	550	600	600	500	650	650	650	550	450	400	350	300
500	150	300	300	200	200	450	950	1200	1050	1050	1050	1100	1200	1200	1250	1350	1450	1350	1150	1000	850	800	600
150	350	300	250	200	200	420	900	1100	1050	950	950	1000	1150	1100	1150	1250	1300	1250	10750	900	250	750	550
500	400	350	250	250	250	450	1006	1300	1150	1100	1050	1100	1200	1200	1200	1300	1350	1350	1100	950	800	100	640
590	490	350	300	250	250	450	1050	1350	3,200	1100	1050	1100	1200	1150	1150	1290	1300	1200	1050	900	750	750	550
350	300	250	200	150	200	300	750	900	800	700	650	700	700	650	650	650	650	650	500	450	400	350	300
250	200	200	150	100	150	250	550	700	600	680	550	600	650	650	650	700	700	100	600	500	450	400	500
350	750	200	200	150	150	300	700	850	750	700	650	650	700	650	650	1850	650	650	590	#50	400	400	300
350	250	200	200	150	150	300	650	850	750	700	700	750	H00	600	900	900	950	900	750	650	550	950	460
200	150	150	100	100	100	200	400	500	450	400	400	400	400	400	400	400	400	400	300	300	250	250	200
15	12	9	ā	7	8	14	50	-50	50	50	-50	50	50	50	50	50	50	50	50	50	50	50	21
50	50	22	19	16	18	50	50	100	100	50	50	50	90	50	50	50	50	50	50	50	50	50	50
50	23	19	16:	13	15	24	50	.50	90	90	50	50	50	50	50	50	.50	50	50	50	24	22	1.7
50	50	19	16	13	15	- 50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	- 50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
103	100	50	50	50	30	100	200	250	200	200	200	200	250	250	250	250	250	250	200	200	150	150	100
22	19	15	12	11	12	- 20	50	50	50	50	50	50	50	50	50	50	50	50	50	50	22	- 22	17
100	100	50	- 50	50	50	100	200	250	200	200	200	200	200	200	150	150	150	150	150	100	100	100	50
68	63	61	59	58	59	- 64	200	200	200	290	200	200	200	200	200	250	250	250	200	200	150	150	122
100	70	66	64	36	63	72	150	200	200	200	200	200	200	200	250	250	300	250	750	200	200	200	122
42	35	29	24	22	- 13	38	100	100	100	100	100	100	100	73	73	70	68	- All	66	66	62	62	31
64	60	38	57	55	56	63	200	200	200	200	172	172	171	119	127	316	115	114	111	111	58	58	57
100	100	70	4b	33	38	100	150	200	150	150	150	100	150	100	100	100	150	100	100	100	100	100	74
										150													
10	7	5	-5.	4		B	18	24.	20		14	13	12	11	B	3	5	5.	- 4	- 4	3.	1	3
19	15	12	10	8	3	16	50	50	50	50	50	50	50	:50	22	23	18	-18.	15	13	11	-0	9
21	.18	15	- 13	10	12	21	- 50	50	50	50	50	50	- 50	50	50	50	23	20	18	15	13	12	1.0
50	50	23	20	1,6	19	50	50	106	100	50	50	50	50	50	50	50	50	50	50	50	50	-50	50
50	50	23	. 20	16	19	50	50	100	100	50	50	50	50	50	50	50	50	50	50	50	50	50	30

Road	X1	Coordin Y1	x2	Y2	(including	Height (m)	Road Type (caline 4)
Rt03				822530.25	mixing zone)	0	1
R163	833177.37	822330.25			20	0	- 1
R003	833221.06	822345.76	837414.80	822408.45	20	0	1
R(0)	832434.80	822408.45	933900,46	822643,00	20	0	1
R103	833960.45	622643,95	£33995,46		20	0	. 1
8104	833116,28	822308.10	413/15/51		19	0	. 1
R004	833185.93	822315.62	833425.15	822296.41	19	0	_ 4
R004	833425:15	82238E.41	833518.28		19	0	1
RI05	833616.28	822421.55	813673.75		19	0	- 4
R005	823671.75	822 49 6.5E	E11913.47	822414.65	16	0	1
RI005	633933.67	822614.88	W33973.71		ty.	0	- 1
R005	833973.71		63454610		19	0	7
R005+R007	833527.80	622410.61	633527.55	822455.21	14	0	
R006+R007	833627.55	822A55.21	83373297		16	0	- 1
R005+R007	833732.07	822494.47	853762.11		14	0	4
R004-R007	830782.11	822441.65	813840.51	822456.02	76	0	1
R003+R005	833661.17		533692.59		13	0	- 4
RS03+RS09	833693.50	822397.15	E11841.E	822456.38	13	0	4.
9010+R011	833978.15	822463.30	832994.64	822452.8B	12	0	1
H010+H011	833896.64	622432.68	933993.54	822462.AD	12	0	- 3
RE1D+RE11	8336E3.54	822A52.49	833840.51	822456.02	12	0	
R\$12+R\$13	833387.26	822567.47	223433.50		10	0	1
R012+R013	833423.69	822558.02	832416.08	022462.07	10	0	
9012+R013	833416.08	822.482.67	835447.62		10	0	1
W12-用計2	#33447.62	822A25.39	E13544.64	622390.AB	10	0	1
R\$12+R\$13	833544.64		833547.56		10	0	- 1
9014-R015		822318.11			18	0	1
R016+R017		822354.88		022374.51	15	0	. 1
1位16×用非17			633561.17		15	0	1
Ross	833082.67		#23209-07		16	0	1
R021	833209.07			822383.72	16	0	1
Rt22	#33355.60				78	0	- 1
R022	#334E0.61	822340.13	833419-66		16	0	1
M023	833073.42	822119.68			18	0	4
R624	SEASON LANGUAGE	822129.44	STREET,	REPLY THE SALE	74	0	- 1
R1125	#33232.06		633377.69		16	0	1
R128	823377.80		83359334		14	0	. 1
8927	633603.51		811073.82		13	0	- 1
R024	832673.82		833768.11		13	0	1
Rt29	833766.63	822374.15	833848.76	821405.79	13	0	- 4
R930	\$33848.76	822405.79	£13917.£3	822431.11	18	0	4.
H031	633917.63	822431.11	932990.58		14	0	1
H037+R301	##.070CC#	\$2208.5.71	933121.79	822072.07	18	0	7
8833	833121.79	622072.07	£13292.39		18	0	1
R034	833253.39	822120.94	8333HE77	822175.17	98	0	1
RESE	#33396.77	#22176.17	£33524.35	822221.21	18	0	
PI036	833524.35		#32913.40		78	0	- 1
R637	633653.40	822299.00	833694.86	822284.07	19	0	1
REDE	633694.68	822284.56	833763.79	622339.61	78	0	1
BODY	833761.98			822229.76	14	0	1
R040	833789.11	822318.08	832833.16	R22335.11	18	0	1
R041	833833.10	822335.57	833902.94	822160.57	16	0	- 4
R342	83390E.96	822360.57	631965,46	822320.A5	-18	0	7
R043	813950.46	822320.6E	83401490		18	0	- 4
R044	B34024.90	822250.62			18	0	1
RMS	834148.62	822162.67	834211.76	822086.A5	. 19	0	1
RSAS	834231.72	822086-65	834323.21		18	0	1
R947	\$34322.77	#22910.68	834384.01		18	0	- 1
R048	833097.20		833156.56		17	0	7
R549	833156.66		833434.10		16	0	1
9155	833101.47	821942.33	51327446		21	0	1
RUST	833274.56		233416.70		16	0	- 1
R051	833434.10	822080.21	832668.33	822174.73	16	0	- 1
RISS		\$22123,44			18	0	1
R953	833736.68	#2219.1.2S			16	0	- 1
R054	833438.83	822967.29	#3251671		16	0	7
RI054	#33584.71		833649.55		78	0	- 1
ROSA	63364R.55	622144.43	A11613.61		16	0	1
R254	633661.68		833713.65		- 18	0	- 1
ROSA	623712.85		633757.83		16	0	4
R054	633767.83	822128-66	833778.49		16	0	1
R053	#337# 6.53	\$22123.04	£13872,14	822651.30	19	0	1
R256	833778.49	622113.3 8	8118h7.20	822039.12	16	0	7
WOST	833673.20	822082.68	034119.21	821B1478	16	0	- 1
ROSE	634159.21	821614.78	834250:10	821738.42	16	0	- 3
R059	633867.29	822039.23	43485E34	821680 22	-97	0	- 1
R065	834058.34	821380.22	234241.E1	821727.AS	16	0	. 1
R061	£3311£.37	821890.28	833139.76	821889.31	16	0	1
R082	633139.76	821889.31	833216.78		16	0	- 1
RIN3	833256.88	821947.56	813410.51	10 700158	36	0	4
ROSA	833450.49	#2250E-03	#11543.73	822038.72	13	0	7.
H064	833543.73	832034.72	¥33842.70	821983.31	15	0	- 1
R064	633480.98	821962.82	813543.70	821982.31	15	0	- 1
ROSS	833166.17	823834.07	613315.56		16	0	1
R066	833316.56	321301.68	#33491.00	821952.71	16	0	1
ROST	833164.01	821778.07	833178A7	821783.68	10	0	1
R068	833178.74	621783.16	833253,69		18	0	- 1
RIGHT	833166.60	621757.67	833260.16	821795.91	29	0	1

11-00	then I	11-00	11-02	11-04	U-AF	1 4-05	1 11-07	11-00	11-00	11-10	NO _X x 10	0 (g/VMT) Hr12	0.42	11-44	Hr15	11-10	11.47	I Hr18	1 11-10	1 11-00	T 10-04	11-00	11-02
Hr00 19.5494	Hr01 19.4771	Hr02 19.2052	Hr03 19.3962	Hr04 19.5347	Hr05	Hr06 19,8130	Hr07	Hr08 31.5659	Hr09 28.1980	Hr10 25.8342	24.8197	22.8104	Hr13 23.2580	Hr14 22.9113	24.2346	Hr16 26,5566	Hr17 25.8228	26.3571	Hr19 21,9808	Hr20	Hr21	Hr22 21.4902	Hr23
19.5494	19,4771	19.2052	19.3962	19.5347	19.3311	19.8130	29.2122	31.5659	28.1980	25.8342	24.8197	22.8104	23.2580	22.9113	24.2346	26.5566	25.8228	26.3571	21.9808	19.5433	21.1212	21.4902	20.4022
19.5494	19.4771	19.2052	19.3962	19.5347	19.3311	19.8130 19.8130	29.2122	31.5659 31.5659	28.1980	25.8342 25.8342	24,8197 24,8197	22.8104	23.2580	22.9113	24.2346	26.5566 26.5566	25.8228 25.8228	26,3571	21.9808	19.5433	21.1212	21.4902	20.4022
19.5494	19.4771	19.2052	19.3962	19.5347	19.3311	19.8130	29.2122	31.5659	28.1980	25.8342	24.8197	22.8104	23.2580	22.9113	24.2346	26.5566	25.8228	26.3571	21.9808	19.5433	21.1212	21.4902	20.4072
19.4103	19.3203	19.2188 19.2188	19.4475	19.4644	19.2535	19.6109	26.3457	29.3148	25.9047	24.1629	23.5913	22.0365	22.7058	22.5276	24.1654	26.9612	27.4013 27.4013	27.9686	23.0232	18.6610	20.1856	20.9439	19.4901
19.4103	19.3203	19.2188	19.4475	19.4644	19.2535 19.2535	19.5109	26.3457	29.3148	25.9047	24.1629	23.5913	22.0365	22.7058	22.5276	24.1654	26.9612	27.4013	27.9686	23.0232	18.6610	20.1856	20.9439	19.4901
19.3732	19.2675	19.2283	19.4611	19.5036	19.2735	19.5271	26.3429	29.3142	25.9014	34.1621	23.5855	22.0289	22.6957	22.5194	24.1552	26.9528	27.3767	27.9581	23.0128	18.6463	20.1708	20.9284	19.4937
19.3732	19.2675	19.2283	19,4611	19.5036	19.2735	19.5271	26.3429	29.3142	25.9014	24.1621	23.5855	22.0289	22.6957	22.5194	24.1552	26.9528	27,3767	27.9581	23.0128	18.6463	20.1708	20.9284	19.4937
19.3732	19.2675	19,2283	19.4611	19:5036	19.2735	19.6271	26.3429	29.3142	25.9014	24.1621	23.5855	22.0289	22.6957	22.5194	24.1552	26.9528	27,3767	27.9581	23.0128	18.6463	20.1708	20.9284	19.4937
33.9045 33.9045	31.9241	39.4086 39.4086	20.5578	20.6808	36.9402	33.3409	35.8747	27.1722	37,1358 37,1358	36.2884 36.2884	36.0657 36.0657	41.2314	32.0238 32.0238	30.5259 30.5259	30.7412	21.0885 21.0885	19.9648 19.9648	16.0990	20.4284	23.8594	36.8327 36.8327	36.8607 36.8607	24.8741
31.9045	31.9241	39.4086	20.5578	20.6808	36.9402	33.3409	35.8747	27.1722	37.1358	36.2884	36.0657	41.2314	32.0238	30.5259	30.7412	21.0885	19.9648	16.0990	20.4284	23.8594	36.8327	36.8607	24.8741
33.9045	31.9241	39.4086	20.5578	20.6H08	36.3402	33.3409	35.8747	27.1722	37.135R	36.2884	36.0657	41.2314	32.0238	30.5259	30.7412	21.0885	19.9648	16.0990	20.4284	23.8594	36.8327	36.8607	24.8741
26.8163	29.9420 29.9420	28.3149 28.3149	20.5578 20.5578	70.6808 20.6808	26.9276	26.7445	31.6731	21.7255	30.9137 30.9137	29.6552	30.7539 30.7539	32.4058 32.4058	24,4742	25.9647 25.9647	28.0925 28.0925	21.5916 21.5916	19.9722	16.5836 16.5836	19.8330 19.8330	24.0367	38.1623 38.1623	38.6791 38.6791	23.3591 23.3591
35.2146	34.4827	32.0860	30.6634	16.1030	39.5935	35.6809	40.2425	30.7164	40.0192	38.9096	41.1550	43.0446	16.2797	37.0436	40.3528	35.5992	32.M621	30.7360	31.0903	37.3796	48.7535	483601	37.8957
35.2146 35.2146	34.4827	32.0860	30.6634	36.1030 36.1030	39.5935	35.6809 35.6809	40.2425	30.7164	40.0192	38.9096	41.1550	43.0446	36.2797 36.2797	37.0436 37.0436	40.3528	35.5992 35.5993	32.8621 32.8621	30.7360	33.0903	37.3396	48.7535 48.7535	48.3601	37.8957 37.8957
73.5522	81.7155	27.0902	30.6634	30.1640	29.6258	73.7733	91.1754	68,0728	80.0829	74.4164	81.4143	82.6046	87,4262	78.4954	81.9052	78.3466	82.1180	84,4488	81.1125	102,7666	116.4097	104.3759	86.1635
73.5522	W1.7155	27.0902	30.0411	10.1640	29.6258	73.7733	91.1754	68.0728	80.0829	74.4184	81.4143	82.6046	87.4262	78.4954	81.9057	78.3466	82.1180	34.4488	81.1125	102.7666	116.4097	104.3759	86.1635
73.5522 73.5522	81.7155 81.7155	27.0902	30.0411	30.1640 30.1640	29.6258 29.6258	73,7733	91,1754	68.0728	80.0829 80.0829	74.4184	81.4143 81.4143	82.6046 82.6046	87,4262 87,4262	78.4954 78.4954	81.905Z 81.905Z	78.3466 78.3466	82.1180 82.1180	84.4488 84.4488	81.1125 81.1125	102.7666	116.4097 116.4097	104.3759	86.1615 86.1635
71.5522	81.7155	27.0902	30.0411	30.1640	29.6258	73.7733	91.1754	68.0728	80.0829	74.4184	81.4143	82.6046	87.4262	78.4954	81.9052	78.3466	82,1180	84,4488	81.1125	102.7665	116,4097	104.3759	86.1635
46.3548	45.6844 47.3405	48.6569	55.541H 43.9506	53.7497 42.9396	52.6549 52.6549	47.6396 45.8180	64.8075	40.1863 38.6106	51.6040 50.3438	52.4614 49.6952	\$5.8943 \$1.8361	57.7004 53.5264	53.2020 47.3265	51.9129 47.7428	56.6202 50.8169	52.4591 41.0996	50.5332 42.0708	47.6379 39.1630	50.1390	57.5428 49.4816	73.7092 63.7171	73.5067 61.1175	54.3156 46.5230
46.3548	47.3405	48.6569	43.9506	42.9396	52.6549	45.8180	62.5803	38.6106	50.3438	49.6952	51.8361 51.8361	53.5264	47.3265	47.7428	50.8169	43.0996	42.0708	39.1630	40,6846	49,4816	63.7171	61.1175	46.9230
75.3328 74.7111	75,0022	71.0747	76.5385	81.3632	72.7908	72.8099	84.2258	67.7910	78.5946	74.4968	79.3433	78.4272	77,3607	70.9450	77.1473	76,1846	68.0813	65,3730	67.4942	80.2735	99.2047	85.6235	78.5434
74.7111 83.4457	79.4268	70.4207 82.5373	77.5037 84.6443	71.7796 81.6938	78.7795 83.5395	74.5060 83.9986	91.2595	68.3911 76.4690	79.1044 86.8886	74.3307 83.2096	79.3480 87.1579	78.4135 86.6152	77.0590 84.9603	71.5159 79.0309	77.9185 84.1199	73.6938 83.0935	69.0680 75.9108	73.2232	67.1931 73.9387	84.3666	95.9959	92.5212	74.0504 81.6140
81.4457	79.4268	82.5373	84.6443	81.6938	83.5195	83.9986	91.2595	76.4690	86.8886	83.2086	87.1579	86.6152	84.9603	79.0309	84.1199	83.0935	75.9108	73.2232	73.9387	84.3666	99.3899	92.5212	81.5140
80.1886 81.4500	74.6269	81.6429 77.7118	80.2971 76.1867	81.1757 81.1757	76.4023 79.3668	78.5313 79.5390	90.5559	77.2466	86.9681 87.1410	82.9207 83.8812	86.5740 86.4127	87.4580 84.5133	85,6543	79.7476	84.7357 84.6308	82.0381 82.7708	78.1148 78.2093	77.0555	75.6183 73.5757	85.2877 85.4758	99.8833 98.7318	91.5230	79.6499 79.6105
80.3075	80.0579	76.5809	81.5751	85.7069	78.0493	78.1135	88.2823	75.5267	88.2891	84.3511	88.0592	86.5369	34.8400	80.9302	86.3209	81,2918	79.6805	76.4050	74.5239	84.2631	101.0790	90.9509	79.3749
84.3382	84.5675	85.4368	87.2904	84.4475	81.5623	85.0380	94.0582	87.2525	93.9079	88.4126	91.6363	88.6754	88.3424	81.0161	86.5133	86.9728	80.8718	75.8060	74.8068	85.0265	96.3518	88.9753	79.1412
73.4780	81.7508 71.9590	82.0469 73.8457	82.1429 R1.1883	85.2170 76.7588	84.7011 71.2688	74.1851	93,4866 82,6079	85.8423 69.5741	95.4484 81.0363	91.7206 76.9347	94.7512 80.9774	93.6937 80.5860	91.7908 78.4162	88.6981 75.3978	90.5237 81.1041	98.3182 76.5887	83.8033 72.8717	71.9168	78,5180	86-9563 80.8649	97.9473	92.5301	81.8013 74.2568
70.5242	66.6285	73,7104	55.5418	58,4908	69.6588	69,3093	85.4797	72.1522	79.6173	72.5849	77.3653	74.9799	77.3949	70.1591	76.4172	78.4275	70.5147	66.6267	68.2059	80.1939	91.1722	84.0577	78.6350
69.6584	73.9213	70.8586 60.1454	71.4835 68.2922	67.4035 68.4908	69.2035 55.2137	71.3096	85,3436 84,8930	70.7846	80.8232 79.9684	73.9301	79.5134	75.1045	78.7401	73.3880 69.9023	79.7150 75.8379	76.2147	73.1956	70.3405 67.0728	68.3740	79,2045	95.0644	85.1684	73.9698
74.5167	73.4801	64.8029	64.8904	64.2762	63.3359	65.1192	76.8050	63.6039	73.1995	69.2569	73.9646	73.1506	72.2920	67.0966	72.2236	69.7054	66.HS80	64.757R	61.5421	74.3446	86.3961	79.4408	69.1024
61.0642	63.4978	65.3326	64.5938	67.4649 64.2551	66.1411	63.8967	77.3274	62.2774	72.1860	68.2085 66.3810	72.3698 71.0937	71.7585	70.5595 69.2122	67.1629 65.9167	72.4656 71.5255	69,7444 68,9444	66.7873 66.1716	63.6657	62,4012	72.5381	87.0422 85.5749	80.1326 79.0830	66.5410
70.2643	70.0212	69.5244	69.3056	59.6483	69.1001	69.6051	83.0379	70.5344	79.5657	75.5791	78.1028	77.8234	76,3257	70.6889	78.1712	74.9385	68.6722	66.1458	65.8439	74.8003	89.6416	82.4407	70.9609
67.4878	67.0957	66.9789	67.8198	67.4990	67.6364	67.3522	79.7972	68.3577	78.6327	72.8334	77.2089	76.3976	75-3654	70.1838	75.5249	72.7781	69.8775	67,6895	66-4637	75.4281	87.7905	81.0056	70.8662
82.3226 81.2997	82.1616 83.1624	81.9705 83.2040	82.8290 83.3700	82.5583 83.7655	82.0096	82.4262	96.1501	84.0594	93.8340	85.1111 85.1111	88.9965 88.4863	85.8234 84.4464	85.6005 83.2922	76.9064	81.439Z 78.0867	77.8356 75.6038	72.9647 67.9891	63.3871	68.1570	77.7810	91.8210 85.2080	84.1558 78.6306	72.8439 67.3681
89.5797	86.5960	86.8454	88.3624	88.6176	87.6623	87,4540	102,6678	97.1827	100.2397	92.4531	95.8234	91.2767	91,1141	79.6874	86.9212	83.5962	72.2305	65,6973	67.6640	76.4481	89.7414	79.4290	74,1813
88.5719 89.5875	89.1959	88.9262 88.0572	90.1738 88.8000	89.4304 88.1500	89.4885 88.7093	89.4398 88.0416	102.3125	93.8875 96.9231	99.5581	91.5758 92.2794	92.7996 95.6723	91.2886	88.2855 90.9326	77.0178	84.3856 86.7971	81.3776	72.1717 72.3042	65.5202	66.1959	75.4647	90.1348	78.8550 79.6100	73.7441
89.7955	88.2363	87.8996	88.5887	88.4337	88.8306	88.4875	102.6431	94.3746	100.1681	89.8183	93.1641	88.7339	88.6925	77.2201	86.5198	83.0841	71.5137	64.6664	65.2119	75.6392	87.3613	78.7727	73.4622
96.9933	97.5150	97.5677	97.7416	98.6860	97.8801	97.7967	108.1918	101.6135	105.8781	97,7790	101.7165	96.7396	98.2690	85.0579	93,6983	91.3825	80.1338	73.0768	73.5005	82.6037	95.9864	85.5038	82.4904
89.5662	80.6696	88.7812 81.2916	90.1266 83.8314	89.3877 84.9420	89.0199	89.3390 89.3701	102.1293	93.8947	99.4590	89.2170 90.0009	92.8282 93.4158	89.1074	88.1968 89.2149	76.9686 78.1055	84.1506 85.1476	82.8832	71.5195	64.669Z 64.8496	66.7697	75.0528	86.8578 88.1390	78.4070	72.5872
90.2689	87.9494	88,0318	89.3187	38.6196	88.7333	90.7061	102.9589	95.1681	100.6545	90.7318	93.9920	89.6132	89.3715	78.3556	85.0881	83.7838	72.5537	65.9515	66.3024	76.4800	87.6874	79.3876	74.4632
90.1996 66.6564	65.6518	87.9984 65.5120	82.97% 65.9062	89.1926 66.0677	88.3564 65.7804	90.7391 66.7536	79.6861	92.9466 75.2117	98.2785 79.9475	90.7332 71.4731	94.1817 74.7406	89.6863 72.1599	74.0872	78.4463 65.5353	85.2840 72.3320	81.9949 70.9990	72.6280 65.1662	65.8691 62.2878	66.2888 59.3883	76.5715	87.8153 80.4817	79.5369 71.9819	74.3827 65.4268
66.7253	66.6587	66.5915	66.9077	67.0671	66.5934	66.3851	78.4791	72.2070	76.8742	68.8519	73.4602	70.9549	71.6482	63.3375	70.0138	68.8270	63.1604	59.5445	57.9235	68.7898	80.5705	72.1385	65.8376
70,6840	70.7937	70.6902	70.8730	70,9937	70,7911	70.8891	83,7149	79.1945	84.8430	74.9481	78.7906 79.7588	75.3450 76.1047	76.0741	67.9406 68.1548	73.6497	71,0641	65,4786	60,7627	58,2053	65,3405 68,5738	75.9857 79.6654	67.4546 70.8419	61.3715
73.6897	71.7944	71.5059	72.3319	72.3614	72.0198	73.4342	82,7780	77.0276	78.4336	71.4458	75.6873	72.4709	74.4028	65.7568	73.5080	72.1719	64,2621	50.3219	59.3225	70.0145	81.5245	72.9162	68.4407
76.0696	74.6637	74.6130	75.0408	75.2855	74.9317	75.9684	85.8335	80.8219	84.0820	74.9507	79.5094	75.7927	78.8598	69.4467	77,0474	76.1488	69.2701	65.1132	63.7257	73.1084	84.4929	74.9618	70.4244
76.0696 78.3615	74.6637 78.4308	74.6130 78.0480	75.0408 78.7105	75.2855 78.9837	74.9317	75,9684 78,5569	85,8335 87,9865	80.8219 82.5295	84.0820 86.8492	74.9507 79.3175	79.5094 83.1545	75.7927 80.9400	78.8598 83.9957	69.4467 74.0917	77.0474 82.7737	76,1488 84.5458	69.2701 75.5355	65.3132 71.0326	69.5974	73,1084	84.4929 90.6648	74.9618 79.4489	77.2430
78.3615	78.4308	78.0480	78.7105	78.9837	78.3977	78.5569	87.9865	82.5295	36.8492	79.3175	83.1545	80.9400	83.9957	74.0917	B2.7737	84,5458	75.5355	71,0326	69.5974	79.6821	90.6648	79.4489	77.2430
78.3615 78.3615	78.4308 78.4308	78.0480 78.0480	78.7105 78.7105	78.9837 78.9837	78.3977 78.3977	78.5569 78.5569	87.9865 87.9865	82.5295 82.5295	86.8492 86.8492	79.3175 79.3175	83.1545 83.1545	80.9400 80.9400	83.9957 83.9957	74.0917	82.7737 82.7737	84.5458 84.5458	75.5355 75.5355	71.0326	69.5974	79.6821	90.6648	79.4489	77,2430
78.3515	78.4308	78.0480	7E.7105	78.9837	78.3977	78.5569	87.9865	82.5295	86.8492	79.3175	83.1545 83.1545	80.9400	83.9957	74.0917	82.7737	84.5458	75.5355	71.0326	69.5974	79.6821	90.6648	79.4489	77.2430
78.3615 74.0649	78.4308	78.0480	78.7105 74.7445	78:98:37 74:5676	78.3977	78.5569 74.2078	87.9865 83.5520	82.5295	86.8492	79.3175	83.1545	80.9400 72.5737	81.9957	74.0917	82.7737	84.5458	75.5395 64.0491	71.0326 60.5820	69.5974 59.0381	79.6EII	90.6648 81.0169	79.4489 72.5347	77.2430
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61.0022	58.4670	58.6195	59.6998	59.5517	59.2738	61.0618	70.4679	65.1698	65.0328	59.8675	62.7930	60.9036	59.9967	53.6489	62.3740	61.3859	52.7218	45.0814	48.0144	54.8176	64.5651	58.3830	56.8144
79.2858 67.4327	76.8661 67.8338	76.7515 67.3472	77.7379 67.5962	77.7733 68.3858	77.7789 67.5427	79.5042	89.3746 77.2768	72.6190	84.7834 70.9005	76.5204 66.2885	80.6722 69.3325	76.1079 66.6418	79.2341 66.7950	58.7475	75.6163 68.9009	74.5680 68.6299	54.7759 56.8265	60.3184 48.4727	51.9814	72.0680 59.4374	83.2309 68.6008	73.8084	69.8249
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103.8301	101.3730 71.8609	73.2184	100.1331 71.9467	34.7418 76.1021	103.5435 74.1722	102:6636 72:8656	104.1567 83.1254	100 9298 71.6483	105.4147 80.5364	103.6333 77.3102	105.3693 81.8264	104.9201 81.5453	104.6087 79.9047	102.2564 74.3298	104.2117 80.2786	103.4120 77.2863	100.6916 72.8964	100.7686 69.8686	99.8966 69.2678	103.3811	107.2129 93.7508	106.1065 86.0193	101.1955 76.7368
75.0483	68.4405	76,5465	75.3473	75.6954	70.6063	73.0922	83.1254 85,3735	68.9773	79.1052	77.3102	79.3701	78.8018	79.9047	74.3298	77.4383	75.5357	69.7228	68.7556	67.6831	79.0107	94.7250	86.0193	76.7368
72.6851	65.3627	71.9463	74.2019	70:1500	69.1997	70.7471	83.9596	67.0823	77.5645	73.2025	78.8648	77.7463	76,3311	70.5116	76.8532	73.9132	67,8480	65.8272	67.1459	78.8448	94.7838	87.2816	77,1631
72.6851 72.6851	65.3627 65.3627	71.9463 71.9463	74.2019	70.1500	69.1997 69.1997	70.7471	83.9596 83.9596	67.0823 67.0823	77.5645 77.5645	73.2025 73.2025	78.8648 78.8648	77.7463	76.3311 76.3311	70.5116 70.5116	76.8532 76.8532	73.9132 73.9132	67.8480 67.8480	65.8272 65.8272	67.1459	78.8448 78.8448	94.7838	87.2816 87.2816	77.1631 77.1631
78.1714	74.5960	76.1951	76.9166	74.3431	72.4993	76.2043	86,1462	72.4195	82.3755	78.5Z35	83.2043	82.5162	80.2138	74.9386	79.3480	77.8239	71.9750	67.6402	68.4519	78.5317	93.2509	87,0086	76.8595
75.9757	75.1998	74.6064	77.7251	75,5978	71.7452	76.0103	86,3811	70.8975	81.0746	77.0981	81.6415	80.4271	78.2527	74.8236	80.1511	74,9798	71.3115	67.9678	68.4259	77,9107	93.7120	86.1439	74.7602
46.9968	47.2373 47.0383	46.9527 46.7929	47.2120 47.1156	47.2854 47.1617	47.2270	47.5099 47.2910	65.6662	53.9132 53.7060	63.9979 63.8522	59.0536 58.8596	63.3376 62.2805	61.2100	62.2924 62.1538	55.7946 55.6514	58.9550 58.8226	56.3127 56.2114	53 6061 53 5115	53.5443 53.4606	52.2000 49.2568	53.5012	62.0581 62.0258	55.7206 55.6957	45.7373 45.6726
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614661	63.3039	63.2292	63.4158	53.7350	63,4064	63.5220	73.7586	62.5451	72.9049	65.6361	69.7415	67.6323	58.3812	62.1346	65.1193	63,4957	61.4932	60.2858	57,0269	65.8966	78.2421	71.5227	60.9801

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Brake Brak	CASSAD AN	401476.80	81400418	#21816.03			ŀ	100 6854	
R147+R148	E33778.84	621688.36		82172774				71.1642	1 2
R149	833728.61	821748.53	833807.73	82168438	14	0		65.6498	98 63
8148	833774.08	821643.52	633807.73	821684.38	13	0		65.6498	-
RTSG	533736.67	821759.23	833667.71	827801.87	.11	0	+	65,6498	98 63
RTST	e23612.61	821619.98	632683.50	821543.78	12	0		65.6498	H
Atst	833693.50	821543.70	833776.28	821547.53	14	0	1	65.6498	-
R152	833774.08	821643.62	833828.17	821609128	200	0		65,6498	98 63.
R163	633991.31	872369.76	834018.77	\$22414.27	18	ø		\$6.5344	-
R154	823950.86	822329.46	33299200	822368.87	11	9		66.1683	67.0
R155	833909,65	833371,38	133910.46	822220.45	18	0	1	66.10	67.
R156	633868.78	672222.14	833908.85	822271.35	81	9		84,2368	F
B157	83388.58	#222228	833827.77	82217288	. 83	0		86.7541	-
RTSR	613827.77	822172.05	8337728.89	6221535	22	0		82.8878	83.7
Ress	834075.91	872799.62	834112.90	622344.34	13	0		63.0412	+
Rt60	624090.29	621287.63	634117.62	822232.61	10	0		69.8754	H
RIGE	E34134.90	822259.52	834075.81	922294.62	. 80			63.8470	+
R162	534549.42	822228.25	83409038	822287.53	18	0		70.3130	H
R163	6331953.96	822301.68	634034.90	822250.01	14	0		66.6385	-
H154	634107.86	622181525	53404842	82223828	16			67,8477	-
8918	613953.31	822151.70	83399447	82220123	. 93		0.00	68.7987	87 68
R166	233872.14	822051.38	83396475	622160.53	19	0		S7,672A	24 56
R167		\$72042.45	834007.86	822109.33	- 18	0		84.9667	67 8
R168+R165	833613.72	521975,47	83387636	822050.03	21	0		33.4172	72
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R172+R173			83377928	821867.65	20	9	+	69 94	946
H174-R176	833581.78	821677.56	83368338	621823.65				72.2117	
RITE	633498.77	621608.49	833565.47	821680.73	20	0		66.5767	29
Rett	613513.09	\$21599.24	93357369	\$21568.47	76			74.1750	2
MITTE	833440.44	821329.90	933413.00	10.00011		0		72.6637	
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8182	834146.63	82216267	63468478	62221238		0		71.56	96
8183	834099.34	822113.33	834146.62	822162.07	10			76.9501	10
R184	634877.01	822132.06	834051.51	822108.94	13			80.6892	92
Rike	124051.51	822100.94	834871.50	822084.18	13	0		80.6892	76
R184	834071.90	822084.18	834097.30	822115.02	14	0		80.68	92
R105	834309.95	822180.58	03438286	822267.44	- 60	0	4	73.9603	03.
8186	634231.54	622/08/6.63	83427334	#2213K#3	1.0	a		80,7438	38 80
8187	234190.59	\$22037.73	83423176	\$22086.45	16	a		78.33	88 80
R188+R189	834004.88	821816.03	83408834	821880.22	18	0		72.0590	96
R100-N191	633831.13	821727,74	034004.98	821816.03	40	0	-	76.2251	+
R182+R193	53.878.52	821689.75	83191688	821727.98	2.0			61.4009	+
R194+R195	61353513	821505.86	833867.51	\$21651.45	28	9		92.8042	+
R196+R202	E35761.01	821523.36	933-828-17	821603.58	30	0	-	91.2764	-
1197	134364.36	\$21000 B4	03440018	82210671	44	0		80,8139	+
RIBE	SPANIETY	99/01/0779	03420430	PZZ DWE DA				72.6813	200
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M 200	E44748.17	210101	87431744	621 MEST 11				79 6500	6 8
Marry .	Beller	_		date of the last	14.			ALC: N	

Hr23	0.5382	3.1517	6.4328	5.3873	0.3044	6.2402	1.1541	81.1541	81.1541	76.0194	76.0194	71.8183	58.8467	58.5328	59.3095	70.4515	70.5372	70.5419	/U.#183	69.2280	5845	2 395.4	64.6883	7.3282	49.5277	7.8738	1.9641	2.7314	4.4302	1.6029	2.3483	4.4577	0.7279	5.5707	6.9340	76.0950	3.2167	49.0624	49.0624	49.0624	78 2167	85.5128	69,6717	4.1748	52.1234	96.3239	38 1535	11.1541	0 1116	9.1330
Hr22	77.2933 6	64.5085 5	80.7764 6	80.2239 6	66.3474 5	619135 4			1	99.8596	99.8596	91.8351 7			1	+	+	+	+	82 5721 6	1	+	-	-	H	87.0774 7	44.0817 3	522770 4	77.7899 6	86.2336 7	82.6941 7	76.5107 6	91,4717 8	92 5008 7	94 8693	91,6494 7	Н	+	+	91 0446 7	+	-	813767 6		1	-		99.8437 8	4920	0476
		Н	-	1	+	+	-	-	4		Н	-			+	+	+	+	+	+	٠	+	۰		۰		Н	Н	Н	Н	+	+	+	+		Н	Н	+	+	+	1	-		32 89	+	+	+	+	718 87	73 85
Hr21	823356	Н	+	84,1167	+	+	1	1	1	102.6816	102.6816	100.0244		78:4053	+	+	+	+	+	84.0635	t	+	+	٠	۰	5 96.4073	45.6083	53,7881	Н	+	+	82.0539	48.0279	t		101 5898	99.5100	69.1765	+	98.1785	36.805	H	865212	96.46	+	105,6413	1	107,6798	93.70	38,33
Hr20	65,6659	59.7623	70.0307	68.8754	52.3662	AS 8150	86.113	86.1131	86,1131	86.113	86,1131	83.7883	62,2213	62.481	64.3137	80.254	79.1863	76.9120	73,5549	74.2107	0015 89	67.7858	70.4397	72.8238	50.5128	81.6956	33.0755	44.2673	69.3397	79.3562	75.7301	67.7380	70.360	82.9711	83.6862	81.1567	81.3977	59.5450	59.5450	80.0668	78 3555	89.5261	73.2508	80.3965	62.0564	98.5654	90.9424	74,4889	85.78KK	65.34p
Hr19	54,9867	47.9811	62,3655	859.4658	45.8377	40.3649	72.7280	72,7280	72,7280	70.6145	70,6145	67.7715	52,2522	53.3643	53.6583	71.9640	70,4597	200.0447	51.6111	56.7498	57.0814	\$6 5138	58.7712	61.8914	45.2423	70.9226	29.0362	40.1726	59.4624	69,2191	65,9204	58.1166	74.5504	69.8560	70.0910	67.1462	67,6611	44.8328	44.8328	69.6528	65 4712	80.6043	61.4978	67.9261	50.9443	90.6990	83.6956	62.3114	27 0801	17,0801
Hr18	55.0758	45.6632	62,6829	61,0052	45.0535	19.2461	75.5585	75.5585	75.5585	73.6681	73.6681	69,4749	51.9729	53,2155	53.7094	74,0527	72,7350	65.8845	152.1638	57,7631	SERVIE	58.0474	61.0293	62.0795	44,8200	70.4507	27,1833	39.0295	603071	70.4503	67.8563	59,3165	27.3677	70.4063	72.7130	69,8488	8609.99	44,8117	44.8117	71 3656	64.3614	80.7207	62.5285	68.9892	48,1589	91,8950	843316	54.8790	57,5534	76.7337
HH17	56.3838		Н	G.1689	+	+	+	+	+	1	72.5237	70.2908	Н	54.6614	564327	+	+	+	+	58.9462	٠	+	٠	٠	۰	3.4369	30.6615	41.9168	Н	H	+	61.2553	78.0947	+	3.9823	1.0589	66.1905	+	+	96.6238 77 1348	t	۰	H	Н	+	+	+	55.9224	70 0084	98266
Hr16	7520 5		68.0561 6	2774 6	+	43.3482 4	+	+	1		70.5321 7	6699	Н		+	+	+	+	1	62 3751 5	٠	+	t	٠	٠	81.4733 7	32.5906 3	Н	Н	+	+	65,2645 6	74 68519	+	73.0780 7	73,1906 7	Н	+	+	26 1254 B	٠	L	67.2522 6	Н	+	92 6363 9	+	69.0010	7551 0	4044 1
-	160 57.			923 64	122 47.	166 43	12	X67 75	15, 75	02 29		69	Н		1	1	+	+	+	+	٠	+	۲	۰	H	H	Н	Н	Н	+	+	+	+	+		Н		+	+	+	+	t		Н	+	+	87.	121 69	192 73	194 1 73
-	5 70,0460		2 77.5838	5 76.3923	1 62.1	240	2 71.80	2 718	2 718	4 71.8	4 71.8067	3 71,4875	Н	-	2 63.3905	7 88.5	83.7941	75.8620	+	70 70 7659	٠	+	٠	t	-	R 84.6299	0 36,1558	Н		Н	+	4 69.4128	+	+	5 78.5546	8 74.7069		+	+	C 78 76/10	1 70.6704	1 87.5517	5 69.8662	9 76.8998	59,9619	B 94,0744	89.2	19 68.2	75.0	5 1 73.3
Hr14	69.544	54.2323	79.520	76.135	62.672	55.337	69.717	69.7172	69,717	68.861	65.8614	66.495	58.6740	60.0265	50.2162	86,704	82.804	74917	95730	66.7677	64 5347	62.336	63.0241	66.3090	51798	78.657	33.7870	45.764	65.6510	74.8045	69.1820	66.7394	72 1453	74.327	72.783	69.4098	73.1408	57,8914	57.891	27.8914	73 371	82.695	67.281	71.741	56.576	92.021	87.550	69.138	73 713	72.733
Hr13	THEFT	55.1340	85.1578	83,7970	67,7519	61.1714	71.7366	71.7366	71,7366	71.7366	71.7366	69.7920	54.6318	64.2788	9689.96	31.7344	91,6592	52.6286	1120.93	71.2871	W 6063	58.0901	70,2327	70.9299	54,2090	38.4496	32.9319	46,4123	71.2853	\$1.2510	73.1704	72,7575	81.6470	80.6022	78.8608	77.8389	78.4780	54.5301	64.5801	70 8 70 5	78.8608	\$5.6015	71.8586	78.4240	64.9765	94.8416	83.2237	69.7882	30,4883	79.03429
Hr12	81,3087	868509	88.3506	87,0785	73,2114	67.3161	72.7452	72.7452	72.7452	72.7452	72,7452	71.3273	67,2535	68.5947	69,3049	97,3384	93.2391	65.8100	10.0274	71 9441	77 3336	69.8588	69.3967	72 9402	59,7588	88.3316	1990/66	51.8042	72.0275	80.4840	73.8821	73.0253	80.9713	81.6770	80.6892	76.3880	80.4192	70,2678	70.2678	78 5710	60.9636	88.3385	74.9349	79.7056	66.1471	96.5373	92.0534	69.1841	27 1406	82.1400
Hr11	85.5725	59.6202	94.6841	11.1564	7.5947	70.7350	70.9546	70.9546	70.9546	70.9646	70.9646	70.2622	58.2801	9609 69	70.0117	8.8026	95.6825	86,0752	70.5982	73 3876	۰	71 39CE	70.7820	73.6383		13.4736	Н	50,4297	Н	81,6953	+	75.2710	81.3747	+	76.4759	76.0445	96,4930	75.1250	75.1250	90,2206	83 3056	8.6220	74.6415	80.2875	65.9330	98.7095	85.6506	12.22.28	135713	1.000
Н	83,1719	Н		88.1940	+	+	+		d	66.8094	-	66.2419	Н	-	+	+	+	+	+	67 5813	٠	+	٠	+	۰	87.3906	Н	Н	Н	Н	+	72.1349	+	٠		71.3381	77.0539	+	+	74 7172	H	H	16	Н	1	+	+	78.0250	17620	82.5330
-		Н	+	+	+	+	+	+	+	-	-	-	Н	-	+	+	+	+	+	+	٠	+	٠	+	٠	H	Н	Н	Н	+	+	78.2179 72	+	+		Н	Н	+	+	+	+	⊦		Н	+	1	+	+	70 FEB.	1067 1 54
-	26 91.9705			11 96.2932	+	+	78 69.082	78 69.0821	78 69.0821	11 69 5909	11 69.5909	78 69,0821	Н		+	+	+	+	+	+	٠	+	۰	٠	H	48 94.6821	36,6869	Н	Н	+	+	+	+	28 85.4235	H	36 74.4236	52 82.3507	+	+	78 9885	45 R2-5339	53 85.9501	34 75.8628	81.4802	53 65,2949	16 95,0177	11 88 2181	000 83 3000	74.74 F.7.77	10 1 07.7
Hr08	77.54	49.8048	87.54	83,038	67.78	62,6815	55.33	55.33	55.33	55.82	55.8211	55.33	59,4549	59.2080	52.8668	+	+	+	+	54.9632	۰	÷	٠	٠	٠	87.27	28.7498	442358	Н		+	68 3477	70.4382	72.3028	62.8877	64 020	70.7152	+	68.4908	68.0550	73.45	76.70	64.03	70.100	55.90	64.07	89.06	68.74	76.60	75.50
Hr07	97,0728	59.1554	98.3258	97.8501	87,7445	82.4608	75.5702	75.5702	75,5702	75.5702	75.5702	75.5702	78.6043	78.7506	80.7297	106.565	108.370	94.2075	720166	76 5017	81.475.7	78 6014	77.4343	78.5165	66.4567	99.6194	39.5956	51.5980	80,8667	86.4633	77,3255	82,7163	2007.00	88.1128	82.3867	81.1363	87.4382	90.0897	90.0897	90.0897	89 988	50.6719	80.4065	87.0160	69.4094	96.8063	91.922	85.3907	60 580	90.5507
Hr06	84,1696	55,5359	89.3120	89.1353	78,8726	72.8490	63.8449	63.8449	63.8449	65.8539	65.8539	63.8449	66.9349	67.2896	67.2568	84.5%	86.9965	82.9820	62.2319	64 4419	70.4083	67.1876	67.9380	69.0155	57.8353	85.3238	33.2715	45.0268	69,3468	71.9489	8225.99	74,0895	78.1.982	76.3556	77.3595	72.2724	76.7092	80,9253	80.9233	26,323	78.4282	79.4284	72.7114	78.1066	62.0816	92.9322	92.0211	68.1141	88,1141	85,2674
Hr05	87.9770	54.0577	91.1777	90.9267	75.6840	76.8650	73.4908	73.4908	73,4908	73.4908	73,4908	73.4908	67.6201	66.3277	66.9497	77.5519	82,4482	63.1555	10.5052	70.4604 63.4115	70.0363	67.1175	67.8209	68.6608	56,6105	85.0707	32.5304	45.7186	69.4449	71.2626	66.7160	74.3437	72.5862	75.3383	68.0077	74.9431	34.3015	90.8016	80.8016	73 8221	95.1765	80.2992	72.5775	77.8559	60.8741	91,4293	K6.3337	68.0077	63.7430	90.5094
Hr04		Н	Н	89.6182	+	+	+		1		Н	5E.490E		-	67.2739	4	+	+	1	68.8995	٠	+	890689	+	-	86.2827	Н	Н	89,0488	Н	1	74.0161	75,7730	+	Н	81.1339	Н	+	77.3355	+	+	\$2,2361	Н	Н	65.1269	-	+	+	58.4908 se 3067	ì
-	-	Н	88.9618 8	+	+	+	+	+	4	-	H	-		66.7250 6	+	+	82 3492 8	+	+	63 1290 6	٠	٠	+	H	٠	85.2047 8	-	Н	69.4977 69	-	4	74.3441	+	╀	Н	72,8193 8	Н	+	+	77,8330 7	t	t		H	+	+	+	+	91 0821 8	
				⇁	+	+	+	-	\neg	\neg					7	_	_	_	+	+	٠	۰	۰	+	Н	Н					_	т	т	+	-	_	Н	+	+	+	+	٠		Н	+	-	+	+	+	-
	15,4633		-	+	-1	+	+	Н	+	-	10 60,3454	60,1454	Н	-	+	+	+	+	-	11 69.7344 15 62.6198	+	+	+	+	-	15 84,5914	Н	16 45 3389	3 68.9400		-	-	12.4692	+		34 73.4556	11 80.6359	+	+	75 0475	+	+	+	Н	+	+	+	+	55 67.8044	-
\neg	83.1039		\neg	+	+	+	7	-	-	_		63,7430	Н		+	-	-	т	63.6436				67.8459		-	$\overline{}$	32,9176		69.3403		7	74.3747	+	T	Н			7	+	72 8183	+	т		Н	7	+	-	-	70.5665	
Hroo	84.2591	\$5,2810	89.6976	89,1399	80.6854	71.1647	65.6498	65.6498	65,6498	65,6498	65,6498	65,6438	66.5344	66.1683	66.1061	84,2368	86,7541	82.8876	63.0432	63.8470	70.31.10	8666385	67.8477	68.7987	57,6724	84.9667	33:4172	45.2713	69.9446	72.2117	66.5767	74.1750	72.0637	75.5252	73.9549	71.5629	76.9501	80.6892	80.6892	73 96.02	80.7438	78.3388	72.0590	76.2251	61,4009	92.8042	91.2764	80.8139	72.0813	82.6155

Road	X1	Coordin Y1	x2	¥2	(including	Height (m)	Road Type (caline 4)
Rt03				822530.25	mixing roset	0	1
R163	833177.37	822330.25			20	0	- 1
R003	833221.06	822345.76	837414.80	822408.45	20	. 0	1
R(0)	832434.80	822408.45	933900,46	822643,00	20	0	. 1
R103	833960.45	622643,95	£33995,46		20	0	
8104	833116,28	822308.10	413/15/51		19	0	-1
R004	833185.93	822315.62	833425.15	822296.41	19	0	- A-
R004	833425:15	82238E.41	833518.28		19	0	1
RI05	833616.28	822421.55	813673.75		19	0	- 4
R005	823671.75	822 49 6.5E	E11913.47	822414.65	19	0	1.
RI005	633933.67	822614.88	W33973.71		ty.	0	- 1
R005	833973.71		83404610	822626.54	19	0	7
R005+R007	833527.80	622410.61	633527.55	822455.21	14	0	
R505+R507	833627.55	822A55.21	833732-97		14	0	- 1
R005+R007	833732.07	822494.47	853762.11		14	0	4
R004-R007	830782.11	822441.65	813840.51	822456.02	74	0	1
R003+R005	833661.17		533692.59		13	0	- 4
RS03+RS09	833693.50	822397.15	E11841.E	822456.38	13	0	4.
M010+R011	833978.15	822463.30	832994.64	822452.8B	12	0	1
H010+H011	833896.64	622432.68	933993.54	822462.AD	12	0	- 3
RE1D+RE11	8336E3.54	822A52.49	833840.51	822456.02	12	0	
R\$12+R\$13	833387.26	822567.47	223433.50		10	0	1
R012+R013	833423.69	822558.02	832416.08	022462.07	10	0	
9012+R013	833416.08	822.482.67	835447.62		10	0	1
W12-用計2	#33447.62	822A25.39	E13544.64	622390.AB	10	0	1
R\$12+R\$13	833544.64		833547.56		16	0	1
9014-R015		822318.11			- 14	0	1
R016+R017		822354.88		022374.51	15	0	. 1
1位16×用非17			633561.17		15	0	1
8019	833082.67		#23209-07		16	0	1
R021	833209.07		833315.00		16	0	1
Rt22	#33355.60				16	0	- 1
R022	#334E0.61	822340.13	833419-66		16	0	1
M023	833073.42	822119.68			18	0	4
R624	SEASON LANGUAGE	822129.44	STREET,	REPLY THE SALE	14	0	- 1
R1125	#33,252.06		\$33377.69		14	0	1
R128	823377.80		83359334		12	0	. 1
8927	633502.51		822073.82		13	0	1
R024	832673.82		833768.11		13	0	1
Rt29	833766.63	822374.15	833848.76	821405.79	13	0	- 1
R930	\$33848.76	822405.79	£13917.£3	822431.11	18	0	4
H031	633917.63	822431.11	932990.58		14	0	1
H637+R301	833076.99	\$2204A.71	933121.79	822072.07	18	0	3
8833	833121.79	622072.07	£13252.36		18	0	1
R034	833253.39	822120.94	833398.77	822175.17	18	0	1
REST	#33396.77	#22176.17	833524.35	822221.21	18	0	
PI036	f33524.35	822221.21	832913.40	822269.00	18	0	- 1
R637	633653.40	822269.00	833694.86	822284.07	19	0	1
REDR	633694.68	822284.56	833763.79	622339.61	78	0	- 1
BRODE	833761.98	822311.12	823718.45	822229.76	14	0	3
R040	833789.11	822318.08	822833.16	R22335.11	18	0	4
R041	833833.10	822335.17	833902.94	822360.51	16	0	- 4
RM2	83390Z.96	822360.57	833955,46	822320.A5	-18	0	1
R043	813950.46	822320.6B	834014.90		18	0	
R044	834024.90	822250.62	934140.62	N22162.67	18	. 0	1
RMS	834140.62	822182.67	834211.76	822086.45	19	0	1
RSAS	834211.72	822086-65	834323.21	822011.22	18	0	- 1
ROAT.	834322.77	#22910.EE	834384.01		18	0	3.
FI048	833097.20		833,156,54		17	0	3
R549	833159.60		833434.10		16	0	1
R158	833101.47	821942 33	51327446		21	0	1
RUST	833274.56		211416.70	822067.62	16	0	1
R051	833434.10	822080.21	832618.33	822174.73	16	0	1
R053		\$22123.44			18.	0	1.
R953	833736.68	82216-1-25			16	0	1
R054	823428.63	822967.29	#32516.71		16	0	. 7
ROS4	#33584.71		933649.55		18	0	- 1
ROSA	633649.55	622144.40	813683.68		16	0	1
R254	633663.68		833713.65		- 16	0	- 1
ROS4	623712.85		833757.83		16	0	4
R054	635767.83	822128:65	\$33778.A9		16	0	1
R053	#33786.53	\$22123.04	833872,14	822651.30	19	0	1
R256	833778.49	622113.30	8118h7.20	822039.12	16	0	- 7
R057	#33673.20	822082.68	034159.21	821B1478	16	0	- 1
ROSE	634159.21	821614.78	834210:10	821738.42	16	0	- 9
R059	633867.29	822039.23	45485E34	821680 22	-97	0	- 1
8060	834068.34	821380.22	834241.E1	821727.AS	16	0	
R061	633116.37	821890.28	833139.76	821889.31	16	0	1
R082	633139.76	821889.01	833296.78	021947.78	16	0	- 1
RINS	833256.88	821947.56	813410.51	621007.91	36	0	- 1
RIGHT	833450.49	#2250E.03	#11543.73	822038.72	13	0	7.
H004	833543.73	832038.72	¥33542.70	821983.31	15	0	- 1
R064	633489.98	821962.82	813543.70	821982.31	15	0	- 1
ROSS	833166.17	823834.07	613315.56		16	0	1
R066	833316.56	321301.68	#33491.00	821952.71	16	0	- 1
ROST	833164.01	821778.07	833178A7	821783.88	10	0	- 1
	833178.74	621783.16	833253,69		18	0	- 1
PI068							
RIGHT	833164.60	621757.67	813210.16	821795.91	29	0	1

											NO ₂ x 10	0 (a/VMT)			_								
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
2.6027	2.6089	2,5734	2.5859	2.6148	2.5977	2.6327	4.3008	4.4813	3.7775	3.4742	3.3921	3.0371	3.1163	3.1131	3.4558	1.6620	3,4434	3.5093	2.9440	2.6662	2.4512	2.5367	2.6627
2.6027	2.6089	2.5734	2.5859 2.5859	2.6148 2.6148	2.5977	2.6327	4.3008	4,4813	3.7775	1.4742	3.3921	3.0371	3.1163	3.1131	3.4558	1.6620	3.4434	3.5093	2.9440	2.6662	2.4512	2,5367	2.6627
2.6027	2.6089	2.5734	2.5859	2.6148	2.5977	2.6327	4.300E	4.4813	3.7775	3.4742	3.3921	3.0371	3.1163	3.1131	3.4558	3.6620	3.4434	3.5093	2.9440	2.6662	2.4512	2.5367	2.6627
2.6027	2.6089	2.5734	2.5859	2.6148	2.5977	2.6327	4.3008	4.4813	3.7775	1.4742	3.3921	3.0371	3.1163	3.1131	3.4558	3.6620	3,4434	3.5093	2.9440	2.6662	2.4512	2.5367	.2.6627
2.5981 2.5981	2.5939	2.5801	2.6038 2.6038	2 5932 2 5932	2.5701 2.5701	2.6087	3,7990	4.1144	3.4203	3.2046	3.1907 3.1907	2.9307	3,0412	3.0759	3.4682	3.7458	3.8124	3.8436	3.1718	2.5509	2.3642	2,4780 2,4780	2.5365 2.5365
2.5981	2.5939	2.5801	2.6038	2.5932	2.5701	2.6087	3.7990	4.1144	3.4203	1.2046	3.1907	2.9307	3,0412	3.0759	3,4682	1.7458	3.8124	3.8436	3.1718	2.5509	2.3642	2,4780	2.5365
2.5858	2.5750	2,5845	2.6100	2.6040	2.5770	2.6142	3.7987	4.1153	3.4198	3.2042	3.1889	2.9281	3.0380	3.0730	3.4648	1.7425	3.8038	3.8395	3.1678	2.5456	2.3586	2,4722	2.5375
2.5858	2.5750	2.5845	2.6100	2.6040	2.5770	2.6142	3,7987	4.1153	3.4198	1.2042	3.1889	2.9281	3,0380	3.0730	3.4648	1.7425	3,8038	3.8395	3.1678	2.5456	2.3586	2,4722	2.5175
2.5858	2.5750	2.5845 2.5845	2.6100	2,6040	2.5770	2.6142	3,7987	4.1153	3.4198	3.2042	3.1889	2.9281	3,0380	3.0730	3.4648 3.4648	1.7425	3,8038	3.8395 3.8395	3.1678	2.5456 2.5456	2.3586	2,4722 2,4722	2.5375
3.0680	2.7529	3.9274	0.9658	0.9680	3.5316	2.9739	3.3561	2.5871	3.4916	3/1881	3.2446	3.5896	3.1281	2.3507	2.4417	1.3276	1.6277	0.9814	1.1041	1.2545	1.9162	1,7987	1.5479
3.0680	2.7529	3.9274	0.9658	0.9680	3.5316	2.9739	1.3561	2.5871	3.4916	1.1881	3.2446	3.5896	3,1281	2.3507	2.4417	1.3276	1.6277	0.9814	1.1041	1.2545	1.9162	1,7987	1.6479
3.0680	2.7529	3.9274	0.9658	0.9680	35116	2.9739	3.3561	2.5871	3.4916	3.1881	3.2446 3.2446	3.5896 3.5896	3.1281	2.3507	2.4417	1.327€	1.6277	0.9814	1.1041	1.2545	1.9162	1.7987	1.6479
1.9682	2.4451	2.2050	0.9658	0.9680	1.9772	1.9502	2.6277	1.9401	2.4103	2.1905	2.3222	2.1848	1.7578	1.6570	2.0435	1.3959	1.6287	1.0585	1.0171	1.2894	2.2440	2,1905	1.4127
1.9682	2.4451	2.2050	0.9658	0.9680	1.9772	1.9502	2.6277	1.9401	2.4103	2.1905	2.3222	2.1848	1.7578	1.6570	2.0435	1.3959	1.6287	1.0585	1.0171	1.2894	2.2440	2.1905	1.4127
4.2429	4.2174	3.6982	2.5373	4.5466	5.3953	4.2472	5,1000	43826	5.0009	4.6822	5.1533 5.1533	4.9276	4.8193	4.2213	4.9362	4.3585	4.1606	3.9695	3.6968	A.5458	5.2969 5.2969	4.8235	4.7632
4.2429	4.2174	3.6982	2.5373	4.5466	5.3953	4:2472	5.1000	43826	5.0009	4.6822	5.1533	4.9276	4.8193	4.2213	4.9362	4.3589	4.1606	1.9695	3.6968	4.5458	5.2969	4,8235	4.7632
11.1591	12.9149	1.2117	1.6557	1.6579	1.6283	11.1871	15.2106	9.5363	12.6931	10,6819	12.8648	12.0725	15,6037	11.5046	11.9538	11.5388	12.9543	14.8600	12.5893	19.9663	23.1409	18 0981	13,6457
	12:9149	1.2117	1.6557	1.6579	1.6783	11.1871	15.2106	9.5163	17.6931	10.6819	12.8648	12.0725	15.6037	11.5046	11.9538	11.5388	12.9543	14.8600	12.5893	19.9663	23.1409	18.0981	13.8457
11.1591	12.9149	1.2117	1.6557	1.6579	1.6283	11.1871	15.2106	9.5363	12.6931	10.6819	12.8648	12.0725	15.6037	11.5046 11.5046	11.9538	11.5388	12.9543 12.9543	14.8600	12.5893 12.5893	19.9663	23,1409	18.0981	13.8457
11.1591	12.9149	1.2117	1.6557	1,6579	1.6283	11.1871	15.2106	9.5363	12.6931	10.6819	12,8648	12.0725	15,6037	11.5046	11.9538	11.5388	12.9543	14.8600	12.5893	19.9663	23.1409	18.0981	13.6457
5.2151 c 2688	5.3245	5.7743	7.1936	6.7790	6.6182	5.5273	8.8976 8.3643	4.7559	6.0286	6.1358 5.5751	7.0168	6.6613 5.7737	7.4475	6.0198 5.1755	6.8623	6.5314	6.8682 5.2374	6.6814	6.2187	8.4476	7.6948	9,6745	6.9304
5.2658 5.2658	5.4667	5.7743	4.6764	4.4318	6.6182 6.6182	5.1328	8.3643	4.4920	5.7443	5.5751	6.1045	5.7737	6.0681	5.1755	5.7187	4.7203	5.2374	4.8787	4.2741	6.3945	7.6948	6,2941	5.3511
13.1769	13.4304	12,2284	14.0753	14.7501	12.3285	12.5179	15,0515	12.1428	13.8749	12.4111	14.0254	12.9830	14.9012	11.6930	13,4885	14.2660	12.2983	11.9876	11.5222	15.6533	19.3037	13.9692	14.7120
33.1436	12.9434	11.7679	13.7873	12-2953	14.4121	12.9748	15.2846	12.3923	14.0521	12.4495	14.0640	12.9257	14.7350	11.8226	13.5598	13.2503	12.3456	12.3743	11.4266	15.5502	18.0471	14.7878	13.6304
16.1990	14.7436	15.9884 15.9884	16.8868	16.0894	15.9088 15.9088	16.2069	17.6154	15.0559	16.8345	15.5212	16.8402 16.8402	15.8462	17.3231	14.4255	15.7514	16.4465	14.6308	14.3518	13.6179	16.9986	19.4797	16.4187	15.6846 15.6846
14.8192	13.1016	14.9755	14.8814	15.1365	13.6828	14.3940	17.3521	14.9175	16.3819	14.9776	16.1701	15.2876	17.0715	13,8688	15.2122	15.3468	14.3888	14.4389	13,2444	16.6262	19.1543	15.5803	14.5574
15.3208	13.6304	14.4525	12.8095	15.1365	14.4468	14.8228	16.9425	14.6451	16.499K	15.0555	16.1954	14.7279	16.8992	13.8065	15.1681	15.5621	14.4251	14.0911	12.8944	16.6867	18.7679	15.6923	14.5279
16.3334	15.1455	14.0865 16.5182	15.758E 17.2044	16.2962	14.1526	16.3944	19.2705	18.2477	18.8661	15.0544	16.2910	16.0202	16.6502 18.0656	13.9110	15.3303 16.1102	15.1286	14.5480	14.2352	13.5581	17.1317	19.1454	15.3460	14.4223
	15.4654	15.2996	15.6157	16.1356	16.5008	15.8148	18,0008	16.7208	18.3272	17.0358	18.0587	17.0037	18.3484	16.0201	16.7033	16,9476	15.7425	15.2535	14.1157	17.0735	19.8500	16.1163	15.2214
	11.9139	12.9355	15.3172	14.1044	12.2557	12.9867	14.5904	12.5174	14.3687	12.9068	14.2611	13.3017	14.9269	12.4141	13.9332	13.9142	13:0753	13.1656	11.8304	15.5006	18.3991	15.0139	13.1403
11.3243	10.5804	12.7328	7,1936	9.9797	11.6856	11.2224	15.3872	13.9104	14.5961	12.4535 11.6888	13.5496	12.2542	15.4711	11.5333	13,7384	15.5229	13.3941	12.6965	12.3596	16.4212	17.7093	13.4429	15.0526
10.5707	12.7577	8.2653	9.9625	9,9797	7.1726	11.4819	16,5463	14.9783	15.260B	13.2556	14.3359	12.4897	15.5582	11.8093	13.4311	14.7251	12.8585	12.4467	11,9111	15.8396	17.6081	14.2969	13-8125
	14.1377	10.9713	10.9582	10.5274	10.5295	10.9890	14.0055	11.6071	13.0831	11.8711	13.3669	12.4321	14,1107	11.5008	12.8706	12.9486	12.3532	12.7251	11.2430	14.6430	16.5520	13:5562	12.7015
11.6903	10.6659	11.7409 10.5369	11.8547	11.9616	10.7141	11.7634	13.9805	11.3755	12.9586	11.6231	12.9580 12.5697	12.0390	13.6426 13.2415	10.9284	12.7214 12.4338	12.7648	12.1364	11.7473	11.0110	13.7662	16.4823 16.0386	13.4972	12.2834
13.1899	13.0781	12.9714	12.7555	12.8503	12.7536	12,9366	15.8142	13.7388	15,0118	13.6727	14.8058	14.0510	15,5244	12.7281	14.6872	14.5562	13.0789	12.8082	12.1083	15,0752	17.7066	14.5406	13.6948
12.1653	12.0201	12.0137	12.1835	12.0328	12.1926	12.0976	14.5949	12.5749	14.2301	12.5924	14.0114	13.0120	14.7111	12.0398	13.4764	11.4957	12.8772	12.7787	11.7535	14.8243	16.8106	13.8692	13.0948
16.2426	16.1551	16.1382	16.3100	16.1673	16.1180	16.2509	19.3437	16.6355	18.6207	15.9363	17.4619 17.3156	15.7712	17.73H3 17.1700	13.9589	15.2811	15.0590	13.8356	13.4321	12.3772	15.7123	18.1377	13.2377	13.8692
19.3999	18.1488	18.3132	18.7953	18.7651	18.5828	18.4568	22.6486	22.0005	21.8804	19.2427	20.5879	18.4731	20,5063	15.9232	18.2462	18.2641	15.1470	13.5324	13.4495	16.2285	18.0991	14.3669	15.4148
18:9925	19.1611	19.0845	19.4619	19.2041	19.3166	19.2424	22.4627	21.2014	21.6183	18 9200	19.8495	17.8671	19.8086	15.2454	17.6434	17.7111	15.0827	13.4109	12.9781	15.8454	17.5152	14.07E3	15.1606
19.3867	18.4239	18.7837 18.7851	18.9295	18.6974	18.9894	18.7305 18.9092	23.1501	21.9245	22.3711	19.1847	20.5279	18.4681	20.4532 19.9842	15.8927 15.3893	18.1955	18.1980	15.1622 14.9568	13.5631	13.1573	16.2468 15.9928	18.2254 17.5460	14,4230	15.4385
21.8160	21.9889	22.0050	21.9694	22.2212	22.0907	22.0167	24.8368	23.9173	24.0050	21.2242	22.7738	20.5503	23.0434	17.8668	20.7172	21.0164	17.6404	15.8015	15.4758	18.5358	20.5846	16.5101	18.1335
19.0632	19.0134	19.0659	19.4281	19.1714	19.1623	19-2165	22.4128	21.1961	21.5851	18.4519	19.8566	17.8051	19.7789	15.2551	17.5669	18-0051	14.9071	13.1908	12.7533	15.7465	17.3551	13.9249	14.9559
19.3762	16.0064	18.5984	17.0431	17:3451	17.0405	19.2706	22.0279	20.7928	21.1999	18.7042	20.0493	18.0548	20.0847	15.6901 15.6919	17.8977	18.0154 18.2559	15.0257 15.1954	13.4177	13.3389	16.0139	17.8339 17.6592	14.5393	15.4942
19.5756	18.4239	18.6851	18.8314	18.9366	18.7821	19.5744	22.7519	21.1238	21.5014	18.9649	20.2967	18.2362	20.1620	15.7415	17.9381	17.9185	15.2505	13.5561	13.1761	16.2438	17.7030	14.3928	15.4529
14.2130	13.7899	13.7643	13.8061	13.8389	13.8347	14.2149	17.1245	16.7141	16.9791	14.5318	15.7810	14,3293	16.5810	12.9507	14.9715	15.3087	13.6081	13.0467	11.9358	15.1266	17.1880	13.8034	13.7324
15.1756	15.1950	14.2133	15.1674	14.2509	14.1752	14.2592	16.8847	16.1074	16.3717	14.0521	15.5408	14.1298	16.0846	13.3125	14.5597	15.1127	13.2723	12.5689	11.7262	15.1835	17.2251	13.8642	13.8575
16.3332	16.3800	16.4014	16,4029	16.4033	16.3995	16.4032	19.2279	18.1742	18.7826	16,0515	17.5428	15.8334	18.1273	14.0949	16.3358	17.0300	14.6192	13.3215	12.5206	15.4058	17.1117	13.6614	14.5972
16.8576	16.1543	16.0996	16.2857	16.2839	16.2392	16,7403	18.9919	18.7664	17.9513	15.7491	17.1055	15.5125	17.3579	13.8146	16.2298	16.4934	14.0866	13.0737	12.4451	15-8011	17.7636	14.2818	14.5802
17.4681	16.8729	16.8838	16.9428	16.9977	16.9696	17.4050	19.9058	19.5137	19.2829	16.5239	18.0226	16.2436	18.7113	14.6931	17.0369	17.4639	15.2097	14.2405	13.4420	16.7276	18.7077	14.9881	15.4998 15.4998
	17.9213	17.8346	17.9743	18.0339	17.9136	17.9533	20,4031	19.5931	19.8746	17.4948	19.0142	17.6054	20.2399	16.0918	1H.5789	20.0611	17.2454	16.1009	15.4068	18.9879	20.9651	16.6785	17.8317
17.9222	17.9213	17.8346	17.9743	18.0339	17.9136	17.9533	20.4031	19.5931	19.8746	17.4948	19.0142	17.6054	20.2399	16.0918	18.8789	20.0611	17.2454	16.1009	15.4068	18.9879	20.9651	16.6785	17.8317
17.9222	17.9213	17.8346 17.8346	17.9743	18.0339	17.9136	17.9533	20.4031	19.5931	19.8746	17.4948	19.0142	17.6054	20.2399	16.0918	18.8789	20.0611	17.2454	16.1009	15.4068	18.9879	20.9651	16.6785	17.8317
	17.9213	17.8346	17.9743	18 0339	17.9136	17.9533	20,4031	19.5931	19.8746	17.4948	19.0142	17.6054	20.2399	16.0918	18.8789	20.0611	17.2454	16.1009	15.4068	18.9879	20.9651	16.6785	17.8317
17:9222	17.9213	17.8346	17.9743	18.0339	17.9136	17.9533	20.4031	19.5931	19.8746	17.4948	19.0142	17.6054	20.2399	16.0918	18.8789	20.0511	17.2454	16.1009	15.4068	18.9879	20.9651	16.6785	17.8317
16.5471 20.3916	16.5541	16.5292 20.3605	16.5337 20.4076	16.6070 20.4573	16.6010 20.4886	16.5754 20.4295	18.9149	17.7738	18.1032 21.4279	15.75@	16.9836 20.9736	15.1879 19.0674	17.3237 22.1194	13.4797	15.5742 20.7292	15.7500	13.7196 17.8956	12.9182	12.1232 16.2353	15.4757 20.0887	17.4492 21.7323	14.0526	14.2113
	12.4755	12.5656	12.8212	12.7669	12.7677	13.3824	15.3606	16.0491	14.1826	12.7009	13.5058	12.3688	13.5630	10.8716	13.5559	14.1071	11.5773	9.3056	9.7464	11.4579	12.1967	9.7546	12.0504
18.6981	17.7720	17.7249	17.9945	17.9857	18.0831	18.7359	21.2694	20.7273	20.0061	17.3345	18.6987	16.7203	19.0823	14.6477	17.0101	17.3670	14.4412	13.2394	12.9793	16.4580	18.3260	14.6568	15.3997
19.2561	15.7894	15.6941	19.5962	15.9154	15.7179 19.6166	15.7556	17.8897	18,7994 21,4438	16.3930 20.4536	14.9544	15.8395 20.2628	18.4942	15.9598 21.5808	12.7208 16.5816	15.9348 20.3641	16.7205 21.6379	13,1746	10.5576	11,2230	13.1620	13.7488	10.9349	13.8778
22.5421	21.5760	21.7000	21.6177	20.0507	22.0165	22.1962	22.3146	21.7256	22.6146	22.0951	22.6305	22.3119	22.7212	21.9134	22.4542	22.4681	21.7531	21,8784	21.6137	22.5353	23.2595	22.6888	21.7104
	12.1227	12.2622	12.17(3	12.9634	12.9180	12.3509	14.7264	12.9703	14.0575	12.9463	14.4323	13.6060	15.1447	12.2481	13.9824	14.2451	13.0642	12.6698	11.5510	14.8614	17.4024	13.9378	13.6716
13.0631	10.1467	13,1894	13.2061	13.2823	11.7252	12.5584	15,5471	12.6756	14.1165	12.7576	14.1329	13.0846	14,9951	12.1090 11.4606	13.5118	13.3611	12.6076 12.0068	12.6583 11.9815	11.5775	15.2026 15.0732	17.7482	14,6494	13.8359
12.3170	10.1467	11.8944	12.7736	11.7241	11.2025	11.8147	15.0227	12.0508	13.5479	12.0377	13.8578	12.6461	14.5021	11.4606	13.1954	13.3611	12.0068	11.9815	11.3605	15.0712	17.6793	14.4922	13.9570
12.3170	10.1467	11.8944	12.7736	11.7241	11.2025	11.3147	15.0227	12.0508	13.5479	12.0377	13.8578	12.6461	14.5021	11.4605	13.1954	13.3611	12.0068	11.9815	11.3605	15.0732	17,6793	14.4922	13.9570
13.3977	13.2114	13.5897 12.8960	13.7371	13.3184	12.6822	14.3170	15.7892 15.8055	13.5148	15.1462 14.6626	13.8167	15.3474	14.3594	15.6206 14.9997	12.8480	14.0390	14.4751	13.0697	12.2865	11.5419	14.7424	17.3238 17.4054	14.3215 13.9963	13.6179 13.1922
9.5846	9.5740	9.5429	9.5499	9.5555	9.5700	9.5956	12.9709	10.2801	12.4458	10.8004	12.1911	10.9616	12.8157	9.9371	10.6937	10.5106	10.0933	10.5191	9.4407	11.4175	13.0899	10.5814	9.0305
9.500R	9.5064	9.4886	9.5197	9.5166	9.5268	9.5362	12.4771	10.2157	12.3946	10.7318	12.0021	10.9116	12.7733	9.8881	10.6485	10.4797	10.0659	10.4959	9.0003	11.2021	13.0755	10.5690	9.0106
7.1064 12.4001	7.1311	7.0866	7.0938	7,1223	7.1020	7.1288	8.6644	6.9182	8.5087 14.2134	7.1868	8.1622	7.5666	8,9148	7.2613	7.8570 11.9908	7.7701	8.5965 11.5855	9.4394	7.3777	10.0294	12.1828	9,8821 13:2468	7.8503
124001	12.3366	12.3494	15.1906	12.3/35	14.3511	15.3919	14,5/91	11.9476	24.2134	IL 1967	15.3529	12.3246	14:0790	11.2800	11.9908	11.9450	11.3835	11.2636	10,4954	1 13.6720	10/0055	13-6408	11:6213

Calli	C 7 III	Put ic		ے برد	Width		200
Road	W.	Coordin		140	(including	Height (m)	Road Type (caline 4)
P.DII	X1 #353E7.93	Y1	X2 533397.24	Y2	mixing rose)	0.	(camin a)
RU72	8333E7.91 833597.24	\$21809.29 \$21876.22		821675.22	20	0	- 1
R073	8334E1.50		833397.24	821875.22	17	0	1
RIG74		821790.34			20	0	- 1
91074 91875		621961.09		821683.08	16	0	1
Proper Mr.							1
1007 8	\$33501,48	921897.80	81351846	821699.77	16	0	
R076	633548.66			821866.90	16	0	4.
R074	832603,43	821688-99	93398492	821822.32	14	0	1
R622	833564.57	821884.14	833563.57	821884.38	32	0	1
R077	\$33563.57	821084.3%	833600.48	821871.38	17	0	4
PIOTZ	£33000.48	821971.28	933973.84	821812.00	17	0	
ROTE	833062,38	621822.35	833875.32	821660.76	16	0	7
B379	833673.29	623831.43	633867.51	821651.AB	16	0	
R060	833675,67	221661.12	833999.54	821557.91	16	0	1
R091	833867.01	821650.85	933913.09	821852.08	26	0	4
R082	833458.18	821864.41	813510.76	021821.12	14	. 0	- 1
Rita2	823510.75		833518.39	821785.93	14	0	- 1
ROSZ	833526.39	821785.93	E11570.11	821667.58	18	0	- 1
R043	833424.83	821885.11	833496.18	821813.12	14	0	1
R083	833494.18	621813.12	833574.36	821772.28	14	0	1
	. 4496,745,9114				14	0	
	¥33524.38	821772.29	813559.61	821652.62			
R094	\$33567.54			821644.65	13	0	1
R094	833,682.69	821644.RS	832607.71	821003.8F	13	0	1
Ross	833009.34	821605.64	833640.24	021575.51	14	0	1
RISKS	E33640.24	82) 57 5-52	813691.67	821645.20	14	0	1
R065	\$336E1.67		821720.62	821512.85	19	0	1
HOSE.	633500,70	821649.89	#339603.88	021103.08	17	0	1
Rote.	833603.88	621533.58	411646.83	021545.45	12		1
Rear	633646.49	82154E-43		821508.30	13	0	1
ROSS	833254.24	821811.68		821856.64	17	4	4
0.004	#333254.24 #33384.50			821865.51	12	•	-
Rose		821806.64 821885.51			17	9	1
ROSS	8334E7.63	821BA1.09	#33.533.63	821788.07	17	10	4
Ross		621786.07			1T		
HOER.		821657.75		821605.82	17	d	
RISER	#33690.16		633712.66	621511.11	37	6	
R099		821801.44		821845.87	16		
R089	633370.06	821846.87	833427.36	821652.03	16	3	4
RORS	833427,36		833410.60	821829.25	16	0	4
Atas	833480.60	821929.25	83352246	821786.30	76	10	
Rides	833522,46	821784.32	E13545.10	821725.AT	16		
HOEK	833543.19		831512.07	821652.37	16	1	
RORY		621653.37	W3350E.99	821584.44	16	0	4
6089	63229-2-07	94199.4-31	61369351	821508.87			
	823596.99				16	. 6	
050+R091	833259.78	821629.64	833337.54	621634.13	97	0	1
R992+R993	#33327.92	#21632.93	£13449.56	821640.31	29	0	- 1
1092×11093	822449.50	921640.31	#32512.09	021599.24	20	0	
R094	833337.84	821634.13	833341.61	821576.41	16	0	- 1
R095	833609.59	621501.72	833548.49	821548.A3	97	0	4
095+R097	#33980.58	822A54.38	E3402E77	822414.27	18	0	1
00 8 + R 000	#3402#.77	822414.27	934127.62	#22332.11	18	0	- 1
100-R101	834127.62	822332.11	83421831	822256.38	18	0	- 4
192+R103		822258.35	834309.95	822190.58	-18	0	- 1
104+R105	814300.95	822180.SE	834407.46	822098.55	12	0	- 1
R106	B33917.B3	822431.11	833991.74	622300.30	18		-
8157	833991.68	822270.04	834890.33	822287.53	10	0	1
						0	- 1
R108		622288.06	834181.98	822212.22	36	_	
R169	#341E1.9E	#22212.22	834275.08	\$22138.AB	17	0	- 1
R110			#3436436		17	0	3
R111	834363.46		834410,74		18	0	1
R112	833846.76	822 AD 5.79	£11992.95	822380-5T	19	0	1
R113	833832.16	822334.17	233909:65	822271.35	18	0	1
R114	833309.65	822271.05	833994A7	022301.23	18	0	1
R115		822200.75	834977.01	822132.08	18	0	1
Rtis	83A076.99	822131.94	834097.50	822115.02	18	0	- 1
RHIT	634007.30	822115.02	E34110.89	822007.73	18	0	
Ritt			834243.28	021003.08	19	0	- 1
RITE		621993.65	#34292.16	821961.A5	19	0	1
R120	838281.93		#34359.17	221295 PA	18	0	1
R121		822376.15			18	0	1
R121	833764.98	822376.46	833769.11	822218.98	18	0	1
R123	\$33848.7E	\$22222.16	£13954.75	822150.50	18	0	1
R124	833671.92	622341.72	STIENASE	822284.02	16	0	7
R125	833494.86	822254.07	822827.77	822172.05	18	0	1
R126	E33053.40	822269.00	832988.33	822174.73	12	0	- 1
R127	633469.65	822315.75	633502.51	822278.AB	-98	0	- 1
R128	12.£000.51	82227 E-66	E33574.36	822221.21	18	0	. 1
#329	833377.80	822222.03	833355.00	822293.72	18	0	1
R120	833377.80	822232.63	833318.77	822175.17	- 18	0	- 1
R131	833394.42	522175.04	813434.10	8210KD.78	91	0	1
R132	#33431.92	822080.70	#13410.51	822007.97	16	0	- 1
	#33450.45		#33461.00	821952.74	16	0	1
R(53	833481.00 833209.07	821962.76	813506.97	821887.08	16	0	- 1
R 124		822239.78	811212.04 811213.39	822178,01	78	0	1
R134 R135				822120.94	18	0	. 1
R134 R135 R136	633232.03						
R134 R135 R136 R137	833232.03 833080.91	822162.63	833100.63	822129.44	18.	0	- 1
R134 R135 R136 R137 R138	833232.03 833080.81 833106.63	822182.63 822129.64	833100A3 833121.79	822129.44 822672.07	- 11	0	- 1
R134 R135 R136 R137 R138 R139	833232.03 833080.91 833100.63 633121.68	822162.63	#33100.83 #33121.79 #33138.56	822129.44 822672.07 621877.95			

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11.00	11.01	111.00	Hr03	1 11-01	1 11.00	1 11.00	1 11.02	Hr08	Hr09		NO ₂ x 10	Hr12	(1.42	Hr14	Hr15		11.49	Hr18	Hr19	111.00	T 17-04	11.00	11.00
Hr00	Hr01	Hr02	12.1959	Hr04	Hr05	Hr06	Hr07	11.3800	13.5552	Hr10	12.9657	11.7674	Hr13	10.8816	11.6497	Hr16	Hr17	11.4357	10.1258	Hr20	Hr21	Hr22	Hr23
10.5826	10.5384	10.4960	10.6031	10.7619	10.4538	10.4684	12.3256	10.2045	11.2403	9.8516	10.9138	9.8927	11.1392	8.7436	9.9097	9.8284	9.0124	8.5951	8.0310	10.7447	12.5229	10.1942	9.5040
10.9670	10.8290	10.9648	11.0253	11.0398	10.8453	10.9312	12.5428	9.8142	11.8017	10.5505	11.6626	10.8099	12:0414	10.0566	10.6740	10.4589	10.2399	10.5245	9,7079	12.3436	14.2410	12.0899	11.0046
11.1731	11.0R83	11.2383	11.0470	11.1667	11.1244	11.1678	12.7310	10.1769	11.8736	10.6696	11.6877	10.6949	11.9310	9.6921	10.2831	9.9683	9.7538	9.9264	8.9535	12:0545	14.2305	11.8584	10.2518
10.0655	10.0951	9.9726	10.1254	10.0516	10.2001	10.1366	13.2455	9.2031	10.7427	9.6013	10.6128	9.7030	10.8018	9.7537	9.4012	9.0836	8.8483 10.0468	9.0238	9.2857	12.8437	13.101ff 15.1503	10.8907	9.2713
11.2394	11.4995	11.2708	11.4880	11.4573	11.2751	11.3537	13.2455	11.1003	12.0642	10.6965	11.8663	10.7656	12.4504	9.7537	10.8622	10.7659	10.0468	10,2274	9.2857	12.8437	15.1503	12.3357	10.7606
11.2394	11.4995	11.2708	11.4890	11.4573	11.2751	11.3537	13.2455	11.1003	12.0642	10.6665	11.8663	10.7656	12.4504	9.7517	10.8622	10.7659	10.0468	10.2274	9.2857	12.8437	15.1503	12:3357	10.7606
10.2999	10.3714	10.3397	10.3531	10.4377	10.3720	10.3724	12.0014	9.5824	11.2005	9.9131	11.0318	10.0879	11.4987	9.2700	9.9821	9.7500	9.6750	9.9896	8.9596	12.2729	14.6036	12.0248	10.2476
10.2999	10.3714	10.3397	10.3531	10.4377	10.3220	10.3724	12.0014	9.5824	11.2005	9.9131	11.0318	10.0879	11.4987	9.2700	9.9821	9.7500	9.6750	9.9896	8.9596	12.2729	14.6036	12.0248	10.2476
10.2999	10.3714	10.3397	10.3531	10.4377	10.3220	10,3724	12 0014	9.5824	11.2005	9.9131	11.0318	10.0879	11.4987	9.2700	9.9821	9.7500	9.6750	9.9896	8.9596	12.2729	14.6036	12.0248	10.2476
12.8502 9.3978	12.6809 9.5801	12.7216 9.4452	9.5221	9.5114	12.9130	12.8665 9.5035	14.8060	12.8629 8.2828	13.6717	9,1760	13.3357	9.5485	13.6719	10.8745 8.9248	11.9321 9.4292	9.1551	10.8927	10.9863	10.1284 8.9266	13.3700	15.6292	12.8988	10.6659
12.0142	12.0972	12.0810	12.1608	12.1334	11.8711	12.0365	13.9307	10,7010	12.8653	11.2483	12.6523	11.3882	13.2170	10.2577	11.1143	10.8544	10.2977	10.7220	9.5757	13.3026	15.8694	12.8877	11.1274
10.0917	10:2417	10.1487	10.1739	10.1655	10.0641	10.2226	11.5740	9.0611	10.8234	9.9459	11.0191	10.2184	11.4722	9.5932	10.0678	9.7544	9.8440	10.6366	9.4854	12.7586	15.1155	12.7695	10.6263
14.6402	14.8319	14.5758	14.6210	14.6828	14.4969	14.6822	17.0060	13.3927	16.7853	14.7130	16.3320	15.0534	17.0625	14.0659	14.6720	14.3772	13.9929	14.6131	13.4448	16.9785	19.6048	16.5357	14.5109
14.6482	14.8319	14.5758	14.6210	14.6828	14.4969	14.5822	17.0060	13.3927	16.7853	14.7130	16:3320	15.0534	17.0625	14.0659	14.6720	14.3771	13.9929	14.6131	13.4448	16.9785	19.6048	16.5357	14.5109
14.6402 5.2709	64947	14.5758 6.5338	14.6210 6.6264	14,6828 6,7338	14.4969 6.5138	6.4130	6.9369	6.3707	16.7853	14.7130 6.7278	7.1518	6.9352	17.0625 7.1008	14.0659 6.4941	6.7158	14.3772 6.3265	13.9929 6.2159	6.1633	5.9929	7.0816	19.6048 8.3172	16.5357 7.5062	6.5304
6.2709	6.4947	6.5338	6.6264	6.7338	6.5138	6.4130	6.9369	53707	7.2876	6.7278	7.1518	6.9352	7.1008	6.4941	6.7158	6.3265	6.2159	6.3633	5.9929	7.0816	3.3172	7.5062	6.5304
6.2709	5.4947	6.5338	6.5264	6.7338	6.5338	6.4130	6.9369	6.3707	7.2876	6.7278	7.1518	6.9352	7.1008	6.4941	6.7158	6.3265	6.2159	6.3633	5.9929	7.0816	8.3172	7.5062	6.5304
14.7211	14.5955	14.5463	14,6826	14.6564	14.5356	14,6460	16.9664	13.0505	16.4025	14.7047	16.4603	15.2211	17,4716	14.4355	14.7431	14,4389	14.8152	15.9303	14.3624	18.4391	21.4601	18.2796	15.1900
14.7711	14.5955	14.5463	14.6826	14.6564	14.5356	14.5460	16.9664	13.0505	16.4025	14.7047	16.4603	15.2211	17.4716	14.4355	14.7431	14.4389	14.8152	15.9303	14.3624	18.4391	21.4601	18.2796	15.1900
15.5611	15.6875	15.6197 15.6197	15.6767	15.6548 15.6548	15.6578 15.6578	15.7726 15.7726	17.7505	14.4118	17.3525	15.8249	17.4253 17.4253	16.2352	18.1579 18.1579	15.3746 15.3746	15.5894 15.5894	15.2316 15.2316	15.2171	16.4855	14.7094	18.7665	21.7003	18:2714	15.7945
15.5611	15.6875	15.6197	15.6767	15.6548	15.6578	15.7726	17.7505	14.4118	17 3525	15.8249	17.A253	16.2362	18.1579	15.3746	15.5894	15.2316	15.2171	16.4855	14.7094	18.7665	21.7003	18 2714	15.7945
14.9848	14.8913	15.0849	14.7389	14.9522	14.9506	14.9648	16.7223	12.9485	16.2786	14.3316	15.8603	14.5572	16.4169	13.6118	13.806#	13.2823	13.2657	14.2293	12.8166	16.5459	19.3915	16.7196	13.5015
14.9848	14.8913	15.0349	14.7389	14.9522	14.9506	14.964H	16,7223	12.9485	16.2786	14.3316	15.8603	14.5572	16.4169	13.6118	13.8068	13.2823	13.2657	14.2293	12.8166	16.5459	19.3915	16.7196	13.9015
21.2453	21.2279	21.2337	21.0882	21.0861	21.0250	21.1326	21.7721	20.8808	22.0868	21.6765	22.1740	21.7378	22.2692	21.4364	21.4749	21.2404	21.0639	21.4444	20.6927	21.8494	22.6575	21.7804	21.0856
2.3536	2.3421	2.3359	2.3483	2.3263	2.3406	2.3687	3.8283	4.0346	3.9726	1.6886	3.1486 3.1486	2.9047	2,5412	2.6321	2.4637	2.2704	2.2197	1.9471	1.5720	1.6906	1.6629	1.7455	1.5482
2.3536	2.3421	2.3359	2.3483	2.3263	2.3406	2.3687	3.8283	4.0346	3.9726	1.6886	3.1486	2.9047	2.5412	2.6321	2.4637	2.2704	2.2197	1.9471	1.5720	1.6906	1.6629	1.7455	1.5482
2.3536	2.3421	2.3359	2.3483	2.3263	2.3406	2.3687	3.8283	4.0346	3.9726	3.6886	3.1486	2.9047	2.5412	2.6321	2.4637	2.2704	2.7197	1.9471	1.5720	1.6906	1.6629	1,7455	1.5482
2.3536	2.3421	2.3359	2.3483	2.3263	2.3406	2.3687	3.8283	4.0346	3.9726	1.6886	3.1486	2.9047	2.5412	2.6321	2.4637	2.2704	2.2197	1.9471	1.5720	1.6906	1.6629	1.7455	1.5482
2.3536	2.3421	2.3359	2.3483	2.3261	2.3406	2.3687	3.8283	4.0346	3.9726	1.6886	3.1486	2.9047	2.5412	2.6321	2.4637	2.2704	2.2197	1.9471	1.5720	1.6906	1.6629	1,7455	1.5482
2.3536	2.3421	2.3359	2.3483	2.3261	2.3406	2.3687	3.8283	4.0346	3.9726	1.6886	3.1486	2.9047	2.5412	2.6321	2.4637	2.2704	2.2197	1.9471	1.5720	1.6906	1.6629	1.7455	1.5482
2.3086	2.2978	2.3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2.4605	2.3854	2.1364	2:2413	2.0956	1.9858	2.1068	1.9314	1.4677	1.6271	1.6283	1.6637	1.5109
2.3086	2.2978	2.3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2.4605	2.3864	2.1364	2.2413	2.0956	1.9858	2.1068	1.9314	1.4677	1.6271	1.6283	1.6637	1.5109
2.3086	2.2978	2,3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2,4605	2.3864	2.1364	2.2413	2.0956	1.9858	2.1068	1.9314	1.4677	1.6271	1.6283	1.6637	1.5109
2.3086	2.2978	2.3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2.4605	2.3854	2.1364	2.2413	2.0956	1.9858	2.1088	1.9314	1.4677	1.6271	1.6283	1.6637	1.5109
2.3086	2:2978	2.3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2.4605	2.3864	2.1364	2.2413	2.0956	1.9858	2.1088	1.9314	1.4677	1.5271	1.6283	1.6637	1.5109
2.3086 2.3086	2.2978 2.2978	2.3054	2.3147	2.3357	2.3087	2.3264	2.9233	3.0026	2.8796	2.7815	2.4605 2.4605	2.3864	2.1364 2.1364	2.2413	2.0956	1.9858	2.1088	1.9314	1.4677	1.6271	1.6283	1.6637	1.5109
9.1426	9,2361	9.0477	9.1390	9.2835	9.0640	9.1309	11.6107	9.2095	10.9803	9.4809	10.7446	10.0358	11,1738	9.1542	10.6321	10.4461	10.3257	9.9053	9.0267	11.6452	14.0238	10.9605	9.9514
8.8942	8.7286	9.4229	9.6050	9,4732	8.4388	8.9973	11.2822	8.9206	10.5436	9,5499	10.6714	9.9740	11.2710	9.0182	10.4865	10.4629	10.1241	9.6955	8.8630	11.5904	13.7230	11.0146	10.3518
8.8942	8.7286	9.4229	9.6050	9.4732	8.4388	8.9973	11.2822	8.9206	10.5436	9.5499	10.6714	9.9740	11.2710	9.0182	10.4865	10.4629	10.1241	9.6955	8.8630	11.5904	13.7230	11.0146	10.3518
5.5708	5.5610	5.5253	5.6649	5.6842	5.6551	5.4958	6.4988	4.5975	6.1359	5.1449	5.4453	4,8078	4.7924	3.7463	3.7883	1.2426	3.1408	2.6657	2.3787	3.2215	4.1059	1.6234	2.9717
23.2870	23,0371	23.1194	21.2336	13.2293	23.1680	23.3639	24.3953	23.7418	24,4877	24,1288	24.7124	24.3186	24,7079	23.7965	24,0459	23.8757	23,3717	23.7214	22.6838	24.0686	25.1245	24,1110	23.3486
12.3168	70.4801	10.6809 20.8023	6.4025	6.4132 70.5302	13.7739	11.7346	15.8480 21.5497	23.3350	16.2668 24.6935	21.5468	15.3370	19.9007	16.2048 21.9125	13.0916	14.6960	14.1561	13.2248	14.9811	11.1954	14.4235	17.4395	14.3759	15,6704
16.3997	16.4308	18.8803	16.7508	17.9396	15.0810	18.6901	19.8785	18.9268	21.5842	18.7840	19.1795	18.5274	19.3047	16.0592	18.3390	16.8112	15.3506	14.3151	13.3710	16.4457	19.3543	15,4895	15.7561
16.1508	18.1392	15,3613	16.4274	16.4624	17,2103	16.2888	20.8533	18.1240	19.9099	16.7431	18.5055	15.8974	17.7099	13.5231	15.8547	15.0950	12,7412	11.6533	11,2159	15.4438	18.0350	13.9707	14.1399
14.3211	16.6922	14.3043	14.0753	14:1044	16.0254	13.9483	18.9951	16.9954	17.9710	15.9407	17.6416	15.2423	16,7053	13.1373	15.0623	14.1975	13,0641	11.9886	11,5112	15.2910	17.5628	14,4069	14.3439
10.9398	10.3344	11.4609	11.7873	12.2953	10.3918	10.7897	13.2842	10.8687	12.8243	10.8076	12.9879	12.0859	14.0894	10.6047	13.1502	13.1217	12.5246	12.0690	11.2260	13.8828	17.2567	13.5333	13.7510
11.5919	10.5049	11.6395	13.2440	12.6133	11.8394	11.5469	13.1056	10.5212	12.2195	11.2779	12.5092	11.8115	13.5021	10.9467	12.2929	13.2696	12.1831	11.3832	10.5416	14.4975	17.0551	13.5007	12.8118
11.2550	10.1076	11.3097	12.9800	12.3072	11.5082	11.2064	12.8172	10.2983	11.8864	10.9457	12.2211	11.3487	13.2096	10.6515	12.2332	12.8010	11.7637	11.2745	10.3302	13.8279	16.4290	13.5440	12.8577
10.7429	10.8952	10.3991	11.8226	11.3675	10.3651	11.3488	13.0875	10.1498	11.9236	10.7635	12.1375	11,3500	13.0235	10.4893	12.1092	12.3645	11.3627	11.2677	10.4291	13.6144	15.8681	13.3979	12.6956
11.0395	11.4107	10.4187	11.6004	11.0752	10.3676	11.0074	12.9223	10.6381	12.390R	10.9473	12.3755	11.4346	12.9428	10.5931	11.9150	12.4810	11.4630	10.9254	10.3830	13.8508	16.4986	13.1415	11.6759
10.7086	21.9597	23.7511	8.9799	21.7025 8.1703	21.8509 11.5658	10.2473	24.8780	9.6613	24.6087 11.3563	10.0129	22.8975	21.3135	23,5535	9.7408	20.5490 11.1705	19.1988 11.7762	16.6126	10.3774	9.4181	18.2566	20,2525 15,0702	16.1666 12.4552	17,3073
12.8173	12.3294	12.6079	12.6985	12.5061	12.4547	12,6945	14.6882	13.1456	15.1578	13.8207	14.7417	13.8597	15.0729	13.2037	14.1303	14.6185	13.4698	12.9510	12.0169	14.6680	15.0702	13.8115	13.2161
17.7419	17.7013	17:8117	17.8492	17:2850	17.6437	17.7018	19.8769	18.0997	19.7047	17.3705	18.6904	17.1156	18.9006	15.3420	17.0076	17.0192	14.8857	14.0014	13.5927	16.4049	18.5316	15-2601	15.5843
11.9021	11.9331	12,5021	12.5726	12.3088	12.2633	12.0731	13.7145	11.5288	13.3768	12.1306	13.3397	12.5581	13.8526	11.7170	13:0278	13,7100	12.4038	11.9387	11.3720	13.9942	15.9358	13.3859	12.8008
11.9914	12.4776	12.0895	12.6495	12.5825	12.3318	12.2257	13.7542	11.7071	13.2329	12.3371	13.4992	12,6744	13.9495	11.8779	13.0541	13.8829	12.5502	12.0516	11.4818	14.0392	16.0313	13 5 3 7 6	13.0779
12.5425	12.5240	12.2567	12.7961	12.7343	12.4911	12.3339	13.9005	11.8672	13.366H 13.2723	12.5159	13.5816	12.7807	13.8343	12.0103	13.1919	13.9914	12.6531	12,4475	11.5718	14.4703	16.0925	13.6467	12.9918
12.3404	12.4053	12.3751	12.2289	11.9367	12.5725	12.2048	14.1805	12.0589	13.6151	12.6897	13.8685	13.0876	14.3100	12.2577	13.5335	14.0865	12.9477	12.4930	11.6174	14.4648	16.0682	13.5447	13.1620
11.1893	11.8640	14.0777	12.7315	12.7537	12.7169	12.2932	15.1574	9.9791	14.1228	12.2818	14.5718	13.9721	17.0761	13.6108	13.9503	14.5058	15.2572	17.4666	14.8563	21.5774	25.9970	21.0778	16.4715
14.2247	14.7794	15.0009	15.5530	15.5959	14.6368	13.9080	16.5119	11.6799	16.5603	13.5798	15.0247	13.2310	14.9225	11.7449	11.6789	10.1221	10.4099	11.2397	9.7032	13.0178	15.4336	12.9587	10.3585
6.3021	6.2503	6.1517	6.0960	5.5741	6.7478	6.4659	8.1734	5.3874	7.2810	6.4767	7.4562	7.0810	7.9185	6.5042	7.2305	6.8904	7.6077	E.0756	6.7344	9.5037	11.9773	9.9162	7,4594
16.0967	15.7194	15.6750	16.3858	15.7194	16.2511	15,7896	17.6797	14.1765	17.2965	16.0292	17,7581	16.9995	19,4711	16.4412	16.7213	17,5708 8.1182	17.1705 8.1368	18.7908 8.3387	7.4318	22.0867 10.0358	25.6113	22.1671 10.4718	17.3918 8.2384
13.1697	13.4524	12.6452	14.5273	13.8414	12.7940	13.6199	15.4411	13.0404	14.9800	13.4180	14.9993	13.7834	15.5207	12.9224	14.5659	14.3166	13.5327	13.6317	12.4352	15.7734	18.7887	15.1238	13.8217
12.6020	13,4234	12,6999	12.5318	11.9549	12.4889	12.8342	14,5976	11.2199	13.9248	12.9100	14.3847	13.4497	15.0221	13.1197	13.5504	11.8331	13,9617	15.0908	13.3168	17.4269	20:6447	17,0227	14.0515
1L4623	11.3894	11.9379	11.8622	11.3904	11.2232	11.2561	13.1039	9.5587	12.2287	11.1896	12,7010	11.9216	13,6074	11.6653	12.1367	12.3361	12.6842	13.8253	12.1698	16.1285	19.4437	16.3973	13.1432
9.3975	9.3683	9.2253	9.4661	9.3080	9.4037	9.4318	11.3378	7.9910	10.5569	9.5836	10.8559	10.3562	11.8621	9.9575	10.4643	10.1817	10.7654	12.1191	10.3328	14.5369	17.3311	14.3414	11.3701
9.0145	9.0061	8.9252 9.9685	8.9251 9.9232	9.0526	8.9185 9.9185	8.5810 9.5408	10.9656	9.5103	10.1817	9.1616	10.4574	9.7291	12.0160	9.3331	10.0454	9.7278	10.3904	10.9662	9.6843	14.3847	17.0876	14.0356	10.5538
6.9735	7.1274	7.2441	7.2067	7.0968	6.9062	6.5494	7,4941	6.9714	8.1121	7.1532	7.5083	7.1054	7.1474	5.9715	6.1610	5.6938	5.4385	5.3773	4.8191	5.7058	5.6956	5,6685	5.0424
14.4106	15.1496	15.7737	164353	15-9345	14.9719	13.9827	16.2827	13.9129	16.0886	13.7227	15.0758	13.3791	14.9697	11.5658	12.2776	11.1185	10.7288	10.7953	9.7518	13.0442	14.9761	11.9449	10.7142
10.7571	11.3569	12.7251	12.8527	12.2291	11.2581	10.2821	12.2402	10,1401	11.5470	10.3019	11.3182	10.4792	11.5502	9.4574	10.4340	10.4174	10.0947	9.8768	8.8591	11,2187	13.4280	11.0159	9.8784
12.7268	16.1828	18,8840	19,4275	18.2020	17.3992	13.4424	13,0811	8.4146	11.8386	10.9551	12.0133	11.5798	13,2331	11.0863	11.6318	10.9089	11.1062	11.9434	10.9699	16.1346	18.8080	16.6159	13.4943
7.1661 8.9642	9.9448 8.9749	12.6938	1.6557	1.6579	12.7169	11.1503 8.1534	11.3034 10.3876	7.5800 6.3777	9.1449	9,0741 7,7878	9.2253	9.0593	11.8352	9.6038 8.2084	10.1276 8.9163	9.5731	9.3249	10.5292	9,9899	13.8419	17.4014 16.5320	15.0617	10.7165
8.9642	8.9749	11.4304	1.5525	1.5581	11.4532	8.1534	10.3876	6.3777	9.1449	7.7878	9.2253	9.0593	10.5989	8.2084	8.9163	9.3034	9.3249	10.5292	9.2445	18.0139	16.5320	14.3227	10.7165
8.1401	8.0300	8.3216	7.7420	8,1717	8.2327	8.2166	9.9866	6.5034	8.9850	7.9255	9.4319	8.7691	10.5047	8.4328	8.9878	9.1028	9.6140	10.9513	9.1567	13.5232	16.7263	13.6830	10.3053
15.8238	15.5565	15.2889	15.6812	15.4865	16.2595	15.7435	18.1286	13.6505	17.0489	14.4425	15.4590	13.4986	14.7034	11.1994	11.1795	9.2009	9.3684	9.5422	5,2790	11.2143	13.6322	11.4358	9.6208

Road		Coordin	nate (m)		Width	Height	Road Type
Pair	X1	Y1.	X2	Y2	(including	(m)	(caline 4)
R141	833295.35	821947.25	533315.56	821891.57	13	0	1
R162	#33329.69	821353.67	E13315.96	821691.84	13	0	- 1
R143	833129.75	621889.31	R33160.17	821834.07	- 13	0	1
R164	833160.17	821834.07	933178.74	821783.15	13	0	
R145+R146	833612.49	621976.58	85490458	821516.02	17	0	1
#147+#168	833736.44	821588:35	833931.13	821727.34	16	0	1
R149	833728.61	821749.52	833807.73	821684.30	14	0	4.
RIAD	833774.08	821643.62	833807.73	821684.38	13	0	- 1
R150	833734.67	821759.23	833607.71	821683.81	. 0	. 0	- 1
R151	833613.61	821610.98	E13493.50	821543.70	13	0	- 1
R151	833493,50	821543.70	¥3577526	821642.63	14	0	1
R152	833774.08	621643.52	833826.17	821600.58	20	0	1
8153	833991.31	622369.76	634828.77	822414.27	18	0	1
R154	\$33060.46	822320-45	#33992.00	822399.67	18	0	1
R155	833909.65	822271.36	933900.44	822320.45	18	0	4
R156	833048.78	82222216	813509.65	822271.36	18	0	- 1
R157	833866.58	522222.34	813807.77	822172.98	- 10	0	
R158	833827.77	822172.95	E11778.49	822113.30	18	0	- 1
Risk	834071.91	822299.62	83411290	822784.34	15	0	1
R160	834090.39	622207.53	034117A1	622332.11	16	0	1
RIST	834054.90	822250.52	834W5.91	622799.62	15	0	-
R162	£34049.42	822236.28	#34090.39	822287.53	15	0	1
R162	832993,86		R34014.90	622250.52	16	0	1
		822201.65 822186.33	_			0	
R164	834007.86	240,189,00	834549,42	022238.28	15		1
R163	#33953.31	822151.70	E1391447	622201.23	16	0	1
R166	833872.14	822051.39	831954.76	822150.50	19	0	- 1
R167	833,691.47	822042.45	834007.86	822109.33	16	0	1
R168-R169	833813,72	821975,47	£1387£.16	822050.03	21	. 0	1
R170-R171	633716.44	821888-35	633812.49	821978.50	18	0	1
R172+R173	833684.92	821822.32	833719.28	821887.65	29	0	1
R174-R178	833541,78	\$21677.56	833683.38	821823.65	16	0	1
R176	833496.77	521808.49	533540.47	821680.73	20	0	1
R177	#33513.09	821599.24	83351348	821665.A7	20	0	1
R176	835440.44	821529.90	833466.60	821608.61	16	0	4
R179	833451.64	821626.21	833511.32	821400.38	17	0	1
R120	834216.31	622256.35	854325.94	622585.39	18	0	1
R191	628161,98	822212.22	E3421E31	\$2225E-35	18	0	1
R182	634140.62	822162.67	834111.78	822212.39	16	0	1
R183	234099,34	822113.33	934140,62	822162.07	18	0	1
R184	834077.01	822132.66	834051.51	822100.94	13	0	- 1
RISK	\$3A061.51	822100.94	834071.90	822084.18	13	0	4
R184	834071.90	822984.18	834097.30	822115.02	14	0	1
R185	834305.98	\$22180.58	034302.04	822267.A4	19	0	1
8.195	834251.54	622084.63	634273.34	622135.63	19	0	1
R197	834190.59	822037.73	834231.76	822086.A5	- 18	0	1
R199+R199	#3A004.98	#21815.03	834019.34	821890.22	19	0	- 1
R190+R191	822921.42	821727.74	834004.98	821816.02	19	0	1
R192-R193	833878.32	\$21660.75	833930.89	821727.98	20	0	1
R194+R195	833825,79	621500.86	833867.61	821651.48	20	0	- 1
R196+R292	A33761.01	#21523.18	813826.17	821699.58	20	0	1
R197	834264.36	822000.94	834400.15	#22104.71	17	0	-
R198	834322.77	827010.68	83436436	822660.94	18	0	- 4
R199	834251.93	821961.17	634323.00	822810.AB	-19	0	1
R200	634239.17	82191A-13	834210.0E	821983.18	14	0	1
R200	B34239.17	821914.13	\$34327.69	821840.33	18	0	1

									-		NO ₂ x 10	0 (g/VMT)	-		-						V	-	
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
14.3510	14.0933	11.5867	11.1492	14.1406	15.4324	14.2409	17.8008	12.8659	16.4930	13.4465	14.6289	12.5405	13.8360	10.3087	10.2706	7.9099	8.2558	8.5826	7.4578	10.6927	13.3065	10.8932	8.5287
7.6933	6.2694	6.9131	5.8988	5.4689	6.8523	7.6437	8.5591	6.6613	8.3703	7.8348	8.6933	8.3446	8.8398	7.6981	8.4224	8.1109	7.5048	7.4588	7.1947	8.8569	10.9436	9,4090	8.3991
16.3417	16.2872	15.9080	16 1524	16,0385	16.8101	16.1950	18,4426	153325	18.4738	16.0830	17.0220	14.7675	15.9419	12.8743	12.4611	10.8680	10.4938	10.5499	9,4830	12.0386	14.3876	12.3178	10.3780
16.1220	16.0368	15.7046	16.2441	16.0584	16.6991	16.0582	18.2517	143152	17.6641	15.2037	16.2283	14.2905	15.5514	12.1584	12.0893	10.0449	10.0868	10.1199	8.8757	11.7241	14.0967	12.0765	10.0442
12.7047	11.8640	14.0777	B.3012	15.9239	11.6081	12.2915	14.3905	9.4880	13.5436	10.7418	12.0042	10.0679	10.9641	8.1601	7.9188	5.5570	6.1515	6.0892	5.2343	7.1291	3.9163	7.7212	6.0839
10.6430	10.8688	12.6938	14.1160	12.7537	11.8640	10.9878	13.1246	8.6262	12.0611	9.6476	10.4556	8.8092	9,4118	6.7964	6.5585	4.7683	5.2885	4.8970	4.2495	6.2244	7.1159	6.5112	5.2037
9.4467	9.0207	8.2653	9.9625	9,9797	11.1328	9.0369	11.4750	7.3857	10.1884	9.1324	10.5072	9.9685	11.9032	9.7206	9.9536	11.0621	11.3918	12.9012	10,8634	15.7254	19.1174	16.8663	12.7613
9.4457	9.0207	8.2653	9.9625	9.9797	11.1328	9.0369	11.4750	7.3257	10.1884	9.1324	10.5072	9.9685	11.9032	9.7206	9.9536	11.0621	11.3918	12.9012	10.8634	15.7254	19.1174	16.8661	12:7613
9.4467	9.0207	8.2653	9.9625	9.9797	11.1328	9.0369	11.4750	7.3857	10.1884	9.1324	10.5072	9.9685	11.9032	9.7206	9.9536	11.0621	11.3918	12.9012	10.8634	15.7254	19.1174	16.8663	12,7613
9.4467	9.0207	8.2653	9.9625	9,9797	11.1328	9.4720	11,4750	7.4674	10.3043	9.1324	10.5072	9.9685	11.9032	9.5466	9.9536	10,0281	11.1053	12.4837	10.4288	15.7254	19.1174	16.8663	11.6497
9.4457	9,0207	8.2653	9.9625	9,9797	11:1328	9.4720	11.4750	7,4674	10.3043	9.1324	10.5072	9.9685	11.9032	9.5466	9.9536	10.0281	11.1053	12.4837	10.4288	15.7254	19.1174	16.8663	11.6497
9.4467	9.0207	8,2653	9.9625	9.9797	11.1328	9.0369	11.4750	7.3857	10.1884	9.0168	10.3486	9.6658	11,4446	9.0655	9.8904	9.8613	10.6732	11.5595	9.8451	15.1328	18.3380	14.6766	10.7403
10.0685	10.2801	9.8669	9.8935	10.3593	10.2746	10.1909	12.4331	8.7192	11.4732	9.6042	10.2401	9.1432	10.3917	7.7008	8.2897	7.649E	7.5220	7.7865	6.7842	9.7550	12.1236	10.2628	8.2125
10.0003	10.3703	9.6439	10.0222	10.5235	10.0083	10.2723	12,4767	8.6926	11.3602	9.5128	10.3384	9.2074	10,2400	7.7831	8.2312	7.5389	7.6417	7.9172	6,8396	9.7755	12.0606	10.0782	8.0342
10.0026	10.3887	9,8636	9.8888	10.2184	10.1503	10.2845	12.7843	9.2088	11.7932	9.8521	10.4777	9.4000	10.7276	7.8778	8.4606	7.9901	7.9245	8.0524	6.9418	10.1054	12.6654	10.4775	8.2877
14.2069	13.7313	13.4770	13.4255	13.0994	13.1595	14,2560	18.5262	14.4135	17.5390	15.4551	16.5951	15.1481	16.1509	13.3184	13.5080	12.4821	12.5337	12.3906	10.8208	13.6187	15.5692	13.4391	10.9642
14.7245	14.3770	14.3756	13.9693	14.0901	14.0563	14,7301	18.9684	15.1545	17.9279	15.3788	16.1287	14.5380	16.2372	12.7121	12,7635	11.8311	11.8192	12.2434	10.6731	13.6935	15.7857	13.4732	11.0203
14.4950	14.5722	14.5149	14.5215	14.7007	14.5250	14,4782	16.9354	13.1264	16.4134	14.1352	14.9174	13.4614	15.0268	11.7975	11.8095	10.9549	10.9273	11.4612	10.2161	13.6408	15.9110	13.5223	11.1956
10.4028	10.6646	11.5213	11.5688	8.9968	11.5658	10.2922	12.2195	9.7385	11.8272	10.6627	12.2212	10.9926	12.6182	9.8563	10.9037	11.2955	10.8660	11.2609	10.0548	14.1714	16.5455	13.7106	12.3378
12.1884	12.1172	12.0861	12.3986	11.7632	12.4479	12.5966	14,7086	11.2241	13.6637	11.4325	12.7862	11.5164	13,2854	9.9213	10.5034	10.1971	9.7225	10.0468	0808.9	12.6360	15.3341	12.4324	10.2378
10.5862	10.5491	10.5599	10.2903	10.8785	10.4527	10.7851	13.0276	9.8673	11.9917	10.6451	12.2051	11.2365	13.0627	10.3540	11.3767	11.2906	11.0909	11.4675	10:3037	14.0425	16.9454	13.7034	11.6019
12.2916	12.2457	12.1098	12.1562	12,0938	12.1867	12.3003	14,6174	11.2503	13.5493	11.4687	12.8718	11.5028	13.0868	9.9964	10.7555	10.1835	9.7373	10.0600	8,7819	12,4988	15.3365	12.4133	10.2445
11.5384	11.6829	11.7886	11.4287	11.5444	11.6678	11.5701	14.0621	11.0947	13.0550	11.1543	12.3573	11.1131	12.6280	9.6558	10.7363	10.2447	9.7998	9.8876	8.6949	12.2857	15.0467	12.0568	10.2545
11.4499	11,4518	11.4978	11.2027	11.6806	11.4077	11.3962	13.5366	10.1216	12.6217	10.5387	11.9154	10.7146	12.7627	9.6138	10.1278	10.0269	10.0043	10.5490	9.1272	12.9872	15.8051	12.8105	10.4441
9.6661	93644	12.4925 9.4715	12.5827 9.4998	12.4599 9.5369	9.4925	12.8871 9.6966	14.7522	9.3070	13.7099	9.4912	13.5067 9.8168	12.5480 9.1288	13.7325 8.9312	11.2735 8.1708	12.1484 8.5685	7.7573	7.8047	7.1087	10.4800 6.5839	13.9458 7.6093	15.9735 3.6756	13.2905 7.8461	73406
3.9662	17.6210 3.9356	4.0370	17:\$838 4.1140	17.8484 3.8429	17.6202 3.8958	17.6573	20.9740 4.8234	3.9274	19.7296	17.1940 4.1335	18.6492 4.3592	16.8895 4.3155	18.9702 4.1404	3.7612	16.4695 4.2598	16.3716	14.2835 3.9944	3.4025	13.1923 3.1865	16.9822 3.8237	19.635K 4.8208	15.7700 4.1454	15.1761 3.6649
5.9408	5.9541	5.9484	5.7943	5.9766	5.9608	5.8751	7.0867	5.7206	7.0789	6.3895	6.8162	6.5622	6,7676	5.7784	5.9993	5.6510	5.6543	5.5507	5.0571	6.2682	7.4531	6,4528	5.6330
12.0024	11.8541	11.8315	11.8575	11.6961	11.9347	11.8392	14.2599	10.7591	13.3854	11.3310	12.6829	11.4011	13.0957	10.2979	10.9821	10.6900	10.3885	10.5535	9.4405	12.7107	15.1288	12.4187	10.6755
12.7722	12.7635	12.7229	12.7879	12.6795	12.7995	12.8014	15.6870	12.8976	14.8580	13.3183	14.5640	13.3682	15.4128	12.3752	13.1991	13.1236	12.9022	12.8701	11.6888	15.1234	17.5296	14.6438	12.5810
11.9275	11.9016	11.9512	11.9900	12.0608	11.3075	11.9073	14.1211	11.6973	13.1957	12.1738	13.4655	12.6846	14.2385	12.0146	13.1977	13.2256	12.9469	12.9934	11.8559	14.9823	17.3198	14.6003	13.4040
13.2614	13.2859	13.3065	13.2209	13.0849	13.3034	13.1941	15.1768	11.8748	14.1916	12.3073	13.4579	12.1435	13.7560	10.9765	11.6113	11.2391	10.6916	10.6306	9.6196	12.6132	14.9592	12.4519	11.0567
13.8658	13.7676	13.7538	13.8555	14.0219	13.7270	13.9853	16.0205	13.9529	15.1645	14.1311	15.5589	14.6890	16.5574	14.0151	15.1351	15.0941	14.8647	15.3909	13.9703	17.5890	20.1249	17.2348	15.4151
14.8712	14.8048	14.8388	14.8597	14.8758	14.8017	14.8803	17.2867	13.9790	16.1747	14.3180	15.8088	14.3994	16.3724	13.0382	14.3591	14.2983	13.1141	12,9009	12.1306	15.H220	17.9285	14.7176	13.8880
12.6304	12.7421	12.9519	12.9048	12.9226	12.5379	12.9062	15.3511	12.0293	14.6898	12.4268	14.0828	12.8595	14.8935	11.6126	12.7211	12.3351	12.0436	12.4087	11.1185	15.4780	18.8305	15.1582	12.8099
12.9503	9.9448	9.0034	9.9625	11.1686	9.9448	13.7953	13.9176	9.7297	12.5817	10.9773	12.4785	13.0110	14.6977	11.5019	12.7705	11.9970	12.8022	13.2569	11.3270	16.0254	19.5891	16.3378	12.9200
11.4384	11.5325	12.2478	12.2185	14.2432	12.7950	11.5705	13.4779	10.3333	12.0597	10.8450	12.4147	11.5099	14.3311	10.3232	11.5287	12.0635	11.7647	12.2289	10.3531	15.0740	19.3761	15 1545	12.4512
12.8425	13.3603	14.0500	14.3476	14.7501	15.1819	12.8913	15.1698	11.7701	14.0289	12.2290	13.6672	12.6729	14.4482	11.4974	10.9731	10.5991	10.5683	11.3889	10.5133	15.1308	18.7062	14.3922	13.6392
12.7061	12.2751	12.1111	12.0393	11.9002	12.7169	12.7370	14,9522	9.6074	13.8224	10.4505	11.4462	9,4396	10.2039	7.3160	7.3589	6.0794	6.1149	6.1241	5.1271	7.4294	9,2948	8.1062	5.8142
12.7061	12.2751	12.1111	12.0393	11.9002	12.7169	12.7370	14.9522	9.6074	13.8224	10.4505	11.4462	9.4396	10.2039	7.3160	7.3589	6.0794	6.1149	6.1241	5.1271	7,4294	9,2948	8.1062	5.8142
12,7061	12.2751	12.1111	12.0393	11.9002	12.7169	12.7370	14.9522	9.5074	13.8224	10,4505	11.4462	9.4396	10.2039	7.3160	7.3589	6.0794	6.1149	6.1241	5.1271	7.4294	9.2948	8.1062	5.8142
12.2913	12.1647	12.6925	12.2551	12.9226	12.2118	12.6560	14.4839	11.1825	13.4312	11.9001	13.6820	12.2832	14.6838	11.5746	12.6210	12.7134	12.1172	12.6647	11.1315	15.5095	18.3460	15.0760	12.7356
11.8792	14.0793	15.1497	15.8092	17.1305	15.7981	13.4773	16.0078	12.7048	14.2970	12.5355	14.5291	12.9690	14,6977	11.5071	10.6315	10.0462	10.2424	10.9197	10.1090	14.4028	17.6676	14.3922	13.6392
13.8025	14.4473	13,7730	14,4457	14.9027	14.4290	14.1209	16.4980	13.6920	15,4454	14.5501	16.1917	15.2522	16.7868	14.4225	15.6408	15.4299	15,2365	15.5388	14,5378	17.8615	20.4694	17.6383	15.8351
11.9403	11.3512	12.1733	12.9337	11.8067	11.5767	11.9468	13.7027	10.1916	12.5741	10,9390	12.2387	11.4338	12.7114	10.0490	10.6226	10.5507	10.2750	10.5440	9.1820	13.0521	15:2345	12.6932	11.1187
12.7322	13.4211	12,9196	11.3620	13.8873	13.2382	13.2243	15.2971	11.8072	13.9578	12.0446	13.5771	12.5046	14.4441	11.1243	12.1355	12.1104	11.4332	12.0628	10.6627	14.9769	17.8403	14.6817	12.2893
10.0252	9.8434	9.7450	10.4855	11.0407	9.8864	9.6977	11.0445	8.2848	10.0243	8:9007	10.3345	9.5556	11,2748	8.0013	8.8166	8.2043	7.6826	7.2975	7.2374	11.2586	10.5608	8.9706	10.3133
18.3023	17.2317	17.7220	18.7562	18.8597	17.9183	18.1392	18.8163	16.0883	18,5182	17.5476	19.7128	18.5440	19.3345	17.7177	18.3727	18.4371	18.4320	18.9404	18.1701	20.5624	21.6447	20.0414	19.5700
3.R.3087	18.7271	15.1979	16.8290	16.9593	16.9858	18.6477	18.1450	18.2274	17.2660	15.3401	16.3406	17.8155	16.5898	17.0467	17.5105	17.4531	19.7769	17.2116	16,5637	18.8156	20.3989	18.7071	20.5983
15.2885	11.1328	8.2653	8.3012	9.9797	9.9448	9.9615	15.1763	11.4377	14.6535	13.0205	14.8139	9.2074	11.4429	9.6021	9.2562	9.7309	7.9060	8.3418	8.7214	12.7626	20.5802	168592	12.7613
12.3156	10.4992	9.5260	8.3012	9.9797	9.0207	9.9615	13.5196	9.1299	12.1345	10.7165	12.3447	11.5766	15.9989	11.0884	12.1364	12.3727	11.9437	12.1005	10.9697	16.9460	18.7202	14.7031	16.8897
15.0564	15.2711	15,5439	17.6700	17.4824	17.6322	15.6537	16.8699	14,1090	16.1796	14.6056	14.4107	13.8605	15.0804	11,8065	12.5739	12.5655	14.4951	14.2995	13.7694	16,2916	19.0036	14.6405	14.1271
13.7559	12.6898	13.4226	13.4576	14.2296	14.0303	13.8151	15.6570	12.4990	15.2096	12.1489	13.8183	12.2054	14.5633	11.0748	12.6817	12,7491	12.0442	12.1448	10.8900	14.5621	17.3937	14.0366	12.8468
13.7559	12.6898	13.4226	13.4576	14.2296	14.0303	13.8151	15.6570	12.4990	15-2096	12.1489	13.A183	12.2054	14.5683	11.0748	12.6817	12.7491	12.0442	12.1448	10.8900	14.5621	17.3937	14.0366	12.8468

Road	X1	Y1	X2	¥2	including	Height (m)	Road Type (caline 4)
REDZ	833126,78	52224.51		820 On 25	mixing room	0	1
RIGI	833177.37	£22334.28			29	0	7
FI063	633231.00		#11414H0		20	0	- 1
-R003	833434.00		#11905.49		- 76	0	- 1
R(0)	822969,46	622643.00	\$13005.46	82364E76	29	0	1
RIDA	833118-28	#22306.10	SERGES!	82225562	19	0	-1
F1004	633166.93		83542538		16	0.00	- A
R004	833420,10	622396:41	037516.26	022421.58	19	0	1
RIDE	833616.28	£22,421.55	851671.75	622496.58	36	10 - 10	4
RSSS	\$33671.75	822.49 t.58	833933.47	822414.65	16	0	4.
H008	633933.67	822614.60	#30973.71	822424.0¥	19	0	1
Meas-	632973.71	622625.09	E3404E14	612520.54	18		1
P005-8307	833527.00	622410.61	633/07.55	622455.21	14	0	
Rdos-indo7	833627.65	222455-21	811712.67	472494.A7	14	. 0	1
NO-6-8-007	833732-07	822494.47	832792 (C	922441.05	14	0	- 1
HEOR-HEO?	833762.11	622441,65	\$13840.01	822456.02	34		- 1
1003-R105	E23664 17	622394.31	825 m 2.59	622497.15	13	-0-	*
Rdolf + Ristor	\$33693.50	822397.15	E1384134		13	0	
M010×H011		622463.30	#32986.64	832452.8E	(1	0	1
#610+#611	632,819.64	\$22432:88	832883,54	STEMS2.45	12	0	- 3
RB1>-RB11		822A5E49	813540.51	822458-02	12	0	- 1
	633387.26	822567-47	833423.59		16	0	1
H012-R013	833423.09	\$22669.02	635416/6	012462.07	10	0	1
R012+R612	633416.08	622,482.07	#23417A2	022425.39	10	0	1
CISR-Ciss	E33447.62	622A25.36	ED514.64	622.000.A3	10	0	
R012+R015		822390.48	813367.56	822354.50	16	0	1
MO14-H014		02231E11	#32807.6W	83235430	14	0	
R\$14-R\$17	833587,56	\$22354:m	#2161217	022374-91	15	. 0	1
BU15+9U17	103611.17	822374.91	41364147	6213M-31	15	0	1
R210	8330k2.67		311219.07		18	. 0	1
M621	#33269.01		813305.00		78	. 0	1
R102	E38355,80		#15410.61		78	0	4
R1122	EXPRES 81	#22340.IS	EISEN9.44	622218.35	16	0	1
W423	W33072.42	422119.68			14	0	- 7
M624		622129.64			74	. 0	- 9
R825		622176.ST			14	. 0	1
Ru2s		822232.6S			14	0	1
R027	633503.91		#1167X#2		13	0	1
8626	813675.82	417341.00	810708-11	ATTERDAT	13	-0	1
RH29	B33766.03		# E184E76	622405.79	13	0	- 1
Reso	833848.76	822404 TV	#21917#1		14	0	- 1
H631	633917.63		#30960.ER	677454 TE	14	0	- 1
M012/H101	823078.98		#10 ULT		10	0	1
REST	833121.79	\$4440.0.E1	#D2019		78	0	-
MOJ4	633251.79	422120.94	#2529E77	622175.17	- 0	0	1
					7.0		-
R635 R634	633396.77	#22176.17	833524.35	#22221.21	18	0	1
	823524.35			622289.00			
9627	613653.40	62229-0,00	853694.86	622284.07	15	0	1
REDA	833664.68	622284.56	613761.79		96	0	4
RUSE	A337E4.00		#23795.45	622325.74	12	0	,
H040	833789.11	622316.09	#35#03.19	822225.11	18	0	1
R642	\$23,533.16		\$13,002.96		18	0	- 1
R242	和3級(())	422360.57	944299246	622125.A5	18	0	1
ROSS	£33050.46	222120 At	ENGIAGE		48	0	1
R044	E24034.00		E544062		18.	0	- 1
R543	124141.12	RIZMENT	834203.74	822581.45	.19	0	
RISAB	E2A234.72	622084.65	634323.21	822011.22	1,0	0	1
RUAT ROSE	R3A322.77	827010.KB	ENCHART	821959.68	- 18	0	1
	X33097.20		#3248E3#		12	0	3
9543	X33155-56		81343410		18	. 0	,
RISS	E20101.47		83127446		71	-0-	1
RIST	633274.50		38141E70		- 18	. 0	- 1
R052	633434,10	822080:21	\$15A66.13	822174.73	98	-0	1
R653		\$22120.44			58	. 0	1.
R955		62216.5.28			18	0	1
FI054	432419-43	622967.29	AMMETS	822122.03	18	0	
R054	633586.71	822122.03	#3354#45	BEETALAS	18	0	3
ROSA	823649.55	622164.45 822152.60	#1351268	822152.80	18		1
H054	8330E3.68	822152.60	SEL712.66	622149.92	18 - 1	0	1
MORA -		927140.82			16	0	- 4
R054	613767,63	822128-96	855775.48		10.	-0	1
Ross .	823786,53	\$22120.04	811872.14	622051.39	.19	- 0	1
RIBS	83377 E.49	622113.86	831M7.20	822039.12	- W	0	7
HOST	833873.20	932642.68	134111.21	821814.71	16	0	1
Ross.	634159.21	12161478	#34290.10	821708.42	16	0	- 4
91009	833867.29	422039-21	634858.34	821890 22	97	0	- 1
Auso	R34056.34	#21380.ZZ	834261.61	821727.A5	48	0	1
R061	813116.37	821680.26	82211976	821889.31	16	0	- 1
8082	823159.76	621889.31	615216.78		10	0	1
RIB2	823294.88	621947.56	8134(0.51		16	0	1
	833460.49	#21968.03	#11543.73	82200M.T2	18	0	-
Block Co.	833460.49 833541.73						1
ROMA	623480.98	63293E72	#33841.70		15	0	-
H004		\$21952.82	833563.70 83336556	821982.31	- 18		1
R084				621691.61	16	0	- 1
RODA RODA RIPE	833166.17	#21834.07		*****	- 24		7
HORE HORE HORE	833169.17 833316.96	821891.6E	#334H.00	821952.75	16	. 0	1
HORE HORE MOSE MOSE	83316.95 833316.96 833184.01	921391.6E 921779.07	833494.00 633478.47	021763.88	10	0	1
HORA HORA HINE ROSS	833169.17 833316.96	821891.68 821773.07 621783.16	#334H.00	821613.88 821613.88			

	-										icle count	194 5 4 5 5 5 5 5				-							
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr05	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16 4350	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
1250	800	550	400	450	650	1650	4900	5500	4650 4650	4200	1950	3600	3600	3800	4000	4350	4800	4900	4150	2750	2600	7550 2550	1750
1250	800	550	400	450	650	1650	4900	9500	4650	4200	3950	3800	3600	3800	4000	4350	4800	4900	4150	2750	2600	2550	1750
1250	800	550	400	450	650	1650	4900	5500	4650	4200	3950	3800	3600	1800	4000	4350	4800	4900	4150	1750	2500	7550	1750
1250	800	550	400	450	650	1650	4900	5500	4650	4200	1950	3600	3 <i>E</i> 00	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1100	700	500	350	400	600	1500	4350	5150	4200	1950	3750	3500	3650	3900	4250	4700	5350	5500	4750	1100	3000	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3950	3750	3500	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4850	9150	4200	3950	1750	3500	3650	3900	4250	4790	5350	5,500	4750	3100	3000	2950	7000
1100	700	500	350	400	600	1500	4350 4350	5150 5150	4200 4200	3900 3900	1750 3750	3500 3500	3650	1900 3900	4200	4700 4700	5350 5350	5500 5500	4750	1100 3100	2950 2950	2950 2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	5350	5500	4750	3100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3660	1900	4200	4700	5350	5500	4750	3100	2950	2950	2000
17	10	6	4	4	7		60	69	71	72	73	100	100	100	200	68	70	67	64	:59	56	31	- 25
17	10	6	4.	- 4	7	18	60	69	n	72	73	100	100	100	100	- 68	70	67	- 64	59	- 58	- 31	- 25
_ 17	10	- 6	4	4	7	18	60	69	n_	72	73	100	100	100	100	- 65	70	67	- 64	.59	- 58	- 31	25
17	10	- 5	- 4	4	7	38	60	69	71	72	73	100	100	100	100	68	70	57	64	59	511	31	25
62	- 11	13	B B	10	16	62	73	150	150	150	150	150	1/50	150	150	100	100	100	100	100	74	72	37
100	72	B 3)	- 21	24	16 38	100	73	150 350	150	150 350	150 350	150 350	150 350	150 150	150 350	250	100	100	250	100	150	150	100
100	72	31	. 21	24	38	100	200	350	400	350	350	350	350	150	350	250	300	350	250	150	150	150	100
100	72	31	-21	24	38	100	200	350	400	350	350	350	350	350	350	250	300	350	250	150	150	150	100
7	- 1	2	1	1	2	7	12	25	- 27	24	23	25	26	30	29	23	32	35	- 27	20	16	14	11
	- 4	2.	1	1.1	1	7	12	.25	27	24	.23	25	- 26	30	29	29	32	- 35	27	20	36	14	11
7	1	2	1	1	2	7	12	25	27	24	23	25	26	30	29	33	32	35	27	.20	16	- 14	11
7	3	2	1	- 1-	2	7	12	25	27	24	23	25	26	30	29	- 11	32	35	27	20	16	14	31
- 7	27	16	12	13	20	- FI	100	25	27 200	190	150	25 150	150	30	150	23	100	35 150	27	100	16	100	72
66	26	16	11	12	20	67	100	200	200	150	150	150	150	150	150	100	100	100	100	100	100	100	45
66	26	16	21	12	20	67	100	200	290	150	150	150	150	150	150	180	100	100	100	100	100	100	46
-50	50	16	11	13	19	50	100	200	200	200	150	150	150	150	100	50	100	50	50	50	50	50	21
50	50	20	24	16	24	50	100	250	250	250	200	200	300	200	300	150	200	200	150	100	100	100	50
50	50	17	12	14	20	50	100	200	200	200	200	200	200	250	250	200	250	250	200	150	100	100	100
50	50	17	12	14	20	50	100	200	290	200	200	200	200	250	250	Z00	250	250	200	150	100	100	100
50	23	14	11	11	17	50	100	200 150	200	200	200	250	250	300	300	250 250	400 150	450 400	350	250 250	200	200 150	150
50	50	18	12	15	21	50	100	200	250	250	250	300	300	350	400	300	450	500	400	300	250	200	150
50	50	17	12	14	20	-50	100	250	250	250	250	250	250	300	300	250	350	350	300	200	150	190	100
100	50	50	72	25	50	100	200	350	100	350	350	350	350	450	400	350	450	500	400	250	250	700	150
50	23	15	10	11	16	50	100	150	200	200	200	200	200	250	250	200	300	350	250	200	150	150	100
50	15	9	6	- 8	10	50	50	150	150	100	100	100	100	100	300	100	100	106	100	50	50	50	50
50	50	24	17	19	50	-50	150	300	350	300	300	350	350	400	AOC	300	450	500	400	500	250	200	150
106	105	54	54	A SA	55	108	50 320	450	100 450	100 373	371	100 421	100	469	100	100 519	150 619	150 618	100	100	30H	50 258	205
200	150	100	100	100	150	200	550	800	750	700	650	750	750	850	900	950	1150	1200	900	650	550	500	350
200	150	100	100	100	150	200	550	850	800	700	700	750	750	850	950	1000	1200	-1200	950	650	550	500	150
300	250	200	200	200	256	480	900	1400	1350	1150	1050	1100	1090	1100	1150	1150	1300	1300	1000	700	600	390	400
350	300	250	250	250	250	450	1050	1650	1550	1150	1250	1300	1300	1400	1450	1450	1700	1700	1300	900	750	700	500
300	250	200	200	700	200	350	850	1350	1250	1100	1000	1050	1000	1050	1100	1100	1250	1200	950	850	550	500	350
300	250	200	206	200	200	350	900	1350	1250	1100	1000	1050	1000	1100	1100	1150	1300	1300	1000	700	600	990	150
200	150	150	150	150	150	250	650 550	1000	950 850	700	750 650	750 650	750 650	650	800 650	650 650	950 750	700	700 550	500	400	300	230
200	150	150	150	150	150	250	700	1050	1000	850	750	800	750	800	300	800	900	850	650	450	400	350	230
250	200	206	150	150	200	350	900	1250	1150	1000	950	1000	1000	1050	1100	1150	1350	1350	1050	700	600	550	460
150	150	100	100	100	1.00	200	450	506	700	600	550	600	600	650	70G	700	850	850	650	450	400	390	250
200	150	150	150	100	150	250	550	900	850	750	700	750	700	750	300	750	950	950	750	500	450	400	300
150	100	100	100	100	100	150	400	850	600	500	500	550	550	600	600	650	750	750	600	400	350	800	200
290	150	150	150	100	150	750	600	900	850	750	700	750	700 650	800	800	H50	950	950	750	500	450	430	300
200 550	150	450	100 450	100	190	260 850	2000	300	750 2900	650 2450	2200	700 2250	2150	700	750 2250	2200	900 2500	900 2350	700	1250	1050	350 950	750
550	450	400	400	350	450	700	1700	2650	2500	2050	1850	1900	1750	1800	1750	1700	1900	1750	1350	950	800	700	500
650	500	450	450	450	500	\$00	1950	3000	2850	2450	2300	2450	Z350	2550	2650	2700	3150	3100	2400	1650	1400	1300	900
550	450	350	350	350	400	700	1650	2500	2350	2050	1850	1950	1900	2000	2050	2100	2450	2350	1800	1250	1100	950	780
350	300	250	250	250	250	450	1100	1700	1600	1850	1250	1350	1/00	1400	1450	1500	1750	1700	1300	900	800	700	500
400	300	300	250 250	250	300	550	1250	1950	1850	1600	1500	1600	1550	1700	1750	1800	2150 2150	2100	1650	1150	950	900	600 500
450	300 150	300	300	300	350	550	1250	7050	1950	1650	1500	1650	1550	1750	1800	1850	2150	2100	1650	1150	1000	900	650
45/3	150	300	300	300	350	550	1350	7050	1950	1650	1550	1650	1600	1750	1300	1850	2200	2150	1650	1150	1000	900	630
450	150	300	300	300	350	550	1350	2050	1950	1650	1950	1650	1600	1750	1800	1350	2200	2150	1650	1190	1000	900	650
450	350	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	21,50	1/550	1150	1000	900	650
450	350	300	300	300	350	550	1350	2050	1950	1650	1550	1550	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650
450	150	300	300	100	350	550	1350	2050	1950	1690	1550	1650	1600	1750	1800	1ES0	2200	2150	1650	1150	1000	900	650
250	200	350 150	350 350	150 150	200	300	750	1350	1100	1900 950	1750	950	1750 950	1850	1900	1950	2250 1250	2200 1250	1700	1150	1000 550	900	650 150
350	250	250	250	250	250	450	1100	1650	1550	1300	1200	1250	1200	1250	1250	1250	1400	1350	1050	700	600	500	460
300	250	200	700	200	750	400	950	1500	1400	1200	1050	1100	1050	1100	1100	1300	1200	1150	900	600	550	500	150
200	150	150	150	150	150	250	600	950	900	800	750	800	800	900	950	1000	1200	1200	900	650	550	900	150
200	150	150	150	150	150	250	600	900	850	750	700	800	750	850	900	900	1100	1100	850	600	500	450	300
50	22	14	9	11	16	50	100	150	200	150	150	150	150	150	150	100	100	100	100	50	50	50	50
50	50	50	18	20	50	100	150	300	350	300	300	300	300	350	300	250	350	350	300	300	150	150	100
50	20	13	10	10	15	50	100	150	150	150	150	200	200 150	200	200	100	150	300	200	150	150	100	100
50	21	13	9	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	50
50	21	13	9	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	30
50	50	17	12	14	.20	50	100	200	250	200	200	200	150	200	150	150	150	156	150	100	-50	50	50
-50	50	21	15	17.	.24	- 50	100	250	250	250	250	250	250	30G	300	250	350	400	300	200	200	150	100
1500	1200	1000	1000	950	1150	1900	4450	4750	4750	4730	4750	4750	4750	4750	4750	4750	4750	A750	4750	3350	2850	2600	1800
1350	1100	950	900	900	1050	1750	4100	4750	4750	4750	4700	4750	4750	4750	4750	4750	4750	4750	4500	3150	2650	2400	1300
	750	650	600	600	700	1200	2850	4350	4100	3500	3400	3600	3550	3900	4050	4200	4750	4750	3800	2650	2250	2050	1450
950 400	300	250	250	250	300	500	1200	1800	1700	1450	1350	1400	1.850	1450	1450	1500	1700	1650	1250	300	750	700	500

Road		Coordin			proclusting	Height	Road Type
Pair	X1	Y1	X2	¥2	mixing room	(m)	(caline 4)
REF	B30527.91	1521,059,29		621675.22		0	1
RUT-2		821875.22			29	0	- 1
R073	XXX4E1.50	621680.64	#39397.24	#21A75.22	13	0	- 1
HOTA .		621796.3A			70	0	. 1
9376	E23449.42			621583.06	16	0	. 1
RU78	E3360 (.48	821897.60	SERVICE	821699.37	18	0	-1
A076	633546.66		632402.43		34	0.00	4
M074	R13693.43	621685/90	83369492	621622.52	14	0	1
R877	833564.57	S21884.54	A\$1542.67	821654.38	12	100	1
8077	\$33561.87	821884.30	833665.68	821871.28	17	0	4.
H077	633,600-48	621971.29			17	0	1
MOTE	\$356£1.3E		853875.52		16	0	7
R679	833673.29	623311.43	833597.51	821651.48	16	0	
Ross	\$33675.67	821661-18	833999.54		16	. 0	
R091	833667.01	921000.84	932993.08			-0	1
M082	\$22.65E.18	621884.41	813510.76	821621 12	34		1
RR32	H23516.75	621821.12	611508.16	621785.93	G .	-0-	*
R062	833526.39	821785/33	811570.13		18	0	
HOET	833424.63	82188E.81	#33,416.18	821812.72	18	0	1
F062	833,499.18	621613.12	83352436	821772.29	14.		- 3
出籍2	833524.38	821772.29	8335951	821652.62	34	0	- 1
MONA	633567.56	821687.02	831567A0		15	0	1
M094	813692-09	\$21644.05		021603.07	13	0	A
Ross	833009.34	\$21644.65 \$21605.64	813540.24		14		1
RIBS.	E33840.24	823 87 8 ST	£35691.67	621645.20	18	0	- 4
MOSS.	#33 681 67		823729.52		14	0	1
HORE.		621641.09			17	0	- 1
Rose.	#23.661.88		\$33646.83		12	0	1
HIST	#23644 AT	621583.56 621548.47			33	0	7
RIST FORE					17	4	4
mudit	833254.24		833345.60			- 1	4
4044	#33365.50	521650.64	833416.50	021000.01	12		4
8.19.6		521885.51			17	-6-	4
RIBS	E334E7.63	821841.0V	£33,533.4.3		17	10	4
FROM		621785.07			17	- 4	
more:	\$33,074.00		#33860;19		17	C. (4)	
ROEE	\$23.66G.16		£13712.58		- 32		
RIBS		621801.44			18	- 4	
FI089	633370.06	221046.97	833427.26		16	1.1	- 4
-9809	813427,36	621682.01	833419.60	021629.25	16	- 0	4
Aita9	833455.60	621829:25	851522.46	821786.30	- 18	- 10	14.
MORY	\$33522.46	821786.32	E11343.19	821725.A7	16		
HOME	83354I-19		932942.07	#21862.37	16		
HORK	\$33.64T.07	\$21633.37	132575.05		16		4
RIPS	823596.99	623594.64	613699.51	621509.91	16		4
ROSOVEOS1	833269.78	821629.64	811317.54	621634.10	97	0	- 1
R692+8491	633327.92	#21632.93	833449.56	821660.31	30	0	- 1
N092-R093	833449.56		432512.09		20	0	- 1
2004	633337,84	821034-55	855541.61	621670.41	- 10	-0-	- 1
Riss	833604.59	421501 TZ	613545.49	621548.43	42	0	- 1
R095+R397	433080.54		83401877	822414 27	10	0	-
1000-100	63402 N.77	922414.27	E34127.E2	822202.11	18	0	- 1
#100+R101	834127.62		STAZIEJI		18	0	- 1
1192+R103	834216.31	#22258:35		822190.58	18	0	1
194-R199	634309.95		#34907.66		48	0	1
R106	633917.63				18	0	1
R100		84240111	610H176	822287.53	10	0	
	133591.55	622384.04 622384.04	834890.39				- 1
R108	H2A090.84		8349134	822212.22	3,6	0	
Rise	E30181.08	\$2221E22	634273.65	822136.AE	47	0	1
WHE		422134.63			12	0	,
8111	E24363.46		834400.74		18	. 0	,
R112	E20646.78	622A05.79	#\$1902.96		18	-0-	-1
RIII		922334.17	3176(8/00	922271.35	48	. 0	- 1
R114	633,909,65	822271.56	655994.47	022201.23	(8	0	1
RIIS		\$22200.75			18	0	1
RITE		622131.94			16	0	1
RHI	834097.20		£3696.63		18	0	
RIFE			834245:29		- 19	0	9
RITE	874242.94	621993.85	634282.16 634389.17	821961.AS	- 19		1
R120	E3N281.93				- 38 1	0	- 1
#121	633768.03	92227 E. 66			16	0	- 4
R(22	633761.88	822351.52	633668.78		18.	-0	1
R122	\$22656,78		511954.75		19		1
R124	631671.62		\$25m4.66		10	0	- 1
8125	823 CR4-80	\$2738 4.07	#33#PE77	822172.05	18	0	- 1
R128	833093.40	8222FF 00	#33M637	822174,73	12	0	- 4
R127	823455.65	42231575	\$1350251	BEEDBAS	18	0	- 1
#128	\$33903.61	#22 27 B. 44	SENSON 16	822221.21	- 43	0	1
#128 #129	833377.60	822272.03	#10255.00	022203.72	16	0	-1
RIZE	623377.60	\$22232.03 \$22232.03	612316.00 612316.77		18	0	1
R110	623377,80 623396,42		813434.10		18	0	1
RISE	A33431.62	#22080.70	#23415.51	6 22 007 .0.7	- 18	0	- 1
RISS	823450.45		#33481.00		18	0	- 1
R134	E234E1.00	921952.76	932506.97	821982,08	18		- 1
ROS	833205.07	#22229.7%	#11X12.04	822178.01	78	0	-1
R116	833232.01		8.83Z42.30	922120.04	18	. 0	1
	833090.01	822182-63	682400.63	0.02120.4E	18	0	1
#117			815123.79	822672.01 T	18	0.	1
RESE	833100.63	447 173 06		-			
	833121.68	822072.03 822007.07	813198.56	621977.96	16	0	- 1

										Vah	iele count	for each o	and	_				_				_	
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hros	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
450	350	300	300	300	350	550	1505	2000	1900	1650	1500	1500	1500	1650	1650	1700	1950	1900	1450	1000	850	800	550
200	150	150	150	150	150	250	600	900	850	750	700	750	750	800	850	ESO .	1000	1000	500	558	450	400	390
250	200	150	150	150	200	300	750	1100	1050	900	800	850	B00	650	850	RSQ	950	900	700	500	400	350	250
750	200	150	150	150	150	300	700	1050	1000	#50	800	850	HOO	900	900	950	1100	1050	1100	652	500	450	300
150	150	100	100	100	100	200	450	750	650	600	550	550	550	550	550 550	600	650	650	500	150	300	250	300
150	100	100	100	100	100	200	450	700	650	550 550	500	550 550	500	550 550	550	600	650	650	500	150	300	250	200
150	100	100	100	100	100	200	450	700	650	550	500	550	500	550	550	600	650	650	500	350	300	250	300
300	250	200	200	700	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	350	480
300	250	200	200	200	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	950	400
300	250	200	200	200	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	.950	400
150	150	100	100	100	100	200	500	750	700	600	550	550	500	550	550	550	600	600	450	300	250	250	150
250 150	200 100	150	150	150	100	300	750 450	1150	1100	950	850	900	550	900	900	950 650	1050 750	750	900	550	450. 350	300	100
250	200	200	200	200	200	350	800	1250	1200	1090	960	1000	1000	1050	1100	1150	1300	1300	3000	700	600	550	200
200	700	150	150	150	150	300	650	1000	1000	850	750	-800	790	800	350	850	950	950	700	500	400	400	250
200	200	150	150	150	150	300	650	7000	1000	950	750	800	750	BOC	850	950	950	950	700	500	400	400	150
200	200	150	150	150	150	300	650	1000	1000	650	750	800	750	500	850	BS0	950	950	700	500	400	400	150
100	50	50	50	50	50	100	250	400	400	350	300	300	300	100	300	300	100	300	250	150	150	150	100
100	50	50		50	50	100	250	600	400	350	300	300	300	100	300	300	300	300	250	150	150	150	100
200	50 200	150	50 150	50 150	150	300	250 650	1000	400 950	350 850	300 750	800	750	300 850	300. 850	300 850	300 1000	950	750 750	150 500	150 450	400	10G 36G
200	200	150	150	150	150	300	650	1000	950	RSO	750	300	750	#50	850	RSO	1000	950	750	500	450	400	100
200	150	150	150	150	150	250	650	1000	950	800	750	750	750	800	300	800	900	900	650	450	400	350	250
200	150	150	150	150	150	250	650	1000	950	800	750	750	750	800	800	800	900	900	650	450	400	350	150
250	150	150	150	150	150	250	650	1000	950	800	750	750	750	600	300	800	900	900	650	450	400	350	250
100	50	50	50	50	50	100	250	400	400	350	300	300	300	300	300	300	350	350	250	200	150	150	100
100	100	100	100	100	100	150	350	500	500	450	400	400	400	400	400	400	400	450	350	200	200	190	150
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	2850	3150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850	600	400	400	650	3400	2950	3600	3600	3700	3100	2950	2890	3150	3250	3250	3600	3600	3200	2450	2500	2500	1960
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	2850	1150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	7250	3150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850 850	600	400	400	650	1400	2950 2950	3600	3600	3200 3200	3100	2950 2950	2890 2890	3150	3250 3250	3250 3250	3600	3800	3200	2450 2450	2500 2500	2600 2600	1950
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2990	2850	1150	3250	3250	3600	3600	3200	2450	2500	2600	1960
350	600	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	600	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	800	400	300	100	450	2600	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	500	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	Z500	2650	2750	2800	3450	3800	2900	2100	2250	2350	1750
850 850	600 600	400	300	300	450	1000	2100	2850 2850	2750	2400 2400	2400 2400	2350 2350	2300	2650 2650	2750 2750	2800 2800	3450 3450	3600	2900	2200	2250 2250	2350	1750
250	800	400	300	100	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3500	2900	7100	2250	2350	1750
850	600	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	1100	2250	2350	1750
350	250	250	250	250	250	-450	1050	1600	1500	1250	1100	1200	1100	1150	1150	1150	1300	1200	950	650	550	500	150
250	200	150	150	150	20G	350	750	1150	1150	950	900	900	850	90G	900	950	1000	1000	750	550	450	400	100
250 50	200 50	150 50	150 50	150 50	50	350	750 200	1150 300	1150 300	950	200	900 200	200	200	900	950	1000 750	1000	750	100	450 100	400	300
100	100	100	50	50	100	150	350	500	500	250 450	400	400	350	400	200 400	200 400	400	400	300	200	200	100	160
57	19	110	7	7	14	57	64	150	150	150	150	150	150	150	150	70	150	150	121	68	63	62	58
52	-56	25	17	70	78	8	150	300	300	300	250	250	250	500	250	200	250	300	250	700	150	150	73
100	100	73	34	40	100	150	300	800	650	550	500	550	500	550	550	350	500	500	450	250	250	250	150
1.00	36	22	16	16	26	100	150	250	300	250	250	300	300	300	300	250	350	356	250	200	200	150	100
71	27	16 24	11	20	19	50	100	300	300	300	20G 250	250	250	250 300	250	290	300	300 300	200	150	150	100	100 100
50	50	20	14	16	22	50	100	250	250	200	200	200	150	150	150	100	100	100	100	50	30	50	50
50	50	22	16	17	.50	30	150	250	300	250	200	200	200	200	200	150	200	200	150	100	100	100	50
50	50	21	15	16	24	50	100	250	250	250	200	200	- 200	200	150	100	150	100	100	50	50	- 50	50
103	50	50	20	- 21	50	100	150	350	350	300	250	250	250	250	200	150	150	150	150	100	100	50	50
50	50	23	17	18	58	90	100	300	300	250	250	200	200 250	300	300	150 750	150	150 450	350	250	200	200	150
50	20	12	8	9	15	50	50	150	150	150	150	150	100	150	100	100	100	100	100	30	50	50	30
200	100	50	50	50	100	200	450	850	950	850	750	750	700	800	750	550	700	750	550	400	350	300	250
200	100	50	50	50	.50	200	400	750	850	750	700	700	650	750	700	550	700	750	600	400	350	300	230
290	100	50	50	50	100	200	400	300	850	750	700	700	700	750	700	550	700	750	600	400	350	300	150
200	100	50	50	50	50	200	350	750	800 800	700	650 700	650 700	650 700	700 III00	750	500	650 800	700 850	700	500	400	350	300
200	100	50	50	50	100	250	450	900	950	#50	800	800	900	850	900	650	800	850	700	500	400	390	380
250	150	100	50	50	100	250	500	950	1050	950	900	900	850	950	900	700	900	950	750	500	450	4110	300
21	13	- 6	6	6	9	- 50	50	100	100	100	100	100	100	150	150	100	150	200	150	100	100	100	50
100	50	50	50	50	30	100	200	400	450	400	400	400	400	500	450	350	500	550	450	300	250	250	200
50	50	22	15	17	.50	50	150	250	300	250	250	250	750	300	300	200	300	350	250	200	150	150	100
50	50	20	14	16	23	50	100	250	250	250	200	200	200	200	200	150	150 200	150 290	150	100	100	50	50
50	90	22	15	16	15	50	150	250	300	250	250	300	300	350	350	300	400	450	350	750	700	200	150
50	23	15	10	12	16	50	100	150	200	200	200	200	200	250	250	200	250	300	250	150	150	100	100
50	50	18	. 14	15	21	50	100	700	250	250	250	250	250	300	300	250	350	400	300	200	200	250	150
150	100	100	100	100	100	200	400	650	600	500	450	500	450	500	500	500	600	\$50	450	500	250	250	150
200 300	190 250	200	206	200	150 250	400	900	(400	1300	700 1050	950 950	650 950	900	650 900	700 850	700 850	900	800 800	650	450	350 350	300	250 250
290	150	150	150	150	150	250	550	350	800	700	700	750	700	500	800	RSO.	1000	1000	750	950	450	400	100
200	100	50	50	50	100	200	350	750	800	750	700	700	700	500	750	500	600	850	700	500	400	350	500
200	100	100	50	50	100	200	400	800	900	850	800	850	H50	950	950	750	1000	1100	900	600	500	450	350
- (6	5	- 1	2	- 4		14	50	50	50	50	50	50	50	50	50	50	50	50	50	26	19	.14
6	4	3	1	1	3	7	13	50	50	50	50	50	-50	50	50	50	50	50	50	22	18	17	13
- 6	4	3	1	- 2	3	9	17	50 50	50 50	50	50	50	50 50	50 50	50	50 50	50	50	50	21	17	16.	13
100	50	50	24	50	50	100	200	400	450	400	400	450	450	550	550	400	500	650	500	150	300	750	200
100	50	50	50	50	50	100	200	450	450	450	450	500	500	600	600	500	650	750	600	400	350	300	250

Road		Coordi	nate (m)		Oncluding	Height	Road Typ
Pair	X1	Y1	X2	¥2	mixing room	(m)	(calline 4)
Rist	B30294.35	521947.25	885315.56	821691.57	13	0	1
B162	K13329.69	621853.67	\$10315.94	621691.04	13	0	7
R143	XXX129.75	621689.31	#33465.67	#21#34.07	- 13	0	- 1
TIME	XXX160.17	62183A.07	#33.978.74	821783.18	13	0	1
PUSTRIAL	H2381Z.49	621976.5%	\$34\$P458	621516.03	- 32	0	1
21127+2110	E33734-44	82188638	SELECTED S	821727.34	18	0	-1
R146	833728.61	821749.62	632607.73	821684.38	14	0.00	- A
R140	E33774,00	621643,62	832897.73	821684.38	13	0	1
RISO	833756.67	#21786-23	853687.71	821603.81		0-	- 1
R151	833612.61	821610.98	813663.50	821663.70	13	0	4.
R151	WINCEN.	021543.70	#3377628	#21842.83.	14	0	1
WH2	835774.08	621643.52	#138J#17	821500.58	20	٥	7
R193	833991.31	622300.76	634E/877	622454.27	78.	0	1
R194	\$33950.66	822530-65	#EXWIZ.CO	\$22189.07	18		1
RIN	633'009.40	102271.36	X33900.44	932130.45	16	0	4
#186	833688.78	622222.16	811909-01	8E.773.55	18		- 1
B197	E23866.58	6222223.54	61360777	622172.98	28	- 0	-
P153	833827.77	822172.95	215772.49	\$22113.30	18	0	
Ritte	634070.01	622299.62	E3AN1X#0	632384.34	18	0	- 1
Rico	834090.38	\$2228 F 63	E34527-62	6III32.11	15		- 1
8191	E34014 NO	#222350.52	834075.91	822299.62	15	0	1
R162	634049.42	822228.28	234000.14	822287.53	15	0	1
#163	E33993.00	62220186	X34534.00	032250.02	- 00	0	- 1
RIGA	834007.86	622194-31	#34/SANAT	0222M.20	15		1
R165	#33953.31	622151.78	#259/A47	622221 25	16	0	- 1
R158	833872.14	822651.39	82191476	822190.50	18	0	1
R167	633,683,47	822042.45	E34007.E8	822180.33	19	0	1
R163+R160	833813.72	\$21 97 E 47	EDWESS.	WEETOSD AT	29	. 0	1
2170-9171	833716.44	621 FR 8 15	#21812.49	AZIVERSO	18	0	1
R172-R173	#33864.92	821822.12	811719.26	821687.65	26	. 0	1
\$174×8.173	#33061,78	621407.56	£13M3.38	821623.58	18	0	1
ROL	833496.77	f21508.49	#1565.38 #1560.47	621680.73	20	0	1
_							
R177	8335410.44	#21529.74 #21529.70	EDSTAILS	621688.AT	16	0	1
						0	
.803	\$33451.04	42162E.31	83591173	821600:38	12		1
8190	E34218.31	622256.35	\$34X75.96	621585.59	18	0	1
R191	E24181.98	822211Z.ZZ	#3421831	822258-36	-18	0	1
R182	13A140.62	822162.47	834191.76	022212.3#	16	0	1
用4年2	#34099.34	622113.33	E34440/62	822162.67	18	10	1
R134	E34077.01	622132,66	#\$4851.51	622100.94	15	0	- 1
R162	SMOKE ST	E22100.94	834EF194	\$22094.18	13	. 0	- 1
H184	£34071.00	07208 s. 18	E34007.30	622115.02	14	0	1
RIES	634369-95	\$22180.58	E3439246	SEE287.44	10	0	, ,
8.96	E3#221.54	62236 A 63	EM27134	622136.83	19	0	- 1
RIAT	834190.59	822037.73	#362D176	622086.A5	- 9	0	- 1
R153+R159	834004.93	#21815-03	836HE34	\$21600.22	10	0	. 1
R190-R191	823921,12	921727,74	E34004.08	621816.03	19	0	1
H192-R193	633876.32	821660.78	#45KH0.65	621727.56	29	0	1
R394-R195	833825,79	621600.86	823B751	621631.AB	20	0	4
R395+R202	A33784.01	621323.35	A2300517	821690.58	20	0	7
E197	634364.00	822040.04	E3440E18	#12104.71	17	0	1
RISE	834322.77	822010.68	83439439	622060.94	18		- 1
R199	139 20 1.93	423161.17	E34323:00	BZZEIS:AB	-38	0	-1
R100	834239.47	#21914.12	834290.06	821983.18	148	9	1
#100	B34230,47	821914.13	#34327.69	021840.33	18	0	- 1

										Vet	ricle count	for each	road	-				-			_		
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	16	10	7	8	12	50	50	100	150	150	150	150	200	750	250	200	100	350	250	200	150	150	100
50	22	14	10	11	17	-5D	100	200	290	200	150	200	200	200	200	150	250	250	200	150	100	100	100
150	50	50	50	50	50	150	250	550	600	500	500	450	450	500	450	350	450	A50	350	250	200	- 200	130
100	50	50	50	50	30	100	250	450	500	450	400	400	400	450	400	300	400	400	300	200	200	150	130
24	13	- 8	. 5	7	10	25	63	100	150	124	122	123	322	174	172	117	222	. 224	168	113	11.1	110	. 58
-57	18	12	ä	9	13	58	65	150	150	150	150	150	150	150	150	100	200	200	100	100	100	100	100
17	- 9	5	4	4	7	-18	50	50	50	50	50	-50	90	50	50	50	50	- 50	22	16	13	12	9
17	9	5	- 4	4	2	118	50	50	50	50	. 50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	5	4	.4	7	- 10	50	50	50	50	50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	- 3	4	4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	25	16	13	12	10
17	9	- 5	4	- 4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	23	16	13	12	10
. 17	9	- 5	4	. 4.	7	18	50	50	50	50	50	50.	50	50	50.	50	50	50	50	.20	17	14	- 11
100	100	100	50	50	'50'	100	250	300	250	250	200	200	250	200	200	200	200	200	150	150	156	100	100
100	100	100	50	50	50	100	250	300	250	250	250	250	300	50G	300	350	350	350	300	250	200	200	150
100	100	50	50	50	50	100	250	300	250	250	200	200	250	200	200	250	250	200	200	150	150	150	100
500	400	350	300	250	250	450	100	800	800	100	800	800	100	800	900	800	800	750	650	550	450	450	350
600	500	400	300	250	300	550	1200	1500	1300	1,200	1100	1100	1150	1100	1050	1050	1050	1000	950	750	650	600	450
500	400	350	300	250	250	450	1000	1300	1100	1050	950	1000	1050	950	950	1000	1000	950	800	700	600	980	450
50	23	18	15	12	15	24	50	50	50	50	50	50	50	50	50	100	100	100	50	50	50	50	50
100	100	50	50	50	50	100	200	250	250	200	200	200	200	150	150	150	150	150	150	100	100	100	- 50
150	150	100	100	50	100	150	350	400	350	350	350	350	400	350	350	400	400	406	350	300	256	250	200
500	150	150	100	100	100	200	400	550	450	450	400	400	450	400	400	450	450	450	350	300	250	750	200
750	200	150	150	100	100	200	450	600	550	500	500	550	600	600	600	650	700	700	550	500	450	400	100
150	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	400	300	300	250	250	700
150	150	100	100	100	100	150	350	450	400	350	350	350	400	400	400	400	450	490	350	300	250	250	200
300	250	200	200	150	150	300	650	850	750	700	650	700	750	750	750	800	850	800	650	530	500	450	350
250	700	150	150	100	150	250	550	650	600	550	550	550	600	600	500	650	650	650	550	450	400	350	300
500	150	300	300	200	200	450	950	1200	1050	1050	1050	1100	1200	1200	1250	1350	1450	1350	1150	1000	850	800	600
150	350	300	250	200	200	400	900	1100	1050	950	950	1000	1150	1100	1150	1250	1300	1250	1050	900	750	750	550
500	400	350	250	250	250	450	1006	1300	1150	1100	1050	1100	1200	1200	1200	1300	1350	1350	1100	950	800	100	600
590	490	350	300	250	250	450	1050	1350	1200	1100	1050	1100	1200	1150	1150	1290	1300	1200	1050	900	750	750	550
350	300	250	200	150	200	300	750	900	800	700	650	700	700	650	650	650	650	650	500	450	400	350	300
250	200	200	150	100	150	250	550	700	600	680	550	600	650	650	-650	700	700	100	600	500	450	400	500
350	250	200	200	150	150	300	700	850	750	700	650	650	700	650	650	750°	650	650	550	#50	400	400	300
350	250	200	200	150	150	300	650	850	750	700	700	750	H00	600	900	900	950	900	750	650	550	950	460
200	150	150	100	100	100	200	400	500	450	400	400	400	400	400	400	400	400	400	300	100	250	250	200
15	12	9	ä	7	8	14	50	-50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	24
50	50	22	19	16	18	50	50	100	100	50	50	50	90	50	50	50	50	50	50	50	50	50	50
50	23	19	16	13	15	24	50	50	50	90	50	50	50	50	50	50	50	50	50	50	24	22	17
50	50	19	16	13	15	50	50	106	50	50	50	50	50	50	50	50	50	50	50	50	50	56	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
103	100	50	50		30					200		200		250		250							100
	19	15		50		20	200	250	200	50	200	50	250	50	250	50	50	250	200	200	22	150	17
22			12		12		50					200		200		150							50
1.00	100	50	- 50	50	50	100	200	250	200	200	200		200		150		150	150	150	100	100	100	
68	63	61	59	\$8	59	64	200	200	200	290	200	200	200	200	200	250	250	250	200	206	150	150	122
100	70	66	64	16	63	12	150	200	200	200	200	200	200	200	250	250	300	250	750	700	200	700	122
42	35	29	24	22	.13	38	100	100	100	100	100	100	100	73	73	70	68	.68	66	66	62	62	31
64	60	58	57	55	56	63	200	200	200	2/00	172	172	171	119	13.7	116	115	114	111	111	58	- 58	57
100	100	70	40	- 33	38	100	150	200	150	150	150	100	150	100	100	100	150	100	100	100	100	100	74
10	7	5	-5.	4	- 4	B.	18	24.	20	17	14	13	12	11	6	3	5	5.	- 4	- 4	3.	1	3
19	15	12	10	8	3	16.	50	50	50	50	:50	50	50	:50	22	23	18	18.	13	13	11.	-0	9
22	18	15	- 13	10	12	- 21	50	50	50	50	50	50	- 50	50	- 50	50	.23	20	18	15	13	12	10
50	50	23	20	1.6	19	50	50	106	100	50	50	50	50	50	50	50	50	50	50	50	50	-50	50
50	50	23	.20	16	19	50	50	100	100	50	50	50	50	50	50	50	50	50	50	30	50	50	50

Road		Coordin		- 02-	(including	Height	Road Type
Pair	X1	Y1	X2	Y2	mixing zone)	(m)	(caline 4)
R103	833125.78		133177.37	821530.25	28	0	1
R163		822330.25		6223A576	20	0	1
R003		822345.76 822408.45	E33414.80	822408.45	20	0	- 1
R003	833966.45		\$33905,46	821645.00	20	0	1
RIGA		822306.10		822315.62	19	0	1
R004		822315.62		822395.41	19	0	4.
R004	833425.15		833518.28	822421.55	19	0	1
Atos	833016.28			822496.58	19	0	1
R005	833671.75	822494.58	E11913.47	822414.65	19	0	1
RIGOS	633933.67	822614.88	W32973.71	822426.00	19	0	-
ROOS		822626.09		822626.54	19	0	-
005-R007	833527.80	622410.61	633637.55	822455.21	14	0	- 1
004-R007		822A55.21	811712-97	822494.A7	14	0	1
1005+R007	830732.97	822494.47	833782.11	822441.AB	14	0	4
1004-R007	833782.11	822441.65	813840.01	822456.02	14	0	1
003+R009	833661.17	622398.31		822197.15	15	0	- 1
503+R509	\$33693.50	822397.15	E11841.E	822456.38	13	0	- 1
010-R011	833978.15		832004.64	822452.88	12	0	1
010-R011	E33894.64	622432.88	933993.54	821462.AD	12	0	- 1
813+R\$11	8338E3.54	822A52.49	833840.51	822458.02	12	0	-
012+R013		822567.47		822556.02	10	0	1
012-R013	833423.69	822658.02	832416.08	822482.07	10	0	- 1
012+R013	833416.08		833447.62	022425.39	10	0	- 1
U+2+R9+3	E33447.62	822425.39	#1354464	627190 AB	10	0	- 4
\$12+H\$13	quantities.	822390.48	- and the same	822254.50	10	0	- 1
		822318.11			14	0	- 1
016+R017	833587.56		833633.17	022374.51	15	0	- 1
815+R\$17		822374.91	833661.17	822398.31	15	0	-
ROID			833209.07	822239.78	16	0	1
R021	833209.07	822220.76		822783.72	16	0	1
R622		522291.72			18	0	4
R022	8334E0.61	822340.13	833419-65	622315.75	16	0	- 1
PI023		822119.68		822129.44	19	0	9
W624		822129.44		822178.07	14		- 1
RH25		622178.57		622232.03	14	0	1
B128		822232.03			18	0	- 1
8027	633503.51	822278.46		822241.72	-13	0	4
8028		822341.72	833768.11	822375.93	13	0	- 1
R129	833766.63	822374.15	833843.76	821405.79	13	0	- 1
RISSIS	833848.76	822405.79	£13917.£3	822431.11	18	0	4.
H031	633917.63	822431.11		822454.38	14	0	- 1
037+R301			933121.79	822072.01	10	0	7
8833		622072.07	£13252.36	822120.94	18	0	1
R034	833253.39	822120.94	83339E77	822175.17	18	0	- 1
8935	833394.77	822175.17	#33524.35	822221.21	18	0	- 1
P034			#32913.40	022269.00	78	0	1
R637	633653.40	822269.00	833694.86	822284.07	19	0	- 1
RESE	633694.68	822284.56	833763.79	622109.61	10	0	- 4
ROSE	833761.98	822311.12	823788.45	822329.74	14	0	1
R040	833789.11	822318.08	833833.16	R22305.11	- 11	0	4
R041		822335.17	833902.96	822160.57	18	0	- 4
R342	833902.96	822360.57	633965,46	822320.A5	-18	0	- 1
R043	813950.46	822320.6E	834014.90	822250.52	12	0	1
R044	834034.90	822250.62	934140.62	812162.67	18	0	1
RIMS	834140.62	822162.67	834211.76	822086.45	19	0	1
RISAS	834211.72		834323.21	822011.22	18	0	- 1
ROAT	83A322.77	#22910.EE	834384.01	821959.48	- 18	0	- 1
H048	833097.20		833156.56		17	0	3
R549	833155.56	821977.96	833434.10	822580.78	16	0	1
R150	833101.47	821942 13	51327446	822007-01	21	0	1
R051			215416.70		16	0	1
R052	833434.10	822080.21	832668.33	822174.73	16	0	1
R153		\$22123,44		822163.25	18	0	1.
R153	833736.68	822161.25	811698.T3	822174.73	16	0	1
R054	823438.63	822067.29	#32516.71	822122.03	16	0	. 1
PI054		622122.03		822144.40	78	0	- 1
ROSA	833649.55	622144.43		822152.80	16	0	1
R254	633661.68		E13712.66		16	0	- 1
ROS4		822140.82			16	0	- 1
R084	635767.83	822128-66	833778.49	822113.30	16	0	1
R053	#337#4.53	\$22123.04	833872,14	822651.30	19	0	1
R256	833778.49	822113.30	8118h7.20	822039.12	16	0	7
ROST.	#33673.20	822012.66	034119.21	821B1478	16	0	1
ROSE	634159.21	821614.78	834210:10	821738.42	16	0	- 9
R059	833867.29	822039.23	63485E34	821680 22	-97	0	1
R065	83A056.34	821380.22	834241.E1	821727.AS	16	0	
R061	£3311£37	821890.28	833139.76	821889.31	16	0	1
R082	633139.76	821889.01	833216.78	821947.78	16	0	1
RINS	833256.88	821947.56	813410.51	821007.91	16	0	- 1
R064	833460.49	#2250E.03	#11543.73	822038.72	13	0	7.
FI064	833543.73	832034.72	¥33842.70	821983.31	15	0	- 1
R064	633480.98	821962-82	813543.70	821982.31	15	0	- 1
R085	833166.17	823834.07	613315.56	821691.67	36	0	- 1
R056	833316.56	321391.68	#33461.00	821952.78	16	0	- 1
R087	833164.01	821778.07	833178A7	821783.88	19	0	1
	833178.74		833253,69	821813.88	18	0	- 1
ROSE							
RIGHT		621757.87	813210.16	821795.91	29	0	1

											NO 40	0 (=0/147)											
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	NO _X x 10	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
15.1040	15.0973	15.7296	15.3577	14.9956	15.4356	15.6532	23.2742	25.1823	27.4099	20.9956	19.9406	18.4733	19.1157	18.7562	19.9913	21.8051	21.7257	21.0759	17.5127	15.0869	16.4832	16.5546	15.6712
15.1090	15.0973	15.7296	15.3672	14.9956	15.4356	15.6532	23.2742	25.1823	22.4099	20.9956	19.9406	18.4733	19.1157	18.7562	19.9913	21.8053	21.2257	21.0759	17.5127	15.0869	16.4832	16.5546	15.6712
15.1090	15.0973	15.7296	15.3672	14.9956	15.4356	15.6532	23.2742	25,1823	22.4099	20.9956	19.9406	18.4733	19,1157	18,7562	19.9913	21.8053	21.2257	21.0759	17,5127	15.0869	16.4832	16.5546	15.6712
15.1090	15.0973	15.7296	15.3672	14.9956	15.4356	15.6532	23.2742	25.1823	22.4099	20.9956	19.9406	18.4733	19.1157	18.7562	19.9913	21.8051	21.2257	21.0759	17.5127	15.0869	16.4832	16.5546	15.6712
15.0006	15.0973	15,7296	15.3672	14.9956	15.4356	15.6532	23.2742	25.1823	20.5132	20.9956	19.9406	18,4733	19.1157	18.7562	19.9913	21.9053	21.2257	22.0759	18.2195	14.2595	15.5972	16.5546	15.6712
15,0006	14.9683	15.7408	15.4122	14.9336	15.3678	15.4896	20.9354	23.3399	20.5132	19.5722	18.8839	17.7783	18.5841	18.3553	19.8333	22.0189	22.4108	22.2287	18.2195	14.2595	15.5972	15.9632	14.8088
15.0006	14.9683	15.7408	15.4122	14.9336	15.3678	15.4896	20.9354	23.3199	20.5132	19.5772	18.8839	17.7783	18.5841	18.3553	19.8333	22.0189	22.4108	22.2287	18.2195	14.2595	15.5972	15.9632	14.8088
14,9685	14.9232	15.7488	15.4234	14.9689	15.3854	15.5037	20.9327	23.3392	20.5100	19.5716	18.8787	17.7716	18.5750	18.3481	19.8242	22.0116	22,3894	22.2198	18.2106	14.2473	15.5847	15.9501	14.6121
14.9685	14.9232	15.7488	15.4234	14.9689	15.3854	15.5037	20.9327	23.3392	20.5100	19.5716	18.8787	17.7716	18.5750	18.3481	19.8242	22.0116	22.3894	22.2198	18.2106	14.2473	15.5847	15.9501	14.8121
14.9685	14.9232	15.7488 15.7488	15.4234	14.9689	15.3854	15.5037	20,9327	23.3392	20.5100	19.5716	18,8787	17.7716	18,5750	18.3481	19.8242	22.0116	22,3894	22.2198 22.2198	18.2106 18.2106	14.2473	15.5847	15,9501	14.8121
25.7896	24.1503	32.3286	14.7174	14.1789	29.3139	25.8782	27.6991	21.5453	28.9363	29.0531	28.3454	32.7216	25.8749	24.1391	24.3081	16.1371	15.3607	11.7557	14,9700	16.6354	26.4273	25.9174	17,7227
25.7896	24.1503	32.3286	14.7174	14.1789	29.3139	25.8782	27.6991	21.5453	28.9363	29.0531	28.3454	32.7216	25.8749	24.1391	24.3061	16,1371	15,3607	11.7557	14.9700	16.6354	26.4273	25.9174	17,7227
25.7896	24.1503	32.3286	14.7174	14.1789	29.3139	25.3782	27,6991	21.5453	28.9363	29.0531	28.3454	32.7216	25.8749	24.1391	24.3081	16-1371	15.3607	11.7557	14.9700	16.6354	26.4273	25.9174	17.7227
25.7856	24.1503	32.3286	14.7174	14.1789	29.3139	25.8782	27.6991	21.5453	28.9363	29.0531	28.3454	32.7216 24.8434	25.8749	24.1391	24.3081	16.1371	15.3607	11.7557	14.9700	16.6354	26.4273 27.5852	25.9174 27.5088	17.7227
19.7219	22.4506 22.4506	22.4294	14.7174	14.1789	20.5613	20.1438	24.0167	16.8557 16.8557	23.4172	23.1387	23.6334	24.0434	19.1496 19.1496	20.0732	21.9043	16.5813	15.3671 15.3671	12.1694	14.4618	16.7853 16.7853	27.5852	27.5088	16.4383
26.8695	26.2983	25.7596	23.5853	27.3556	31.5995	27.3746	31.4821	24.5117	31.2972	31.2244	32.6410	34.1369	29.5349	29.7757	32.7123	28-8756	76.5712	24.1932	25.7262	28.0130	36.7414	35.9709	28.7134
26.8695	26.2983	25.7596	23.5853	27.3556	31.5995	27.8746	31,4821	24.5117	31.2972	31.2244	82.6410	34.1359	29.5349	29.7757	32.7123	28.8756	25.5712	24.1932	25,7262	28.0130	36.7414	35.9209	28.7134
26.8695	26.2983	25.7596	Z3.5853	27.3556	32.5995	27.8746	31.4821	24.5117	31.2972	31.2244	32.6410	34.1369	29.5349	29.7757	32.7123	28.8756	26.5712	24.1932	25.7262	28.0130	36.7414	35.9209	28.7134
62.3569	69.8442 69.8442	21.4067	23.1071	22.5685	23.2148	63.4030	79.2996	58.7719	68.9398 68.9398	64,5650 64.5650	70.4799 70.4799	71.3567	77,6952 77,6952	68.4358 68.4358	71.7410	68.7151 68.7151	72.1948 72.1948	73.6985	69.8028 69.8028	88.4546 88.4546	100.6917	88,6001 88,6001	73.1435
62.3569	69.8442	21.4067	23.1071	22.5685	23.2146	63.4030	79.2996	58.7719	68.9398	64.5650	70.4799	71.3567	77.6952	68.4358	71.7410	68.7151	72.1948	73.6985	69.8028	88.4546	100.6917	88.6003	73.1435
62.3569	69.8442	21.4067	21.1071	22.5685	23.2148	63.4030	79.2996	58.7719	68.9398	64.5650	70.4799	71.3567	77.6952	68.4358	71.7410	68.7151	72.1948	73.6985	69.8028	88.4546	100.6917	88.6003	73.1435
62.3569	69.8442	21.4067	21.1071	22.5685	23.2148	63.4030	79.2996	58.7719	68.9398	64,5650	70.4799	71.3567	77.6952	68.4358	71.7410	68,7151	72.1948	73.6985	69.8028	88.4546	100,6917	88.6003	73.1435
37.4873	38.0506	41.4649	46.6301	44.0053	44.4012	39.4851	54.9206	33.7651	42.4143	44.2231	46.8452	48.1973	45.7623	43.8572	48.2600	44.8990	43.3762	40.2658	41.8781	47,2344	60.7682	59.7918	44.3688
37.6996	38.6461	41.4649	35.9378	34.1801	44.4012	37.8180	52.8613	32.3595	41.2526	41.6728	43.1057	44.3365	40.2998	40.0173	42.8963	36.2881	35.6550	32.6551	33.3544	39.8867 39.8867	51.4258	48.2296	37.8005
61.7745	63.5143	62.1633	65.7301	58.8703	62.7796	62.3485	72.7570	58.7489	67.1960	64.2491	68.1723	66.9755	68.0151	61.1342	67.1476	66.8563	59.3606	56.0856	57.3374	67.5943	83.5437	70.4121	66.2422
63.1987	63.2743	61.6058	66,6779	60.1888	68.2038	63.3908	73.3009	59.2978	67.6524	64.0794	68.1675	66.9784	67.7521	61,6577	67.8674	64.5430	60.2627	57.7332	57.0695	67.4926	80.8217	72.9431	62.0064
71.4554	67.9698	73.0900	73.4757	59.4605	72.9374	72.8808	79.5333	66.8371	75.1373	72.6275	75.6895	74.9131	75.2635	68.8776	73.8634	73.4419	66.7000	63.3723	63.4051	71.5165	84.2630	77.1765	69.7286
71.4554 68.4234	67.9698	73.0900	73.4757	69.4605 89.2896	72.9374 66.5110	72.8808 67.8028	79.5333 78.7806	67.2459	75.1373 74.8920	72.6275	75.6895 74.7896	74.9131 75.0961	75.2635 75.9146	68.8776	73.8634	73.4419	66.7000	63.3723	63.4051	71.5165	84.2630 84.1608	77.1765 75.7053	69.2286 66.9047
69.5721	65.5940	68.7864	65.8258	69.2896	69.2549	68.7294	77.5166	66.6502	75.067R	72.0362 72.0195	74.6540	72.6465	75.4313	68.7375	73.91b7 73.831E	72.6530	68.1259 68.2155	64.4312	62.5710	71.7223	83.1505	76.0743	67.0638
68.4635	68.2849	67,4132	70.5224	72.9677	67.7608	67,3604	76,6508	65.6692	75.8363	73.1144	75.9054	74.2197	74,6589	69.9023	75.1733	71.2771	69.3745	65.4527	63.2206	70,7939	84.9320	75.1779	66.6466
72.6327	72.8713	76.0421	76.3086	72.3856	71.3860	74.1437	82.6517	76.6595	81.8599	77.7412	80.0155	77.0966	78.5035	70.9159	76.1718	76.9538	71.1015	65.7117	64.3273	72.4479	82.0703	74.5320	67.3867
71.0789	69.9453	72.5863	71.1420	72.6301	73.8790	72.0535	81.2982	74.5529	82.2262	79:8179	81.9425	80.7632	80,8731	76.9234	79.1254	77.5632	73.1041	68.7796	66,8576	73.2505	86.6564	76.8623	68.8909
62.0695 59.7573	60.8555 56.2809	64.7532	69.9924 46.6301	57.4032	60.2067	G3.5879 59.4432	71.2668	63.1059	69.2212	63.3701	69.4698	68.7629 64.7397	58.8459 58.7902	61.7549	70.4703 67.7291	67.0552 69.5355	63.4554	61.5454	59.4376 58.7912	68.5138	82.2489 77.8274	74.3480 70.5733	62.1841 67.0903
58.9693	58.7512	62,2583	61.4248	56.5124	59.7429	59.8637	74.0032	61.5169	69.2438	63.9106	68,4196	69.8961	69.2960	63.3028	69.3983	66.8480	63.8036	60.3766	58.1013	66.7534	80.0117	70.4383	62.2283
56.1210	62.9823	52.1635	58.3916	57.4032	46.7552	61.2522	74,2047	64.5553	69.5082	64.9698	67.8708	64.9097	68,8361	61.0026	66,6472	67.6760	61.8389	58.1849	58.0761	67.4340	78.5353	70,4207	63.8823
63 1147	62.4226	57.2135	56.0717	\$4.4662	54.9964	56.3128	66.7968	55.3967	62.9404	60.0675	63.9578	62.9193	63.8882	58.2296	63.2550	61.4159	58.6294	55.9684	54,4255	63.1051	73.3987	66-1945	58.5068
56.4297	56.6353 54.2340	58.4826	57.8059	57.1865 54.4046	57.4197	57.4051	67.1416	54.2483 54.6880	60.3374	59.0849 57.6538	62.4835	60.6034	62.3054	58.1409	63.3231	61.3236	58.4311	55.6150 54.9891	54.1524	61.4615	73,7054	66.5269 65.8126	57.2000
59.8157	59.7144	55,3193 61,3161	55.7437 59.8405	59.0242	60.0292	55.1703	72.0254	61.3518	68.3079	65.4313	61.5303 67.4029	66.8049	61,2509 67,3183	57.1550 61.1169	68,3081	65.8951	57.9731 60.0514	56.8071	56.0346	63.0972	72.6009 75.6595	68.1327	56.7345
57.5856	57.3039	59.1130	58.6297	57.2627	58.8394	58.2031	69.2889	59.3916	67,4757	63.1076	56.6591	65.6151	96 5109	60.8332	56.0547	64.0265	61.1620	58.3901	56.8148	63.9441	74,4771	67.4317	59.5686
71.0984	71.0316	73.1162	72.5230	71.0059	72.1093	72.0475	84.4473	73.7056	81.5893	74.4776	77.6108	74.4014	76.1479	67.1076	71.6594	68.8527	64.1000	60.2274	58.4696	66.2604	78.1629	70.3119	61.5040
71.9575	71.9173	74.2525	73.0137	72.0804	73.0739	72,7708	85,6214	74.4588	82.6609	74,4394	77.1014	73.0768	73.9875	64.4480	68.5284	66.6386	59.5386	54.5637	53.4589	60.3433	71.9206	65,0966	56.9099
77.4377	75.0858 77.2360	77.6285	77.5456 79.1151	76.4343	77.2436	76,6375	90.5478	83.0031	87.2541 86.6977	80.7455 80.0017	83.4324 80.9151	78.8743	30,9878 78,5864	67.0410	76.5585	74.2587	63,5360	56.5399	56.4234	63.9864	75.5139	65.5088	62.8995
77.4471	75.6268	78.7066	77.9274	75.9713	78.1577	77.1036	92.5674	85.5124	89.2989	80.5886	83.2980	78.8867	90.8198	69.2521	76.4466	74.1389	63.6050	56.6720	56.6672	61.7912	75.8932	65.6947	63.0507
77,6343	76.4621	78.5405	77.7124	76.2059	78.2506	77,4880	90,5242	83.3762	87.1889	78.4871	81.1823	76.7083	78.8910	67.1717	76.1735	73.7804	62.8899	55.5930	55.7441	61.0008	73.5121	64.8528	62.2248
84.1298	84.6969	87.4303	86,0403	85,3899	86.4715	85.8762	95.8804	90.1625	92.5524	85.6849	88.9385	83.9461	87.7163	74.2959	82.9623	81,6783	70.7720	63.1115	63,2121	70,6780	81.3264	70.9390	70.3542
76.7642	76.8158	79.2920	79.0584	76.9879	78.3626	78.1811	90.0636	82.9692	86.5746	77.9772	80.9164	76.4254	78.4766	66.9722	74.1929	73.6324	62.9169	55.6467	55-5853	63.5674	73.1765	64.6092	61.6792
77.4091 78.0716	70.2328	72.8523	73.7134 78.3717	73.4657	78.1601	78.1771 79.4216	88.2804 90.8107	81.2775 84.0528	84.8372 87.6444	78.6665	81.4251 81.9681	77.0853	79.3771 79.5105	68:0141 68:2438	75.0882 75.0213	73.1145	63.8126	55.9049 56.7512	57.1929 56.7457	63.8318	74.3077	65.9729	63.3021
78.0322	75.8794	78.6844	78.1115	76.9288	77.8523	79.4756	90.9113	82.2363	85.6963	79.3875	82.1604	77.6520	79.6296	68.3342	75.2087	72.9158	63.8892	56.6811	56.7327	64.8545	73.9790	65.6070	63.0693
58 1320	57.2780	58.8130	58.1016	57.3166	58.2766	58.8677	70.6876	66.6785	69.6965	62.6434	65.5242	62,7424	66.4304	57.4771	64.2596	63.6979	57.9464	54,4966	51.7009	59.6.173	69.6016	60.9122	56.5942
58.1967	58.1863	59.8145	59.0357	58.2349	59.0377	58.9905	69.6914	64.1599	67.1577	60.4449	64.4608	61.7553	64.3540	55.6433	62.3129	61.8749	56.2842	52.2799	50.5550	59.8343	69.7026	61.0850	56.5819
64.6731	62.1357	65.6666	62.8643 65.8024	52.0009 64.8245	65,9111	65.6298	74.5755	70.2477	74,3934	66.0073 66.5879	69,2691 70.2830	65.5027 66.4678	58.2060 70.3864	59,5224 59,9108	65.2551	63,5019	57.8977 59.6401	53.9535	50.2584	56,2528 59,4095	65.0707 68.4125	56.5306 59.4414	52.7866 57.8394
64.1806	62.7415	64.3072	61.9469	62,9494	63.9532	64.7741	73.8187	69.0196	5K:8024	62.8125	66.5357	63.1259	66.9054	57.6535	65.5181	65.0135	57.2495	52.6647	51.5400	60.5751	70.1125	61.1489	58.9511
66.7377	65.5416	67.3437	66.5851	65.7672	66.7564	67.3629	76.8537	72.5167	73.9602	66.1285	70.1539	66.2762	71.1359	61.1809	68.8552	68.7956	61.8397	57.2628	55.6225	63.7476	73.1609	63.5129	61.1278
66.7377	65.5416	67.3437	66.5851	65.7672	66.7564	67.3629	76.8537	72.5167	73.9602	66.1235	70.1539	66.2762	71.1359	61.1809	68.8552	68.7956	61.8397	57.2628	55.6225	63,7476	73,1609	63.5129	61.1278
68.9590 68.9590	69.0838 69.0838	70.6397	70.1002 70.1002	69.2791	70.0820	69.8665 69.8665	78.9631 78.9631	74.0414	76.6774	70.1850	73.6314	71.0056 71.0056	75.9745 75.9745	65.4754	74.2072 74.2072	76.3940 76.3840	67.6280 67.6280	62.3531	60,9125	69.7430	78.6884 78.6884	67.4599 67.4599	67.3054 67.3054
68.9590	69.0838	70.6397	70.1002	69.2791	70.0820	69.3665	78.9631	74.0414	76.6774	70.1850	73.6314	71.0056	75.9745	65.4754	74.2072	76.5940	67.6280	62,3531	60.9125	69.7430	78.6884	67.4599	67.3054
68.9590	69.0838	70.6397	70.1002	69.2791	70.0E20	69.8665	78,9631	74.0414	75.6774	70.1850	73.6314	71.0056	75,9745	65.4754	74.2072	76.5940	67,6280	62.3531	60,9125	69,7430	78.6884	67.4599	67,3054
68.9590	69.0838	70.6397	70.1002	69,2791	70.0820	69.3665	78.9631	74.0414	76.6774	70.1850	73.6314	71.0056	75.9745	65.4754	74.2072	76.5940	67.6280	62.3531	60.9125	69.7430	78.6884	67.4599	67.3054
68.9590	69.0838	70.6397	70.1002	69.2791	70.0820	69.3665	78.9631	74.0414	76.6774	70.1850	73.6314	71.0056	75.9745	85.4754	74.2072	76.5840	67.6280	52.3531	60.9125	69.7430	78.6884	67.4599	67.3054
65.0262 74.1160	65.1341 74.0477	66.8077 76.1783	65.9451 75.2728	65.2273 74.2723	66.2266 75.6428	75.1183	74,7940 84,8554	68.1833 80.0020	71.1935 78.1882	64.7966 72.5952	67.3735 77.1102	63.6363 72.6212	67,5105 79,5894	57.6257 66.5080	64.8276 77.2775	79.5370	57,2017 66,9350	53,1954 59,8772	51.5736 61.4354	71.6955	70.1158	61.4234 67.5072	57.8677 70.6333
52.5125	50.4015	52.0793	52.0079	50.9809	51,9405	53.2057	62.0687	58.1885	56.0925	51.8659	54.3148	52.1121	53.1429	46.3118	55.0214	54.9458	46.5327	38.6388	41.0649	46.2725	53,6343	47.1966	48.2360
69.6300	67.8553	69.4685	69.2045	68.1M03	69.5054	70.5823	80.1489	74.8652	74.7646	67.5597	71.2477	66.7484	71.5233	59.9507	67.6940	67.5066	58.0088	53.0015	51.3855	62,7214	71,8841	62.3535	60.5368
58.3068	58.7390	60,0830	59.1601	58.8814	59.4163	59.2641	68,3890	65.2582	61.4470	57.6063	60.1893	57.1980	59.3797	50.9644	61.0545	61,7904	50.3852	41.5859	44,5894	50,4092	57.0467	49.5616	52.6607
71.7838 90.2510	71.5083 88.2149	74.4873	73.5556 88.0732	72.3995 81.6860	73.7174	73.2165	82.9603 91.7349	77.1370 88.6250	76.1133 92.4639	20,6905 91,9545	75.7032 92.9003	71.5640 92.6671	78.6005 93.4281	65.2971 90.7852	76.7956 92.9307	79.3388 92.2507	66.9466 89.3781	59.9120 88.2744	60,9748 87,3935	71.7997 89.0613	93.1634	67.1233 91.5947	70.7544 #7.3317
62.2388	61.0644	64.4236	61.8800	54.4638	64.3633	62.7196	72.0045	62.2376	69.1271	67.0078	70.6009	70.0406	70.4764	64.3927	70.1957	68.0583	63.8209	60.2492	59.1355	66.6779	79.4500	71.4767	64.8238
63.6137	57.9592	67.5918	65.1074	54.2084	61.0827	62.6928	73,8725	59.8644	67.7407	64.8792	68,2784	67.4452	68.4425	62.4006	67.4802	66.2938	60.8898	59.0444	57.5621	66.5258	79.7183	72.6684	63.9996
61.4086	55:1231	63.2580	64.0086	59,0931	59.7394	50,4893	72.5082	58.1182	66,2665	63.0794	67.7456	66.3998	57.0859	60.7634	66.8936	64,7473	59.1510	56.5231	57.0331	66,3468	79.6995	71.9104	64.7781
61.4086	55.1231	63.2580	64.0086	59.0931	59.7394	60,4893	72.5082	58.1182	66.2665	63.0794	67.7456	66.1998	67.0859	60.7634	66.8936	64.7473	59.1510	56.5231	57.0331	66.3468	79.6995	71.9104	64.7781
66.7112	55.1231 63.5999	63.2580 67.2807	64.0086 66.5635	59.0931 62.9879	59.7394 62.8634	67.5030	72.5082	58.1182 63.1207	70.9779	68.2940	67.7456 72.0193	66.3998 71.1430	70.8679	65.0788	69.5016	64,7473 68,5687	63.1112	56.5231	58.5249	66.3468	79.6995	71.9104	64.7781
64.6954	64.1725	65.7689	67.2669	54.0801	62.1348	65.5691	75.0252	61.7397	69.7718	66.9399	70.5462	69.1297	59.0086	64.7122	69.9332	65.8596	62.2650	58.4063	58.1693	65,6720	78.9721	71.1647	62.7964
42.2420	42.1772	42.8654	42,4320	41.9875	42.5886	42.8324	58.5914	47.E797	56.3753	52.2340	55.9549	53.6835	56.1556	49.2729	52.4144	50.3375	47.8104	47.3472	45.6081	47.4513	55.2192	48.5705	40.4040
41.9172	41.9843	42.7092	42.3344	41.8626	42.5589	42.5381	56.2087	47.6856	56.2309	52.0434	55.0593	53.5476	\$6.0229	49.1328	52.2847	50.2403	47.7210	47.2693	43.1982	46.4312	55.1821	48.5404	40.3406
34.8606	34,9882	35,6631	35.1596 56.0270	34.8336	35.3791	35,4060	43.0649	35.6764	63,9534	37.6955 58.6050	40.3418 61.5002	40.000Z	41,4541 51,4601	38.6794	41.6719 57.8286	40.4691	43,7133	44.6212	37,3381	43.0771	53.0791	47.0470 61.2709	37.3464 \$2.7626
35.3023	35.3935	30.8722	36.02/0	55.4626	30.4352	36.1446	65,4480	33.23/2	63.9534	38.0030	61.5002	39.2879	51.4601	54.8485	37.8486	36,3684	34.3946	93.0794	49,7735	57.4440	68.2360	61.2709	52.7626

Road Type (caline 4) Height 627160.31 52716.63 622716.89 622716.89 622717.36 622717.36 622717.36 622717.37 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 622718.47 | Control | Cont

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Road		Coordin	Coordinate (m)		MIGE	Helphi	Hoad Type			
Pair	×1	7.1	X2	Y2	(Including	(m)	(Calling 4)	Hroo	90	ŀ
R141	613/295.35	821547,25	833315.58	821891.67	13	0		71.9576	576	71
R142	833339.89	1821833.87	833318.93	\$2189158	- 43	0		44,0323	323	6
R143	833139.75	821886.31	13311017	621834.07	- 18	0	1	77.0038	820	77
H144	833165.17	621634.07	43341614	621753.15	13	0		75.4820	820	26
R145+R146	633812.49	821976.50	83400458	827816.03	- 47	a		68.8239	582	8
R147+R148	M-247443	821888.35	833921.13	82122128	1.6	a		60.1956	956	61
R149	833728.61	821748.53	833807.73	821684.38	14	0	1	55.1925	925	53
R145	633774.08	621643.52	833807.73	821684.36	13	0		\$5,1925	925	53
R15G	533736.67	821759.23	83366771	821601.87	. 11	0		55,1925	925	53
Rtst	623613.61	821619.98	833683.50	821543.73	- 11	0		55.1925	925	53
R151	133693.30	1121543.70	13377628	121547.53	14	0.	141	55,1925	526	53
R152	833774.08	621643.62	833826.17	821509.58	210	0		55,1925	925	S
R153	633991.31	872389.76	834018.77	\$22414.27	18	o		55.9427	427	5
RISA	823950.86	822339.A6	33399200	822368.87		9		55,6095	960	35
R155	833909.65	833371.38	133910.46	822330.AS	118	0		\$5.5513	513	128
R156	633868.78	672222.14	831908.85	822271.35	118	0		70.9826	826	13
B157	83388.58	#222228	833827.77	822172.95	. 83	0		73.7350	350	72
RTSB	E13827.77	822172.05	83377268	\$221535	22	0		709151	151	7
Ress	834075.91	872799.62	834112.90	822344.34	13	0		53.5410	410	2
RTBG	834090.29	621287 A3	03411762	822232 61	**	0		547776	776	12
RIES	634034.90	822259.53	834075.91	\$22.25W.62	18	0		54.2789	789	3
R162	834549.42	8222238.25	83409039	822287.53	18	0		60.1581	583	[8
R163	633593.96	823201.68	634034.50	822250.01	118	0		\$6.7542	542	57
H164	634707.86	62218133	53404842	82223828	100	0		57,9291	291	57
8165	613953.31	822151.70	83399447	822201.23	. 91			\$8.8092	092	3
R166	233872.14	822051.38	83396475	622160.50	18	0		48,6887	887	4
R167	133005.47	\$22042.45	834007,86	622109.33	18	0		73.3645	809	73
R168+R165	833613.72	521975,47	83387636	822050.03	21	0		26.0538	588	25
R170+R171		821883.35	67738128	#21976.53	- (18	a		35.8760	200	36
R172+R173		82182232	83377938	821867.65	20	.0		59,8247	247	8
H174-R175		821677.58	82589558	421123.55	91	0		61.6798	364	9
RETE	633498.77		833565.47	821686.73	2.6	0		56.7245	245	25
Retty	613513.09	_	83157148	\$21568.47	76			63.8067	290	2
R178	833440.44	821529.90	93348800	821608.61	. 91	0	-	62.2339	339	3
RITE	833451.64	121526.21	133111.02	621609,38	4	0		67,6156	156	9
8180	634218.31	\$2,256.35	634315.96	822286.33				640199	199	3
RIES	C34191.96	8227222	03421631	822256.35				62.5165	165	3
RTB2	834140.62	822162.67	634181.18	82227239	=	0		60.4482	482	8
2014	B-440000.04	200000000000000000000000000000000000000	2000000	10751070				60.0000		8 0
Read	E34061.51	822466.94	83497155	822084 13				68.8278	376	10
R184	834071.90	822084.18	834097.30	822118.02	14	0		68.8274	274	10
R105	834308.95	522160.58	83438286	822267.A4				62.6011	011	13
8186	634231.54	822096.63	83427334	H22136.83	18	a		68.7368	368	13
8187	234190.51	\$22037.73	83421176	\$22086.45	16	a		66,6277	277	3
R188+R189	834004.88	821816.03	83495834	821580.22	10	0		60.4703	203	59
R150-N191	633831.13	821727,74	834004.98	821816.03	- 18	0	. 1	64.6604	604	99
R162+R153	533 FF 52	821669.75	83191688	81727728	2.0			50.7	586	51
R154+R125	613838.79	621505.86	833867.51	\$21681.45	18	. 0		79,6996	966	77
R194-R202	835761.01	821523.38	933-828-17	821603.58	30	0		78.9195	195	2
16197	134344.36	\$22.0000, De	83440018	82210671	13	0	-	68.6322	322	2
R156	634322.77	89'010728	83438436	8727061.94	91			61.4051	051	29
R199	E34281.93	\$21981.17	93432200	822010.48	10	0		70,4308	308	2
N200	834239.17	821814.13	8342H004	621962.18	*	0		67.9981	1967	2
R 200	E3423E 17	521914.13	834317.03	821548 33	-	0				ì

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	Hr23	41 5906	55.4281	St.4858	40.8462	37.1856	68,6316	68.6316	68.6316	64:0070	64.0070	60,2231	48.5048	48 2360	48.9247	58.4820	58.7673	58.9645	59.7460	53,2604	\$8,5269	53 3135	52.4404	54,6142	57.0053	40.8148	66.1413	24:4212	33.1363	54,1809	60,6201	61.5305	54.3354	69.1873	62.2534	64 6959	63.9539	65.7956	39,7275	39.7275	39.7275	63.7663	65,7356	72.5062	62.2150	50,7249	82.3183	84.3535	68.6316	73.5518	64 5483	64.8483
	Hr22	500214	66.6856	66.1156	53.1103	48 9724	84.3855	84.3855	84.3855	84 3855	84.3855	76.8966	61.3527	926809	62.7471	73.6960	35255	71.0312	1599'89	64.6935	69.0436	64,7679	63.8462	66.4448	66.2430	49 1327	72,7122	33.0466	40.0199	64.6285	72.1705	69.5448	63.6265	77.9432	56.7769	79.1481	76.2070	73.4289	54.4273	54.4273	54.4273	75.7529	73.4289	82 2160	74.4328	49.9715	87,1049	82,3988	84.3710	71.9997	73.1301	73,1201
	1	42 9412	٠	70.5200	5,3223	49.5800	87.8563	87.8563	87,8563	87.8563	87.8563	25.3719	65,1463	65.1059	67.5200	78.2378	77,6140	76.2867	5.0491	71.5251	76.5494	71,4661	70.6930	3,2780	72,4024	50.9375	82.1125	15,0081	1,7286	70.9505	8.8050	76,0514	+	+	77.2170	86 2893	1	84,4339			56 5303	+	1	28 5177		2.8085	0.8021	86.2663	92.5297	80.3892	84.4235	0.7168
H	+	41.8634 4	78.5874	H	5160 5	39.2792 4	2750 8		73.2750 8	2750 8	73,2750 8	1562 8	9 \$695	7183 6	1762 6	3796	7 9756 7	64.6522	62.8373	58.1366	69.1361	58.0969	57.1857	59.9443	61.8621 7	3262 5	69.7240 8	25.1217	1686 4	58.5994 7	7 5262	61,6423	-	+	66.7471	20.8307	۰	۰	Н	+	6	+	+	76.1624 8	٠	50.4506 3	64.2995 9	9396 8	Н	72.6414	67.0538 3	Н
Н	+	+	₽	148 57	129	164 39	135 73	-	-	181 73.	-	77 054	192 51	179 51	179 53	111 56			188 62	1		-				184 41	-	Н	75 34	Н	135 67.	Н	+	+	+	t	٠	H	Н	+	+	1	+	+	+	02 50	167 64	188 77.	.23 62	+	+	H
	+	DE 4453	52.83	50.34	37.89	33.24	62.2435	Н	62,2435	£ 60.338	60.3381	17.72	43.7692	44.6479	44.9079	60.4411	3 59,4576	56.3252	52.83	48.4335	54,5803	48.6837	48.0171	50.2944	53,0181	37.93	60.8410	7 22.8424	31.97	50.6580	27.65	\$6,7954	+	+	57.4439	59 7574	t	H	Н		37,0942	+	+	69.1713	57.6937	41.82	3 78.61	72.64	5 52.85	\$6.0878	56.0705 1 58.4745	Н
	Hr18	36.9717	53.7560	52.2650	37,8990	32,730	65,6414	65.6414	65,6414	63.9277	63.9277	60,1274	44.2445	45,2567	45.6970	62.8955	62.0763	57.5980	54.0130	50,0195	55,7129	50.8688	49.9437	52,9190	53.8094	37,9730	60.9979	21,5247	31,4203	52,0217	60.9193	58,9492	51 2228	58,16.45	57.8985	62.8727	60.2326	57.4185	37,7748	37.7748	37,7748	61,483	55.3744	69.9129	59.3954	39.978	80.061	73396	46.8980	58.229	56,0751	59.7960
	HH17	39 5312	56.1373	54.8186	40.2676	35.8959	64.7977	64,7977	64,7977	63,4407	63.4407	61.3942	45.8858	47.0323	48.5333	67.6246	64.1076	58.8358	55.4447	51.6027	57,2469	52.3487	52,1072	53.8811	55.9548	41.6532	64.6310	25.0802	34.5703	53.9713	64.4343	61.0534	\$1.5849	69.0306	67 6154	64 7530	62.0470	57.6532	39.8111	39.8111	39.8111	62.9231	55.9295	72.0707	60.4801	44.1098	80.5645	R3.6932	4R.2934	60.5672	1806 69	62.2991
	Hr16	49,7649	59.1944	55.8694	40,2653	36.5168	66.4M36	66.4436	66,4436	61 5258	61 5258	60.7326	48.6166	49.0507	51.1443	70.2525	82,06.99	61 1954	58.0360	54.7054	59.4371	55.3640	54.4232	55.7297	58.8121	43.5095	72.2150	26.6079	36.0953	56.9423	66.4943	63.1894	57,2584	70,7772	65,4457	63 9291	64.0275	60.0833	42,7518	42,7518	42.7518	66.4853	57.0032	74.2323	64.4676	46.9622	81 9040	77.3961	60.1173	64.5604	64.0288	169979
Н	+	47 1230	7.6325	6.5202	3.3310	6.5487	2.3976	23976	62,3976	2.3976	62.3976	2,1023	3,1401	8,7708	54.4431	76.1512	72.4784	66 0682	8.9655	57,5579	61,7883	59.1593	57.9334		61.5039	8.2565	4.5029	29.5208	8.7924	9.8478	8.5500	1,8505		+	68.37.35	68 5360	t	33939	50.2873	4	502873	85516	1.2766	76.7381	8928	1.1203	3,0382	8 9664	9.1460	5.5796	50202	7,9390
	+	AA 96AR A	69.0382 6	66.0791 6	7293 5	47.0923 4	60.3453 6		60.3453 6.	5565 6	5935565	3758 6	50.1223 S	51 2431 5	51.4067 5	74.2539 7	71.3658 7.	65.0386 6	4306 5	54.8416 5	57.4120 6	55.9241 5	53.7583 5	7390 5	57.6169 6	46,0319 4	GR 5352 7	3822 24	7309 31	56.8876 54	9645 6	60.2338 6	58.0208	+	64.7518 6	S 9410 S	٠	63.2857 6	8460 5		49.4460 5	1240 6	5433 6	2 0986	62.0140 6	8913 5	80.8730 E	1681 7	8123	9432 6	63 1213 6	62.1813 6
Н	+	+	+	H	133 53		Н			21 59		21 57.		H	-				137 54		Н		-	56 54			Н	60 27.	37.		159 64		Н	+	+	٠	٠	H	46 49.			25 64	52 62	77 77	t	47.1	-	35 77.	87 59.1	19 18	+	H
_	+	0 46 2675	ŀ	ŀ	98.98	\$3.2585	5 63.0921		53.092	5 63.092	53.092	51.28	56.2765	55.9610	38.0363	79.7482	5 30,1715	73.0073	8 50.1937	8 53,1048	8 62,7855	62.5508		5 62.1556	52.7103	46.9706	78.6629	7,0560	-	62 9792	5 73.73	5 64.7357	+	+	71.6100	5915.09	t	⊦	36.3846	+	+	+	+	76.4844	H		34.1625	74.03	51.2787	3 72.80	70.1480	Н
NO _x x 100 (g/VMT	Hr12	49 6817	76.428	75.2247	62,660	57.2034	62.229	62,229.	62,229	62.2293	62.2293	60,9167	57,0464	58.1147	58.6610	N2.6982	79.8416	72.3304	59.3368	62,2438	61,7353	62 1902	59.9116	59,7846	62.8580	50,8124	76.4373	31,2237	42.2918	61.9990	69.349	63:6916	63.1894	70.2702	69.8723	69 1994	65.3838	69.0294	59,9359	59.9359	59,9359	67.3179	69.4726	76,2229	68.3734	55.9479	84,226	80,659	58.9327	65.2613	67.780	62.789
NO _x x 10	Hrtt	48.8847	82.1869	79.15KE	8956'99	60.6305	60.8414	60.8414	60.8414	60.8414	ED 8414	60.1935	58.2826	59.3318	59.6899	84,2203	82.2517	74.5985	60.8865	64.0595	62,4515	64.2816	61.6347	51.3407	63,7629	51.4452	79.6640	29.4517	41,1319	64,0099	70.7064	64,0924	65.5303	70.6293	71 76/17	65.7473	65 3411	693837	64.6789	64.6789	54.6789	69.1136	71.9224	76.6764	69.2048	55.8508	86.2084	74.9337	70.7943	64.8957	70.1285	70.2459
	HHO	48 1190	81.0473	77.6342	64.8332	59.8764	57.5427	57.5427	57.5427	57.5427	57,5427	57,0190	57.9347	57.6888	59.4298	82.6720	82,7789	74.4285	56.7151	60.8821	58.4857	60.9654	58,6437	57.9403	61.0665	50.4904	76.3426	28.7144	41.0989	60,8513	68.1338	60,6087	63.0834	66.8437	69.0104	62 0871	61.5431	66.7684	63,5130	63.5130	63.5130	64.5785	67.0654	72.8069	65.6442	52.2718	80.9972	72 5025	67.5338	61.0146	71.7562	66.7830
	+	48.0706	6.6877	83.5313	2.3861	66.3707	8:7730	S8.7730	58.7730	59.2433	59.2433	58.7730	62.4031	61.9970	64.0164	86,6834	1620'6	79.9487	8.K745	66.3333	69.9749	65.9171	63.1829	3.4960	63.3522	53,2323	82.3451	29.0670	2,1054	56,5683	1.3215	62.4055	+	15 (1945)	73 1616	164 3791	٠	70.8373	3.5152	3.5152	73,5152	7.6893	70.9517	73.8965	70.0020	4.8002	2.3967	6.8316	1.6155	3.9626	5.6795	6969
Н	+	40 9027	8961 8	2034 8	5166 7	9557 6	3954 S		47,3954 5	Н	47.8272 9	٠	51.0313 6	8124 6	8597 6	8644 8	80.9196 8	25	2910	-	51,7160 6	56.6187 6		53.5818 6	57.0009 6	0726 5	8544 E	2987	2113 4	4147 6	4455 7	8553 6	1	+	65.0296 7	54 2377 6	٠	7 3865 7	59.1454 7		59.1454 7		+	66.4046 7	+	2997 5	2015 8	9892 7	5280 7	9708 6	63 3409 7	7609
	+	+	H	356 72	278 58	133 53	734 47.	Н		Н	Н			828 50	381 53.	589 73	-		129 50.01		258 51	232 56	118 54		960 57.	396 46	512 76.	53.	529 36.	259 56	122 63	336 54	371 59	994 6L	53 818	+	t	178 61		+	+	579 58	176 63	160	969	335 47.	180 73	103 77.	154 59.	15 090	90 666	н
	+	48.0500	H	H	9 76.1	1 71.2	4 64.8		4 64.8714	1 64.5714	1 648714	4 64.8714	1 67.4483	2 67.5	0 69.198	3 910	4 93.3542	819563	62,4029	8 71,2843	299 5	5 710	2 68.3	6 67.4513	4 68.2	2 57.0	9 87.5612	3 31.7	7 41.7	3 70.4	0 75.0	2 67.1	1 724	4 72.5	3 78.3	4 71 1167	t	0 75.7			5 78.2957	8 72.6	78.1	78.5	5 75.3	8 \$8.5835	D SAA	7 80.6	7 73.8	7 70.2	76.0	76.6532
	HIOB	45,1219	77,5317	T7.4547	68,069	62.557	543164	8336	\$4,3164	56,155	56.1551	54.3364	57.090	57.4142	57.3820	72,2553	74,9434	71,9120	53.4829	61,3838	55,5305	61.0105	\$8.0022	58,7646	59.7534	49.4832	74.5799	26.5273	36.373	60,0243	62.3060	57.4532	64.512	65.5024	66 6363	+	H	65.9700	69.9485	69.9485	69.9485	61.5068	67.5192	68.4923	67.2455	\$2.0348	80,8320	80.531	58,7237	58.733	73,770	68.88
	Hr05	44 1111	79.8160	79.5689	65.5875	66.6740	63.5698	8698 89	63.5698	63.5698	83.5698	B695.E9	58.1240	56.9335	57,5050	1896 99	71.6750	725111	56.8086	61.451R	54.951B	61.0617	SR3150	59.0301	1608 65	48.8003	74.8032	26.0635	37.3583	60,5651	62.1230	57,9351	65.1247	63.1236	68.8089	58 5254	54,7261	73.3303	70.7956	70.2956	70,2956	63.7758	74.0889	60.7296	67.4599	51,4859	79.9588	75.8364	58.5254	54.6020	79.2648	70,7589
	Hrod	28.9941	75.9413	76.5855	32,2851	69.0148	57.4032	57.4032	57.4032	57.4032	57,4032	57.4032	56.9415	\$75900	56.2312	65.5278	70.2368	71.5210	51.0724	58.5388	55.1480	59.8429	56.7287	58.5597	57.7782	101674	74.2508	25,0390	36.4702	38.7466	60.6712	57.2334	63.3197	62.8537	57.6436 54 pheq	62 1796	68 6569	58.8703	65.4420	65,4420	65.4420	54.8059	77.2889	69.7458	67.6203	\$3.8508	\$1,9191	74.1566	57.4032	57.4032	14.9797	59,4404
	Hr03	42 5530	77.4200	78.3181	51.3347	76.0338	58 3916	58.3916	58,3916	58.3916	583916	58 3916	56.3799	56.8997	56.2478	069189	71.1928	72.3580	56.6751	61.3524	54.3166	9566 09	57.4141	58,2067	59,2059	48,7084	74.5879	27,2657	36.3534	60 2536	62.7593	57.9819	54,7600	63.3776	68,7005	58.3916	62.3865	70.0526	67.2127	67.2127	67,2127	63.9985	73,9397	69.8967	+	-	۰	75.0013	Н	+	79.1417	H
H		44.8767		-	77,1268		Н			Н	-	۰	57,5836	Н	-	-	74,4097	_	_	_	_	_	59.4762	_	59.6762	4904	5.4502	27,6443	7.9284			58.7642	. 7866.3	54.1402		3334	54 4247		Н	-	68,6806	-	+	-	899679	-	_	Н	-	+	50 7007	+
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Н		-		₽			\vdash	\neg	-	25 53.5327	-	-	-	Н	⊢	Н				_	_		1715.171	91 57.9	\$8.8092 \$8.6613	87 47.580B	73.7	26.0538 25.7097	00 36.2577	17 59.4	98 61.4	56.7245 56.7568	57 64.0	139 65	96 64 3305	8 57.4	12 60.1		74 67.1601		109179 14	\neg	-	77 68.7195				-	Н	-	05 70.5685 81 64.8700	+
Ш	PIO PI	4 0173	77.0028	75.4820	68.8339	50.1956	55.1925	55.1925	55,1925	55,1925	55,1925	55,1925	55.9427	55.6095	55.55	70.9826	73,7350	10 9151	53.5410	59,7776	54.2789	50.15	56.7582	57.92	58.80	18,68	73.36	26.05	35.8760	59.82	29.19	56.72	53.80	62.23.59	57.6136	5915 65	50.4482	65.3233	68.3274	58.8274	68.8274	62.6011	88.7368	56.6277	24.66	50,7586	36696	78.9195	68.6322	61.4051	57.0941	67.9921

| Califord Honey Control Months | Califord Honey | Market
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1116 17 17 17 17 17 17 17
H401 2.1350 2.1
HOO HOO HOO 1100 12890<

| High | Hard | Road Type (caline 4) Height Width (Including 2049 Q3 | Caline 4 input for 20049 | Read | Att |

| 1897 | 40077 | 11298 | 9.8564 | 11897 | 40077 | 11298 | 9.8564 | 11897 | 40077 | 11298 | 9.8564 | 11897 | 11297 | 11298 | 9.8564 | 11897 | 11299 | 11299 | 9.8564 | 11897 | 11299 | 11299 | 11299 | 9.4599 | 11299 | 11299 | 11299 | 9.4599 | 11299 | 11299 | 11299 | 11299 | 9.4599 | 11299 | 11299 | 11299 | 9.4599 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 11299 | 1129

	Coordi	nate (m)		Width	Height	Road Typ
X1	Y1	X2	Y2		(m)	(caline 4)
833295.35	821947.25	833315.54	821891.67	13	0	1
#33329.69	821353.67	E13315.96	821691.84	13	0	- 1
A33129.75	621689.31	833160.17	821834.07	- 11	. 0	1
833160.17	821834.07	933178.74	821783,15	13	0	1
833812.49	621976.58	85490458	821516.02	- 57	0	1
833738.44	821588.35	811931113	821727.34	16	0	7
833728.61	821749.52	833807.73	821684.38	14	0	4.
833T74.08	821643.52	833807.73	821684.38	13	0	1
833734.67	821759.23	813607.71	821603.87	- 0 -	0	- 4
833613.61	821610.98	E11493.50	821543.70	13	0	4.
833493.50	821543.70	W3577526	821642.63	14	0	1
833774.08	621643.52	833826.17	821600.58	- 20	0	7
833991.31	622369.76	634528.77	822414.27	18	0	1
233060.46	822320-45	#33992-00	822399.67	18	. 0	1
833909.65	822271.36	833900.44	822320.45	18	0	4
833048.78	822222.16	813509.65	822271.36	18	0	- 1
833066.58	622222.34	88380777	822172.95	- 19	0	- 1
200 00 1777		144-040-0			_	1.
	822299.62	83411230	822284.34		0	1
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533825,79	621500.86	833867.61	621651.48	20	0	1
	#21523.1K	813826.17	821699.58	20	0	1
A33761.01	-					
814264.26	822000.94	834400.15	#22104.71	17	0	1
834384.36 834322.77	822010.68	83436436	822960.94	18	0	- 4
814264.26						
	833295.35 833129.75 833139.75 833139.75 833146.17 833712.40 833774.08 833774.08 833774.08 833774.08 833774.08 833965.31 833965.31 833965.46	X1	1922-1935 1934-26	X7	X2	X1

											NO ₂ x 10	0 (g/VMT)			-								
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
12.9662	12.8034	10.7520	10.2060	12.8332	14.1910	12.9621	16.2635	11.6598	15.0103	12.2684	13.3308	11.4018	12.7781	9.3973	9.4091	7.2447	7.5395	7.7774	6.7087	9.6113	12.0288	9.7430	7.5160
6.3318	5.1567	5.9654	4.9525	4.4656	5.7836	6.3951	7.1790	5.5687	7.0483	6.6848	7.3410	7.0780	7.6134	6.5670	7.2291	6.9497	6.3730	6.2022	5.9494	7.1850	3.9947	7.6795	6.8295
14.7979	14.7673	14.7609	14.7814	14.4992	15.4046	14.7837	16.9032	13.9096	16.8157	14.6991	15.5177	13,4746	14.7295	11.7709	11.4548	9.9961	9.6184	9.5760	8.5614	10.8486	13.0365	11.0715	9.3178
14.5855	14.5281	14.5635	14.8591	14.5098	15.2891	14.6477	16.7185	13.0233	16.1036	13.9036	14.8145	13.0272	14.3@9	11.1191	11.1003	9.2434	9.2366	9.1763	8.0193	10.5571	12.7604	10.8401	9.0075
11.5381	10.7725	13.0904	7.5554	14.4734	10.6584	11.2399	13.2017	8.6181	12.4223	9.8732	11.0074	9.2109	10.1590	7.4601	7.2505	5.0645	5.6010	5.4940	4.6804	6.3730	3.0230	6.8749	5.4063
9.6414	9,8566	11.7913	12.9670	11.5575	10.8965	10.0313	12.0238	7.8262	11.0444	8.8535	9.5677	6.0393	8,7030	6.2021	5.9914	4.3289	4.7988	4.4046	3.7864	5.5422	5.3564	5,7573	4.6009
8.5407	8.1556	7.6342	9.1015	9,0061	10.2163	8.2232	10,4888	6.6865	9.3037	8.3733	9.6157	9.1184	11.0401	8.9274	9.1636	10.1994	10.4742	11.8007	9.8690	14.2660	17.4660	15.3215	11.5173
8.5407	8.1556	7.6342	9.1015	9.0061	10.2163	16.2232	10.4888	6.6865	9.3037	8.373.1	9.6157	9.1184	11.0401	8.9274	9.1636	10.1994	10.4742	11.8007	9.8690	14.2660	17.4660	15.3215	11,5173
B.5407	8.1556	7.6342	9.1015	9.0061	10.2163	8.2232	10.4888	6.6865	9.1037	8.3733	9.6157	9.1184	11.0401	8.9274	9.1636	10.1994	10.4742	11.8007	9.8690	14.2660	17.4660	15.3215	11.5173
8.5407	8.1556	7.6342	9.1015	9.0061	10.2163	8.6265	10.4888	6.7615	9.4115	8.3733	9.6157	9.1184	11.0401	8.7652	9.1636	9.2349	10.2078	11.4147	9.4693	14.2660	17.4660	15.3215	10.5001
8.5407	8.1556	7.6342	9.1015	9.0061	10.2163	8.6265	10.4888	6.7615	9.4115	6.3733	9.6157	9.1184	11.0401	8.7652	9.1636	9.2349	10.2078	11.4147	9,4693	14.2660	17.4660	15.3215	10.5001
8.5407	8.1556	7.6342	9.1015	9.0061	10.2163	R.2232	10.4888	6.6865	9.3037	8.2656	9.4683	8.8366	10.6099	8.3168	9.1045	9.0793	9.8060	10.5608	8.9323	13.7218	16.7447	13.2991	9.6678
9.0633	9.2545	9.1081	8.9968	9.3002	9.3761	9.2415	11,3155	7.8817	10.4075	8.7358	9.3193	8.2986	9.5648	7.0166	7.5850	7.0027	6.8669	7.0604	6.1022	8.7632	10.9544	9.1860	7.3206
8.9993	9.3368	8.8979	9.1159	9,4501	9.1270	9.3165	11.3552	7.8569	10.3044	8.6552	9.3984	8.3487	9,4307	7.0861	7.5233	6.8907	6.9783	7.1691	6.1426	8.7902	10.9110	9,0298	7.1708
8.9995	93511	9.1034	8.9898	9.1673	9.2584	9.3258	11.6264	8.2917	10.6693	8.9463	9.5209	8.5184	9.8609	7.1673	7.7309	7.2949	7.2235	7.2893	6.2317	9.0617	11.4274	9.3661	73925
12.6983	12.3103	12.3979	12.1956	11.7556	11 9945	12.8537	16.6265	12.8652	15.7061	13.9261	14.8870	13.5951	14.6936	12.0034	12.2293	11.2986	11.3154	11.0788	9.6396	12.0885	13.9470	11.9536	9.7715
11.2512	12.9766	13.2834	12.7695	12.7148	12.8670	13.3843	17.1463	13.5495	16.1804	13.9461	14.6069	13.1641	14.8505	11.5502	11.6374	10.7901	10.7326	11.0091	9.5635	12.2400	14.2341	12.0599	9.8549
13.1397	13.2203	13.4647	13.3051	13.2992	13.3133	13.2270	15.4929	11.9105	14.9610	12.9444	13.6444	12.3031	13.8764	10.8162	10.8596	10.0698	10.0194	10.4186	9,2333	12.2842	14.4573	12.1976	10.0623
9.4174	9.5484	10.6549	10.5473	8.1948	10.5587	9.3877	11.2213	8.8836	10.7816	9.7292	11.1594	10.000%	11.7035	9.0188	10.0408	10.4370	10.0059	10.2728	9.1220	12.8592	15.0986	12.4017	11.1153
11.0481	10.9908	11.2143	11.3633	10.5496	11.4166	11.5172	13.5124	10.2280	12.4759	10.4522	11.6904	10.4887	12/3122	9,0841	9.6726	9,4205	8.9574	9.1779	7.9895	11.4696	13.9935	11.2339	9.2356
9.5880	9.5571	9.7827	9.4268	9.8321	9.5881	9.8508	11,9381	8.9712	10.9130	9,7101	11.1275	10.2092	12.0993	9.4484	10.4520	10.4080	10.1812	10.4326	9.3097	12.7287	15.4105	12.3594	10.6102
11.1447	11.1108	11.2359	11.1553	10.9588	11.1918	11.2512	13,4313	10.2536	12.3762	10.4915	11.7713	10.4823	12.1324	9.1395	9.8954	9.3959	8,9543	9.1785	7.9656	11.3592	13.9879	11.2125	9.2381
10.4253	10.5621	10.9033	10.44K3	10.4110 10.5824	10.6804	10.6415	12.8878 12.4621	9.2267	11.8771	9.6694	11.2609	9.8021	11.6745	8.7947 8.8503	9.8554 9.3458	9.4416	9.2162	9.6536	7.8404 8.3025	11.1054	13.6487	10.8339	9.2170
11.6187	11.5400	11.5633	11.5166	11.2538	11.6992	11.7570	13.5112	11.5135	12.4740	11.4449	12.3234	11.4170	12.6992	10.3013	11.1735	10.9128	10.4447	10.3939	9.4814	12.6187	14.5212	11.6342	10.7351
8.7747	8.5230	8.8020	8.7287	8.6522	8.7358	8.8764	10.1318	8.4921	9.4679	8.7288	8.9874	8.3544	8.2444	7.4886	7.8792	7.1302	7.1610	6.4542	5.9555	6.8372	7.8372	7.0391	6.5948
15.8156	15.8808	16.1223	16.0332	16.0519	16.0815	16.046K	19.1606	16.9707	17.8347	15.5487	16.8668	15.1991	17.4448	13.3190	15.0593	15.0727	13.0454	17.4902	11.8117	15.2523	17.6287	13.9979	13.5359
3.3531	3.3245	3.5635	3.5709	3.2244	3.3521	3.3722	4.1661	33677	3.8010	1.5866	3.7577	3.7178	3.6351	3.2643	3.7220	3.4210	3:4822	2.9060	2.6992	3.1986	4.0846	3.4428	3.0572
4.8732	4.8918	5.1214	4.8753	4.8948	5.0250	4.9133	5.9434	4.7830	5.9452	5.4423	5.7435	5.5514	5.8236	4.9145	5.1332	4.8269	4.7961	4.6080	4.1656	5.0704	5.1054	5.2506	4.5580
10.9034	10.7868	10.9926	10.8995	10.6180	10.9816	10.8431	13.1124	9.7975	12.2361	10.3819	11.6114	10.4023	12.1371	9.4146	10.0968	9.8487	9.5308	9.5908	8.5272	11.4978	13.7498	11.1868	9.5958
11.5700	11.5737	11.7991	11.7308	11.4752	11.7485	11.7012	14.3302	11.6822	13.5067	12.1418	13.2671	12.1582	14.2144	11.2948	12.1159	12.0661	11.8009	11.6753	10.5525	13.6510	15.9147	13.1917	11.3358
10.7852	10.7654	11.0583	10.9659	10.8865	10.9074	10.8648	12.9364	10.6620	12.0085	11.1160	12.2910	11.5522	13.1778	10.9979	12.1644	12.2315	11.9287	11.8496	10.7796	13.5925	15.7613	13.1838	12.3043
12.0991	12.1273	12.3977	12.1893	11.9220	12.2775	12.1399	14.0130	10.8212	13.0579	11.3351	12.3736	11.1272	12.7672	10.0601	10.6960	10.3771	9.8264	9.6729	8.7135	11.4224	13.5890	11.2008	9.9530
12.5390	12.4577	12.7328	12.6760	12.6592	12.5744	12.7618	14.6806	12.7287	13.8003	12.9217	14.2237	13.4107	15.3519	12.8737	13.9875	13.9905	13.7329	14.0935	12.7557	16.0226	18.4114	15.6605	13.9821
13.5000	13.4501	13.7777	13.6442	13.4861	13.6102	13.6249	15.8920	12.7662	14.7801	13.0903	14.4324	13.0922	15.1365	11.8814	13.1861	13.1951	12.0219	11.6734	10.9150	14.2480	16.1875	13.1459	12.4517
11.3491	11.4538	11.9273	11.7154	11.5811	12.4222	11.6872	13.9636	10.8487	13.2667	11.2704	12.7635	11.6141	13.6909	10.5333	11.6144	11.3012	10.9838	11.1910	9.9651	13.8682	16.9348	13.5160	11.4206
11.5672	9.0061	8.3271	9.1015	10.0996	9.1109	12,4405	12.6848	8.8549	11.4267	9.9901	11.3453	11.7502	13.5279	10.4423	11.6832	11.0113	11.6847	11.9656	10.1784	14.3761	17.6173	14.5556	11.5334
10.2877	10.3608	11.2711	11.0549	12.7444	11.5207	10.5752	12.2868	93418	10.9510	9.8683	11.2812	10.4396	13.1991	9.3991	10.5592	11.0709	10.7460	11.0597	9.3129	13:5475	17.4867	13.5268	11.1347
11.5557	12.0229	12.9453	13.0190	13.1660	13.8110	11.6831	13.8459	10.6510	12.7583	11.1300	12.4105	11.4771	13.3129	10.4478	10.0558	9.7318	9.6597	10.3265	9.4665	13.6108	16.8893	12.8343	12.1383
11.5395	11.1507	11.2443	11.0343	10.7725	11.6901	11.6527	13.7245	8.7277	12.6815	9.6017	10.4888	8.6261	9.4460	6.6864	6.7392	5.5517	5.5673	5.5384	4.5935	6.6487	8,3735	7.2305	5.1597
11.5395	11.1507	11.2443	11.0343	10.7725	11.6901	11.6527	13.7245	8.7277	12.6815	9.6017	10.4888	8.6261	9,4460	6.6864	6.7392	5.5517	5.5673	5.5384	4.5935	6.6487	8.3735	7.2305	5.1597
11.5395	11.1507	11.2443	11.0343	10,7725	11.6901	11.6527	13,7245	8.7277	12.6815	9.6017	10.4888	8.6261	9,4460	6.6864	6,7392	5.5517	5,5673	5.5384	4.5935	6.6487	3.3735	7.2305	5.1597
11.0374	10.9397	11.6837	11.1381	11.5811	11.1188	11.4559	13.1964	10.1040	12.1791	10.8047	12.4134	11.1137	13.4991	10.5000	11.5262	11.6468	11.0515	11.4194	9.9958	13.9205	16.5434	13.4647	11.3599
12.4844	12.6581	13.9458	14.3249	15.3140	14.3413	12.2037	14.6041	11.4930	12.9757	11.3862	13.1796	11.7257	13.5279	10.4360	9.7284	9.2120	9.3539	9.8885	9,0894	12.9339	15.9099	12.8343	12.1383
12,4472	13.0317	12.7239	13.1671	13.3928	13.1725	12.8330	15.0330	12.3899	14.0309	13.2655	14,7225	13.8536	15.4672	13.1580	14.3453	14,1860	13.9510	14.0651	13.0989	16.0722	18.5029	15.8323	14.1963
10.5820	10.1436	11.1602	11.7050	10.5516	10.5199	10.7517	12.3647	9.1309	11.3080	9.8545	11.0054	10.2437	11.5984	9.0442	9.6171	9,5980	9.2916	9.4357	8.1407	11.5369	13.4610	11.1040	9.8243
11.4488	12.0671	11.9184	12.1538	12.4357	12.0581	11.9885	13.9427	10.6800	12.6744	10.9503	12.3329	11.3228	13/3080	10.1112	11.0883	11.0978	10.4317	10.8876	9.5619	13.4512	16.0774	13.1028	10.5601
8.7041	8.5353	8.7153	9.2415	9.5540	8.7226	8.5096	9.7983	7.2857	8.8815	7.9570	9.2056	8.5279	10.20H7	7.0738	7.8427	7.2787	6.7596	6.3246	6.2140	9.5837	3.9886	7.5703	8.8455
16.5447	15.6397	16.4402	17.1909	17.0557	16.4346	16.5542	17.2252	14.6566	16.9099	16,1108	18.0424	17.0037	17.9179	16,3238	16.9837	17.6484	16.9898	17.3018	16,5442	18.5823	19.6622	18.1315	17.6563
16.7023	17.0989	14.1738	15.5111	15,4482	15.6800	17.1464	16.7154	16,7003	15.8590	14.1819	15.0716	16.4374	15,4527	15.7751	16.2460	16.1838	18.2780	15.7803	15.1323	17.0832	18.6503	17,0324	18.6741
11.6200	10.0996	7.6342	7.5554	9.0061	9.1109	9.0802	13.8046	10.3456	13.2812	11.7915	13.3693	N.4098	10.6085	8.8168	8.5119	8:9576	7.2327	7.5875	7.8990	11.5453	18.8209	15.3158	11.5173
11.0247	9.5164	9.1931	7.5554	9:0061	8.2512	9.0802	12.3306	8.2571	11.0241	9.7499	11.2109	10.4885	14.6950	10.0801	11.0906	11.3516	10.8844	10.9030	9,7954	15,1511	16.2077	12.9199	14.5509
13.5453	13.7298	14.2988	16.0479	15.5994	16.0390	14.2064	15.3845	12.7767	14.7049	13.2956	13.1217	12.6151	13.9026	10.8449	11.5863	11,5707	13,3141	13.0096	12,4895	14.6853	17.2735	13.1910	12.7003
12.4722	11.5079	12.4538	12.3259	12.8792	12.8840	12.6198	14.3436	11.3597	13.8718	11.1687	12.6649	11.1821	13.5005	10.1733	11.6910	11,7479	11.0590	11.0428	9.8727	13.1478	15.8268	12.6870	11.5635
12.4722	11.5079	12.4538	12.3259	12.8792	12.8840	12.5198	14,3436	11.3597	13.8718	11.1687	12.6649	11.1821	13.5005	10.1733	11.6910	11.7479	11.0590	11.0428	9.8727	13.1478	15.8268	12.6870	11.5635

Road	X1	Coordin Y1	X2	¥2	including	Height (m)	Road Type (caline 4)
RIDI		52224.51		820 Da 25	mixing room	0	1
RIGI	833177.37	£22334.28	#EXZ0106	622345.38	29	0	1
R003	633231.00	02234578	#33414.E0	#25406.45	20	0	1
. H003	633434.00	622468-45	#33909.49	811043.00	- 76	0	- 1
RIGO		622643.00			29	0	1
RIDA		#22306.10			19	0	-1
F1004	633166.03	822315.62	63342516	622286.41	39	- O.	- 4
R004	833425.10	622386:41	032518.26	022421.58	19		1.
RIDE	833616.28	£22,421,55	853673.75	622496.58	39	0.	
R003	\$33671.75	822.450 SE	833953.47	822414.65	16	0	4.
HOOR	633933.67	022014.60	#33973.71		19	0	1
Meas		622625.09	PHONESS	422478 SA	18	٥	-
005-R807	823527.00		633/637.54	622455.21	54	0	1
dos-8407	833627.66		811712-67	477494 AT	16	. 0	1
	633732.07	827494.47			14	0	1
MO6-8407			#1079244	942441.05	34	-	1
1004-1107	833782.11	622441,65	811840.01	822456.02			1
1003-R105	123661 17				13	- 0	- 1
hard + Kobi	\$33693.50	822397.65	813841.E		13	0	- 1
	633976.40				(1	0	1
1010×4011		122432:88	832883,54		12	. 0	- 3
R81>-R611	\$33681'2t	822A5 E 49	813662.51	822458-02	12	0	
	633387.26		833423.59		16	0	1
1012-R013	E33423.09	\$22659.02	E55416/4	012462.07	10	0	1
W12+R612	633416.08	\$22,482.07	#21417A2	022425.39	10		1
物でを用される	\$33A47.62		CDSM64	622.000.A3	10	0	1
1012+FI015	833544.64	822390.48	813967.E6	822354.60	16	0	- 1
1014-H014	6334ES.77	92251E11	#32867.6W	X22354.80	14	. 0	1
9814-R817	833587,56	\$22354:m	#2561217	022374-91	15	. 0	1
W15+9W17		822374.91			15	0	1
Rose	#330k2.67		811219.07		18		1
8621	#30309.01		#13305.00		16	0	1
R102	RIDGES IN	622291.72	#15410.E.	ADDISON AT	18	0	1
	E334E0.61		STREET		16	0	-
RN22 R023	R33AEC.N1	422119.68	STREET	642216.75	19	0	1
MO23					14		1
		622129.64					
R825		622176.ST			74	0	1
Rt28		#22232.65			- 18	0	. 1
R027	633503.91	922278-46	BMM*X82	022241.72	13	0	1
8024		622341.52			13	0	1
R129	B33766.03	£22374.16	#8164E76	622405.73	15	-0-	- 1
R010	\$33848.76	E22405.79	#EX917.E3	\$22431.11	18	0	- 4
H421	633917.63	972431.14	#30900.88	0.12 454 AR	14	0	. 1
1017/1101	89.910CE9	\$22555.71	#35 U.S. F.	\$22072.07	18	0	7
8633	830121.79	622072.07	##125119	622120.94	78	0	
MO34	633251.79	822120.94	##S9HE77	622175.17	- 0	0	- 1
Ridge	633396.77	#22175.47	83352435		12	0	1
M034			633963.40		18	0	- 1
9627	613653.40	62229-0,00		622284.07	- 15	. 0	- 1
RESE	B22664.58	422284.56	613762.79	622339.51	16	0	-
RUSE	6337E4.98		#23793.45	estima.	12	0	1
H040	833789.11	622318.09	#35#03.18	822225.11	18	0	1
R042	823,833.10		\$33.802.96	477141.41	18	0	-
RD42		822380.57		622120.A5	18	0	-
	#3390E#		\$25995.46 \$34014.00				1
R061	£13950.46	222120 At			48	0	1
R044	E24034.00		EM44062		18.		1
RMI	124141.12	RIZMENT	83420374	822581.45	.19	0	
RISAE	E2A234.72	622084.65	63A323.21	622E11.22	1,6	0	1
RUHT ROSE	R39/322.77	022010.KB	EMBART	821959.68	- 18	0 -	1
		421163-43			12	0	,
R543	X33155-56	\$21977.M	81343410	822580.28	18	. 0	1
RISS	ED101.47	821942.53	83327446	622007 OT	71	0	1
RIST	633274.50	922504.66	31141E76	922007 A2	18	. 0	-1
R051	633434,10	822080:21	\$33AHE.33		98	0	1
R033		f22123.44			58		1
R965	\$33756,6E	622165.28	81500 E.11	\$22f7x.75	18	0	1
FI054	632419.63		AMMET'S		18	0	7
9054		822122.03			18	0	1
ROSA	823649.55	622 544 45	#1361343	622152.85	-16		1
RUS4	#330#3.68	622164.45 822152.60	IDPAG	A221/49 07	18	0	- 1
		922140.82			16	0	- 4
R054	633767,63	822129-96	833775.48		10	0	1
	823786,53		#11872.14		19	- 0	1
Ross							-
RING	63377 E.AF	622113.50		822039.12	16	0	,
HOST	RE33873.20	102052.68	134111.21	821814.78	16	0	1
Ross	834159.21	92181478	W34250.10	821708.42	16	0	- 4
9.089	833867.29	422039-21	£3485£34	821690 22	37	0	- 1
Also	\$340EE.34	#21380.7Z	834261.E1	821727.A5	-48	0	- 1
8061	833115.37	821680.26	93231976	821689.31	16	0	1
R002	633319.76	621889.01	A15214.74	021947.25	38	0	1
RINZ	833294.88	621947.56	6154(0.51	822607-91	36	0	- 1
	A33460.49	#22568 k)	811543.73	62200M.T2	18	. 0	- 1
RUSA	823541.71		#33841.70		15	0	- 1
	823480.98	921952.82	933543.70	821982.31	- 18	0	- 1
H00+		#21834.GT	813315.55	621691.61	16	0	1
R084	\$13156.ex			weraterio.			
H00+	\$33166,17 \$33316.96			821052.75			
HODA HODA HIDE ROSG	£33316.96	821891.6E	#11491.00	821952.74	16	. 0	
RODA RODA RODE ROSE ROSE	833316.96 833184.01	821391.6E 821778.07	833491.00 632478.47	021763.88	10	0	1
HODA HODA HIDE ROSG	£33316.96	821891.68 821773.07 621783.16	#11491.00	821613.88 821613.88			

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Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr05	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
1250	800	550	400	450	650	1650	4900	5500	4650	4200	1950	36/30	3600	3800	4000	4350	4800	4900	4150	2750	2600	7550	1750
1.750	800	550	400	450	650	1650	4900	2200	4650	4200	3950	36700	3600	3800	4000	4.750	4800	4900	4150	2750	2600	2550	1750
1250	800	550	400	450	650	1650	4900	9500	4f50	4200	3950	3800	3600	3800	4000	4350	4800	4900	4150	2750	2600	2550	1750
1250	800	550	400	450	650	1650	4900 4900	5500	4650 4650	4200	3950 1950	3600	3600 3600	3800	4000	4350	4800	4900	4150	2750 2750	2500	7550 7550	1750
1100	700	500	350	400	600	1500	4350	5150	4200	3950	3750	35200	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3950	3750	3500	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4150	9150	4300	3950	3750	3500	3650	3900	4250	4700	5350	5500	4750	3100	3000	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	3900	1750	3500	3650	1900	4200	4700	5350	5500	4750	1100	2950	2950	2000
1100	700	500	350	400	600	1500	4350	5150	4200	1900	3750	3500	3650	3900	4200	4700	- 5350	5500	4750 4750	3100	2950	2950	2000
1100	700	500	350 350	400	600	1500	4350	5150	4200	3900	3750	3500	3650	3900	4200	4700	5350	5500	4750	3100 3100	2950	2950	2000
17	10	6	4	4	7	28	60	69	71	72	73	100	100	100	200	68	70	67	64	59	56	31	25
17	10	6	4.	- 4	7	18	60	69	71	72	73	100	100	100	100	68	70	67	- 64	59	- 58	- 31	- 25
17	10	- 6	4	4	7	18	60	69	n	72	73	100	100	100	100	- 65	70	67	64	.59	- 58	- 31	25
37	10	5	4	4	7	18 62	60 73	69 150	71	72	73	100	100	100	100	-88	70	57	64	59	5H 74	72	37
62	22	B B	8	10	16	62	73	150	150	150	150	150	150	150	150	100	100	100	100	100	74	72	37
100	72	31	- 21	24	38.	100	200	350	400	350	350	350	350	150	350	250	100	350	250	150	150	150	100
100	72	31	. 21	24	38	100	200	350	400	350	350	350	350	150	350	250	300	350	250	150	150	150	100
100	72	33	21	24	38	100	200	350	400	350	350	350	350	350	350	250	300	350	250	150	150	150	100
7	- 1	2	1	1	2	7	15	25	27	24	23	25	26	30	29	21	32	35	27	20	16	14	11
7	1	2	1	1	2	7	12	25	27	24	23	25 25	26	30	29	29	32	35 35	27	20	16	14	11
7	3	2	1	- 1	2	7	12	25	27	24	23	25	26	30	29	33	32	35	27	20	16	14	11
7	-3-	- 2	1	1-0	2	7	Ω	25	27	24	23.	25	26	30	29	21	32	35	27	20	16	14	11
66	v	16	12	13	20	68	100	200	200	190	150	150	150	150	150	100	100	150	100	100	100	100	72
56	26	16	- 11	12	20	67	100	200	200	150	150	150	150	150	150	100	100	100	100	100	100	100	6
66	26	16	11	12	20	67	100	200	200	150	150	150	150	150	150	100	100	50	100	100	100	100	46
50	50	16	11	13	19	50	100	250	290 250	260	150 200	200	200	150 200	200	190	200	200	150	100	100	50 100	50
50	50	17	12	14	20	50	100	200	200	200	200	200	200	250	250	200	250	250	200	150	100	100	100
50	50	17	12	14	20	50	100	200	290	200	200	200	Z00	250	250	200	250	250	Z00	150	100	100	100
23	23	14	11	n	17	50	100	200	200	200	200	250	250	300	30/0	250	400	A50	350	250	200	200	150
50	22	12	3	11	16	90	100	150	200	200	200	200	250	100	300	250	150	400	300	250	200	150	150
50	50	18	12	15	21 20	50	100	250	250 250	250	250 250	300 250	300 250	300	400 300	300 250	450 350	350	400	300 200	250 150	200 190	100
100	50	50	72	75	50	100	200	350	400	350	350	350	350	450	400	350	450	500	400	750	250	700	150
50	23	15	10	11	16	50	100	150	200	200	200	200	200	250	250	200	300	350	250	700	150	150	100
50	15	9	6	- 8	10	- 50	50	150	150	100	100	100	100	100	300	100	100	100	100	50	50	50	50
50	50	24	17	19	50	50	150	300	350	300	300	350	350	400	AOC	300	450	500	400	300	250	200	150
106	105	51	54	A SA	- 55	108	320	450	450	100	371	421	100	469	300	100 519	150 619	150 618	100	100	308	50.	205
200	150	100	100	100	150	200	550	800	750	700	650	750	750	850	900	950	1150	1200	900	650	30R	500	350
200	150	100	100	100	150	200	550	850	800	700	700	750	750	850	950	1000	1200	-1200	950	650	550	300	150
300	250	200	200	200	250	400	900	1400	1350	1150	1050	1100	1090	1100	1150	1150	1300	1300	1000	706	600	390	400
350	300	250	250	250	250	450	1050	1650	1550	1150	1250	1300	1300	1400	1450	1450	1700	1700	1300	900	750	700	500
300	250	200	200	700	200	350	850	1950	1250	1100	1000	1050	1000	1050	1100	3100	1250	1200	950	850	550	500	350
200	250	200 150	206 150	200 150	150	350 250	900 650	1950	1250 950	1100	750	1050	750	1100	11,00	1150	950	1300	700	700 500	400	550	250
200	150	150	150	100	150	250	550	900	850	700	650	650	650	650	80G 650	650	750	700	550	400	350	300	200
200	190	150	150	150	150	250	700	1050	1000	850	750	300	750	800	300	800	900	850	650	450	400	350	230
250	200	200	150	150	200	350	900	1250	1150	1000	950	1000	1000	1050	1100	1150	1350	1350	1050	700	600	550	480
150	150	100	100	100	100	200	450	500	700	600	550	600	600	650	70G	700	850	850	650	450	400	3090	250
150	150	150	150	100	150	250 150	550 400	900	850	750 500	700 500	750 550	700 550	750 600	300 600	#50 650	950 750	950 750	750 666	500 400	350	800	200
290	150	150	150	100	150	250	600	900	850	750	700	750	700	800	80G	H50	950	950	750	500	450	430	300
200	150	100	100	100	150	200	550	800	750	650	650	700	650	700	750	800	900	900	700	500	400	350	250
650	500	450	450	400	500	850	2000	3100	2900	2450	2200	2250	2150	2250	2250	2200	2500	2350	1300	1250	1050	950	790
550	450	400	400	150	A50	700	1700	2650	2500	2050	1850	1900	1750	1800	1750	1700	1900	1750	1350	950	800	700	500
550	500	450	450	450	500	\$00	1950	3000	2850	2450	2300 1850	2450	2350	2550	2650	2700	3150 2450	3100 2350	2400	1650	1400	1300	900
350	450 300	350 250	350	350 250	400 250	700 450	1100	2500 1700	2350 1600	2050	1850	1950 1350	1900	1400	2050 1450	2100 1500	1750	1700	1300	1250	1100	950	780 500
400	300	300	250	250	300	550	1250	1950	1850	1600	1500	1600	1550	1700	1750	1800	2150	2100	1650	1150	950	900	600
400	300	300	250	250	300	550	1250	1950	1850	1600	1500	1600	1550	1700	1750	1,800	2150	2100	1650	1150	950	900	500
450	150	300	300	300	350	550	1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	T150	1000	900	650
4521	150	300	300	300	350	550	1350	7050	1950	1650	1550	1650	1500	1750	1300	1250	2200	2150	1650	1150	1000	900	630
450 450	350	300	300	300	350 350	550	1350 1350	2050	1950	1650	1550	1650	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650
450	350	300	300	300	350	550	1350	2050	1950	1650	1550	1550	1600	1750	1800	1850	2200	2150	1650	1150	1000	900	650
050	150	300	300	100	350	550	1350	2050	1950	1690	1550	1650	1600	1750	1800	1890	2200	2150	1690	1150	1000	900	650
500	400	350	350	350	400	-650	1500	2350	2200	1900	1750	1850	1750	1850	1900	1950	2250	2200	1700	:1150	1000	900	650
250	200	150	150	150	200	300	750	T500	1100	950	900	950	950	1000	1050	1050	1250	1250	950	650	550	500	150
350	250 250	250	250	250	250	450	1100	1650	1550	1300	1200	1250	1200	1250	1250	1250	1400	1350	1050	700	600	550	460
200	250 150	200 150	700 150	150	250 150	250	950	1500 950	900	1200 800	750	1100 800	1050	900	950	1300	1200	1150	900	650	550	500	150
200	150	150	150	150	150	250	600	900	850	750	700	800	750	850	900	900	1100	1100	850	600	500	450	300
50	22	14	9	11	16	50	100	150	200	150	150	150	150	150	150	100	100	100	100	50	50	50	50
50	50	50	18	20	50	100	150	300	350	300	300	300	300	350	300	250	350	350	300	300	150	150	100
50	20	13	10	10	15	50	100	150	150	150	150	200	200	200	200	200	250	300	200	150	150	100	100
50	21	13	9	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	50
50	71	13	3	10	14	50	100	150	150	150	150	150	150	150	150	100	150	150	100	100	50	50	30
50	50	17	12	14	20	50	100	200	250	200	200	200	150	200	150	150	150	156	150	100	-50	50	50
-50	50	21	15	17.	24	- 50	100	250	250	250	250	250	250	30G	300	250	350	400	300	209	200	150	100
1500	1200	1000	1000	950	1150	1900	4450	4750	4750	4730	4750	4750	4750	4750	4750	4750	4750	A750	4750	3350	2850	2,900	1800
1350	1100	950	900	900	1050	1750	4100	4750 4350	4750	4750 3600	4700	4750	4750	4750	4750 4050	4750	4750 4750	4750	4500 3800	2610	2650	2400	1700
950	750 300	250	250	250	700	1200	1200	1800	1700	3500 1450	3400 1350	3600	1.850	1450	1450	4200 1500	1700	4790 1850	3800 1750	2650	750	2050	1450
400	200	2.30	2.50	250	300	300	1200	1000	2700	14.50	1336	2400	1.00	1450	2430	1.80	1700	1000	1130	300	734	900	340

Road		Coordin	rate (m)		WHOLEY	Height	Road Type
Pair	X1	Y1	X2	¥2	producting	(m)	(calline 4)
REF	B38527.91	121859.26		821675.22	mixing rooms	0	1
RUTE:	E33507.24	821875.22	£23,511.7.5	821697-01	29	0	7
R073 -	HXX4E1.50	421680.54	#39397.24	#21#75.22	12	0	1
- HOTA -	X33251.04	621660.64 621790.34	#3349150	821500.64	20	0	
8876		421851.09		621583.08	16	0	
RU78		821897.60		821699.37	18	0	-1
R076	633546.66	921694,77		821E00.00	16		4.
M074		621685.99		621622.52	10		1
8877	E33564.57		851543.57	821654.36	12	0.	
8077	\$33561.57		833660.48	821871 28	17	0	- 1
H077	633,600,48	621971.28		#21812.0¥	17	0	-
MOTA		621822.35			16	٥	1
	833673.29	42181.43	633597.51	821651.46	16	0	1
R050	833675.67			821557.96	16	0	1
	833697.01					0	1
M081		921600.86	932993.08	821652.08	30	0	
M082	\$33A68.18	621884.41	813510.76	821621/12	34		1
RRB2	E23516.75	621921.12		821785.93	a	- 0	- 5
R062		82178533		821657.55	18	0	
HOET		62161.0.11		821817.11	- 18	0	1
MOE2	\$13,499.18	621(1)3,12		821772.29	14.	. 0	- 3
H192	\$33524.38	821772.29	8335951	821652.62	34	0	- 1
#60R		821687.02	83356249	821644.65	11	0	1
M094	813682-03	\$2164A.65 \$21605.64	052007.71	021603.07	13	0	1
Rost	833609.34			021675.52	14		1
MIRZ-	E33840,24		£13691.67	821645.20	- 12	0	1
ROSS	#33/EE1.67	821545.20	821729.52	821212.65	-14	0	- 1
		\$21641.89	#37643.83	821161.5k	17	0	
R086	833663.88	821533.58	\$33646.83	021545.45	12		
R197	H33648,49	\$2354E-47	E1369E46	621508.30	12	0	- 1
RIDE		821811.68			12	4	- 4
1808E	#33365-50	621650:04		021600.01	12		- 4
8.59.6		621885.51	515417.53		12	- 6-	4
	E334E7.63	#21841.0V		621786.07	17	10	4
		#21785.UT	#115554-PO	421457 TK	17	- 4	
moss.		921697:75			17	- 1	-
RAFE .		621505.62		621511.11	- 32	. 6	•
		821801.44			18		
Ross	633370.06	421801.44	832427.26	821652.03	16	1.1	1
4085	833379.98	621682.01			14	- 1	1
Altas	833455.60		833419.69		16	- 10	4
	Andrew Proper	621829:26		821786.38			
HORS	833522.46	821786.32	E23343.19	821725.A7	16	0	- 4
HOLE	833541.18			#2186E.37	16	0.	
HORK				821504.64	16		4
ROPE		(Z)594.44		821508.81	16		- 4
idsoy#d91	833284.78	821629.64		621634.13	97	0	7
R692+R993	633317.92	#21632.93	833449.56	821640.31	30	0	- 1
1092-R093	833449.50	921640.31	432812.09	021599.24	30	0	- 1
R094	633337,84	\$21024.55	853341.61	621670.41	- 10	- 0	1
R095	833604.59	621501.72	61359849	621648.43	42	0	- 4
095+R397	433980.58	622.454.38	83491877	822414.27	10	0	7
109 K - 11 DOW	63402 K.77.	822414.27	E34127.E2	822302.11	18	0	- 1
1100+R101	834127.62	822332.11	STATISTIC	STIMM 35	18		- 4
9192+R103	834216.31		EJATEM 95	822190.58	38	0	- 1
194-R199	634309.95	922180.5E	BB440TAG	927098.55	48	0	1
R106	633917.63	\$22451.11	612091.74	01210938	18.	0	- 1
B187	832501.55	612370.04	83409031	822287 A3	.0		
R108		622784.04		822212.22	3,6	0	- 1
Rise	EXATE CON	\$2221E ZZ		822136.AB	47	0	1
		422134.63			12	- 0	3
B157		622059.85			- 10	0	1
R117	R30646.78	622405.79			39	-0	1
				822271.35	18		1
R114		822335.17 822271.56			18		1
		822271.05 822200.75		622201.23		0	
RIS					19		1
RITE		622131.94			18	0	
RHIT	834097.30		EXCHISES		18	0	- 1
			834245.29				- 1
RIFE			The second second				
	834790.09 834242.94		634292.16	821951.A5	-39		1
RIJY RIJO	834242.94 834391.93	621993.85 821961.17			38	0	- 1 -
R179 R120 R121	824242.94 834391.93 633768.03	821993.85 821981.17 822278.46	822789.44	022218:98	18 18	0	1
R179 R120 R121 R122	824242.94 834291.93 833768.03 633761.88	821993.85 821981.17 822278.68 822311.12	833799.44 833898.78	022218:98 622222:18	18 16 18 18 18 18 18 18 18 18 18 18 18 18 18	0 0	1
R179 R120 R121 R122 R122	E34242.94 E34391.93 633768.03 633761.88 E33666,78	621993.65 621981.17 822374.46 622311.12 622322.16	833789.11 833898.78 833954.75	022218.98 822222.18 622150.50	18 18 18 18 18 18 18 18 18 18 18 18 18 1	0 0	1 1
R179 R120 R121 R122 R122	E34242.94 E34281.93 E33768.03 E33761.88 E33666,78 E33673.82	621993.85 82998-1.17 92227-8-16 82233-1.32 622222-36 62234-72	833698.78 833698.78 833994.75 833994.66	022218.98 622222.18 622150.50 622284.07	39 38 38 38 48	0 0 0 0 0 0 0	1 1
R179 R120 R121 R122 R122 R124 R124	E34242.94 E34291.93 633768.03 633761.88 83366,78 633673.82 633674.82	621993.85 82198-0.17 82237-8-68 822311-1.32 822322-16 622341-72 822328-07	832789.44 833898.78 832894.75 833894.76 833897.77	022218.98 622222.18 622150.50 622284.07 822172.85	155 146 148 148 148 148	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R124 R124 R125 R126	E34242.94 E34281.93 E33768.03 E33761.86 E33666,78 E33671.82 E33684.86 E33693.40	621992.85 621981.17 822276.46 622311.12 622222.16 622341.72 622369.07	832799.44 833898.78 833994.75 833894.66 833897.77 833888.33	022218:98 632222:18 622180:50 622184:07 622172:98 622174:55	155 146 148 148 148 148 148 148	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R123 R125 R126 R127	E34262.94 E34281.93 E33768.03 E33761.88 E33665.76 E33667.82 E33693.40 E33693.40	621992.85 823981.17 822276.46 822331.12 822222.16 622343.72 822389.00 8223192.05	#22799.44 #32898.78 #32994.75 #23894.66 #33898.37 #23898.33 #23892.51	622218.98 622222.18 622180.50 622784.07 622172.05 622174.73 622278.45	35 36 36 38 38 38 18 18 12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R124 R124 R125 R126	E34242.94 E34281.93 E33788.03 E33781.88 E33866,78 E33671.82 E33084.86 E33083.40 E33456.65 E33603.61	621993.65 621981.17 822276.46 8222311.52 622222.16 622341.72 832388.00 622315.75 822276.46	83369878 83369878 83389875 83389875 833898777 83389833 82359251 83359251 83359351	022118.98 022322.18 022130.50 022130.50 022172.05 022174.73 022178.45 022221.24	39 38 36 48 48 38 19 18 41 41 42 48	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R123 R125 R126 R127	E34262.94 E34281.93 E33768.03 E33761.88 E33665.76 E33667.82 E33693.40 E33693.40	621992.85 823981.17 822276.46 822331.12 822222.16 622343.72 822389.00 8223192.05	#22799.44 #32898.78 #32994.75 #23894.66 #33898.37 #23898.33 #23892.51	622218.98 622222.18 622180.50 622784.07 622172.05 622174.73 622278.45	35 36 36 38 38 38 18 18 12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1
R178 R120 R121 R122 R122 R124 R125 R126 R127 R128	E34242.94 E34281.93 E33788.03 E33781.88 E33866,78 E33671.82 E33084.86 E33083.40 E33456.65 E33603.61	621993.65 621981.17 822276.46 8222311.52 622222.16 622341.72 832388.00 622315.75 822276.46	83369878 83369878 83389875 83389875 833898777 83389833 82359251 83359251 83359351	022118.98 022322.18 022130.50 022130.50 022172.05 022174.73 022178.45 022221.24	39 38 36 48 48 38 19 18 41 41 42 48	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R119 R120 R121 R122 R122 R124 R125 R126 R127 R128 R128	E24242.04 E24201.93 613768.03 613761.08 E21666,76 E21666,76 E21664.06 E21693.40 E23456.65 E33903.40 E33456.65	621992.65 62196.1.17 62276.46 622311.52 62222.16 622341.72 622369.00 622315.75 622276.46 62272.63 62272.63	#32798.40 #33898.78 #32898.75 #23898.66 #33897.77 #33868.33 #23592.51 #33578.36 #33578.36	02218.08 02222.18 022150.50 022150.50 022150.50 022150.50 022150.50 022174.33 02227.25 02220.37	39 36 36 46 48 48 19 18 42 38 42 48	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R124 R125 R126 R127 R128 R128 R129	E24242.94 E24281.93 623764.03 623764.08 E22666,76 E23666,76 E23666,76 E23666,76 E23666.06 E23666.06 E23666.05 E23666.05 E23676.05 E23277.60 E23277.60	621992.65 62196.1.17 62276.46 622311.52 62222.16 622341.72 622369.00 622315.75 622276.46 62272.63 62272.63	832798.40 833898.78 832898.75 823898.66 833897.77 833868.33 823592.51 833298.77	62218.98 622122.18 622150.50 622284.07 822172.05 822174.73 622278.45 822221.24 932293.72 622175.17	192 193 194 195 195 195 195 195 195 195 195 195 195	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R125 R121 R122 R122 R124 R125 R126 R127 R128 R128 R128 R121 R121 R121	EN262.94 632708.02 632708.02 632708.03 632704.98 833673.82 832693.60 833693.60 833693.61 833903.61 833977.60 833977.60 833377.60 833377.60	621992.85 62198.1.17 822278.46 622331.82 62222.16 622347.72 832238.67 832238.67 832238.60 832232.60 832232.60 832232.60 832232.60 832232.60	832799.40 833698.78 833898.75 83389.85 83389.77 83388.35 82359.35 813398.77 83348.75 83348.77	02218.08 03252.18 022180.05 022180.05 022184.05 022174.35 022278.45 022221.24 02220.37 02200.75 02200.76 02200.76	19 18 18 18 18 18 18 18 18 18 18 18 18 18	9 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R124 R125 R126 R127 R128 R128 R120 R121 R121 R121 R121 R122 R122	EN262.94 934291.93 433798.03 833791.86 933673.82 833673.82 833673.82 83363.40 833673.83 833673.83 83367.60 833576.84 833576.84 833576.84 833576.84 833576.84	627991.65 629981.07 822298.64 6122311.52 622222.16 622241.72 622241.72 622241.73 822296.78 822296.78 822296.76 822296.76 822296.76 822296.76 822296.76 822296.76 822296.76	832799.46 833698.78 833994.75 833994.75 833994.77 833982.37 833592.37 8333982.77 633494.55 833493.51	0221808 03252218 02218080 02218080 02218080 022172.05 022174.35 022272.35 022273.5 022273.5 022275.17 022907.07 021942.16	55 58 58 68 53 53 53 54 54 54 54 54 54 54 54 54 54 54 54 54	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R124 R125 R126 R127 R128 R129 R121 R131 R131 R131	EN262.04 EN262.93 83378.03 83378.83 83366.78 83367.82 82368.86 83390.40 83390.81 83390.81 83397.60 833377.60 833377.60 833377.60 833377.60 83340.43 83340.45 83340.45	627993.85 622984.17 822774.46 522314.72 822202.16 622347.72 822288.00 622398.00 622398.00 622398.00 622398.00 622398.00 622792.03 822775.64 822775.64 822775.64 822775.64	8336878 83368476 83368476 83368476 83368777 8336833 82359348 83336877 63348436 83348454 83348459 83348436 83348436	622118.08 62222.18 622150.50 622150.50 622152.05 622172.05 622172.05 622173.13 62221.29 622175.17 62266.78 62207.07 62208.78 62208.78	19 18 18 18 18 18 18 18 18 18 18 18 18 18	0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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R179 R120 R121 R122 R122 R124 R125 R126 R127 R128 R127 R121 R131 R131 R132 R133 R133 R128	EN242.94 EN291.93 833784.93 E32784.83 E32086.78 E32086.78 E32085.05 E32085.05 E33077.60 E32377.60 E32377.60 E32377.60 E32377.60 E32377.60 E32377.60 E32377.60 E32377.60 E32377.60	627993.85 822984.97 822274.46 822294.97 822294.97 822294.97 822395.75 822395.75 822395.75 822395.70 82395.70 82395	#22796.14 #228967.6 #228967.6 #22896.67 #22897.5 #22897.54 #22897.54 #22297.54 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56 #22297.56	022198.98 022522.18 022530.55 022530.07 0225730.07 022573.45 022273.75 022273.75 022590.75 022590.75 022590.78 022590.78 022590.78 022590.78 022590.78 022590.78 022590.78 022590.78 022590.78	98 98 94 18 18 18 18 18 18 12 28 14 14 14 18 18 18 18 18 18 18 18 18 18 18 18 18	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
R179 R120 R121 R122 R122 R122 R124 R126 R126 R127 R128 R127 R128 R132 R132 R132 R132 R132 R132 R133	EN262-94 EN261-93 63276-1-8 E3266-78 E3266-78 E3266-78 E3266-86 E3266	627992.85 822985.17 92278.46 92220.46 92220.16 92220.17 92220.17 92220.95 92220.00 92200.00 92200.00 92200.00 92200.00 92200.00 92200.00 9	#22796.11 #23894.75 #23894.75 #23894.75 #23892.51 #23892.51 #23892.51 #23892.51 #23892.51 #23494.50 #23494.50 #23494.50 #23494.51 #23492.56 #23492.56 #23492.56	622198.98 922522.18 922525.93 922595.93 922572.94 922572.94 922572.94 922572.94 922572.94 922572.94 922572.94 922597.97 922597.97 921992.14 921992.14 921992.14 921992.14	10 10 10 10 10 10 10 10 10 10 10 10 10 1	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 d d d d d d d d d d d d d d d d d d d
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Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hros	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hrt7	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
450	350	300	300	300	350	550	1505	2000	1900	1650	1500	1500	1500	1650	1650	1700	1950	1900	1450	1000	850	800	550
200	150	150	150	150	150	250	600	900	850	750	700	750	750	800	850	ESO .	1000	1000	500	558	450	400	390
250	200	150	150	150	200	300	750	1100	1050	900	800	850	B00	650	850	RSQ	950	900	700	500	400	350	250
750	200	150	150	150	150	300	700	1050	1000	#50	800	850	HOO	900	900	950	1100	1050	1100	652	500	450	300
150	150	100	100	100	100	200	450	750	650	600	550	550	550	550	550 550	600	650	650	500	150	300	250	300
150	100	100	100	100	100	200	450	700	650	550 550	500	550 550	500	550 550	550	600	650	650	500	150	300	250	200
150	100	100	100	100	100	200	450	700	650	550	500	550	500	550	550	600	650	650	500	350	300	250	300
300	250	200	200	700	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	350	480
300	250	200	200	200	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	950	400
300	250	200	200	200	250	400	950	1450	1400	1200	1100	1150	1100	1150	1200	1200	1400	1350	1050	750	600	.950	400
150	150	100	100	100	100	200	500	750	700	600	550	550	500	550	550	550	600	600	450	300	250	250	150
250 150	200 100	150	150	150	100	300	750 450	1150	1100	950	850	900	550	900	900	950 650	1050 750	750	900	550	450. 350	300	100
250	200	200	200	200	200	350	800	1250	1200	1090	960	1000	1000	1050	1100	1150	1300	1300	3000	700	600	550	200
200	700	150	150	150	150	300	650	1000	1000	850	750	-800	790	800	350	850	950	950	700	500	400	400	250
200	200	150	150	150	150	300	650	7000	1000	950	750	800	750	BOC	850	950	950	950	700	500	400	400	150
200	200	150	150	150	150	300	650	1000	1000	650	750	800	750	500	850	BS0	950	950	700	500	400	400	150
100	50	50	50	50	50	100	250	400	400	350	300	300	300	100	300	300	100	300	250	150	150	150	100
100	50	50		50	50	100	250	600	400	350	300	300	300	100	300	300	300	300	250	150	150	150	100
200	50 200	150	50 150	50 150	150	300	250 650	1000	400 950	350 850	300 750	800	750	300 850	300. 850	300 850	300 1000	950	750 750	150 500	150 450	400	10G 36G
200	200	150	150	150	150	300	650	1000	950	RSO	750	300	750	#50	850	RSO	1000	950	750	500	450	400	100
200	150	150	150	150	150	250	650	1000	950	800	750	750	750	800	300	800	900	900	650	450	400	350	250
200	150	150	150	150	150	250	650	1000	950	800	750	750	750	800	800	800	900	900	650	450	400	350	150
250	150	150	150	150	150	250	650	1000	950	800	750	750	750	600	300	800	900	900	650	450	400	350	250
100	50	50	50	50	50	100	250	400	400	350	300	300	300	300	300	300	350	350	250	200	150	150	100
100	100	100	100	100	100	150	350	500	500	450	400	400	400	400	400	400	400	450	350	200	200	190	150
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	2850	3150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850	600	400	400	650	3400	2950	3600	3600	3700	3100	2950	2890	3150	3250	3250	3600	3600	3200	2450	2500	2500	1960
1200	850	600	400	:400	650	1400	2950	3600	3600	3200	3100	2950	2850	1150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2950	7250	3150	3250	3250	3600	3600	3200	2450	2500	2600	1950
1200	850 850	600	400	400	650	1400	2950 2950	3600	3600	3200 3200	3100	2950 2950	2890 2890	3150	3250 3250	3250 3250	3600	3800	3200	2450 2450	2500 2500	2600 2600	1950
1200	850	600	400	400	650	1400	2950	3600	3600	3200	3100	2990	2850	1150	3250	3250	3600	3600	3200	2450	2500	2600	1960
350	600	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	600	400	300	300	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	800	400	300	100	450	2600	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	2200	2250	2350	1750
850	500	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	Z500	2650	2750	2800	3450	3800	2900	2100	2250	2350	1750
850 850	600 600	400	300	300	450	1000	2100	2850 2850	2750	2400 2400	2400 2400	2350 2350	2300	2650 2650	2750 2750	2800 2800	3450 3450	3600	2900	2200	2250 2250	2350	1750
250	800	400	300	100	450	1000	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3500	2900	7100	2250	2350	1750
850	600	400	300	300	450	1600	2100	2850	2750	2400	2400	2350	2300	2650	2750	2800	3450	3600	2900	1100	2250	2350	1750
350	250	250	250	250	250	-450	1050	1600	1500	1250	1100	1200	1100	1150	1150	1150	1300	1200	950	650	550	500	150
250	200	150	150	150	20G	350	750	1150	1150	950	900	900	850	90G	900	950	1000	1000	750	550	450	400	100
250 50	200 50	150 50	150 50	150 50	50	350	750 200	1150 300	1150 300	950	200	900 200	200	200	900	950	1000 750	1000	750	100	450 100	400	300
100	100	100	50	50	100	150	350	500	500	250 450	400	400	350	400	200 400	200 400	400	400	300	200	200	100	160
57	19	110	7	7	14	57	64	150	150	150	150	150	150	150	150	70	150	150	121	68	63	62	58
52	-56	25	17	70	78	8	150	300	300	300	250	250	250	500	250	200	250	300	250	700	150	150	73
100	100	73	34	40	100	150	300	800	650	550	500	550	500	550	550	350	500	500	450	250	250	250	150
1.00	36	22	16	16	26	100	150	250	300	250	250	300	300	300	300	250	350	356	250	200	200	150	100
71	27	16 24	11	20	19	50	100	300	300	300	20G 250	250	250	256 300	250	290	300	300 300	200	150	150	100	100 100
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50	50	21	15	16	24	50	100	250	250	250	200	200	- 200	200	150	100	150	100	100	50	50	- 50	50
103	50	50	20	- 21	50	100	150	350	350	300	250	250	250	250	200	150	150	150	150	100	100	50	50
50	50	23	17	18	58	90	100	300	300	250	250	200	200 250	300	300	150 750	150	150 450	350	250	200	200	150
50	20	12	8	9	15	50	50	150	150	150	150	150	100	150	100	100	100	100	100	30	50	50	30
200	100	50	50	50	100	200	450	850	950	850	750	750	700	800	750	550	700	750	550	400	350	300	250
200	100	50	50	50	.50	200	400	750	850	750	700	700	650	750	700	550	700	750	600	400	350	300	230
290	100	50	50	50	100	200	400	300	850	750	700	700	700	750	700	550	700	750	600	400	350	300	150
200	100	50	50	50	50	200	350	750	800 800	700	650 700	650 700	650 700	700 III00	750	500	650 800	700 850	700	400 500	400	350	300
200	100	50	50	50	100	250	450	900	950	#50	800	800	900	850	900	650	800	850	700	500	400	390	380
250	150	100	50	50	100	250	500	950	1050	950	900	900	850	950	900	700	900	950	750	500	450	4110	300
21	13	- 6	6	6	9	- 50	50	100	100	100	100	100	100	150	150	100	150	200	150	100	100	100	50
100	50	50	50	50	30	100	200	400	450	400	400	400	400	500	450	350	500	550	450	300	250	250	200
50	50	22	15	17	.50	50	150	250	300	250	250	250	750	300	300	200	300	350	250	200	150	150	100
50	50	20	14	16	23	50	100	250	250	250	200	200	200	200	200	150	200	150 290	150	100	100	50	50
50	90	22	15	16	15	50	150	250	300	250	250	300	300	350	350	300	400	450	350	750	700	200	150
50	23	15	10	12	16	50	100	150	200	200	200	200	200	250	250	200	250	300	250	150	150	100	100
50	50	18	. 14	15	21	50	100	700	250	250	250	250	250	300	300	250	350	400	300	200	200	250	150
150	100	100	100	100	100	200	400	650	600	500	450	500	450	500	500	500	600	\$50	450	500	250	250	150
200 300	190 250	200	206	200	150 250	400	900	(400	1300	700 1050	950 950	650 950	900	650 900	700 850	700 850	900	800 800	650	450	350 350	300	250 250
290	150	150	150	150	150	250	550	350	800	700	700	750	700	500	800	RSO.	1000	1000	750	950	450	400	100
200	100	50	50	50	100	200	350	750	800	750	700	700	700	500	750	500	600	850	700	500	400	350	500
200	100	100	50	50	100	200	400	800	900	850	800	850	H50	950	950	750	1000	1100	900	600	500	450	350
- (6	5	- 1	2	- 4	II.	14	50	50	50	50	50	50	50	50	50	50	50	50	50	26	19	.14
6	4	3	1	1	3	7	13	50	50	50	50	50	-50	50	50	50	50	50	50	22	18	17	13
- 6	4	3	1	- 2	3	9	17	50 50	50 50	50	50	50	50 50	50 50	50 50	50 50	50	50	50	21	17	16.	13
100	50	50	24	50	50	100	200	400	450	400	400	450	450	550	550	400	500	650	500	150	300	750	200
100	50	50	50	50	50	100	200	450	450	450	450	500	500	600	600	500	650	750	600	400	350	300	250

Road		Coordin	rate (m)	-	Width	Height	Road Typ
Pair	X1	Y1	X2	¥2	producting	(m)	(caline 4
Rist	B30 254.35	521947.25	885315.56	821601.57	mixing rotal	0	1
8162	E33329.69	621853.67	ED31534	621691.04	13	0	7
RIAS	833129.75	621689.31	#33:460.47	#21#34.07	- 13	0	1
2144	XXX140.17	621834.07	#33.97E.74	821783,18	13	0	1
PLES-RIAL	H2581Z.43	421974.55	\$3497458	621516.03	- 32	0	1
2117+2180	E33734.44	#21886:3K	SERVICES.	821727.34	16	0	1
R146	833728.61	921749.AZ	632607.73	821694.38	14	0.0	- 4
R149	833774.00	621643.52	032807.73	821684.38	13		1
R150	833755.67	621704.23	853607.71	821603.81	- 17	Oc	1
R151	833612.61	821610.98	833663.50	821663.70	13	0	- 4
R151	ADDRESS.	621543.70	#337762H	F21142.63	14	0	- 1
W192	835774.08	621643.52	#1387#17	821500:58	28		1
R193	833991.31	622399.76	83467877	622454.27	18	0	1
B194	833960.66	222520-65	#EVWZ.00	\$22189.07	18	. 0	1
8198	£33'909.46	922271.36	X33900.44	932120.45	16	0.	1
#186	833684.78	622222.16	#11M(9/85	022271.30	18		1
B197	E23866.58	622222.54	65362777	621172.96	18		
P153	833827.77	822172.95	#15772.44	\$22113.30	18	0	
KIRK	634070.01	622259.62	E3431X#0	632384.34	18	0	1
Miles	834090.38	\$2228 F 53	T34527-62	6III332.11	15		- 3
891	E34014.00	822250.52	834075.91	827299.62	15	0	- 1
R162	634049.42	822238.28	2340NO:19	822287.53	15	0	1
#163	£30,990,00	62220186	834634.00	032250.01	- 10	0.	1
B164	834007.86	622194:35	#34/94% AT	0225W-28	15		1
RIES	F33951.31	622353.78	#ESSWAA7	622221 25	16	0	1
R158	835872.14	822651.29	82191475	822190.50	18	0	1
R147	633,683,47	822042.45	834007.88	822100.33	19	0	- 1
R163+R169	833815.72	121975-07	EDWEN	WEIGHT AT	21		1 1
R179-9171	833736.44	821 FEB 2.35	#31812.49	821978-50 L	18	0	1
R172+R173	833864.92	821822.12	811719.26	821687.65	26	. 0	1
RU4-RU3	#33061.78	621407.56	£12M(3.34)	821623.58	18	. 0	1
804	E30496.77	f21508.49	\$11580.47	621680.73	20	-0-	4
R177	E33513.09	821599.24	2237344	621688.A2	- 29	0-	1
RITE	R35440.44	621529.90	EXTENSES.	#21608.41	16	0	7
8173	X23451.04	621626.31	#30511.33	821600/38	17	. 0	- 1
R 120	E34218.31	622256.35	\$54375.90	621585.39	18	0	1
R131	E38181.98	4223°1.72	#3421E31	822258-36	18	0	1
R187	K3A140-62	822162.47	834591.76	022212.38	16	-0-	1
8182	834099.34	622113.33	E34540-62	822162.67	18	-01	1 1
R134	E34077.01	622152.66	#54851.51	622100.94	13	0	- 1
P184	STADE 1.51	E22100.94	834EF194	\$22094.18	13	0	- 1
H184	#34071.00	07204 s. to	#34007.30	622115.02	14	0	- 1
HIES	834309.95	\$22180.58	E3430240	813167.A4	10	0	1
8176	834231.54	62238 à 63	6M27134	622136 83	19	0	1
RIAT	834190.59	822037.73	834ZD176	622086.A5	- 18	0	1
R153+R199	834004.93	#21915 CD	#34WE534	\$2100.22	10	0	- 1
R190-R191	833921,12	921727.74	E34004.08	021016.03	19	0	1
#192-R (92	633876.32	\$21460.75	#45.830/d9	621727.50	29	0	1
R194-R 195	823825.79	621600.86	611m7.51	621631.A8	20	0	- 4
R395+R202	6337E1.01	621323.38	82305 17	\$21450.58	20	0	1
RIST	634364.00	827040.84	E34400 13	62210471	17	0	1
Rtss	834323.77	822010.68	83436436	622060.94	78		- 4
R199	839291.93	421961.17	63A323.00	622015.AB	-38	0	- 1
R100	834239.67	#21914.12	834210.00	821983.18	14	0	1
#100	834239,47	821914.13	#34327.69	021540.33	18	0	1

										Val	nicle count	for each	road										
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
50	16	10	7.	8	12	50	50	100	150	150	150	150	200	750	250	200	100	350	250	208	150	150	100
50	22	14.	10	11	17	-50	100	200	290	200	150	200	200	200	200	150	250	250	200	150	100	100	100
150	50	50	50	50	50	150	250	550	600	500	500	450	450	500	450	350	450	A50	350	250	200	- 200	130
100	50	50	50	50	50	100	250	450	500	450	400	400	400	450	400	300	400	400	300	200	200	150	130
24	13	8	5	7	10	25	63	100	150	124	122	123	322	174	172	117	222	. 224	168	113	11.1	110	-58
-57	18	12	ä	9	13	58	65	150	150	150	150	150	150	150	150	100	200	200	100	100	100	100	100
17	- 9	5	4	4	7	-18	50	50	50	50	50	-50	90	50	50	50	50	- 50	22	16	13	12	9
17	9	5	4	4	2	18	50	50	50	50	. 50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	5	4	.4	7	- 19	50	50	50	50	50	50	50	50	50	50	50	50	22	16	13	12	9
17	9	- 3	- 4	4	7	17	50	50	50	50	50	50	50	50	50	50	50	50	25	16.	13	12	10
17	9	- 5	4	A	7	17	50	50	50	50	50	50	50	50	50	50	50	50	23	16	23	1.7	10
. 17	9	- 5	4	.4.	7	18	50	:50	50	50	50	50	50	50	50	50	50	50	50	.20	17	14	11
100	100	100	50	50	50	100	250	300	250	250	200	200	250	200	200	200	200	200	150	150	150	.100	100
100	100	100	50	50	50	100	250	300	250	250	250	250	300	300	30C	350	350	350	300	250	200	200	150
100	100	50	50	50	50	100	250	300	250	250	200	200	250	200	200	250	250	200	200	150	150	150	100
500	400	350	300	. 250	250	450	100	800	800	100	800	800	100	800	900	.800	800	750	650	550	450	450	350
600	500	400	300	250	300	550	1200	1500	1300	1,200	1100	1100	1150	1100	1050	1050	1050	1000	950	750	650	600	450
500	400	350	300	250	250	450	1000	1300	1100	1050	950	1000	1050	950	950	1,000	1000	950	800	700	600	750	450
50	23	18	35	12	15	24	50	50	50	50	50	50	50	50	50	100	100	100	50	50	50	50	50
100	100	50	50	50	50	100	200	250	250	200	200	200	200	150	150	150	150	150	150	100	100	100	50
150	150	100	100	50	100	150	350	400	350	350	350	350	400	350	350	400	400	400	350	300	250	250	200
500	150	150	100	100	100	200	400	550	450	450	400	400	450	400	AOG	450	450	450	350	300	250	250	200
750	200	150	150	100	100	200	450	600	550	500	500	550	600	600	600	650	700	700	550	900	450	. 400	100
150	150	100	100	100	100	150	350	450	400	350	350	350	400	350	350	400	400	400	300	300	250	250	200
150	150	100	100	100	100	150	350	450	460	350	350	350	400	400	400	480	450	490	3.50	300	250	250	200
300	250	200	200	150	150	300	650	850	750	700	650	700	750	750	750	800	850	300	650	530	500	450	330
250	200	150	150	100	150	250	550	650	600	550	550	550	600	600	500	950	650	650	550	450	400	350	300
500	350	300	300	200	200	450	950	1200	1050	1050	1050	1100	1,200	1200	1250	1350	1450	1350	1150	1000	850	300	600
450	350	300	250	200	200	400	900	1100	1050	950	950	1000	1150	1100	1150	1250	1300	1250	1/750	900	250	750	550
500	400	350	250	250	250	450	1006	1300	1150	1100	1050	1100	1200	1200	1200	1300	1350	1350	1100	950	800	300	600
550	490	350	300	250	250	450	1050	1350	1200	1100	1050	1100	1200	1150	1150	1290	1300	1200	1050	900	750	750	550
350	300	250	200	150	200	300	750	900	800	700	650	700	700	650	650	650	650	650	500	450	400	350	300
250	200	200	150	100	150	250	550	700	600	680	550	600	650	650	-650	700	700	100	600	500	450	400	500
350	250	200	200	150	150	300	700	850	750	700	650	650	700	650	650	1890	650	650	590	#50	400	ADG	300
350	250	200	200	150	150	300	650	850	750	700	700	750	H00	600	900	900	950	900	750	650	550	950	400
200	150	150	100	100	100	200	400	500	450	400	400	400	400	400	400	400	400	400	300	300	250	250	200
15	12	9	ā	7	8	24	50	-50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	- 21
50	50	22	19	16	18	50	50	100	100	50	50	50	90	50	50	50	50	50	50	50	50	50	50
50	23	19	16	13	15	24	50	50	90	90	.50	50	50	50	50	50	50	50	50	50	24	22	17
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
50	50	19	16	13	15	50	50	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
100	100	50	50	50	30	100	200	250	200	200	200	200	250	250	250	258	250	250	200	200	150	150	100
22	19	15	12	11	12	20	50	50	50	50	50	50	50	50	50	50	50	50	50	50	22	- 21	17
1.00	100	50	- 50	50	50	100	200	250	200	200	200	200	200	200	150	150	150	150	150	100	100	100	50
68	63	61	59	\$8	- 59	- 64	200	20G	200	290	200	200	200	200	200	250	250	250	200	200	150	150	122
100	70	66	64	35	63	72	150	200	200	200	200	200	200	200	250	250	300	250	750	200	200	700	122
42	35	29	24	22	.13	38	100	100	100	100	100	100	100	73	73	70	68	.68	- 66	66	62	G2	31
64	.60	58	57	- 55	.56	63	200	200	200	200	172	172	171	119	13.7	116	115	1134	111	111	58	- 58:	57
100	100	70	40	- 33	38	100	150	200	150	150	150	100	150	100	100	100	150	100	100	100	100	100	24
10	7	5	5.	4		B	18	.24	20	17	14	13	12	11	Б.	3	5	5.	- 4	- 4	3.	1	- 3
19	15	12	10	8	9	16	50	50	50	50	50	50	50	:50	22	- 23	18	-18.	15	13	11.	-0	9
22	18	15	- 13	-10	12	21	- 50	50	50	50	50	50	- 50	50	- 50	.50	.23	20	- 18	15	- 13	12	10
50	50	23	20-	1.6	19	50	50	106	100	50	50	50	50	50	50	50	50	50	-50	50	50	-50	50
50	50	23	.20	16	19	50	50	100	100	50	50	50	50	50	50	50	50	50	50	50	50	50	50

	(Callon 4)			1					+		-								+								-										-												-							+	,													,						1.4							
	Meight		G	0	0		9 0	0	0	0	0	0	0 0			0	0	0.	0		0	0			0	0	0			0	0 4			0	0					0		a	a	0	0		0	0	0	0	0	0	0 0	a	0	0		9		0	0	0	0	0			0	0	0	0				0	0	0	0		0			0	
	(Including	4	20	20	19	28		. 01	- 118	2						. 0	12	11	11	13	10	10	10	- 18	- 61	14	15	48										2 5		*		91	118	100		118	83	14	- 12	. 91	16	- 01		**	- 18	- 11	108	21	16	20	18	+48	- 81	81		116	- 63	- 18	1.0	13	0		. 93	1.6	115	11	18	2 :			20 02	13	
9 04	5	82230625	\$22346.7E	823409.45	622543.00	822546.7E	*********	823424.55	822496.53	822614.65	822626.09	622626.54	22,400,27		873464.07	822387.55	\$22866.34	822432.88	822462.45	\$2345K.02	822556.02	623462.07	122425.39	822386.48	622354.59	822384.6B	822574.91	622396.31	277778	82228372	822340.13	BZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ	## CZ1728	022178.07	02222201	20000000	27.167.75	87745674	822424 11	851484.18	822072.07	822126.94	822178.17	822231.31	822269.00	822264.07	822308.61	622330.74	122235.17	12236157	\$22320.45	822250.62	822162.07 8223006.45	622011.22	621367.66	821877.95	922086.76	822007.07	822474.73	82236228	822174.73	822-122-03	822144.43	8221228	432138.66	822113.33	82258(3)	\$23039.CE	621814.78	821738.42	62188022	BELLEVAS	823847.78	12200028	12203172	12(10112)	12196231	821891.67	921962.70	10111111	42191200	121822.57	
r 2049	ate (m)	83357737	833231.06	833434.80	833969.46	83196546	1	83391828	83367378	83383387	13397371	03409415	697985799		STABLE AT	83396388	83384185	13329664	833883.54	93384651	83342248	633416.03	033447.02	93354454	833587.55	833587.56	033633.17	833864.17	93355807	03335500	0334850	02346500	933100.53	92222268	933377.00	03306434	**********	81181878	833917.83	ATT SHOW A	83311178	83325339	833394.77	833634.35	833863.40	833664.88	833744.79	#3371845	833833.16	92390296	83395646	634034.90	83478478	63432121	134384.01	833158.58	63343410	933274.46	63568833	833735.68	833468.33	13355671	93364955	92785789	41176783	835778.45	83387254	832867.20	93410921	834255.10	83400634	1000000	93325678	83346651	83354373	133543.70	833563.70	832315.56	03348100	4414144	93129.700 *******	833376668	
input for	Coordin	622324.11	822330.25	822345.74	622408.45	922543.00	*********	522386.41	85125228	822496.58	832614.05	877678 09	2000000	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	ET1441 AA	E22398.31	822397.16	822463,30	822432.88	822462.40	822567.47	822556.02	522482.05	85242538	822350.48	522316.11	622354.80	822374.91	2074178	1000000	27.292.72	STEAMS, TO	522119.68	100,000	942178.07	10777750	044478	RPTYTE 18	672405.79	827411 11	822055.71	822672.07	822129.94	822178.17	627221.21	82228	822284.50	822311.12	822318,58	\$2235.17	822360.57	872320.48	62246367	822081.65	822010.68	821955.43	821977.96	621862.33	622080.21	822 (23.44	822163.25	82200228	82212203	25,144.60	27.44.67	622128.55	822 (23.04	82211230	822062,06	621014.78	822039.23	27 689 75	62188331	821947.50	\$22008.03	822028.73	621952.62	821834.07	97,481,78	B21/78/07	411782.15	821826.73	
e 4 in	3	633125.78	127771228	833231.08	833434 B)	633960.46	B1010E01	633425.19	633596.26	623673.75	131633,67	633973.71	002225.00	*******	611782 11	633681.17	613693.59	833978.15	633696,64	813 HB 3. S4	823387.36	835423.89	633416,00	E13447.62	233544.64	133488,77	833587.56	613633.17	423002.07	10,802,01	833393.06	TO CONCESS	833073.42	833100.63	833232.00	20,277,000	********	REAL PRINCE	213848.74	815047.83	833076.99	813121.78	823255.39	833368.77	E33624.34	633653.40	E13694.68	833761.98	833765,11	813133316	E11502.96	833950.40	E34125.90	£14231.72	834322.77	833097.20	613156.56	#13101.87	833434.18	38.367653	833734.66	833438.83	633586.71	613649.55	833743.66	533757.63	623734.53	833778.49	833873,29	634195,21	E13867.79	24050.74	633139.76	813298-86	49.094.03	833543,73	633460.98	77.091073	833715.00	613164.01	\$33178,74 **********	833249.90	
C	Road	R003	R003	R003	11003	R003	BOOK S	9:00:6	Ross	READS	Roof	REGS	B0004-0000	BOOK - DAGT	Signal a Start	RDIS+R009	ROOM-ROOM	R010+R011	Agid-Hott	B#13+8014	RO12+R013	R012+R013	RD12+R013	RDC2+RDC3	RD12+RD13	Rota-Rots	REST &- RIGHT	RQ16+BQ17	MOLD	1700	MOZZ	777	KOZZ	NO.	6756	1000	1700	BANK	Rebo	#400#	R012+R101	RESTS	Res4	ROSS	8656	REST	Rate	R028	8,049	RE41	N042	N943	1044	Ross	H947	HOM	8049	1000	Resz	RESCO	RIGH3	H054	H054	1000	100	R054	RIDES	MONE	#(057	Resa	HOK9	2000	ROSZ	Ribts	HD64	#100 W	H054	MORE	N N N	1000	HOSE HASE	Nore	

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	Y2	821675.22	821697.57	621875.23	621860.04	82388238	\$21EPR.77	921286.99	821822.32	82188436	82187128	921812.09	82100075	92389148		100000	*********	***********	87,1887.78	20000		**********	# S4 # A B P	42147442	621546.25	421612.64	621533.58	821546.45	821508.35	***		641860.01	40 198128	\$21786.57	821657.75	821805.82	823531.57	821886.87	821862.03	82.828.159	821766.33	\$21725.47	621453.37	821894.44	821508.87	821634.13	\$2164E.31	82189824	A DA ESTE A V	\$21548.43	822414.27	822332.11	82225635	822180.58	822008.55	822368.38	822287.K3	62221223	BESTORAK	822060.94	8230228	822360.57	622271.35	62220123	8221228	200010200	*********	100000	100000		1000000	0.77770	20 10 177		82217471	822275.46	822221.31	822253.72	822175.17	822080.75	822007.87	621362.76	823883.06	822178.07	#12170.84	822129.44	Section 1	And in case of
iate (m)	X2	83536724	833501.75	833397.14	833491.50	83350597	833548.68	833603,43	833684.92	031553.57	833600.48	83367384	83381832	633887.01	4000000		2701075	********	9330013	13341011		*********	*******	8336an 24	43364167	433713.63	83340348	83369683	83369649	*********	03520000	933416-20	033487.03	93151163	93357430	133600.16	93371268	83137008	633427.36	133480.60	83352246	833542.19	833562.07	033501175	83366893	833337.84	13344358	83111168	RITMAKET	83164849	63401877	834127.62	83421631	834309.95	834407,44	833961.76	834091.39	834161.93	134273.01	83438438	626460874	83390256	83330988	833994.47	834077.01	200000	3074367	27700000			100000	93300076	0000000		*********	83356351	83363436	633386.00	033350.77	933454.10	83346051	833481.00	633506.57	80222258	63324339	83316663	Street of Street	
Coordin	٧.	821859.29	821875.22	821860.54	621795.34	821861.09	821897.80	821899.77	621086.09	821684.14	821884.38	121171.20	621822.35	SCHOOL ST		10000000			201/22/20	1100011	********	B11687 A1	********	E21454.64	821675.62	201446.36	821648.89	821583.58	821508.43	*******		94109604	621000.51	821841.09	821786.07	821657.76	821505.82	821891.86	821646.87	821952.03	821629.25	821786.30	821725.47	821553.37	821594.44	821829.64	821632.03	821646.31	67403413	621501.72	822454.38	822414.27	82233211	822256.36	822180.68	822431.11	822378.04	822238.06	122313.33	622136.63	96.650228	822405.79	831335.17	822271.38	022.200.73	84411.04	BOOKED DE	*************	*********		100000	11111111	4477774	20000000	B0738 NO	822315.75	823278.46	822232.03	822232.03	822175.04	822086.70	822007.66	821952.76	822239.78	822178.06	872182.63	20,000,000	
	X1	633327.51	822397.24	833451.80	833281.64	633443.48	82350 C.68	833548.00	633663,43	533556.57	433653.67	H33600,48	633682.38	*********	********	107/46/27	200000		20000	173436.83		Division as	811685 85	613105.34	KINGS 24	411681.67	833568.70	833603.88	STOREGE AN	21116414	********	633369.00	633478.00	613487.61	833633.63	833574.80	633690:16	e33255.85	833370.0E	833427.36	633.480.60	£13522.48	833543.19	833562.07	633598.99	27.625552	833337.92	833443.84	63337.64	613609.53	832565.68	834628.77	634127.62	ENTHER	834309.05	633917,63	SETSERI SS	834090.84	834151.86	83427334	634363.46	813848.76	833633.16	833303.65	613994.00	0.0000000000000000000000000000000000000	074150 00	200000000000000000000000000000000000000			200700	833761.80	517896.78	207,000	*******	ETSABBASE	E35563.61	833377.80	633377.68	23398-42	833433.02	833460.45	633483.00	10.002513	13212.03	E33060.91	Security 1	
Road	Pair	8071	Ratt.	HOT3.	H57.6	8175	Pig76	F-07-6	8676	REFT	FI077	F1017	#078	Briefe B	2000	None of	2000	200		MUB.	-	200	2000	ROSA	ROSE	RABIE	ROBG	RESE	9087	Bedde	0.000	2000	MORE.	ROLL	ROSS	ROBE	ROSS	9,000	RORS	R089	ROSS	Ribbs	Rotte	#100 H	RORS	1608-0608	S092+R093	592+8483	BOSA	RANK	0000-R007	5050-R000	1446-R161	1902+R102	1104+R104	N 106	R107	Ritte	R109	R110	Rett	Arr2	RT13	ATTA	RIES			2000	2000	N. C.	N. C.	27	27.11		8476	8127	Reza	R129	R13G	Rede	R122	R133	RESA	Retail	Retail	8137	1011	

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X1 123.28.49 123.28.40 123.28.40 123.28.40 123.28.40 123.28.40 123.29.40 123.29.40 123.29.40 123.29.40 123.29.40 123.29.40 123.29.40 123.20.	Y Y X X X X X X X X X X X X X X X X X X	X2 233316.58 53316.67 53316.77	Y2 82380.437	(Including mixing zone)	(m)	(caline 4)	Hr00	토
10110110101010101010101010101010101010		13331558 13331598 13311971	823881.8T	13			82.6626	87.1
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820 194 79 820 195 84 820 195 85 820 19		133118717		- 43	a		53.8940	49.4
123.00 A 10 A		13317874	821834.01	18	0		88.0443	87.7
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202728.5. 253728.6. 253774.60 253774.60 253774.60 253774.60 253774.60 253774.60 253774.60 25369.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 253699.37 2536999.37 253699.		83100438	827816.03				79,1227	74.9
233774.00 233774.00 233774.00 23377.40 23377.40 23377.40 23377.40 23377.40 23377.40 23377.40 23377.40 23377.70 233		833931.13	82122128	- 10	a		69,6468	70.4
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12.25 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2		633807.73	82168438	13	0		64.1527	62.0
123-195-2 (1) 12		93366771	827803.87	. 11	Ď.	,	64.1517	62.0
12369.2 10 (25391.27.4 (10 (25		833683.50	821543.73	17	0		64.1527	620
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123.06.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0		833828.17	821509.55	20	0		64,1527	62.0
123962.00 123962		83401E77	\$22414.27	16.	0		65,0244	653
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62366.57 6346.57 6346.54 6346.54 6356.54 6336.54 6336.57 6336.57 6336.57 6336.57 6336.57 6336.57 6336.57 6336.57 6336.57	4	83390825	\$22271.35	1.0	0		82.4165	79.4
10 10 10 10 10 10 10 10 10 10 10 10 10 1	M.Z.C.ZZ	83382777	88223228	- 69	0		85,0130	82.4
15400-23 15400-23 15400-34 155	822172.98	83277268	6221533		0		81.2844	813
EMONG 29 EMONG 46 EMO	822299.62	134112.90	152344.31	13	0		61.6802	620
624624.50 62369.52 62369.34 623623.31 62362.37 62362.32 62362.32 62364.37 62364.79 62364.77	822287.63	834137.62	822232.51	- 10	0	+	68.4873	68.0
137893.06 137893.06 137893.07 13782.04 13782.04 13782.04 13782.04 13784.07 13784.07 13784.07 13784.07	-	834075.91	\$22.25W.62	. 51	a		62.4817	62.0
623993.84 623953.37 623872.44 832868.47 632778.44 632778.44 823888.52 83388.77	-	83409038	822287.53	18	0		68.9157	68.5
61367.34 61367.34 81368.67 613778.44 61378.44 61358.77 61358.77 61358.77 61358.77	-	634034.90	822280.01	118	0		65.2514	553
61367.2.4 83368.2.7 83368.3.7 69778.4 69778.4 63368.0 63368.7 63368.7 63368.7 63368.7 63368.7 63368.7	-	534048.42	82223828	16			66.4630	66.2
62367274 63361372 63377844 63377844 63356137 63356177 63356177	+	83399447	822201.53	. 91			673777	699
83368.92 83368.92 83568.92 83568.78 83568.78	+-	83396475	622168.55	1.9	0		56.2866	147
\$35613.72 \$3561.78 \$3561.78 \$3561.78 \$3561.78	-	834007.86	822189.33	10	0	-	83.4734	83.3
E23684 92 E33581 76 E33581 76 E33592 77 E33513.08		83387636	822050.03	21	0		32,2805	316
633498.77 633498.77 633498.77	-	82381249	#21976.52	8)	ø		44.0777	44.0
633498.77 633498.77 623513.09	-	83377938	821867.65	20	0	4	68.5469	67.6
633498.77	821677.50	82268328	421523.55	. 91	0		70.7537	70.0
613513.09	621608.49	83356547	82168673	26	0		65.1627	643
#1144A 44	821599.24		\$21558.47	2.6			72,7475	72.6
823860.04	-	933413.00	821608.61	. 81	0	1	71.1988	70.8
833451.64	121526.21	133911.32	621609.38	- 11	0.	4	77.0005	594
634218.31	-	834315.96	822258 33	- 69	a		73,9636	73.8
624181.98	2	10312168	822256.35	- 14	a		72.3870	66.2
834140.62	-	834484.78	6222228	- 48	0	4	70.0219	693
834099.34	-	834149.62	822162.07	18	0		75.3841	76.6
634877,01	-	034061.51	822109.94	13			79,1261	76.8
E34051.51	-+	834971.50	822284.18	13	0	4	79.1261	76.8
834071.90	-	834297.30	822118.02	1.4	0	-	79.1261	76.8
834308.05	2	03431286	822267.44		0		72.4055	71.9
634231.54	+	9342/334	HZZY3A.B.		0		78.1575	78.8
55-041 FC2	-	834211.78	822096.45	2	0		76,7200	78.6
834004.BI	-	3401634	921580.22	18	0		70.5363	69.5
633831.13	-	034004.90	821816.03	10	0	-	74.6614	76.4
633 FF 52	-	831916.85	821727.98	7.0	0	-	60,0390	593
613838.79	-	833867.51	\$21681.48	- 28	0		91.0319	87.7
02 835761.01	-	933-828-17	821503.58	30	0		89.5592	90.1
EMM4.30	-	83440018	82210471	- 43	0	+	79,1988	71.6
634322.77	-	83436436	822061.94	. 16	0		71.1262	68.7
	-	93432300	822010.48	19	0		80.9786	80.6
834239.17	-	83429004	621962.18	**	0		78.0650	74.2
634238.17	821814.13	834317.68	621648.33	14			78.0030	74.2

Hr23	58.7887	51,4504	64.6214	63.5943	48,6374	44.6038	79.2542	79.2542	79.2542	74.1582	74.1582	69.9889	57.1088	56.7998	57.5687	68,488A	68.6175	68.5076	68.752K	61.6174	67.5676	61.7056	60.7786	63.0730	65.6762	47.9519	76.0815	30.6434	41,2729	62.7636	69.8609	70.6214	62.8093	78.5330	71.5727	25.0416	74.2111	76.3046	47,4047	47.4047	47.4047	74.0215	76.3046	83 5059	72,3040	60.4564	94.1187	95.9638	79.2542	85,0070	77.0916	75.0186
Hr22	74.9282	62.4423	78.A456	77.8878	64.0011	59.5702	97.4906	97,4906	97,4906	9734906	92,4906	89.4714	72 9017	723854	74.5390	87.3832	85.5360	83.0752	79.7348	75.4819	80,4072	75.6071	74.9259	77.2362	77,1372	58.7749	84.3667	42.1508	503505	0019'52	83.9959	80.5910	74.3973	893825	165608	92.4521	89.2316	861725	65.4113	65.4113	65,4113	88.5640	861775	30,0001	87.2455	61.1930	100.0409	94.3254	97.4761	85.0566	82.7910	DESCRIPTION
Hr21	80.2419	65 3913	82,8554	82.0399	1968.59	59,7916	100.4816	100.4816	100.4816	100,4816	100.4816	97.8405	76.4215	76.3461	79.1924	91,6788	90,3554	88 1036	85.9340	£2,1699	\$7,8276	82,1267	\$1.6363	83,9461	83.1677	60,3216	54.3091	43,9162	519813	81,8135	90.4863	86,9808	80.1596	96.0796	58.6215	99.4371	99.3308	97.2705	67,1802	67,1802	67.1802	95.9335	93.5879	44 2216	94.2392	63.8859	103,4469	97.9122	105.4493	93.4756	96,4582	
Hr20	63.8551	52:0382	68.1766	67.0391	50,6433	47.1141	81.1802	84.1802	84.1802	84.1802	54.1302	81.8699	60.4337	60.6938	62.4750	79.0384	77.0945	74.9784	72.0099	66.8921	72,4957	5658.99	66.0952	68.7921	71.1061	48,8786	79.9040	31.6946	42.7535	67.6317	77,4883	73.9955	66.0917	83.7803	76.5899 8ri 9018	81 7411	79,2263	79.4761	51.8148	51.8148	51.8148	80.1249	76.4515	21.5028	78.4782	60.3997	6298 96	68.9120	72.6283	83.8103	83.8689	
Hr19	54,1526	47 3365	61.4886	\$8,6159	44,9816	39.7153	71.9169	71.9169	71.9169	8008.69	59 NDOR	66.9545	51,4156	52.5140	52.8079	70.9654	5905'69	65.3786	6838.09	55.9997	63.0685	56.3246	55.7407	58,0265	651119	44.4115	70.1520	28.4434	39,5862	58.6825	68.3883	65.1203	57.3396	74.0720	66.1586	69 2694	66.3175	6818 99	43,9683	43.9883	43.9883	68.2043	64.6460	19.7073	67.0885	50.2977	89.6716	82.7273	61,4878	65.2473	76,0905	
Hrt8	53,4735	44.2195	60.9186	59.2787	43,5035	37,7732	73.8022	73.8022	73.8022	71.9262	71.9263	67.7657	1861 05	51.5942	52.0834	71,9257	70,7085	65,1015	60.6601	56.2715	62,7365	57,3421	56.4876	59,4935	11:05:09	43,2865	68.7712	26.0022	37,7284	58,7197	68.6835	66.1536	57.7358	76.1554	68.1598	70.9501	68,1029	64.9098	43,2954	43.2954	43,2954	69.5713	62.6783	20.0714	67.2364	46.7378	89,6193	82.2320	53,2837	1116.59	74.5908	
Hr17	54,4054	45.8167	62.4663	61.0425	45.3289	40.5253	71.8255	71.8255	71.8255	70.3559	70.3559	68.1396	51.3449	52.6723	54.380A	75.8694	71.6548	65.3893	61.2396	57.1052	659219	56.0345	57.8540	59.6465	8318.19	46.4874	71.3468	29.1438	40.1877	59.8425	71.4263	E2.3098	59.3115	75.8812	67.1138	71.7850	88888	64.0919	44,7655	44.7635	44.7655	9116	62229	61 03.00	67,2430	50.1863	88 6517	91.8379	613613	67.2523	77,4108	
Hrde	54,6166	48.1369	64.6102	68(9) 99	44.4713	40.4689	72.4238	72.4238	72.4238	67.1727	67.1727	66.1258	53.3720	53.9092	56.2186	77.2830	73.3585	66.7851	62.9604	59.4447	64.6201	60.2385	59.2206	60.6324	63.8014	47.5472	78.0924	30.1282	40.8315	61.9823	72.3306	68.4298	62.1892	76.4694	71.4748	69 6663	69,7730	0685-59	47.1265	47.1265	47.1265	72.4748	62.2856	63 6473	70.3083	\$2.1615	88.5557	83.5420	65.6690	70.3285	69.7213	
Hr15	65.6524	52 3692	72.9335	71,7809	57.8657	50,6140	67.4130	67,4130	67,4130	67.4130	67.4130	67.1000	57,6102	58.3478	59.0637	82,7234	78,5049	1272.17	63.4653	62,0828	5985.99	63.7415	62,4570	61,7872	66.1418	52.1473	80.0792	32.8290	43.2076	64,4985	73.8506	69,6525	623059	77.2596	73.4622	73.9647	70,2060	68.4933	54.5768	54.5768	545768	74.0677	66.2525	25 4536	72,2693	55.9919	88.9181	843970	9996'89	70.8313	71.2898	
Hr14	64,6414	49.5873	74.1271	5096'04	57.9457	50.8849	54.8703	64.8703	64.8703	64.0379	64.0379	61.7367	54.1077	55.3474	55.5264	80.2293	76.8894	69.8051	58.4288	5E 8563	8789.19	60.0643	57.8159	58.7154	61.7872	49 5065	73.5772	30.2233	41.6778	61.0925	69.7423	64.5290	62,2009	72.1950	68.3725	67.7394	54.4902	6K.0945	53.3688	53.3688	51.1688	65.0541	67.3297	63 3001	66,7425	521727	86.2534	K2.1347	64.3077	2599399	67.6092	
Hr13	72,1663	50.2815	79.6391	78.3518	52,9855	0665.96	66.8529	66.8529	66.8529	66.8529	66.8539	54.9656	59.8392	59.5038	61.7335	94.9899	\$5,2315	9121.77	53.6143	56.6984	66,4231	66.1176	5895-89	6889'59	56,2836	49.9105	33.0995	29.4157	42.1700	0909'99	75.9320	58.4013	58.0697	76,777.1	N 2474	73 6526	72.6737	73.2973	8858.65	8858.66	59.8588	74.5418	73.6525	60.9529	73,2441	60.2529	38.8057	78.0095	54.9621	77.1272	74.2727	
Hr12	75.3273	54.9342	82,0940	HO.8554	67.5401	61.7915	67,0854	67,0854	67,0854	67.0854	67.0854	65.7028	51.6797	62.8718	63.4573	89,5430	86.1534	27.7.72	63.8402	609699	66.4894	66,8932	64.5414	64,2540	67.5513	54,7162	82,2164	34,6191	46.8346	66,6717	74.5893	68,4329	111119	75,3184	75,0129	74 6353	70.5261	74,4129	64,6696	9699799	64.6696	72,6109	74.9078	619517	74.7194	60.7854	90.0213	RS 9795	63.6131	70,4108	76,0836	
Hr11	81,2137	55.5435	19.9272	86.5964	73,4893	66.7825	0900749	0900'29	090079	H	H	66.3192	64.3495	65.5712	65.9592	93.1590	90.5248	81.6672	56.7195	70,1439	68.5399	70.3752	67.6219	67.1283	69.8082	56,6689	87.0395	33.7283	46.8584	6620'02	77.4698	70,1882	71.5078	+	78 9082	72 3277	71,9027	76.2296	71.0742	71.0742	71.0742	+	+	20.4000	76.0327	62.0617	93.8994	81.4914	77.8507	71,4366	76.9301	
Hr10	80.1708	55.2900	89.6318	85.8545	72.0036	66,7183	64.2301	64 2301	64.2301	64.2301	64.2301	63.6717	64.8510	64 5822	66.5756	91.8583	92,2017	82.4519	1820'59	67.5268	9020799	Н	65.2014	64.2538	6569729		Н	33.4501	Н		+	+	69.6446	73.9050	76.2137	٠	t	74.2487	70.5959	9665.00	70.5950	71.9405	74.6068	50,7622	73 0611	58.8695	89.2669	79,7256	75.1721	68.0723	79.5846	
Hr09	89,0541	56,4327	96.8312	93.2643	81,0685	74.6466	66.5354	66.5354	66.5354	67.0375	67.0375	66.5354	+	٠	72,5577	98.3667	-	89 5024	66.1611	-	68,6294	-	70.9155	71.1574	71,0679	60,3084	Н	34.7265	Н	-		4	75,7462	+	81.9720	٠	71.7673	9872.87	82.2740	82.2740	82.2740	76.2517	79.7464	63.0279 71 15.74	78.7126	62.7638	91.9638	RS-4502	80.4915	72,2018	54.8101	
Hr08	76.2556	48.6219	85.9002	81.6692	1829 99	61.6035	54.3760	54.3760	54,3760	H	+	t	t	٠	+	84.7410	92.6376	77.4547	56.6289	63.9331	1969'85	63.9379	61.5656	60.6783	64.2581	52.5589	85.9470	28.0788	43.1688	120619	71.9632	+	+	+	73.0811	t	62.9516	69.5370	67,3209	+	1	1	+	75.4302	+	t	╁	۰	786279	59.3454	75.3486	
Hr07	97.1922	671165	98.4529	97.9754	87,9030	82.6454	75,7894	75.7894	75.7894	75.7894	75,7894	t	78.8219	H	٠	9092.90	108.5255	94.3646	72.2229	81.9044	76.6926	81.6413	78.7819	77.6152	78,7122	66.7226	99.7195	39.7862	51.6292	81.0374	86.6394	+	+	+	89.4731	+	81.3334	87.6037	90.2360	90.2360	1	+	+	90.8000	87.1853	+	96 9922	92.1079	85.5694	81.6313	90,7498	
Hr06	84,1696	6515-53	89.3120	89,1353	78,8726	72 8490	63.8449	63.8449	63.8449	65.8539	-	+	-	H	+	84.5362	86.9965	82.9820	62,2319	71.3428	61,4419	70.4083	67.1876	67,9380	69.0155	57.8353	85.3238	33.2715	45.0268	69.3468	71.9489	66,5728	74.0895	+	78.5420	77 3505	72.2774	76.7092	80,928	80.923		+	+	72.4284	+	+		-	62.1141	68.1141	85,2674	
Hr05	87.8549	53 9436	97.0508	1 7997	75.5733	76.7530	73.3824 6	73.3824 6	73.3824 6	-	H	+	H	H	+	77,4345	82.3262 8	83.0164 8	65.4155 6	70.3655	63.3247	69 9421	67.0261 6	67.7291 6	68.5697 6	56.5354	84.958N B	32,4659 3	45.6242 4	69.3518	71.1632 7	66.6261	74.2465	+	78.787.8	67 9051	74.8309 7	14.1792	90.6854		1	+	+	37 4650	+	H	+	۰	150675	63.6450	1089'06	
Hr04	36.9518	19.0231	8 1659	38935	821578	E695 UK	57.8044	57.8044	7.8044	7.8044	77.8044	57.804A	57.3585	8.0726	16.5812	77,1161	12.0668 8	333416	19.981X		54.5492	9 6740	6.3446	16/2/85	57.3897	56,4489	15.6223	32,0353	15.6826	81.4218	70,6657	56.8936	13.3723	73.1023	78.1863	137750	10.4184	10.6667	75.6416	76.6416	76.6416	76.0904	089668	51,4979	9 7213	34.5345	M 8550	\$5.6335	57.8044	57.8044	7.4552	
Hr03	72,7265	513469	87.8421 8	88.8776 8	59,6689 9	86.3281	67.2858 6	67,2858 6	67.2858 6	67.2858 6	67.2858 6	67.2858 6	65.1583 6	65,7201	65.0186	78.6054 7	81.2479	82.2975	64.8486 3		62,2312 6	69.4154 6	65.6216	66,4097 6	67.4835 6	56,0856 3	84.1884	33.3558	43.9911 4	68 5735 6	71.4303 7	66.2558 6	73.3903	72.1087	77.6900	67.2858 3	71,7722	80.0500	76.8070 7	76.8070 7	76.8070 7	73.4421	84,3048	75.55149	77.8695	61.1705	94,6630	84.8079	6899 6	59.6689 6	89.9287	
Щ				86.6112 8			Н	Н	-	Н	۰	٠	۰	٠	-	78.0120	-				62,4077 6	н	66.1564	Н		55,4014 5			-	67,6873 6	_	_	72.9668	-	76.9133	+	+	۰	Н	Н	+	+	82.5405	+	+	٠	٠	۰		_	-	
Hr01	81.1415 7	49,4938 5	87,7233 8	87.1222 8	74,9693 8	Н	62.0198 5	62.0198 5	1	۰	+	+	۰	+		79.4762 7		81 3009	62.0567 6	Н			65.5377 6		66.9037 6		83.3843 8					64.9225 6	72.6626 7	70.5148	76.5335		т	⊢	Н	н	-†	\neg	7	78 5019	+	۰	1	+-				
Hroo	_	53.8940 4	88.0443 8	⊢	79,1227	Н	64.1527 6	54.1527 6	-	۲	۰	+	+	+	+	-	-	Н	1.6802 6	-	$\overline{}$	Н	-	66.4630 6	57.3777 6	56.2806 5			-	+	\vdash	65.1627 6	72.7475 7	1988	77.0006	+	₽	-	Н	-	+	+	+	10,7200	+	₩	+	٠	٠	71.1262 6	-	

Road	X1	Y1	x2	Y2	(including	Height (m)	Road Typ (caline 4)
Rt03	833125.78	522324.11		821530.25	mixing rose)	0	- to
RSSS	833177.37		#13231.06		20	0	- 1
R003	833221.06	822345.76	833414.80	822408.45	20	0	1
R(0)	832434.80		933900.46		20	0	
R103	833966.46	622643.96	533995,46	621646.78	20	. 0	
RIOA	833116.28	822308.10	41341551	822315.62	19	0	- 1
R004	833185.93	822315.62	833425.15	822296.41	19	0	4.
R004	833425.15	82238E.41	833518.28	822421.55	19	0	- 1
R005	833616.28	822A21.55	813573.75	822496.58	19	0	- 4
R005	833671.75	822 494 SE	E11913.67	822414.65	19	0	4.
FI605	633933.67	822614.88	W33973.71	922426.00	19	0	1
R005	833973.71	622626.09	834046.10	822626.54	19	0	- 1
R005+R007	833527.80	622410.61	633637.55	822455.21	14	0	1
8505-R507	833627.55	822A55.21	833732-97	822494.A7	16	0	1
R006+R007	833732.07	822494,47	833782.11	922441.6B	14	0	4.
1004-R507	830782.11	822441.65	813840.01	822456.02	14	0	- 4
1003-R009	833661.17	622398-31	533693.59	822197.15	12	0	
1003+R009	\$33693.50	822397.15	E11841.E4	822456.38	13	0	4.
1010×R011	833978.15	822463.30	832094.64	822452.88	12	0	1.
1010+R011	833896.64	622432.68	933993.54	822462.40	12		
(株) D+ R(1)	833683.54	822A62.43	833840.51	822456.02	12	0	- 7
1912+R913	833387.26	822567.47	833413.50	822556.02	10	0	1
1012-R011	833423.00	822558.02	832416.08	822482.07	10	0	- 1
1012-R013	833416.08	822482.67	833447.62	022425.39	10	0	1
田12・円113	833447.62	822425.39	#13544.64	627190-A1	10	0	- 4
1612×1613	833544.64	822390.48	833547.56	822334.00	10	0	1
014+R015	833544.64 833488.77		#33547.50		18	0	1
014-H019	833587,56	822354.88	#32597.56 #32533.17	022374.91	15	0	1
助うち・用力37 助うち・用力37	833631.17	82235-4.95 82237-4.95	833661.17	622398.31	15	0	1
R019	833613.17 833082.67	822374.91	833561.17	622398.31 822239.78	16		1
1000			35.55			0	1
R021	833209.07	822239.78	833315.00	823393.72	16		
R622	833555.60	522291.72			18	0	1
R022	R334E0.61	822340.13	833419-65	622315,71	16	0	- 1
R023	835072.42	822119.68	833100.53		18	0	7
R624	\$33100.53	822129.44	833232,04	822178.07	74	0	- 1
R125	#33232.06	622178.57	633377.69	621132.01	16	0	1
B1528	823377.89	822232.63	83359334		18	0	1
8027	633502.51	822278-46	822073.82	822281.72	13	0	1
R028	832673.82	\$12341.72	833768.11	822375.93	13	0	1
R629	833766.63	822374.15	833848.76	821405.79	13	0	- 4
ROSO	\$33848.76	822405.79	E13917.E3	822431.11	18.	0	4.
FIGS1	633917.63	822421.11	932940.58	822454.38	14	0	1
1637+R301	833070.99	\$22015.71	933121.79	822072.07	18	0	7
8833	833121.79	622072.07	£13252.39	822120.94	18	0	1
R034	833253.39	822120.94	833398.77	822175.17	18	0	1
8935	#33396.77	822176.17	£13524.35	822221.21	18	0	- 1
R034	633524.35	822221.21	#32913.40	822269.00	78	0	- 1
R637	633653.40	822269.00	833694.86	822284.07	19	0	- 1
RESE	633694.68	822284.56	833763.79	622309.61	10	0	- 1
ROST	833761.98	822311.12	823788.45	822329.76	14	0	1
H040	833789.11	822318.08	833833.16	822335.11	18	0	-
R041	833833.10	822335.17	833902.96	822360.57	18	0	
RIA2	833902.96	822360.57	£11965.46	822320.45	-18	0	1
8043	813050.46	822320.68	83401490	822250 A2	14	0	1
R044	B34024.90	822250.62	#34140.62	822250.52	18	0	1
RISAS	834140.67	822182.67	834211.76	822086.45	19	0	-
	834231.72	82218-E-R7	834303.21	822000.45			- 1
RISAS				-	18	0	1
ROAT ROAR	83A322.77	#22910.68	834354.01	821939.48	- 16	0	- 1
	833097.20	821988.43	833156.56		17	0	1
R549	833159.68	821977.96	833434.10	822580.78	16	0	- 1
R155	833101.47	821942.33	E3327446	822007-01	21	0	1
R051	833274.56	822604.80	233416.70	822067.62	16	0	1
R052	833434.10	822080.21	832668.33	822174.73	16	0	1
R153	#337#6.#E	\$22123.44	513736.66	822163.25	18	0	1
R153	833736.68	622161.28	811898.13	0111111	16	0	- 1
F1054	833438.83	822967.29	#3251671	822122.03	16	0	
PIQS4	#33584.71	622122.03	933649.DS	822144.40	- 48	0	- 1
ROSA	633649.55	622144.40	833683.68	822152.80	16	0	1
R254	633663.68	622152.80	813712.65		- 16	0	- 1
ROS4	623712.85		833757.83		16	0	4
PI054	633767.83	822128:65	\$33778.A9	822113.30	16	0	1
R053	833786.53	\$22123.04	533872,14	822651.30	19	0	1
R256	833778.49	822113.30	8118h7.20	822039.12	16	0	7 -
ROST.	#33673.20	822082.68	834119.21	821B1478	16	0	- 1
ROSE	634159.21	821614.78	834210:10	821738.42	16	0	- 9
RUSS	633867.29	822039.23	43485E34	821680 22	-97	0	- 1
8089	834058.34	821380.22	834241.51	821727.AS	16	0	. 1
R061	633116.37	821890.28	833139.76	821889.31	16	0	- 1
R082	633139.76	821889.31	833296.78	021947.78	16	0	- 1
RIBS	833256.88	821947.56	813410.51	821007.91	16	0	- 1
ROSE	833460.49	#2250E.03	#11543.73	822038.J2	13	0	7
H064	#33543.73	#2290E.E3	¥33843.70	821983.31	15	0	,
200.00	833480.98				15	0	- ;
DAC.	83316G.17	821962-82 821834-07	813543.70	621591.07	16	0	1
R064		821834.07 821891.68	#33491.00		16		
R085			#43491.00	821952.78	16.	. 0	. 1
ROSS ROSS	833316.56				- 11		-
ROSS ROSS ROSS	833164.01	821778.07	83317847	621765.68	10	0	- 4
ROSS ROSS				821783.88 821813.88 821795.91	19 18 29	0	1

											NO ₂ x 10	0 (all/MT)											
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
2.5556	2.5379	2,5214	2.5501	2.5933	2.5925	2.6327	4.2904	43828	3.6440	1.3399	3.2040	2.8146	2.8877	2.8993	3.2569	3.4892	3.3329	3.4268	2.9244	2.6001	2.3865	2,4759	2.5987
2.5556	2.5379	2.5214	2.5501	2.5933	2.5925	2.6327	4.2904	4.3828	3.6440	1.3399	3.2040	2.8146	2.8877	2.8993	3.2569	3.4892	3.3329	1.4268	2.9244	2.6001	2.3865	2,A759	2.5987
2.5556	2.5379	2.5214	2.5501	2.5933	2.5925	2.6327	4,2904	4.3828	3.6440	1.3399	3.2040	2.8146	2.8877	2.8993	3.2569	3,4892	3,3329	3.4268	2.9244	2.6001	2.3865	2,4759	2.5987
2.5556	2.5379	2.5214	2.5501	2.5933	2.5925	2.6327	4.2904	4.3828	3.6440	1.3399	3.2040	2.8146	2.8877	2.8993	3.2569	1.4892	3.3329	3.4268	2.9244	2.6001	2.3865	2,4759	2.5987
2.5509	2.5230	2.5280	2.5678	2.5718	2.5650	2.6087	3,7923	4.0164	3.2928	3.0852	3,0088	2.7174	2.8162	2.8625	3.2689	1.5674	3,6945	3.7452	3.1502	2.4836	2.3002	2,4156	2.4748
2.5509	2.5230	2.5280	2.5678	2.5718	2.5650	2,6087	3,7923	4.0164	3.2928	3.0852	3,0088	2.7174	2.8162	2.8625	3.2689	3.5674	3,6945	3.7452	3.1502	2.4836	2.3002	2.4156	2.4748
2.5509	2.5230	2.5280	2.5678	2.5718 2.5826	2.5650	2.6087	1.7923	4.0164	3.292K	1.0852	3.0088	2.7174	2.8162	2.8625	3.2689	1.5674	3,6945	3.7452	3.1502	2.4836	2.3002	2.4156	2,4748
2.5388	2.5046	2,5323	2.5739	2.5826	2.5719	2.6142	3.7920	4.0173	3.2923	1.0848	3.0071	2.7151	2.8132	2.8597	3.2656	15642	3.6860	3.7412	3.1462	2.4784	2.2947	2,4099	2.4758
2.5388	2.5046	2.5323	2.5739	2.5826	2.5719	2.6142	3,7920	4.0173	3.2923	1.0848	3.0071	2.7151	2.8132	2.8597	3.2656	3.5642	3.6860	3.7412	3.1462	2.4784	2,2947	2.4099	2.4758
2.5388	2.5046	2.5323	2.5739	2,5826	2.5719	2.6142	3.7920	4.0173	3.2923	1.0848	3.0071	2.7151	2.8132	2.8597	3.2656	3.5642	3.6860	3.7412	3.1462	2.4784	2.2947	2,4099	2.4758
3.0033	2.6688	3.8468 3.8468	0.9306	0.9419	3.5255	2.9739	3.3522	2.5204	3.3505	1.0510	3.0417	3.2935	2.8746	2,1497	2.2634	1.2230	1.5577	0.9353	1.0867	1.1967	1.8504	1,7240	1.5864
3.0033	2.6688	3.8468	0.9306	0.9419	3.5255	2.9739	1.3522	2.5204	3.3505	3.0510	3.0417	3.2935	2.8746	2.1497	2.2634	1.2230	1.5577	0.9353	1.0867	1.1967	1.8504	1.7240	1.5864
3.0033	2.6688	3.8468	0.9306	0.9419	3.5255	2.9739	3.3522	2.5204	3.3505	3.0510	3.0417	3.2935	2.8746	2.1497	2.2634	1.2230	1.5577	0.9353	1.0867	1.1967	1.8504	1.7240	1.5864
1.9193	2 3688	2.1553	0.9306	0.9419	1.9743	1.9502	2.6260	1.8947	2.3020	2.0858	2.1636	1.9738	1.5886	1.4963	1.8817	1.2888	1.5587	1.0109	1.0000	1.2309	2.1712	2.1093	1.3557
1.9193 4.1589	2.3688 4.0953	3.6212	0.9306 2.4854	0.9419 4.5010	1.9743	1.9502	5.0907	1.8947	2.3020 4.8115	2.0858 4.4942	2.1636 4.8546	1.9738	1.5886 4.4528	1.4963	1.8812	1.2888	1.5587	3.8646	1.0000	1.2309	2.1712 5.1602	2.1093 4.6978	1.3557
4.1589	4.0953	3.6212	2.4854	4.5010	5.3860	4.2472	5.0907	4.2880	4.8115	4.4942	4.8546	4.5446	4.4528	3.9088	4.6328	4.1357	4.0233	3.8545	3.6672	4.4247	5.1602	4.6978	4.6395
4.1589	4.0953	3.6212	2.4854	4.5010	5.3860	4.2472	5.0907	4.2880	4.8115	4.4942	4.8546	4.5446	4.4528	3.9088	4.6328	4.1357	4.0233	3.8646	3.6672	4,4247	5.1602	4,6978	4.6395
11.0496	12.7348	1.1866	1.6113	1.6225	1.6276	11.1871	15.2027	9.4181	12.4546	10.4591	12.4940	11.5954	15,0482	11.0779	11.5838	11.2426	12.7498	14.6849	12.5431	19,7459	22.8849	17.9008	13,6744
11.0496	12.7348	1.1866	1.6113	1.6225	1.6276	11.1871	15.2027	9.4181	12.4546	10.4591	12.4940	11.5964	15.04H2	11.0779	11.583H	11.2426	12.7498	14.6849	12.5431	19.7459	22.8849	17.9008 17.9008	13.6744
11.0496	12.7348	1.1866	1.6113	1.6225	1.6276	11.1871	15.2027	9.4181	12:4546	10.4591	12.4940	11.5964	15.0482	11.0779	11.5838	11.2426	12.7498	14.6849	12.5431	19.7459	22.8849	17.9008	13.6744
11.0496	12.7348	1.1866	1.6113	1.6225	1.6276	11.1871	15,2027	9.4181	12.4546	10.4591	12.4940	11.5964	15,0482	11.0779	11.5838	11.2426	12.7498	14.6849	12.5431	19.7459	22,8849	17.9008	13.6744
5.1459	5.2382	5.7088	7.1215	6.7323	6.6123	5.5273	8.9010	4.6977	5.8867	5.9861	6.7816	6.3450	7.1310	5.7488	fi.6047	6.3294	6.7402	6.5796	6.1840	8.3265	10.4834	9.5395	6.8227
5.1963	5.3786	5.7088	4.6168	4.3903	6.6123	5.1328	8.3686 8.3686	4.4368 4.4368	5.6068 5.6068	5.4346	5.R910 5.R910	5.4843	5.7937	4.9289	5.4877	4.5523	5.1299	4.7940	4.2428	6.2912	7.5815 7.5815	6,1841	5.2580
13.0337	13.2092	12.0863	13.9483	14.6759	12.3156	12.5179	15.0419	11.9817	13.5731	12.1060	13.5477	12.3563	14.2666	11.1639	13.0072	13.8733	12.0737	11.8098	11.4693	15.4405	19.0242	13.7676	14.4955
12.9994	12.7356	11.6139	13.6661	12.2284	14.3963	12.9748	15.2744	12.2277	13.7458	12.1414	13.5836	12.3044	14.1110	11.2890	13.0794	12.8940	12.1224	12.1932	11.3740	15.3397	17.7947	14.5778	12.6391
16.0367	14.5283	15.8175	16.7485	16.0116	15.8923	16,2069	17.6027	14.8702	16.4981	15.1791	16.3136	15.1617	16.6363	13.8403	15,2373	16.0277	14.3837	14.1560	13.5611	16.7794	19.2178	16.2040	15.4698
16.0367	14.5283	15.8175 14.8284	16.7485	15.0676	15.8923	16.2069	17.6027	14.8702	16.4981	15.1791	15.6427	15.1617	16.6363	13.8403	15.2373	16.0277	14.3837	14.1560	13.5611	16.7794	19.2178	16:2040 15:3628	15.4698
15.1665	13.4415	14.3099	12.7091	15.0676	14.4337	14.8228	16.9306	14.4683	16.1619	14.7099	15.6680	14.0651	16.1832	13.2081	14.6378	15.1487	14.1591	13.8823	13.8269	16.4594	18.4992	15.4743	14.3158
14.7551	14.9089	13.9318	15.6267	16.2189	14.1377	14.3339	16.5789	14.1194	16.1202	14,7019	15.7467	14.2446	15.9385	13.2903	14.7894	14,7233	14.2753	14.0213	12.8272	16.0785	18.8661	15.1314	14.2101
15.7179	15.7967	15.1409	17.0782 15.4896	16.4054	15.5546	15.3944	17.9845	18.0129	18.5127	16.6044	17.3875	15.3915	17.3776	14.0539	15.6117	16.8885	15-2086 15-4548	14.2555	13.4945	16,9220	18.1607	15.0176	15.0036
12.8250	11.7266	12.7859	15.1920	14.0298	12.2425	12.9867	14.5817	12.3574	14.0521	12.5846	13.7693	12.6567	14.2818	11.8448	13.4260	13.5261	12.8285	12.9644	11.7653	15.2872	18.1298	14.7981	12.5470
11.4219	10.4258	12.6024	7.1215	9.9260	11.6758	11.7224	16.3531	13.7411	14.3092	12.1922	13.5133	11.7522	14.8824	11.4790	13,1057	15,1269	13.1731	12.5320	12.3098	16.2169	17.4869	14.4477	14.8588
11.2139	11.1681	11.6722	11.3847	10.4290	11.1935	11.2830	15.3759	12.6023	13.4639	11.4285	13.0803	12.3527	13.9650	11.0369	12.7913	13.2495	12.3608	12.2297	10.9333	14.6200	16.9732	13.2644	12.5504
10.4615	13.8899	8.1779 10.8604	9.8766	9.9260	7.1661	10.9890	16,5336	14.7916	14.9680	12.9791	13.9080	11.9783	13.5587	11.0367	13.0069	12.6266	12.6392	17.0573	11.3624	15.6423	17.3898	14.1227	13.6321
11.5676	11.5411	11.6093	11.7614	11.9077	11.6995	11.7634	13.9747	11.2429	12.6938	11.3576	12.5505	11.5025	13.1039	10.8172	12.3026	12.4390	11.9257	11.8313	10.9523	13.9293	16,2634	13.3178	12.1167
20.4276	10.5172	10.4259	10.8717	10.8256	10.9022	10.8193	13,4473	11.1893	12.0578	10.8176	12.1944	11.1489	12,7449	10.4817	12.0378	12.2099	11.7450	11.5871	10.6504	13.6022	15.8335	13.0057	11.8982
13.0450	11.8385	12.8198	12.6528	12.7915	12.7375	12.9366	15.8040 14.5888	13.5661	14.6877	13.3438	14.3072	13.3882	14.8746	12.1529	14.1741	13.1533	12.6545	12.6168	11.6928	14.8719	15.5894	14.3314	13.4973
16.0813	15.9150	15.9647	16.1907	16.1007	16.0992	16.2509	19.3282	16.4372	18.2447	15.6401	16.9140	15.0836	17.0537	13.3828	14.7909	14.6856	13.6000	13.2475	12.3152	15.5198	17.8989	14.6778	13.6855
16.3023	16.1602	16,2779	16.2818	16,4411	16.3691	16.3973	19.6433	16.5903	18,5220	15.5692	16.7650	14.6976	16.4976	12.7143	13.9937	14.0806	12.5187	11.7747	11.0405	13.7814	15.8712	13.0571	12.3122
19.1985	17.8744	18.1109	18.6535	18.6871	18.5604	18.4568	22.6239	21.7248	21.4041	18.7597	19.8770	17.5771	19.6441	15.1969	17.6256	17.8015	14.8796	13.3272	13.3795	16.0117	17.8252	14,1540	15.1961
18.7981	18.8567	18.8670 18.5729	19.3119	19.1222	19.2928	19.2424	22.4388	20.9403	21.1575	18.4495	19.1524	17.0126 17.5726	18.9894	14.5634 15.1685	17.0509	17.2767	14.8206	13.2110	12.9142	15.E387 16.0298	17.2591	13.8731	14 9503 15.2201
19.2531	18.4943	18.5729	18.7699	18.7486	19.0504	18.9092	22.6134	21.1283	21.3789	18-2312	19.3257	17.0787	19,1435	14.6893	17.5069	17.6563	14.6911	13.0385	12,8078	15,7775	17.2809	13.9099	14.9726
21.5908	21.6330	21,7501	21.8001	22.1275	22.0634	22.0167	24.8088	23.6242	23.4854	20,6970	21.9953	19.5541	22:0743	17.0579	20.0164	20,4997	17.3306	15.5634	15.4032	18.2938	20.2743	16.2673	17.8794
18.8673	18.7112	18.6471	16.9249	19.0896	19.1386	19.2165	22.3888	20.5194	20.7443	18.2448	19,1873	16.9507	19.2454	14.5686	17.2919	17.5683	14.6459	13.2171	13.2731	15.5386	17.0978	13.7194	15.2760
19.3703	18.2589	18.3938	18.8279	18.6514	18.8434	19.6520	22.6950	21.2899	21.4922	18.4885	19.5376	17.3356	19.2647	14.9904	17.2490	17.7945	14.9278	13.3486	13.0957	15.9764	17.3952	14.1217	15.2051
19.3746	18.1458	18.4799	18.6914	18.8583	18.7596	19.5744	22,7274	20.8682	21.0439	18.5047	19.6158	17:3693	19.3220	15.0376	17:3312	17.4733	14.9817	13.3506	13.1106	16.0268	17.4377	14.1798	15.2338
14.0857	13 6109	13.6358	13.7152	13.7862	13.8250	14.2149	17.1116	16.5166	16.6362	14.1991	153025	13.7042	15.9707	12.4289	14.5150	14.9782	13.3943	12.8790	11.8901	14.9747	16.9907	13.6433	13.5748
15.0470	15.0030	15.0518	14.1231	15.1281	14.1650	14.2592	16.8806 18.1573	17.0566	16.0594	13.7379	15.0724	13.5147	15.5112	12.0790	14.1286 14.5991	14.5899	13.0721	12.4218	11.6826	15.0316	17.0279	13.7044	13.6993
16.1916	16.1658	16.2476	16.2970	16.3431	16.3877	16.4032	19.2190	17.9800	18.4308	15.6985	17.0163	15.1431	17.4636	13.5186	15.8401	16.6597	14.3828	13.1385	12.4705	15.2405	16.8953	13.4860	14.4211
16.6941	15.9292	15,9385	16,1737	16.2205	16.2264	16,7403	18.9788	18.5571	17.5906	15.3867	16.5656	14.8085	16.9107	13.2365	15.7388	16.1402	13.8739	12.9060	12.3955	13-6293	17,5378	14.0951	14,7929
17.3106	16.6473	16.7215	16.8305	16.9340	16.9566	17.4050	19.8917	19.3208	18.9020	16.1497	17.4754	15.5308	18.0339	14.0969	16.5296 16.5296	17.0990	14.9753	14.0571	13.3913	16.5559	18.4836	14.8082	15.3198
17.7662	17.6840	16.7215	16.8305	17.9682	16.9566	17,4050	19.8917	19.3208	18.9020	17.1094	18.4527	15.5308	19.5171	15.4443	16.5296 18.3200	17.0990	16.9784	15.8896	15.3495	16.5559	20.7041	16.4716	17.6220
17.7562	17.6840	17.6655	17.8579	17.9682	17.9003	17.9533	20.3888	19.3829	19.4975	17.1094	18.4527	16.8441	19.5171	15.4443	1K.3200	19.6336	16.9784	15.8896	15.3495	18.7892	20.7041	16.4716	17.6220
17.7662	17.6840	17.6655	17.8579	17.9682	17.9003	17.9533	20.3888	19.3829	19.4975	17.1094	18.4527	16.8441	19.5171	15.4443	18.3200	19,6336	16.9784	15.8896	15.3495	18.7892	20.7041	16.4716	17.6220
17.7662	17.6840	17.6655	17.8579	17.9682	17.9003	17.9533	20.3888	19.3829	19.4975	17.1094	18.4527	16.8441	19.5171	15.4443	18.3200	19.6336	16.9784	15.8896	15,3495	18.7892	20.7041	16,4716	17.6220
17.7662	17.6840	17.6655	17.8579	17.9682	17.9003	17.9533	20.3888	19.3829	19.4975	17.1094	18.4527	16.8441	19.5171	15.4443	18.3200	19.6336	16.9784	15.8896	15.3495	18.7892	20.7041	16.4716	17.6220
16.4013	16.3374	16.3741	16.4269	16.5462	16.5890	16,5754	18.9034	17.5871	17.7696	15.4194	16.3986	14.5629	16.7346	12.9736	15.1321	15.4290	13.5248	12.7663	12.0783	15.3200	17,2476	13.8893	14.6495
20.2043	19.9939	20.1539	20.2683	20.3796	20.4717	20,4295	23.0624	22.A477	21.0113	18.8200	20.3148	18.1991	21,3018	16.5266	20.1150	21.4675	17.6230	15.8139	16.1744	19.8672	21.4391	16.9374	19.2460
18.5274	17.5442	17.5584	17.8775	17.7122	18.0693	18.7359	15.3529 21.2578	15.8675 20.5147	13.8703	12.3838	13.0370	15.9791	13.0071	10.3724	16.5154	13.7930	11.3799	9.1570	9.6999	16.2862	12.0053 18.1016	9,5936 14,4768	15.7190
15.5447	15.5460	15.5191	15.5502	15.8472	15,7036	15.7556	17.8773	18.6051	16.0353	14.6042	15.2827	13.7244	15.2960	12,1260	15,4196	16.3524	12,9513	10.3857	11,1706	12.9924	13.5236	10.7484	13.6878
19.0884	18.8934	19.3836	19.4666	19.4544	19.6011	19.5110	22.1440	21.2385	20.0734	17.9494	19.6506	17.6774	20.8202	15.9126	19.7827	21.2156	17,4515	15.6391	15,7747	19,6474	21.5207	16.5226	19.0555
22.3406 12.3861	21.2918	21.4972 12.1385	21.4687 12.0783	19.9679	21.9962 12.9058	22.1962 12.3509	22.2956 14.7195	21.4843 12.7696	13.7790	21.6831 12.6591	22.0123 13.9824	21.5110	21.9121	21.1739	21.8283	21.9589	21.4312 12.8439	21.621# 12.4997	21.5380	14.6812	22.9853 17.1825	13.7608	21.4614
12.9247	10.8553	13.0567	13.1001	13.2181	11.7144	12.5584	15.5366	12.5096	13.7/90	12.4501	13.6602	12,4722	14.3675	11.7534	13.5251	13.5171	12.3822	12.4723	11.5251	14.6812	17.1825	14.4458	13.6349
12.1832	9.9978	11.7725	12.6694	11.6636	11.1921	11.8147	15.0131	11.8906	13.2536	11.7421	13.3870	12.0426	13.8887	10,9463	12.7281	12.9921	11.7893	11.8061	11,3083	14.8699	17.4309	14.2842	13.7534
12.1832	9.9978	11.7725	12.6694	11.6636	11.1921	11.8147	15.0131	11.8906	13.2536	11.7421	13.3870	12.0426	11.8887	10.9463	12.7281	12.9921	11.7893	11.8061	11.3083	14.8699	17.4309	14.2842	13.7534
12.1832	9.9978	13.4542	13.6694	13.2536	11.1921	11.3147	15.7805	13.3527	13.2536	11.7421	13.3870	13.7401	13.8887	10.9463	13.7291	12.9921	11.7893 12.8548	12.1219	11.4929	14.8699	17,4309	14.2847	13.7534
13.2652	13.0251	12.7669	13.6290	13.1521	12.2096	13.3210	15.7966	12.7905	14.3712	13.0270	14.3062	13.0019	14.4024	11.9610	13.4848	13.2698	12.5153	12.1114	11.3686	14.5202	17.1688	13.8048	13.0067
9.5274	9.4976	9.4891	9.5103	9.5301	9.5632	9.5956	12.9684	10.1884	12.2646	10.6174	11.8994	10.5932	12.4433	9.6248	10.4163	10.3038	9.9599	10.4086	9.3993	11.3198	12.9953	10.4974	8.9614
9.4463	9.4304	9.4350	9.4800	9.4911 7.0985	9.5200	9.5362	12.4762	10.1242	12.2135	10.5492	11.7164	10.5433	17.4016	9.5763	7.6777	10.2731	9.9326	10.3856	8.9687	11.1760	12.9809	10.4850	8.9416
7.0628	7.0784	7.0471	7.0599	7.0985 12.3312	7.1001	7.1288	8.6738	6.8546 11.6312	13.9877	7,0806	8.0131	7.3489	13.6413	7.0653	11.6684	7.6273	8.4850 11.4186	9.3455	7.3518	9.9610	15.9131	9,8115	7,7935
101010	30.00						1.000		2010017	30.00	12.2.10	34444	and the	Jane and J	24.000		32.00	24.10	-7777848			20.0000	25.000

Road	V-	Coordin		1/2	(including	Height (m)	Road Type (caline 4)
Pair	X1	Y1	X2	Y2	_mixing_rose)	(11)	(came a)
RUT2	8333E7.91 833597.24	621869.26 621876.22	53339724 F3169176	821675.22	20	0	1
ROTS		821890.54		821875.22	17	0	1
RIGTA	#354E1.50	821790.34	822297.24	82187532	20	0	- 1
R074						0	1
Proper Mr.		621961.09		821683.08	16		1
RU78		\$21897.80	83356846	821699.77	16	0	
R076		821899.77		821899.99	16	0	4
R074	832603,43	821688-99	93398492	821822.32	14	0	1
R677	833564.57	821884.14 821884.14	833553.57	821884.38	32	0	1
R077	\$33563.57	821084.3%	833600.48	821871.38	17	0	4.
HOTE	833000.48	821971.28	933973.84	821812.08	17	0	- 1
ROTE	833061,38	621822.35	833875.32	821660.78	16	0	7
B379	833673.29	623831.43	633867.51	821651.AB	16	0	
R086	833674,67	221661.12	833999.54	821557.91	16	0	1
R091	833867.01	821650.85	933913.09	821852.08	20	0	4
R082	833458.18	821864.41	813510.76	021821.12	16	. 0	- 1
Rta2		621821.12		821785.93	14	0	
ROSZ	833526.39		E11570.11	821657.58	18	0	1
R043	633424.63		#354H6.18	821813.12	14	0	1
R083	833494.18	621013.12	833574.36	821772.28	14	0	- 1
777444	, exp., reprise.				14	0	
B183	\$33524.3E	821772.29	813559.61	821652.62			. 1
R094		821687.02		821644.65	13	0	1
R094	833,582.69	821644.RS	832607.71	821003.8F	13	0	
Ross	833009.34	821605.64		021575.52	14	0	1
RISKS	E33640.24	82) 57 5-52	813691.67	621645.20	14	0	1
R065	\$33.6E1.67	821545.20		821512.85	- 18	0	- 1
HOSE.	833580,70	821649.89	#32603.88	021103.58	17	0	1
Rote.		621533.58		021545.45	12		1
R087		82154E-43			13	0	1
Aces		821811.68			17	1	- 4
ROBE	833304.50	821856.64	833416.50	821865.51	17	,	-
RISBE		521905.51			17	9	1
ROSS	833487.63		833533-63	821788.07	17	10	
Ross	833467.83	621786.07	#13/23/41	821786.01	17	10	-
ROES.		821657.75			17	- of .	
Ritta		621605.82		621511.11	- 57	6	
8299		821801.44			16		
8089	633370.06	821846.87	833427.36	821852.03	16	13	4
RORP	833427,36		833410.60	821829.25	14		4
Ritas .	833480.60	821929.25	83352246	821786.30	78	10	
Ridge	833522.46	821786.32	E11543.19	821725 AT	16		
HOEK		821725.47		821653.37	16	1	
RORR			W3350E.99	021504.44	16	0	4
6099		621594.44		821508.87	16	6	
MAGON BORT	833259.78	821629.64	833337.54	621634.13	97	0	- 1
Seam Linear					20		1
R992+R993	#33337.92	821632.93	£13449.56	821640.31		0	1
1092×11093				021509.24	20		
R094		\$21634.13	833341.61	821576.41	18	0	- 1
Rith's	833609.59	621501.72	833548.49	621548.43	97	0	1
R095+R097		#22A54.38		822414.27	18	0	3
400 A + P(000	834028.77	822414.27	834127.62	B22302.11	18	0	1
1100-R101	834127.62	822332.11	83421831	822258.38	18	0	- 4
R102+R103	83A216.31	822258.35	E34309.95	822190.58	-18	0	1
194+R195	834309.95	\$22180.SE	834407.46	822098.55	18	0	1
R106	B33917.83	822431.11	833991.74	622300.30	18	. 0	1
R107	832991.55	822270.04	894890.33	822287.53	- 0	0	- 4
Ribs			634181.96	822212.22	36	0	- 1
Riss		822212.22		822138.48	17	0	1
RITO		#22212.02 #22134.83			17	0	- 1
R111			834410,74		- 18	0	- 1
R112	833846.76	822 AD 5.79	£11992.96	622380-5T	19	0	1
R113		822334.17			18	0	1
R114		822271.35		822201.23	18	0	1
R115		\$22200.75		821132.08	18	0	1.
ROF		822131.94			16	0	1
RHT	834097.30	822115.02	E34110.89	822007.73	18	0	7 .
RITE	834190.59	622037.73	834243.28	021003.00	- 18	0	3
R119		623393.65		021961.45	19	0	1
R120		821961.17		821895.90	-18	0	- 1
R121	833768.03	822374.46	#33799.51	822316.08	-18	0	- 1
R122	833761.98	822311.12	\$33818.78	022222.16	18	0	1
R123	833848.7E		£13954.75	822150.50	18	ů.	1
R124		622341.72	E11694.56	822284.02	16	0	7
R125	#33694.80	822284.07	82382777	822172.05	18	0	1
R126	833053.40	822269.00	832688.33	822174.73	12	0	- 4
R127	633489.65	822315.75	633502.51	822278.AB	-38	0	- 1
R128	12.£006.61		833574.36	822221.21	18	0	- 1
R129	833377.80	822222.03	833355.00	822293.72	18	0	- 1
R120	833377,80	822732.63	833318.77	822175.17	18	0	1
R131	833594.42	822175.04	813434.10	6220KD:76	n .	0	- 1
R132	A33431.92	#22580.70	#13410.51	822007.97	16	0	- 1
W123		822007.05		821952.78	16	0	- 1
REZA	823481.00	821962.76	833506.97	821882.08	16	0	
R135	833209.07	822239.7E	613232.66	622178,01	78	0	1
P1156		822178 DE		822120.94	18	0	. 1
R137	B33080.91	822162.63	#33100A3	822129.44	18	0	1
	833100.63	\$22129.44	833121.79	822672.07	18	0	- 4
R138							
R139	630121.68	822072.63 822507.67	813156.56	621977.95	17	0	1

											110 10	0 (-01147)											
Hr00	11.01	Hr02	Hr03	1 11.61	1 11-60	1 11.00	11.02	11.00	11.00	Hr10	NO ₂ x 10	Hr12	(1.42	Hr14	Hr15		11.49	Hr18	Hr19	11.00	1 11.01	11.00	11.05
11.9851	Hr01	12.0602	12.1249	Hr04	Hr05	Hr06	Hr07	Hr08	Hr09	11.5901	12.6499	11.3596	Hr13	10.5243	11.1361	Hr16	Hr17	11.3093	10.0891	Hr20	Hr21	Hr22	Hr23
10.4884	10.4066	10.4015	10.5332	10.7198	10.4474	10.4684	12.3253	10 1096	11.0436	9.6564	10.6082	9.4949	10.7681	8.4217	9.6222	9.6171	8.8767	8.4887	7.9969	10.6364	12.3843	10.0761	9.3929
10.8809	10.7134	10.8795	10.9614	11.0013	10.8399	10.9312	12.5438	9.7287	11.6202	10.3810	11.3882	10.4567	11.6918	9.7530	10.4025	10.2508	10.1023	10.4145	9.6728	12.2327	14.1074	11.9750	10.8915
11.0831	10.9650	11.1468	10.9812	11.1270	11.1184	11.1678	12.7314	10.0881	11.6906	10.4897	11.4020	10.3303	11.5767	9.3882	10.0142	9.7664	9.6195	9.8216	8.9205	11.5471	14.0976	11.7449	10.1450
9.9813	9.9793	9.8900	10.0629	10.0139	10.1946	10.1366	13.2436	9.1221	10.5712	9.4331	10.3441	9.3581	10.4738	9.4105	9.1479	10.5452	9.9063	10.1158	9.2516	10.9237	12.9764	10.7829	9.1743
11.1399	11.3539	11.1679	11.4126	11.4125	11.2679	11.3537	13.2436	10.9960	11.8510	10.4537	11.5378	10.3427	12.0493	9.4105	10.5621	10.5452	9.9063	10.1158	9.2516	12.7269	15.0013	12.2126	10.6458
11.1399	11.3519	11.1679	11.4126	11.4125	11.2679	11.3537	13.2436	10.9960	11.8510	10.4517	11.5378	10.3427	12.0493	9.4105	10.5621	10.5452	9.9063	10.1158	9.2516	12:7269	15.0013	12.2126	10.6458
10.2149	10.2531	10.2548	10.2897	10.3992	10.3165	10.3724	12.0025	9.4951	11.0160	9.7407	10.7565	9.7364	11.1564	8.9761	9.7206	9.5536	9.5435	9.8863	8.9274	12.1658	14.4698	11.9123	10.1427
10.2149	10.2531	10.2548	10.2897	10.3992	10.3165	10.3724	12.0025	9.4961	11.0160	9.7407	10.7565	9.7354	11.1564	8.9761	9.7206	9.5536	9.5435	9.8863	8.9274	12.1658	14.4698	11.9123	10.1427
10.2149	10.2531	10.2548	10.2897	10.3992	10.3165	10,3724	12.0025	9.4961	11.0160	9.7407	10.7565	9.7364	11.1564	8.9761	9.7206	9.5536	9.5435	9.8863	8.9274	12.1658	14.4698	11.9123	10.1427
9.3224	12.5209 9.4765	12.6066 9.3715	12.7353 9.4655	9.4766	9.3833	12.8665 9.5035	14.8017	12.7419 8.7(30	9.9583	9.0274	12.9690	9.2374	13.2316	10.4972 8.6601	9.1913	11.6066 8.9735	9.2048	10.8667	10.0919	13.2473	15.4746	12.7691	9.9430
11.9204	11.9622	11.9544	12.0899	12.0912	11.8649	12.0365	13.9290	10.6073	12,6709	11.0581	12.3457	11.0013	12.8318	9.9357	10.8280	10.6501	10.1602	10.6114	9.5420	13.1866	15.7217	12.7662	11.0137
10.0117	10.1313	10.0698	10.1142	10.1292	10.0592	10.2226	11.5764	8.9849	10.6626	9.7878	10.7625	9.8931	11.1487	9.3139	9.8178	9.5632	9.7170	10.5338	9.4532	12.6525	14.9869	12.6596	10.5212
14.5096	14.6345	14.4354	14.5241	14.6264	14.4815	14.6822	16.9962	13.2455	16.4862	14.4256	15.8811	14.4870	16,4656	13.5547	14.2386	14.0348	13.7750	14.4318	13.3833	16.7863	19.1744	16.3482	14.3338
14.5096	14 6345	14.4354	14.5241	14.6264	14.4815	14.5822	16.9962	13.2456	16.4862	14.4256	15.8811	14,4870	16.4656	13.5547	14.2386	14.0348	13.7750	14,4318	13.3833	16.7863	19.3744	16.3482	14.3338
14.5096 6.1530	14.6345 6.3074	14.4354 6.3964	6.5354	14,6264 6,6833	65185	14.6822 6.4130	6.9228	13.2456 6.2308	7.0272	14.4256 6.4737	15.8811 6.7578	14.4870 6.4309	16,4656 6,5895	13.5547 6.0534	6.8315	14.0348	13.7750	14,4318 6,2097	5,9530	6.9176	19.3744 8.1178	16.3482 7.3427	6.3725
6.1530	6.3074	6.3964	6.5354	6.6833	6.5185	6.4130	6.9228	6.2308	7.0272	6.4737	6.7578	6.4309	6,5895	6.0534	6.3315	6.0304	6.0287	6.2097	5.9530	6.9176	3.1178	7.3427	6.3725
6.1530	5.3074	6.3964	6.5354	5.6833	6.5185	6.4130	6.9228	6.2308	7.0272	6.4737	6.7578	6.4309	6.5895	6.0534	6.3315	6.0304	6.0287	6.2097	5.9530	6.9176	8.1178	7.3427	6.3725
14.5912	14.4051	14.4079	14.5868	14.6007	14.5203	14,6460	16,9566	12.9084	16.1177	14.4239	16.0176	14.6698	16,8806	13.9338	14.3237	14,1031	14.5878	15.7448	14.3012	18.2416	21.2273	18.0894	15.0148
14.5912	14.4051	14.4079	14.5868	14.6007	14.5203	14.5460	16.9566	12.5084	16.1177	14.4239	16.0176	14.6698	16.8806	13.9338	14.3237	14.1031	14.5878	15.744H	14.3012	18.2416	21.2273	18.0894	15.0148
15.4252	15.4832	15.4716 15.4716	15.5750 15.5750	15.5958 15.5958	15.6416 15.6416	15.7726 15.7726	17.7396	14.2554	17.0518	15.5267	16.9583	15.6536 15.6536	17.5436	14.8470	15.1504	14.8803	14.9912	16.2943	14.6516	18.5659	21.4648 21.4648	18.0885	15.6140 15.6140
15.4252	15.4832	15.4716	15.5750	15.5958	15.6416	15.7726	17.7396	14 2554	17.0518	15.5267	16.9583	15.6536	17.5436	14.8470	15.1504	14.8803	14.9912	16.2943	14.6516	18 5659	21.4648	18.0885	15.6140
14.8538	14.6998	14.8930	14.6429	14.8957	14.9350	14.964K	16.7137	12.8099	16.003X	14.0735	15.4525	14.0457	15.8713	13.1606	13.4151	12.9759	13.0705	14.0649	12,7701	16.3704	19.1819	16.5467	13.7379
14.8538	14.6998	14.8930	14.6429	14.8957	14.9350	14.964H	16,7137	12.8099	16.0038	14.0735	15.4525	14.0457	15.8713	13.1606	13.4151	12.9759	13.0705	14.0649	12.7701	16.3704	19.1819	16.5467	13.7379
21.0662	20.9566	21.0381	20.9566	21.0098	21.0040	21.1326	21.7559	20.6643	21.7189	21.2957	21.6037	21.0029	21,5145	20.7465	20.9006	20.7761	20.7611	21.2008	20,6230	21.6192	22.4110	21.5861	20.8515
2.3066 2.3066	2.2739	2.2875	2.3154	2.3058	2,3375	2.3687	3.8223	3.9463	3.8309	3.5514 3.5514	2.9584	2.6789	2.3421	2.4336	2.3108	2.1473	2.1462	1.8941	1.5558	1.6365	1.6111	1.6997	1.4957 1.4957
2.3066	2.2739	2.2875	2.3154	2.3058	2.3375	2.3687	3.8223	3.9463	3.8309	1.5514	2.9584	2.6789	2.3421	2.4336	2.3108	2.1473	2.1462	1.8941	1,5558	1.6365	1.6111	1.6997	1.4957
2.3066	2.2739	2.2875	2.3154	2.3058	2.3375	2.3687	3.8223	3.9463	3.8309	1.5514	2.9584	2.6789	2.3421	2.4336	2.3108	2.1473	2.1462	1.8941	1.5558	1.6365	1.6111	1.6997	1.4957
2.3066	2.2739	2.2875	2.3154	2.3058	2.3375	2.3687	3.8223	3.9463	3.8309	1.5514	2.9584	2.6783	2.3421	2.4336	2.3108	2.1473	2.1462	1.8941	1.5558	1.6365	1.6111	1.6997	1.4957
2.3066	2.2739	2.2875	2.3154	2.3058	2.3175	2.3687	1.8221	3.9463	3.8309	3.5514	2.9584	2.6789	2.3421	2.4336	2.3108	2.1473	2.1462	1.8941	1.5558	1.6365	1.6111	1.6997	1.4957
2.3066	2.2739	2.2875	2.3154	2.3058	2.3175	2.3687	3.8223	3.9463	3.8309	1.5514	2.9584	2.6789	2.3421	2.4336	2.3109	2.1473	2.1462	1.8941	1,5558	1.6365	1.6111	1.6997	1.4957
2.2655	2.2345	2.2574	2.2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1.4516	1.5746	1.5765	1.6104	1.4652
2.2655	2.2345	2.2574	2.2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1.4516	1.5746	1.5765	1.6104	1.4652
2.2655	2.2345	2.2574	2,2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1.4516	1.5746	1.5765	1,6104	1,4652
2.2655	2.2345	2.2574	2.2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1.4516	1.5746	1.5765	1,6104	1.4652
2.2655	2.2345	2.2574	2.2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1,4516	1.5746	1.5765	1.6104	1.4652
2.2655	2.2345	2.2574	2.2821	2.3152	2.3046	2.3264	2.9207	2.9305	2.7706	2.6736	2.3071	2.1958	1.9627	2.0691	1.9617	1.8815	2.0242	1.8787	1.4516	1.5746	1.5765	1,6104	1.4652
9.0329	2.2345 9.0855	2.2574 8.9433	9.0497	9.2269	9.0547	9.1309	2.9207	2.9305 9.0865	2.7706	9,2379	2.3071	2.1958 9.5236	1.9627	2.0691 8.7183	1.9617	1.8815	2.0242	1.8787 9.7456	1.4516 8.9692	1.5746	1.5765	1,6104	9.7949
8.7903	8.5875	9.3134	9.5122	9,4155	8.4303	8.9973	11.2809	8.8020	10.2999	9.3061	10.2869	9.4686	10.7597	8.5880	10.0903	10.1602	9.9258	9.5396	8.8125	11.4202	13.5180	10.8447	10.1918
8.7903	8.5875	9.3134	9.5122	9.4155	8.4303	8.9973	11.2809	8.8020	10.2999	9.3061	10.2869	9.4686	10.7597	8.5880	10.0903	10.1602	9.9258	9.5396	8.8125	11.4202	13.5180	10.8447	10.1918
5.4705	5.4065	5.4161	5.5796	5.6345	5.6442	5.4958	6.4855	4.4902	5.9141	4.9444	5.1363	4.4383	4:4343	3.4650	3,5480	3.0657	3.0326	2.5874	2.3559	3.1266	3.9948	3.5188	2.8848
23.0683	22.7126	22.8881	21.0649	23.1332	23.1461	23.3639	24,3704	23.4670	24.0309	21,6506	23.9936	23.3930	23.7744 15.4955	22,9474	23.3317	23,2986	22,9982	23.4267	22,5991	23.7845	24.8249	23.8486	23.0670
20.3407	20.1309	20.5538	6.3343	6.3674 70.4339	13.7591	11.7346	21.5236	23.0039	15.9027 24.1075	14.0401	21.4107	18.8693	20.8998	17.1060	18.7661	13.7630	12.9765	14.7354	11.1408	17.1402	17.1775 18.6409	14.1650 15.0466	15.4118
16.2197	16.1559	18.6533	16.6044	17.8522	16.0628	18.6901	19.8581	18.6609	21.0716	18:21739	18.4717	17.5658	18.4170	15.2753	17.6422	16.3383	15.0489	14.0826	13.3055	16.2068	19.0484	15.2496	15.5124
15.9731	17.8336	15.1830	16,2809	16.3782	17.1910	16.2888	20,8311	17.8819	19.4648	16.3143	17.8484	15.1054	16.9333	12.8802	15.2823	14.6758	12,5008	11.4680	11,1609	15.2220	17.7574	13.7571	14.1206
14.1639	16.4154	14.1439	13.9483	14.0298	16.0075	13.9483	18.9767	16.7685	17.5706	15.5345	17.0169	14.4888	15.9762	12.5230	14.5200	13.8025	12.8217	11.8042	11.4568	15,0761	17.3002	14.1905	14.1266
10.8143	10.1716	11.3322	13.6661	12.2284	10.8581	10.7897	13.2760	10.7295	12.5398	10.5420	12.5363	11.1261	13.4665	10.8169	12.6663	12.7512	12.2858	11.8826	10.4910	13.6899	16.5800	13 3356	13.5480
11.4633	10.3398	11.6339	13.1266	12.5456	11.8170	11.5469	13.0972	10.5226	11.9571	11.0053	12.0311	11.2512	12.9296	10.4586	12.2140	12.9025	11.9616	11.5842	10.8656	14.2987	16.8119	13.3059	12.6224
11.1290	9,9479	11.1504	12.8639	12.2403	11.4964	11.2064	12.8122	10.1615	11.6290	10.6770	11.8047	10.8025	12.6448	10.1659	11.7927	12.4420	11.5459	11.1039	10,2798	13.6331	16.1922	13,6411	12.6656
10.62.19	10.7195	10.2811	11.7160	113046	10.3544	11.3488	13.0820	10.0150	11.6647	10.4991	11.7243	10.8062	12,4660	10.0121	11.6737	12.0162	11.1529	11.0979	10.3790	13.4751	15.6393	13.2011	12.5050
10.9168	11.2254	10.7984	11.4930	11.0119	10.3567	11.0074	12.9171	10.5035	12.1176	10.6769	11.9531	10.8818	12.3899	10.1083	11.4858	12.1303	11.2514	10.7607	10.3331	13.6568	16.2597	12.9503	11.4997
10.5925	21.5857 10.3828	23.4594	8.9122	21,6015 8.1317	21.8255	10.2473	24.8469	23.6270 9.5484	24.0463	9.7790	22.0622 11.1593	10.0005	22.4685	9.3148	19.7856	18.6666 11.4215	16.2862	10.1201	9.3747	17.9861	19.9202	15.9067	17.0357
12.6866	12.1502	12.4728	12.6036	12.4523	12.4402	12,6945	14.6825	12.9798	14.8454	13.5108	14.2736	13.2581	14.4646	12.6530	13.6601	14.2532	13.2386	12.7710	11.9551	14.4806	16.5712	13.6321	13.0379
17.5670	17.4345	17.6178	17.7173	17.2136	17.6230	17.7018	19.8603	17.8882	19.3048	16.9808	18.1039	16.3622	18.1524	14.7037	16.4562	16.6046	14.6354	13.8044	13.5289	16.2003	18.2751	15.0542	15.3739
11.7815	11.7574	12.3671	12.4781	12.2555	12.2488	12.0731	13.7105	11.3994	13.1114	11.8713	12.9386	12.0274	13.3168	11.2456	12.6080	13.3737	12.1980	11.7750	11.3159	13.8228	15.7266	13.2125	12.6294
11.8705	12.2946	11.9609	12.5538	12.3281	12.3171	12.2257	13.7502	11.5761	12.9766	12.0702	13.0951	12.1430	13.4127	11.4032	12.6356	13.5436	12:3427	11.8872	11,4255	13.8679	15.8215	133636	12.5037
12.4168	12.3404	12.0142	12.6997	12.6794	12.4763	12.3339	13.6027	11.7344	13.1087	12.2512	13.1762	12.2475	13.4911	11.5319	12.7701	13.6500	12,4445	12.2766	11.5153	14.2903	15.8823	13.4716	12.8190
12.2160	12.2237	12.2429	12.1370	11.8846	12.5576	12.2048	14.1751	11.9202	13.3463	12.4133	13.4445	12.5369	13.7602	11.7641	13.1025	13.6936	12.7322	12.3213	11.5607	14.2847	15.8581	13.3710	12.9868
13.0668	11.6969	13.9391	12.6317	12.6938	12.7047	12.2932	15.1496	9.8561	13.8633	12.0330	14.1609	13.4238	16.4665	13.1061	13.5164	14.1448	15.0092	17.2573	14.8007	21.3363	25.7074	20.8525	16.2696
14.0927	14.5722	14.8492	15.4365	15.5282	14.6223	13.9080	16,4977	11.5356	16.2362	13.2928	14.5648	12.6838	14.3421	11.2760	11.2774	9.843€	10.2211	11.0770	9.6545	12.8483	15.2333	12.7943	10.2108
6.2259	6.1526	6.0829	6.0194	5.5300	6.7415	6.4659	8.1765	5.3230	7.1179	6.3200	7.2046	6.7405	7.5754	6.2133	6.9588	6.6785	7.4620	7.9548	6.6869	9.3704	11.8151	9,7766	7.3469
15.9571	15.5059	15.5235	16.2666	15.6510	16-2353	15,7896	17.6681	14.0133	17.4693	15.7157	17.2614	16.3575	18.7660	15.8570	16-2229	17.1463	16,9006	18.5688	16,4895	21.8409	25.3215	21.9317	17.1860
13.0306	13.2389	14.1613	14.7451	15.2916	14.1645	13.6199	17.3249	11.6572	16.2161	13.1570	14.2501	13.1401	13.5744	10.0782	9.9168	7.8815 13.9751	8.1818 13.2818	8.2170 13.4277	7.3929	9.8966	18.5174	10.3254	8.1176
12.4829	13.2405	12.5760	12.4331	11.8955	12.4778	12.8342	14.5918	11.1142	13.6658	12.6513	13.9743	12.9305	14.4707	12.6366	13.1302	13.4911	13.7136	14.9038	13.2553	17.2223	20.4007	16.8338	13.6793
11.3505	11.2297	11.8194	11.7665	11.3327	13.2122	11.2561	13.1001	9.4432	11.9978	10.9610	12.3356	11.4529	13.1107	11.2297	11.7536	12.0257	12.4763	13,6548	12.1206	15.9402	19.2210	16.2124	12.9780
9.3047	9.2399	9.1310	9.3963	9.2669	9.3929	9.4318	11.3387	7.9041	10.3625	9.3624	10.5649	9.9684	11.4582	9.6019	10.1588	9.9357	10.6029	11.9781	10.2861	14.3810	17.1507	14.1941	11.2371
8.9238	8.8811	8.8328	8.8575	9.0120	8.9080	8.9810	10.9671	7.4894	9.9919	2.9756	10.1741	9.3623	11.1048	8.9988	9.7480	9.4896	10.2319	11.6318	9.8987	14.2295	16.9092	13.8902	10.8238
9.8557 6.8492	9.8080 6.9268	9.8670 7.0975	9.8500 7.1109	7.0445	9.9070 6.8904	9.9408 6.5494	7,4781	9.4048 6.8194	7.8284	9.5193 6.8901	7.1025	9.9064 6.6002	11,5996 6,6407	9.0268	10.3016	10.5724 5.4313	10,2454 5,2740	10.8325 5.2458	9.6379	13:2424 5:5703	15.6449 6.5307	12.5706 5.5374	4.9168
14.2823	14.9454	15.6196	16.3246	15.8726	14.9557	13.9827	16.2752	13.7533	15,7819	11.4326	14.6323	12.8329	14.4293	11.1157	11.9038	10.8526	10.5551	10.6519	2.6995	12.8951	14,8002	11.8056	10.5809
10.6518	11.1971	12.0997	12.7538	12.1769	11.2451	10.2821	12.2396	10.0267	11.3180	10.07/29	10.9773	10.0387	11.1169	9.0758	10.1027	10.1564	9.9222	9.7393	8.8075	11.0852	13,2582	10.8738	9.7467
12.5889	15.9411	18,6836	19.2813	18:1223	17,3817	13.4424	13,0758	8.3074	11.6094	10:7227	11.6536	11.1080	12,7358	10.6625	11.2618	10:6191	10.9228	11.7933	10.9257	15.9394	18.5840	16.4264	13.3224
7.0837	9.8014	12.5674	1.6113	1.6225	12.7047	11.1503	11.3024	7.4832	10.7223	8.8775	10.1657	9.6884	11.3926	9.2317	9.7995	9.3139	10.1723	11.2782	9.9483	13.6744	17.1983	14.8869	11.7528
8.8739 8.8739	8.8495 8.8495	11.3195	1.5158	1.5342	11.4407	8.1534 8.1534	10.3902	6.3024	8.9777	7.6293	8.9713 8.9713	8.7112	10.2355	7.9138 7.9138	R.6431	9.0767	9.1833	10.4064	9.2087	12.8748	16.3581	14.1756	10.5885
8.0545	7.9146	8,2332	7.6795	8.1331	8,2227	8.2166	9.9899	6.4267	8.8198	7.7651	9.1736	8.4285	10.1437	8.1303	8.6431	8.8782	9.4687	10.4064	9.1209	13.3793	16.5491	13.5382	10.3885
15.6704	15.3287	15.1314	15.5572	15.4153	16.2426	15.7435	18.1145	13.4806	16.7194	14.1307	14.9920	12.9332	14 1394	10.7519	10.8088	8.9430	9.1990	9.4079	5.2386	11.0653	13.4567	11.2832	9.4832
					-		-					-	-					-					

Road		Coordi	nate (m)		(including	Height	Road Type
Pair	X1	Y1	X2	Y2	mixing zone)	(m)	(caline 4)
R141	833295.35	821947.25	\$33315.54	10.169159	13	0	1
B162	#33329.69	821853.67	E13315.96	821691.84	13	0	- 1
R143	A33129.75	621889.31	833160.17	821834.07	- 11	. 0	1
R164	833160.17	821834.07	933178.74	821783,15	13		1
R145+R146	833812.49	621976.58	85490458	621516.02	- 57	0	1
R147+R144	833738.44	821088.35	811931113	821727.3 8	16	0	7
R149	833728.61	821749.52	833807.73	821694.38	14	0	4.
R149	833T74.08	821643.52	833807.73	821684.38	13	0	1
R150	833734.67	821759.23	813607.71	821683.81	- 0	0	- 4
R151	833613.61	821610.98	E11493.50	821543.70	13	0	4.
R151	833493.50	821543.70	W3577526	821642.63	14	0	1
R152	833774.08	621643.52	833826.17	821600.58	20	0	7
8153	833991.31	622369.76	634528.77	822414.27	18	0	1
R154	233960.46	822320-65	833992.00	822399.67	18		1
R155	833909.65	822271.36	833900.44	822320.45	18	0	4
R158	833048.78	822222:16	813509.65	822271.36	18	0	- 1
R187	833066.58	622222.34	88380777	822172.95	- 19	0	- 1
R158	833827.77	822172.95	E11778.49	822113.35	15	0	1.
RISK	834078.91	822299.62	83411290	622784.34	15	0	1
R160	834090.39	622207.53	034527A2	622332.11	15	0	1
RIST	834054.90	822250.52	834075.61	822799.62	15	0	- 4
R162	\$34049.42	822238.28	23409030	822287.53	15	0	1
R163	832993.96	822201.65	834034.90	632250.52	16		- 1
R164	834007.86	822186-33	834549.4Z	022230.21	15	0	1
R183	#33953.31	822151.78	E3394447	622201.23	16	0	4
RISS	833872.14	822951.39	833954.75	822150.50	19	0	1
R167	833872.14	822042.45	E34007.86	822109.33	16	0	1
R163+R163	833813,72	821975.47	813876.16	822050.03	21	0	1
R170-R171	833736.44	821888.35	E33812.49	821978.50	18	0	1
R172+R173	833684.92	821822.32	833719.28	821887.65	29	0	1
R174+R175	833684.78	821677.56	833683.38	821823.05	16	0	1
RITE	833496.77	521808.49	533540.47	821680.73	20	0	1
R177	833513.09	821599.24	8335/3.6E	821668.A7	29	0	1
R178	835440.44	40.000	83746840				_
R179	833451.64	821529.90		821608.61 821600.38	19	0	4
R179	834218.31	627256.35	833511.32	821600.38	17	0	1
R181	834218.31 834181.98	822212.22	834218.31		18	0	1
R191	634140.62	822212.22	834218.31	822258-35 822212.39	16	0	1
R182							_
	834099.34	822113,33	934140,62	822162.07	18	0	1
R184	\$34077.01	822132.66	#34071.51	622100.94	13	0	- 1
RISK	\$34061.51	822100.94		822084.18	13	0	- 4
R184	834071.90	822984.18	834097.30	822115.02	14	0	1
RIES	834309.98	622100.50	634362.64	822267.A4	19	0	1
8.06	834251.54	622084.63	£34273.34	622136.83	19	0	1
R197	834190.59	822037.73	834231.76	622086.A5	- 58	0	1
R199+R199	#3A004.98	#21856.03	834818.34	821890.22	19	0	1
R190+R191	R23921.43	821727.74	834004.98	821816.03	19	0	- 1
R197-R197	833878.32	\$21660.75	833930.89	821727.98	20	0	1
R194+R195	533825,79	621600.86	833867.61	621651.48	20	0	1
R196+R202	A33761.01	#21523.1K	E13826.17	821699.58	20	0	1
R197	834384.36	822000.94	834400.15	B22104.71	17	0	1
RIM	834322.77	822010.68	83436436	822060.94	18	0	- 4
R199	83A251.93	821961.17	E34322.00	BZZE10.AB	-19	0	1
R290	634239,17	221914.13	834219.06	821983.18	14	0	1
R200	B34239.17	821914.13	834327.69	821840.33	- 18	0	1

									-		NO ₂ x 10	0 (g/VMT)	-		-								
Hr00	Hr01	Hr02	Hr03	Hr04	Hr05	Hr06	Hr07	B0nH	Hr09	Hr10	Hr11	Hr12	Hr13	Hr14	Hr15	Hr16	Hr17	Hr18	Hr19	Hr20	Hr21	Hr22	Hr23
14.2192	13.8954	11.4700	11.0573	14.0777	15.4177	14.2409	17.7867	12.7019	16.1656	13.1478	14.1763	11.9995	13.2960	9.8813	9.9188	7.6768	8.1068	£4601	7.4196	10.5486	13.1338	10.7427	8.4028
7.5593	6.0967	6.7785	5.8110	5.4202	6.8396	7.6437	8.5395	6.5097	8.0780	7.5440	8.2222	7.7509	8.2209	7.1803	7.9555	7.7392	7.2831	7.2859	7.1483	8.6525	10.6881	9.2053	8.2029
16.1859	16.0533	15.7467	16.0274	15.9663	16.7930	16.1950	18,4284	15.1465	18.1117	15.7384	16.5007	14.1601	15.3236	12.3659	12.0530	10.5735	10.3096	10.4056	9.4384	11.8821	14.2056	12.1579	10.2350
15.9671	15.8047	15.5442	16.1182	15.9862	16.6819	16.0582	18.2376	14.1626	17.3216	14.3756	15.7365	13:6966	14.9456	11.6772	11.6879	9.7710	9.9077	3.9797	8.8338	11.5703	13.9166	11.9177	9.9040
12.5848	11.6969	13.9191	B.2235	15.8571	11.5970	12.2915	14.3840	9.3703	13.2926	10.5181	11.6537	9.6517	10.5475	7.8257	7.6350	5.3732	6.0282	5.9923	5.2008	7.0194	3.7918	7.6006	5.9940
10.5373	10.7140	12.5674	14.0092	12.6938	11.8526	10,9878	13.1204	8.5180	11.8319	9.4417	10.1415	8.4306	9,0418	6.5048	6.3124	4.5994	5.1804	4.8122	4.2183	6.1225	7.0080	6.3997	5.1120
9.3489	8.8888	8.1779	9.8766	9.9260	11.1223	9.0369	11.4737	7.2911	9.9868	8.9348	10.1919	9.5553	11.4585	9.3452	9.6296	10,7749	11.2069	12.7439	10.8203	15.5416	18.8982	16.6781	12.5999
9.3489	8.8888	8.1779	9.8766	9.9260	11.1723	9.0369	11.4737	7.2911	9.9868	£.934E	10.1919	9.5553	11.4585	9.3452	9.6296	10.7749	11.2069	12.7439	10.8203	15.5416	18.8982	16.6781	12:5999
9.3489	8.8888	8.1779	9.8766	9.9260	11.1223	9.0369	11.4737	7,2911	9.9868	8.9348	10.1919	9.5553	11.4585	9.3452	9.6296	10.7749	11.2069	12.7439	10.8203	15.5416	18.8982	16.6781	12.5999
9.3489	8.8888	8.1779	9.8766	9.9260	11 1223	9.4720	11.4737	7.3718	10.1009	8.9348	10.1919	9.5553	11.4585	9.1761	9.6296	9.7603	10.9240	12 3301	10.3865	15.5416	18.8982	16.6781	11.4986
9.3489	8.8888	8.1779	9.8766	9.9260	11.1223	9.4720	11.4737	73718	10.1009	8.9348	10.1919	9.5553	11.4585	9.1761	9.6296	9.7603	10.9240	17.3301	10.3865	15.5416	18.8982	16.6781	11.4986
9.3489	8.8888	8.1779	9.8766	9.9260	11.1223	9.0369	11.4737	7.2911	9.9868	8.8211	10.0371	9.2617	11.0137	8.7088	9.5678	9,596€	10.4973	11.4143	9.8038	14.9541	18.1263	14.5046	10.5976
9.9614	10.1233	9,7613	9.3044	10:3024	10.2642	10.1909	12,4271	8.6130	11.2345	9.3805	9.9145	8.7309	9.9621	7,3705	7.9942	7.4219	7.3841	7.6737	6.7478	9.6202	11.9646	10.1196	8.0887
9.8935	10.2122	9.5402	9.9324	10.4661	9.9982	10.2723	12,4706	8.5867	11.1235	9.2917	10.0062	8.7914	9.8190	7.4495	7.9322	7.3112	7.4977	7.8021	6.8022	9.6415	11.9041	9,9379	7.9138
9.8956	10.2300	9.7578	9.7995	10.1616	10.1401	10.2845	12,7799	9.0911	11.5442	9.6725	10.1398	8.9738	10.2770	7.5383	H-1536	7,7601	7.7729	7.9354	6.9041	9.9644	12.4922	10.3299	8.1637
14.0528	13.5141	13,3171	13.3204	13.0413	13.1476	14.2560	18.5061	14.2029	17.1360	15.0678	15.9938	14,4167	15.4051	12.7142	12.9956	12.0940	12.2776	12.2011	10.7568	13.4728	15.3488	13.2500	10.8053
14.5694	14 1560	14.2154	13.8574	14.0316	14.0407	14,7301	18.9518	14.9363	17.5446	15.0091	15.5996	13.8898	15.5238	12.1720	12.3069	11.4819	11.5983	12.0643	10.6199	13.5165	15.5795	13.3033	10.8652
14.3563	14.3644	14.3675	14.4082	14.6329	14.5107	14,4782	16.9211	12.9691	16.0950	13.8371	14,4728	12.9136	14.4376	11.3413	11.4224	19.6578	10.7378	11.3090	10.1701	13.4658	15.7164	13.3549	11.0448
10.2936	10.5027	11.3924	11.4756	8.9564	11.5511	10.2922	12.2181	9.6220	11.5933	10.4244	11.8505	10.5186	12.1479	9.4669	10.5529	11.0128	10.6916	11.1154	10.0136	14.0073	16.3496	13.5497	12.1782
12.0659	11 9385	11.9567	12.3052	11.7119	12.4329	12.5966	14.7017	11.0942	13.3983	11.1835	12.4041	11.0299	12,7974	9.5323	10.1643	9.9382	9.5653	9.9160	8.7699	12.4876	15.1514	12.2822	10.1027
10.4760	10.3910	10.4436	10.2097	10.8294	10.4399	10.7851	13.0249	9.7506	11.7499	10.4045	11.8284	10.7537	12.5718	9.9311	11.0114	11.0036	10.9081	11.3166	10:2498	13.8771	16.7379	13.5360	11.6455
12.1683	12.0656	11.9800	12.0657	12.0419	12.1723	12.3003	14.6107	11.1204	13.2869	11.2206	12.4881	11.0183	12:5979	9.5946	10.4070	9.9256	9.5767	9.9269	8.7440	12.3533	15.1528	12.2627	10.1088
11.4176	11.5049	11.6571	11.3391	11.4923	11.6534	11.5701	14.0562	10.9650	12.7915	10.9015	11.9748	10.6248	12.1391	9.2517	10.3792	9.9820	9.6331	9.7509	8.6470	12:1345	14.8562	11.9010	10.1149
11.3351	11.2847	11.3750	11.1186	11.6299	11.3942	11.3962	13.5329	10.0058	12.3798	10.3161	11.5727	10.2766	12.2955	9.2682	9.8071	9.7756	9.8435	10.4146	9.0893	12.5400	15.6226	12.6630	10.3097
12.7100	12.5615	12.3545	12.4860	12.4048	12.7546	12.8871	14.7451	12.4801	13.4339	12.2600	13.0943	12.0124	13.2037	10.8209	11.7512	11.5228	11.1704	11.2621	10.4281	13.7786	15.7765	13.1291	11.7608
9.5614	9.2286	9.3697	9.4248	9.4925	9.4810	9.6966	11.0575	9.2058	10.1728	9.2908	9.5224	8.7554	8.5680	7.8503	8.2829	7.5441	7.6665	7.0028	6.5362	7.4982	3.5545	7.7316	7.2318
17.3862	17.3475	17.2709	17.4503	17.7731	17.5988	17.6573	20.9543	18.4413	19.3153	16.7817	18.0338	16.1107	18.2068	14.0834	15.9244	15.9605	14.0396	13.6859	13.1269	16.7709	19.3684	15.5588	14.5677
3.8916	3.8332	3.9607	4.0596	3.8130	3.8867	3.9097	4.8236	3.8581	4.2857	1.9872	4.1422	4.0161	3.8704	3.5238	4.0352	1.7450	3.8832	3.3215	3.1527	3.7340	4.7198	4.0428	3.5762
5.8301	5.7829	5.8234	5.7142	5.9318	5.9468	5.8751	7.0726	5.5944	6.8271	6.1485	6.4417	6.0921	6.2929	5.3787	5.6625	5.3894	5.4822	5.4166	5.0119	6.1179	7.2713	6,3053	5.4943
11.8830	11.6845	11.7067	11.7702	11.6460	11.9207	11.8392	14.2545	10.6343	13.1289	11.0886	12.3086	10.9282	12.6097	9.8843	10.6307	10.4155	10.2138	10.4113	9.3879	12.5551	14.9407	12.2623	10.5312
32.6404	12.5765	12.5899	12.6988	12.6246	12.7858	12.8014	15.6766	12.7363	14.5568	13.0195	14.1067	12.7953	14.8031	11.8740	12.7649	12.7751	12.6794	12.6997	11.6369	14.9451	17.3153	14.4681	12:4169
11.8034	11.7208	11.8183	11.8966	12.0068	13.8929	11.9073	14.1154	11.5630	12.9299	11.9054	13.0559	12.1482	13.6959	11.5422	12.7835	12.9048	12.7409	12.8263	11.8088	14.8090	17.1095	14.4278	13.2337
13.1366	13.1021	13.1719	13.1281	13.0317	13.2886	13.1941	15.1706	11.6940	13.9393	12.0595	13.0792	11.6585	13.2495	10.5481	11.7411	10.9581	10.5146	10.4873	9.5781	12.4618	14.7724	12.2958	10.9090
13.7248	13.5599	13.6028	13.7500	13.9612	13.7105	13.9853	16.0112	13.7924	14.8610	13.8260	15.0948	14.0878	15.9440	13.4887	14.6797	14.7410	14.6380	15.2045	13.9191	17.3968	19.8956	17.0474	15.2302
14.7275	14.5908	14.6828	14.7525	14.8147	14.7848	14.8803	17.2750	13.8192	15.8653	14.0091	153315	13.7868	15.7452	12.5060	13.8947	13.9461	12.8957	12.7246	12.0726	15.6277	17.6950	14.5292	13.7030
12.4981	12.5446	12.8084	12.7937	12.8566	12.5248	12.9062	15.3386	11.8766	14.3773	12.1334	13.6228	12.2728	14,2808	11.1146	12.2773	11.9952	11.8273	12.2356	11.0679	15.2757	18.5751	14.9572	12.6303
12.8074	9.8014	8.9095	9.8766	11.1122	9.9354	13.7953	13.9109	9.6626	12.3230	10.7243	12.0812	12.4147	14,1025	11.0101	12.3365	11.6710	12.5801	13.0751	11.2781	15.8198	19.3291	16.1241	12,7409
11.3181	11.3530	12.1111	12.1095	14.1720	12.7815	11.5705	13.4722	10.1984	11.8107	10.5946	12.0173	10.9984	13.7544	9.8901	11.1378	11.7354	11.5606	12.0620	10.3072	14.8817	19:1267	14.9561	12.2802
12.7102	13.1551	13.8950	14.2256	14.6759	15.1657	12.8913	15.1608	11.6178	13.7460	11.9491	13.2282	12:1058	13.8700	11.0101	10.6013	10.3081	10.3843	11.7353	10.4674	14.9394	18.4658	14.2010	13.4468
12.5865	12.1029	11.9898	11.9429	11.8422	12.7047	12.7370	14.9448	9.4884	13.5673	10.2315	11.1088	9.0422	9.8101	7.0095	7.0944	5.8858	5.9964	6.0281	5.0943	7.3172	9.1669	7.9829	5.7168
12.5865	12.1029	11.9898	11.9429	11.8422	12.7047	12.7370	14.9448	9,4884	13.5673	10.2315	11.1088	9.0422	9.8101	7.0095	7.0944	5.8858	5.9964	6.0281	5.0943	7.3172	9.1669	7.9829	5.7168
12,5865	12.1029	11.9898	11.9429	11.8422	12.7047	12,7370	14.9448	9.4884	13.5673	10.2315	11.1088	9.0422	9.8101	7.0095	7.0944	5.8858	5.9964	6.0281	5.0943	7.3172	9.1669	7,9829	5.7168
12.1615	11.9769	12.5512	12.1494	12:8566	12.1990	12.6560	14.4760	11.0428	13.1520	11.6210	13.2389	11.7275	14.0798	11.0785	12.1817	12.3637	11.8998	17.4882	11.0828	15.3105	18.1073	14.8795	12.5576
11.7368	13.8611	14.9806	15.6753	17.0493	15.7810	13.4773	15.9970	12.5197	14.0033	12.2411	14.0587	12.3807	14.1025	12.0102	10.2642	9,7641	10.0620	10.7699	10.0636	14.2167	17,4344	14.2010	13.4468
13.6621	14.2294	13.6258	14.3270	14.8305	14,4143	14.1209	16,4844	13.5230	15.1326	14.2250	15.6800	14.5962	16.1151	13.8423	15.1257	15.0262	14.9764	15.3315	14,4773	17.6396	20.2098	17,4220	15.6261
11.8924	11.1656	12.0310	12.8203	11.7447	11.5642	11.9468	13.6910	10.0465	12.2925	10.6629	11.8077	10.8705	12.1452	9.5825	10.2201	10.2358	10.0780	10.3857	9.1376	12.8622	15,0002	12.5007	10.9508
12,6000	13.2134	12.7794	13.2494	13.8178	13.2242	13.2243	15.2876	11.6538	13.6721	11.7658	13.1423	11.9437	13.8656	10.6527	11.7140	11.7765	11.7283	11.8951	10.6139	14.7847	17.6066	14.4584	12.1166
9.8923	9.6409	9.5982	10.3744	10.9746	9.8728	9.6977	11.0323	8.1475	9.7697	8.5605	9.9402	9.0674	10.7318	7.5720	8.4316	7.902€	7.4991	7.1593	7.1973	11.0551	10.3527	8.8029	10.1301
18.1229	16.9850	17,5410	18.6147	18.7771	17.9008	18.1392	18.8020	15.8941	18.1627	17.1846	19.1308	17.8196	18.6146	17.0755	17.8220	17.9863	18.1432	18.7065	18.1002	20.3171	21.3830	19.8141	19.3269
18.1408	18.4711	15.0483	16.7097	16.8903	16.9690	18.6477	18.1338	18.0204	16.9544	15.0460	15.8971	17.1648	16,0081	16.4603	17.0064	17.0407	19.4765	17.0039	16.5011	18.6000	20.1657	18.5063	20,3535
15.1192	10.9748	8,1779	8.2235	9.9260	9.9354	9.9615	15.1666	11.2890	14.3490	12.7089	14.3108	8.8169	11.0120	9.2300	8.9482	9.4687	7,7649	8.2258	8.6821	12.6044	20.3487	166710	12.5999
12.1815	10.3490	9.8240	8.2235	9.9260	9.0123	9.9615	13.5139	9.0113	11.8852	10.4685	11.9472	11.0570	15.3380	10.6189	11.7168	12.0361	11.7320	11.9299	10.9191	16,7243	17.9548	14.4881	16.6469
14.9018	15.0336	15.1686	17.5251	17.3979	17.6133	15.6537	16.8572	13.9274	15.8530	14.2741	13.9593	13.2694	14.4791	11.3538	17.1731	12.2328	14.2556	14.1094	13.7110	16.0902	18.7757	14.4612	13.9410
13.6235	12.5084	13.2868	13.3506	14.1634	14.0170	13.8151	15.6480	12.3439	14.9122	11.8977	13.4137	11.7144	14.0200	10.6503	17.2821	12.4171	11.8444	11.9838	10.8435	14.3813	17.1853	13.8672	12.6790
13.6235	12.5084	13.2868	13.3506	14.1634	14.0170	13.8151	15.6480	12.3439	14.9122	11.8977	13.4137	11.7144	14.0200	10.6503	12.2821	12.4171	11.8444	11.9838	10.8435	14.3813	17.1853	13.8672	12.6790
	46.5007	1				1 200002	1 22000		- ATTENDED	***************************************					Janeous	********		1					

APPENDIX 4-4

Bus Schedule & Emission Inventory for Buses Start Emission

Bus Schedule

														H	our											
			00:00 - 01:00	01:00 - 02:00	02:00 - 03:00		04:00 - 05:00	05:00 - 06:00	06:00 - 07:00	07:00 - 08:00	08:00 - 09:00	09:00 - 10:00	10:00 - 11:00	11:00 - 12:00	12:00 - 13:00	13:00 - 14:00	14:00 - 15:00	15:00 - 16:00	16:00 - 17:00	17:00 - 18:00	18:00 - 19:00	19:00 - 20:00	20:00 - 21:00			23:00
	кмв	28	0	0	0	0	0	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
	кмв	25	1	0	0	0	0	0	3	4	4	4	4	4	4.	4	5	5	5	5	5	5	5	3	3	3
By Route	кмв	30	0	0	0	0	0	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	кмв	72	1	0	0	0	0	0	3	3	3	3	3	3	3	3	3	3	3	4	4	4	3	3	3	3
	кмв	86C	1.	0	0	0	0	0	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	RB01	30	0	0	0	0	0	2	3	3	3	3	3	3	3	3	3	3	3	3	3	а	3	3	3	3
	R802	28, 2F, 30, 72, 86C	3	0	0	0	0	3	14	15	15	15	15	15	15	15	16	16	16	17	17	17	16	14	14	14
Su Band	RB03	28, 2F, 30, 72, 86C	3	0	0	0	0	3	14	15	15	15	15	15	15	15	16	16	16	17	17	17	16	14	14	14
By Road	RB04	30	0	0	0	0	0	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	RB05	2B, 2F, 72, 86C	3	0	0	0	0	1	11	12	12	12	12	12	12	12	13	13	13	14	14	14	13	11	11	n
	R806	28, 2F, 72, 86C	3.	0	0	0	0	1	11	12	12	12	12	12	12	12	13	13	13	14	14	14	13	11	11	ti

http://iganch.kmb.hk/kms.ava.ust.lenex.ava.thirmen.

Bus Soak Time (min)

														He	our											
			00:00 - 01:00	01:00 - 02:00	02:00 - 03:00	03:00 - 04:00	04:00 - 05:00	LPS-S-C-ST	06:00 - 07:00	07:00 - 08:00	10.000.000	09:00 - 10:00	10:00 - 11:00	100000000000000000000000000000000000000	12:00 - 13:00	13:00 - 14:00	14:00 - 15:00	15:00 - 15:00	16:00 - 17:00	17:00 - 18:00	18:00 - 19:00		20:00 - 21:00	21:00 - 22:00	The second second	23:00 24:00
	кмв	28	N/A	N/A	N/A	N/A	N/A	720	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
	кмв	2F	30	N/A	N/A	N/A	N/A	N/A	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
By Route	кмв	30	N/A	N/A	N/A	N/A	N/A	720	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
	кмв	72	30	N/A	N/A	N/A	N/A	N/A	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
	кмв	86C	30	N/A	N/A	N/A	N/A	720	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
By Road	Ali	IA.	30	N/A	N/A	N/A	N/A	720	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30

The soak time of the buses are found to be <30 minutes during daytime and evening time according to site survey in 10th July 2021. The soak time of the buses during 5:00-7:00 are unknown thus 720 min has been assumpted for conservative assessment.

Bus Schedule & Emission Factor

													Ho	ur											
		00:00	01:00 -	02:00 -	03:00 -	04:00 - 05:00	05:00 - 06:00	06:00 - 07:00	07:00 - 08:00	08:00- 09:00	09:00 - 10:00	10:00 - 11:00	11:00 - 12:00	12:00 - 13:00	13:00 - 14:00	14:00 - 15:00	15:00 - 16:00	15:00 - 17:00	17:00 - 18:00	18:00 - 19:00	19:00 - 20:00	20:00 - 21:00	21:00 - 22:00	22:00 - 23:00	23:00
	RB01	0	0	0	0	0	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	RB02	3	0	0	0	0	3	14	15	15	15	15	15	15	15	16	16	16	17	17	17	16	14	14	14
Hourly Trip count By Road	RB03	3	0	0	0	0	3	14	15	15	15	15	15	15	15	16	16	16	17	17	17	16	14	14	14
Section	RB04	0	0	0	0	0	2	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	RB05	3	0	0	0	0	1	11	12	12	12	12	12	12	12	13	13	13	14	14	14	13	11	11	11
	RB06	3	0	0	0	0	1:	11	12	12	12	12	12	12	12	13	13	13	14	14	.14	13	11	11	- 11
Soak Time (min)	All	30	N/A	N/A	N/A	N/A	720	720	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
	NOs	1.00	N/A	N/A	6/0-	NA	10,710.	10,710	1.110	1.138	1.10	149	1,138	1.138	1.3M	1.438	rin .	(13)	1.139	1.136	149	Lim	100	1139	1114
Fundations Francis (a Audus)	NOZ	0.000	N/A	N/A	N/A	N/A	.688	1.101	0.710	8.130	0.110	0.100	0.430	0.100	0.330	0.110	6,100	0.130	0.110	0.430	ALM	0.110	0.110	6,600	0.110
Emisison Factor (g/trip)	RSP	0.000	WA.	N/A	N/A	WA.	0.000	0.000	0.000	1.000	0,000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0,000
	FSP	0.000	N/A	N/A	N/A	N/A	0.000	0.000	0.000	9.000	0.000	0.000	0.000	0.000	9.000	0.090	0.000	0.000	5.000	0.000	0.000	0.000	0.000	0.000	0.000

Emission Factor for each Road Section

			1000	10.00		2000			come	270.00		5-7-5	-	Ho	ur				Corre			5000				
			00:00 -	01:00 -	02:00 -	03:00 -	04:00 -	05:00 -	06:00 -	07:00 -	08:00	09:00 - 10:00	10:00	11:00 =	12:00 =	13:00 -	14:00 -	15:00 - 16:00	16:00 = 17:00	17:00 - 18:00	18:00 -	19:00 -	20:00 -	21:00 -	22:00	23:00
		RB01	0.001+00	0.000400	0.001+00	0.00E+00	0.001+00	5.11(-0)	7,97E-07	E 47E CB	3.475-08	8.476-08	E 47E-OE	E.471-01	1.47E-08	3.47T-OI	8.476-06	E 975-08	9.47E-09	B-675-08	E 47E-08	1.471-01	IL 47E-CIE	E47E-08	3.475.49	E47F-08
THE RESERVE		RB02	B-47E-08	0.000+00	0.001+00	0,00E+00	0.006+00	7.978-07	1.775-06	4.231-07	4.216-67	4.238-07	4.216-07	4.731-07	4.236-07	6.318-07	4.521-07	4521-07	4535-07	4 S.W-07	4.801-07	4.808.40	8.575.47	1951-07	3.956-07	1991-07
Emisison Factor		RB03	E-47E-08	0.000400	0.001+00	0,000+00	0.006+00	7.578-07	1.775-06	4.231-07	4216-02	4.236-07	4.236-07	4.731-07	4.23E-07	639-67	4.521-07	4.521-07	4535-07	4 B/E-07	4.801-07	4,808.40	8.575.67	1951-07	3.988-07	1991-07
(g/m ² /s)	NOx	RB04	0.001+00	0.000+00	0.001+00	0.00E+00	0.006+00	1.11(-0)	7.97E-07	E.47E-CB.	147(-01	8.471-08	E 47E-08	E.471-01	1.475-08	3.471-OL	8.471-01	E 875-08	B.47E-08	8.47E-08	E-47E-08	1.471-01	31.47E-08	- 8.47E-08	E-67E-68	E47F-08
(8/111/3)		RBOS	B.47E-08	0.000+00	0.00E+00	0.006+00	0.008+00	162-07	2.90E-06	A 2012-07	3.196-07	1.191-07	139(-0)	1.196-07	3.396-07	5.FR-07	1.675-07	1675-07	3.676-67	3.956-07	1.951-07	3.92.07	3.675.67	3.101-07	3.108-07	1:106-07
		RB06	E 47E-08	0.006+00	0.001+00	0.006+00	0.00E+00	168-07	2.90E-06	7 Bill -02	3.196-07	1.191-07	1390-07	3.198-07	3.396-07	5.PE-07	1.675-07	1575-07	3.675-07	3.916-07	1:951-07	3.922-07	1678-07	1,101-07	3.108-07	1.106-07
		RB01	T 0.001-00	0.008+00	0.001-00	0.00(+00	0.007+00	158.0	2.916-07	2.018-08	2.466-01	2.461-08	Z.461-04	2.46-04	2.607.48	248-0	2.461-08	Z#8-04	2467-08	240-08	2.61-01	7.88408	2.464-08	2.401-08	240.00	2.461-08
		RBOZ	2.467-08	0.000+00	0.001+00	0.001+00	0.006+00	2.311.60	1.081-06	1.231.07	1.236-07	1.231-07	1238-07	1.231-07	1.201.07	1.278-01	L31E-07	1.316-07	1316-07	1.192-07	1.198-07	1.00.07	3.512-07	1.03.07	1.151-67	1.156-07
Emisison Factor		RB03	2.462-08	9.000+00	0.005+00	0.000+00	0.005+00	2.111.40	1.081-06	1.231.407	1.236-07	1.231-07	1,238-07	1.231-07	1.201.07	1.218-07	1.31E-07	1.516-07	1316-07	1.596-07	1.108-07	1.8847	3.512-07	1.151-07	1.151-67	1.156-07
1-1-21-1	NO2	RB04	0.001-00	0.000+00	0.005+00	0.001+00	0.005+00	1545.00	1.31E-07	2.400.08	2.445-08	2.46E-08	2.466-08	2.465-OI	2 602-08	2.64-0	2.46E-08	7.603-04	2.46E-08	240-08	2.442-08	7.ME co.	2 462-08	2.601-01	2.465-09	2.464-08
(g/m /s)		RB05	2.46E-08	6,000+06	300000	0.000+00	0.005-00	7.798.48	X.87E-07	9.826-08	9.425-08	9.826-08	9.42E-08	9 421-04	9.826.68	9.475-08	1.061-07	1.008-07	1.06E-07	1.19-07	L DE-07	1.151.07	E.06E-07	9.000-08	100107	9.000.08
		RB06	2.466-08	6000+06	0.000-01	0.000.+00	0.006+00	2.88.68	X.87E-07	5,82E-08	BAREOR	9.826-08	9.62E-08	9 A2E-04	9.828.48	9,635-08	L068-07	1.008-07	1.06E-07	1.19-07	1.03-07	1.85.00	£068-07	9.008-08	100108	9.006-08
	-	RB01	0.004.00	600E+06	2001-01	0.000+00	0.006-00	0.000-00	0.006+00	0.005+00	0.002.400	0.000 +00	9,000-60	G006-00	0.004-00	0.000+00	0.006+00	0.008+00	0.006+00	0.001+00	0.506+00	8.006-60	000E-00	0.000.000	0.00E+00	0.000-00
	1	RB02	0.005-00	5.00E+06	0.001+00	0.000+00	0.006-00	0.000400	0.000.00	0.002+00	0.008-00	8.000-00	0.000+00	0.0001-00	0.001+00	0.008+00	0.000+00	0.006+00	0.000-00	0.001-00	0.005+00	5.00E+00	0.000+00	0.006+00	0.006+00	0.006+00
Emisison Factor		RB03	0.008-00	5.006+06	0.001+00	D-00X+00	0.008-00	0.000.400	0.000.+00	0.002+00	0.008+00	8000-00	0.000+00	0.008+00	0.001+00	0.008+00	0.006+00	0.000+00	0.000.+00	0.001+00	0.000+00	5.00F+00	0.000=00	0.005+00	0.000+00	0.005+00
	RSP	RB04	0.005-00	5.006+06	0.001+00	D-00X+00	0.006-00	0.000405	0.800+00	0.02+00	0.008-00	8000-00	0.000	0.0001-00	0.001-00	0.008+00	0.006+00	0.000+00	0.000+00	0.001-00	0.006+00	E006+00	0.000-00	0.806+00	0.006+00	0.006+00
(g/m²/s) Emisison Factor (g/m²/s)		RB05	0.005-00	5.006+06	0.001+00	D-00X+00	0.008-00	D.00E+08	0.000.00	0.02+00	0.008+00	0.000-00	0.005+00	0.008+00	0.001+00	0.008+00	0.000+00	0.000+00	0.000+00	0.001+00	0.005+00	5.00E+00	0.00E+00	0.005+00	0.000+00	0.005+00
		RB06	0.00f -00	5.00E+00	0.001+00	0.000400	0.00€-00	0.00E+00	0.600(+00	0.002+00	0.000 +00	8.00E+00	3.006+00	00000	0.006+00	0.008+00	0.000+00	0.000-00	900(+00	0.001+00	0.00€+00	5.006+00	00000	0.000+00	5.60E+00	7.00
		RB01	0.001-00	5,000+00	9,007+09	0.000+00	8.005-00	0.00E-00	0.601+00	0.001-00	0.000-00	0.000.00	0.006+00	0001400	0.006-00	0.008+00	nooren	0.000-00	0.000-00	0.001+001	0.000-00	5,000,00	000-00	0.600+00	0.000-00	0.000-00
Emisison Factor	1	RB02	0.005-00	\$00E+06	0.001+00	0.000+00	0.006-00	0.000.400	0.806+00	0.002+00	0.002 -00	0.00E+00	0.00E+00	0001400	0.004-00	0.008+00	0.000+00	0.000-00	00000	0.001+00	0.000-00	5.005+00	200:00	0.806+00	D 000 + 000	0.000.400
	1000	RB03	0.001-00	8.00E+(8)	9.001100	0.000+00	0.007-00	0.000400	9898+00	0.002+00	0.000+00	6.00F+00	0.005+00	0.001=00	0.008+00	0.002400	0.000+00	0.000+00	0.000+00	0.001+00	0.000400	0.007+00	000-00	0.00(+0)	0.000100	0.000-00
	FSP	RB04	0.001-00	6.00(+0)	9.001100	0.000+00	0.007+00	0.00E400	0.001+00	0.00(+00	0.000+00	5.00F-00	0.005+00	0.001+00	0.008+00	0.002400	0.00E+00	0.006+00	0.900 +000	0.001+00	0.000+00	0.006+00	000-00	0.00(+0)	6.005+00	0.000400
(g/m²/s)	1	RB05	0.001-00	6.00E+(8)	9.001100	0.000400	0.007+00	0.000400	0.001+00	0.00(+00	0.001+00	6.00F-00	0.007-00	0.001-00	0.008+00	0.002400	0.000+00	0.006+00	0.007+00	0.001+00	0.000400	0.007+00	0000-00	0.00(+0)	0.000100	0.000-00
	1	RB06	0.008-00	8.000+00	0.001+00	0.000+00	0.006+00	0.000400	0.002+00	0.008-00	0.002+00	B.00E+00	0.006+00	0.002+00	0.008400	0.002+09	0.00E+00	0.006+00	0.002+00		0.000+00	0.000400	0.001-00	0.008+00	5.000+00	

17196-06 17196-06 7.1616-07 2.973E-06 2.977E-06

1.0786-06 1.678E-06 2.31.11-07 LOW EO EO

0.000E+00 0.000E+00 0.000E+00

8,0001+00 8,0001+00 9,0001+00

0.0001+00

Emission Factor Ratio

														Hour					ľ			ĺ				1
			00:00	01:00	02:00	03:00	05:00	00:00	06:00	-00:00	-00:80	10:00	10:00	12:00	13:00	13:00 -	15:00	15:00 1	17:00	12:00 - 1	19:00-1	20:00	21:00 2	22:00 - 22:00	23:00	23:00-
		RB01	00000	_	000000	0.000-00	00-3000	8675-02	3,000-00.	1,088-03	109601	100001	10-9-01	-	1,006-03	10901	109601	-	-	-	-			-	-	1000001
		RB02	22M02	0.008+00	00000-00	0.005+00	00430070	2.145.01	1.005+00	1,146.01	134601	1716601	1146.01	1.148-01	1.146.01	1748-01	123601	131101	131161	10:36:01	1,796-01	158601	topics in	108601	105501	103901
Designation of the land		RB03	3.2 ME-02	0.000	0.000.00	0.000.00	00*3000	0.146.01	3.000-00	103961	1100001	1,166-01	1146-01	10-841-0	103961	1116-01	1216-01	19/127	10:515-01	1236.01	1396-01	15366.01	121/01	101101	10397	100001
Katio to Peak	NOX	RB04	D(000 +400	0018400	0.000-00	B.IDE-OR	0.001-00	6.675-02	3.008+400	10:29)1	109901	1066-01	10.861	10801	10.58).1	1086.01	1055-01	105501	10.561	10.68-01	1,066-01	10801	108.01	101911	1086.01	1066-01
		RB05	19862	0.000	оторго	0.300.400	00-3000	SOR 42	1,000-00	101011	139108	10-2113	10:8917	1368-01	1.18701	1386.01	12361-23	1362923	1705-01	10:861	1,335/03	1335.01	1380	1,091'03	1366-03	10/201
		RB06	7.908.01	0.008+00	000000	0.005+00	0.000*000	NOW OF	1,000,100	1,16701	103917	1.168-01	1198-01	13410	1.168.01	1102017	103901	1.355.01	138501	1335-01	1.308-01	10-3517	CHE 01 10	1001907	1.0520.1	103501
		REGI	00-3000	1018070	0000000	00.000.00	0.00(5:00	10:109	1.005+00	109907	109901	109901	1005-01	10801	1088-01	10:2901	109501	10361	106901	10-2901	1,066.01	10001	10801	10101	109901	1066-01
		RB02	20-WE-Z:	0.000	00-0000	0.001-00	00-3000	3.140.01	1.000+00	1,146-01	1348-01	1,14(-01	1148-01	1346-01	1.166.01	1746-01	1,216.03	121101	LIROS	1,376-03	128601	10.821	1216-01 17	1,088.01	1006-03	109901
Deale or Deal	BIO'S	R803	3.386.02	0.005+00	00000-00	0.006+00	0043000	2,146.01	1,006+00	1,146.01	Lineol	114601	10-3617	11145-01	10.341.1	10.911	15315-01	1315-01	15315-01	1296-01	10:861	10-9671	10 110 11	101901	1,065.03	10-3901
Ratio to Peak	NOS	RB04	11,000:400	0.005+00	0.006-00	(D+3Q/1)	DC+3(X) Q	8,675.02) 00K+(0	102901	109901	102901	10/5/01	10-201	10.38(1)	LOKEL	1.065-01	103601	10-201	10.501	1,006-01	10201	10201	104401	1,066.01	1,050.01
		RB05	2,908.02	0008100	appoin	0.000.00	00+100/0	50 MO 6	1,006.00	1,168.01	1,166.05	116601	10:817	136.01	1.146.01	1105.01	1396.01	126141	120.01	139601	1,356-01	13861	136.01	109601	1,096-03	10-9901
		RB06	2,908-03	0.008+000	0.0001-00	0.005-00	0001400	3.0W.GZ	1.00%+00	3,163.03	1.162.01	1,165.01	1164-01	1380	1,162-01	1.148.01	1385-01	1,366.01	1.16.01	1335-01	1,385.01	LMFOL	138.01	1,0010.01	108901	1.042-01
															ľ											
		REGI	01-202W	0.68+00	0,000-40	0.005-00	0.0015+00	0.0(6-0)	8.00K+(0	0)100010	0.000.400	0.001 +00	00-9000	0,000,000,0	0.006+00	0.008+00	0.000.0	0.000.00	0,000.400	00+3(0:0	0.0018+00	0,08+00	DODE+00 0.0	0.0000+00	0,005-00-0	0.08+00
		RB02	00000	0.000-00	00-00070	0.000+00	00-1000	00-3000	0.000+00	00+300/0	-0.000.00	0.008 +00	00-9000	0001000	000000	0043000	0.000.00	0.000.00	00-3000	0001000	0.0001+000.0	0.00E+00:0	90-3000	0.000.0	0.00E-00.	0000
Date of Date	200	RB03	00000	0008100	000000	0.005+00	00430070	00+90010	000000	00+30010	000000	0000000	00+8000	0.000.00.0	0001000	0049000	0.001100.0	0.00€+00	0.000.000	00+3000	0.004100.0	2000000	000000	0.00000	0.000.00	000 1000
Ratio to Peak	2	RB04	0000-00	0.000-00	0000000	COMPAND.	00-3000	000000	90000	D.400400	0.000.00	0.000.00	0.006-00	000000	0.006+001	0.000.0	0.001.00	0.006+00	000000	00+1000	00-1000	004000	00-1000	0.000000	0.000.0	0001000
		RB05	D 0005 4(0	0.005+00	0.0000-00	n notice	0.005-00	U006+00	0.0000	0.006+100	0.037 +00	0.00 - 300 0	0.000.00	00000	0.000	0.000-00	0.005+00	0000000	0.000-100-0	0005-00	0 00:1:00	0 (00+100	DODE 4995 D.S	0 000010	0.0000	0.000.00
		RB06	0.000.400	0.008+001	0001000	0.000-00	00-10010	0.008.400	0.0000+00	0.00.0	0.001+00	00+100/0	0.001-00	00+100 D	0.008+00	00-1600	00+800'0	0.001400	0.000-00	0.000	0.001-00	0.001+00	00-3000	0 0041000	0.000.0	0.000.00
		RB01	00-3000	0.008+00	0.0005400	0.105+01	0.001.00	0.000	D DOC+100	0)+300/0	0.00.400	0.000.00	00-9000	00*3000	00+3000	000000	0.006+00	0.006+00	0.000.400.0	00000	00-1000	0.008-00	0000-00	0.0000+00	0.000.00	0.000.00
		RB02	00×300 u	0.000	0.0000	0.000 100	0.005+00	0.00E+00	0.0000	0.005+00	0.000.00	0.008+00	0.006+00	0000000	0.000100	0.000	0.000.00	0.00€+00	000000	0.005+00	0.001-000	0.001100.0	0 90×300 D	0.006+00.0	0,001+00.0	0.005 +60
Date to Dank	200	RB03	0.000.400	0.008-00	000000	0.000.00	00-3000	000000	0.000+00	0.000.0	0.000	0001-000	00+300'0	0.000.00.0	0001400	000000	0.001-00	0.00(+00	0.000.000	00-1000	0.0001+000	0,000,000,0	00-3000	0.000.000	0.000.0	00-1000
Natio to Fedr	2	RB04	000000	0.000	0.005900	0.006+00	00-3000	00+3000	0.000+00	90+300'0	0.000	00-8000	00+9000	0001000	0004000	0.005500	0001000	0.005+00	000,3000	0001000	0.001-00.0	0006400	0003000	0.000.000	00000	0.001 +00
		RB05	0)+30010	0.008+00	0.0000-00	0.000+00	00*3000	GO-990.D	9,000.400	D)+300 G	0,000.400	0.000	0000000	00+3000	00+1000	0.000+000	0.00	0000000	000000	000000	0 00-300 0	0 (05:50) 0	0.000000	0.000×100 0	30-300.0	0.000
		R806	0.000.400	0.000 +000	0000000	0.000	00*100'9	0.001	0.000.00	0.001400	0,000.400	0.000 +000	0.001100	00+300D	0001000	0.0001-000	00001-000	0.006+000	0.305.40	00+1000	00-1000	0.006+00	000,3000	0000000	0.001-00.0	0001000

APPENDIX 4-5

Predicted Pollutant Concentration (Air Quality)

	0.000			Same		Daily 1st	Daily 10th	ion no	Daily 1st	Daily 36th	the lines	Hourty 1st	Hourly	1
Assessment Point	PATH Grid	Easting (m)	Northing (m)	Level (mAG)	Level (mPD)	Maximum	Maximum	Annual	Maximom	Maximum	Annual	Maximom	19th Maximum	Annual NO2
	Crite	ria (AQO)	V			RSP	100	50	FSP	FSP 50	35	NO2	NO2 200	40
AP-01	[38,35]	833893,99	822103,34	1.5	6.55	91.98	63.55	27.86	74.88	24.75	15,44	194.63	154,43	37.95
AP-01	[38,35]	833893.99	822103.34	6,35	11.4	91.83	63,37	27,70	74.75	24,55	15.29	193,67	148.26	33.15
AP-02	[38,35]	833881.31	822088.08	15	6.55	92.10	63.60	27.92	74.99	24.76	15.50	198,35	160.49	39.33
AP-02 AP-03	[38,35]	833881,31 833868.63	822088.08 N22072.83	6,35	11,4 6.55	91.89 92.48	63.40	27.72	74.80 75.35	24.56	15,31	195.60 219.17	155,20	33.57
AP-03	[38,35]	833868.63	X22072.83	635	II.A	91.99	63.46	27.72	74,89	24.60	1531	199.02	161.54	33.31
AP-04	[38,35]	833854,78	822084.34	1.5	6.55	92.41	63.61	28.06	75,28	24,72	15,62	219.16	176,41	41.98
AP-04 AP-05	[38,35]	833854.78 833840.93	822084.34 822095.85	6.35	6.55	91.97	63.41	27,72	74.88 75.26	24.61	15.31	199.42	162.47 176.54	33.37
AP-05	[38,35]	833840,93	822095.85	6.35	11.4	91.96	63.39	27.72	74.87	24,60	1531	202.73	163,04	33.27
AP-06	[38,35]	833891.00	N22105.75	1,5	6.55	91.95	63.50	27.83	74.86	24.71	15.42	193.93	153.45	37.13
AP-06 AP-06	[38,35]	833891,00 833891,00	822105.75 822105.75	6,35 10.85	11.4	91.83	63.36	27.70	74.74	24.46	15.19	193,25	145.12	33.21
AP-06	[38,35]	833891.00	N22105.75	14.5	19.55	91.61	63.12	27,53	74.54	24.41	15.14	191.27	140,45	28.41
AP-06	[38,35]	833891.00	822105.75	18	23,05	88.96	62.61	27.24	72.12	21.77	14.71	187.13	133.64	24.10
AP-06 AP-07	(38,35)	833891,00 833873,54	822105.75 822084.74	21.5	26,55 6.35	92.15	62.56 63.58	27.21	72.08	25,75	14,69	186.47	131,61	23.25 39.63
AP-07	[38,35]	833873.54	822084.74	6,35	114	91.92	63.40	27.73	74.83	24.58	15.32	197,02	157.58	33.75
AP-07	[38,35]	833873.54	822084.74	10.85	15.9	91.72	63.23	27.58	74.64	24,47	15,18	192.41	147.29	29.69
AP-07 AP-07	[38,35]	833873.54 833873.54	N22084.74 822084.74	14.5	19.55 23.05	91.62 88.96	63.12	27.51	74.55	24.42	15.12	191.52 187.38	140,93	27.97
AP-07	[38,35]	833873,54	822084,74	21.5	26,55	88.91	62.56	27.20	72,08	23,76	14,68	186.70	131,04	23,08
AP-08	[38,35]	833848,83	\$22105.35	1.5	6.55	92.08	63,40	27.87	74.97	24.61	15.45	201.77	165.67	37,44
AP-08 AP-08	[38,35]	833848,83 833848,83	822105.35 822105.35	6,35	11.4	91.90	63.32	27.73	74.81	24.56	15.31	197.74	160,19 147,26	33,63
AP-08	[38,35]	833848.83	N22105.35	14.5	19.55	91.62	63.14	27.53	74.55	24,45	15.13	190.32	143.22	28.44
AP-08	[38,35]	833848.83	822105.35	18	23.05	88.96	62.64	27.24	72.13	23.80	14.72	186.57	134.13	24.15
AP-08 AP-09	[38,35]	833848.83 833837.20	822105.35 822115.02	21.5	26.55	88.91 92.09	62.58	27.21	72.08	23,78	14,69	186.18 207.16	130.94	23.33
AP-09	[38,35]	833837.20	822115.02	6,15	11.4	91.90	63.31	27.73	74.81	24.55	15.32	197.75	160.93	33.66
AP-09	[38,35]	833837.20	822115.02	10.85	15.9	91.72	63.21	27.60	74.65	24,50	15.20	192.11	150.24	30.33
AP-09 AP-09	[38,35]	833837.20 833837.20	822115.02 822115.02	14.5	19.55	91.62 88.97	63.14	27.54	74.55	24,46	15.14	189.81	143.12	28.60
AP-09	[38,35]	833837.20	822115.02	2].5	26.55	88.92	62.59	27.21	72.09	23.78	14.69	185.82	131.81	23.46
AP-10	[38,35]	833825,54	822124.64	15	6.55	92.12	63.40	27,89	75.01	24.58	15.46	215.75	168.60	37.87
AP-10 AP-10	[38,35]	833825.54 833825.54	822124.64 822124.64	6,35	11.4	91.90	63.32	27.73	74.81	24.55	15.32	202.23 192.20	161.38 151.53	33.92
AP-10	[38,35]	833825.54	N22124.64	14.5	19.55	91.62	63.15	27.54	74.55	24,46	15.14	189,48	144.49	28.75
AP-10	[38,35]	833825.54	822124.64	18	23,05	88.97	62.66	27.25	72.13	23,82	14.72	185,85	135.29	24.45
AP-10 AP-11	[38,35]	833825.54 833837.29	822124.64 822138.78	21.5 1.5	26.55 6.55	88.92 91.96	62.60	27.22	72.09	23.79	14.70	185.59 196.67	132.36 159.69	23.59 35.83
AP-11	[38,35]	833837.29	822138.78	6,35	11.4	91.84	63.26	27.72	74.76	24.53	1531	194.86	155.13	33,62
AP-11	[38,35]	833837,29	822138.78	10.85	15.9	91.71	63.19	27.62	74.63	24,49	15.22	192.06	147.70	30.93
AP-11 AP-11	[38,35]	833837.29 833837.29	822138.78 822138.78	14.5	19.55	91.62 88,97	63.13	27.55	74.55	24.45	15.16	189.48	146.05	29.12
AP-11	[38,35]	833837.29	822138.78	21.5	26.55	88.92	62.59	27.22	72.09	23.78	14.70	185.51	132.59	23.70
AP-12	[38,35]	833847.69	822151.30	15	6.55	91.90	63.29	27.76	74.81	24,55	15.34	195,64	154.24	35.05
AP-12 AP-12	[38,35]	833847.69 833847.69	822151.30 822151.30	6,35	11.4	91.80	63.25	27.70	74.72	24.53	15.29	193,75	151.93	31.01
AP-12	[38,35]	833847.69	N22151.30	14.5	19.55	91.62	63.12	27.56	74.55	24,44	15.16	189.36	145.32	29.32
AP-12	[38,35]	833847.69	822151,30	18	23.05	88.97	62.63	27.26	72.14	23,80	14.74	185.70	137,47	24,86
AP-12 AP-13	[38,35]	833847.69 833866.19	822151.30 822135.93	1.5	26.55 6.55	88.93 91.86	62.59	27.23	72.09	23,78	14.71	185,43	132.25 150.69	23.84
AP-13	[38,35]	833866,19	822135.93	6,35	11.4	91.79	63.26	27.69	74.71	24.54	15.28	192.12	149,39	32.91
AP-13	[38,35]	833866.19	822135.93	10.85	15.9	91.70	63.19	27.61	74.62	24.48	15.21	190.37	147.05	30.73
AP-13 AP-13	[38,35]	833866.19 833866.19	822135.93 822135.93	14.5	19.55 23.05	91.62	62.63	27.55	74.55	24.44	15.15	189.83	144.72	29,06
AP-13	[38,35]	833866.19	822135.93	21.5	26.55	88.92	62.58	27.22	72.09	23,77	14.70	185.76	132.94	23,63
AP-14	[38,35]	833861.54	N22130.31	1.5	6.55	91.89	63.31	27,76	74.80	24.58	15.34	194.46	152.79	34.70
AP-14 AP-14	[38,35]	833861.54 833861.54	822130.31 822130.31	6,35	11.4	91.81	63.26	27.70	74.73	24.54	15.29	193,23 191,08	150.01	33,05
AP-14	[38,35]	833861.54	822130.31	14.5	19.55	91.62	63.12	27.55	74.55	24,44	15.15	189.88	144.82	28.99
AP-14	[38,35]	833861,54	822130.31	18	23.05	88.97	62.63	27.25	72.13	23,80	14.73	186.16	137.18	24.54
AP-14 AP-15	[38,35]	833861.54 833876.25	822130.31 822118.01	21.5	26.55 6.55	88.92 91.89	62.58	27.22	72.09	23,77	14.70	185.81	132.88 151.82	23.57 35.21
AP-15	[38,35]	833876.25	822118.01	6,15	11.4	91.81	63,30	27.70	74.73	24.56	15.29	191,89	147.60	33,13
AP-15 AP-15	[38,35]	833876,25 833876,25	822118.01 822118.01	10.85	15.9 19.55	91.70	63.12	27.50	74.63	24,48	15.20	191.17	145,53 142,67	30.50 28.73
AP-15	[38,35]	833876.25	822118.01	18	23,05	88.96	62.63	27.24	72.13	23,78	14.72	186.76	135,37	24.32
AP-15	[38,35]	833876.25	822118.01	21.5	26,55	88.91	62.58	27.21	72.08	23,76	14.69	186.28	131.66	23.40
TA-01 TA-01	[38,35]	833893,99 833893,99	822103.34 822103.34	29,35 32.5	34.4 37.55	88,84 88,82	62.48	27.16	72.02	23,73	14.65	185.45 185.21	126.47	22.00
TA-01	[38,35]	833893,99	822103.34	35.65	40.7	86.95	62.11	26.99	70.29	23,32	14.63	168,18	118.85	19.69
TA-01	[38,35]	833893,99	822103.34	38.8	43.85	86.94	62.10	25.98	70.28	23,32	14.41	167.53	117.56	19.43
TA-01 TA-02	[38,35]	833893.99 833881.31	822103.34 822088.08	41.95 29.35	34.4	86.93 88.84	62.09 62.48	26.97 27.16	70,27	23,31	14.41	167,09 185,56	116.64 125.99	19.22
TA-02	[38,35]	833881.31	N22088.08	32.5	37.55	88.82	62.46	27.15	72.00	23,73	14.63	185.30	124.72	21.64
TA-02	[38,35]	833881.31	822088.08	35.65	40.7	86.95	62.11	26.99	70,29	23.32	14.42	168.51	119.03	19.69
TA-02 TA-02	[38,35] [38,35]	833881.31 833881.31	822088.08 822088.08	38.8 41.95	43.85 47	86.94 86.93	62.09 62.08	26.98	70.28	23.32	14.41	167.78	117.10	19.44
TA-02	[38,35]	833868,63	822072.83	29.35	34,4	88.85	62.47	27.16	72.03	23.74	14,64	185.67	124.93	21.97
TA-03	[38,35]	833868.63	822072.83	32.5	37.55	88.83	62.45	27.15	72.01	23.73	14.63	185.39	123.87	21.65
TA-03 TA-03	[38,35]	833868.63 833868.63	822072.83 822072.83	35.65 38.8	40,7	86.96 86.94	62.10	26.99	70.30	23,33	14.42	168.85 168.05	118.31	19.69
TA-03	[38,35]	833868,63	822072.83	41.95	47	86.93	62.08	26.97	70,27	23,32	14,41	167.47	116.65	19.23
TA-04	[38,35]	833854.78	822084_34	29.35	34.4	88.85	62.48	27.16	72.02	23.74	14.65	185,70	125.05	22.04
TA-04	[38,35]	833854,78 833854,78	822084,34 822084,34	32.5 35.65	37.55 40.7	88,83 86,95	62.46	27.15	72,00	23,73	14,64	185,43	124,11	21.71
TA-04 TA-04	[38,35]	833854.78	822084.34 822084.34	35.65	43.85	86.95 86.94	62.09	26.99	70.30 70.28	23,33	14.41	169.20	117.66	19.75
TA-04	[38,35]	833854,78	822084.34	41.95	47	86.93	62.08	26.98	70,27	23.32	14,41	167,70	116.65	19.27
TA-05	[38,35]	833840,93	822095.85	29.35	34.4	88.85	62.49	27.17	72.02	23,75	14.65	185.54	125,30	22.12
TA-05 TA-05	[38,35]	833840,93 833840,93	822095.85 822095.85	32.5 35.65	37.55 40.7	88,82 86,95	62.46	27,15	72.00 70,29	23.74	14.64	185.33	124.79	21,77
TA-05	[38,35]	833840,93	822095.85	38.8	43.85	86.94	62.10	26.99	70.28	23,32	14.42	168.14	117.68	19.54
TA-05	[38,35]	833840.93	822095.85	41.95	47	86.93	62.09	26.98	70.27	23,32	14.41	167.59	117.53	19.32
TA-06 TA-06	[38,35]	833891,00 833891,00	822105.75 822105.75	29.35 32.5	34.4 37.55	88.84 88.82	62.49 62.46	27.16	72,02	23,73	14.65	185,48	126.64	22,01
TA-06	[38,35]	833891.00	N22105.75	35.66	40,7	86.95	62.11	26.99	70.29	23.32	14.42	168.28	119.05	19.70
TA-06	[38,35]	833891.00	822105.75	38.8	43.85	86.94	62.10	26.98	70.28	23.32	14.41	167.61	117.55	19.45

Assessment Point	PATH Grid	Easting (m)	Northine (m)	Level (mAG)	Level (mPD)	Daily 1st	Daily 10th	Annual	Daily 1st	Daily 36th	Annual	Hourty 1st	Hourly 19th	Annual
			, and find	(4213)	(34,0)	Maximum RSP	RSP	RSP	Maximom FSP	Maximum FSP	FSP	Maximom NO2	Maximum NO2	NO2
	Crite	ria (AQO)					100	50		50	35		200	40
TA-06 TA-07	[38,35]	833891,00 833873,54	822105.75 822084.74	41.95 29.35	47 34,4	86.93 88.84	62.09 62.48	26.97	70,27	23,31	14,41	167.14 185.62	116.64	19.23 21.98
TA-07	[38,35]	833873.54	822084.74	32.5	37.55	88.82	62.46	27.15	72.00	23,73	14,63	185,35	124.22	21.65
TA-07	[38,35]	833873,54	822084.74	35.65	40.7	86.95	62.11	26.99	70.29	23,32	14,42	168,74	117.93	19,70
TA-07 TA-07	[38,35]	833873,54 833873,54	N22084.74 N22084.74	38.8 41.95	43.85	86.94	62.09 62.08	26.98	70.28	23.32	14.41	167.96	117.53	19.45
TA-08	[38,35]	833848,83	822105.35	29,35	34.4	88.84	62.49	27.17	72.02	25,74	14,65	185,48	125,29	22,12
TA-08	[38,35]	833848.83 833848.83	822105.35 822105.35	32.5 35.65	37.55 40.7	88.82 86.95	62.47	27.15	72.00	23,73	14.64	185.27	124.78	21.77
TA-08	[38,35]	833848.83	822105.35	38.8	43.85	86.94	62.10	26.99	70.28	23,32	14,42	167.93	117.59	19.54
TA-08	[38,35]	833848,83 833857,20	N22105.35 822115.02	41.95 29.35	47 34,4	86.93 88.84	62.09	26.98	70.27	23,32	14.41	167.43 185.28	117.48	19.31
TA-09 TA-09	[38,35]	833837,20	822115.02	32.5	37.55	88.82	62.47	27.17	72,00	23,74	14.64	185.12	126,20 124,82	22.19
TA-09	[38,35]	833837.20	822115.02	35.65	40.7	86.95	62.12	27.00	70.29	23,33	14.43	167.92	117.68	19.85
TA-09 TA-09	[38,35]	833837.20 833837.20	822115.02 822115.02	38.8 41.95	43.85	86.94 86.93	62.10	26.99	70.28	23,32	14,42	167.43	117.55	19.58
TA-10	[38,35]	833825.54	N22124.64	29,35	34,4	88.84	62,51	27,17	72.02	23.75	14.65	185.13	126.88	22.27
TA-10 TA-10	[38,35]	833825.54 833825.54	822124.64 822124.64	32.5	37.55 40.7	88.82 86.95	62.48	27.16	72.00	23.74	14,64	184.70	125.08	21,89
TA-10	[38,35]	833825.54	N22124.64	38.8	43.85	86.94	62.11	26.99	70.28	23.32	14.42	167.05	117.53	19.62
TA-10	[38,35]	833825.54	822124.64	41.95	47	86.93	62.09	26.98	70.27	23,32	14,41	166.79	117.32	19.38
TA-11 TA-11	(38,35)	833837.29 833837.29	822138.78 822138.7#	29,35 32,5	34,4 37,55	88.85	62.51 62.48	27.17	72.02 72.01	23,74	14,66	184,97	126,64	22.28
TA-11	[38,35]	833837.29	822138.78	35.65	40.7	86.96	62.13	27.00	70,30	23.33	14.43	167.17	117.61	19.90
TA-II	[38,35]	833837.29 833837.29	822138,78 822138,78	38.8	43,85	86.94 86.93	62.11	26,99	70,28	23,32	14.42	166.86	117.50	19.52
TA-11 TA-12	[38,35]	833847.69	822151.30	41,95 29.35	47 34.4	88.85	62.09	26.98	70.27	23.74	14.41	166.65 184.67	117,42	22.32
TA-12	[38,35]	833847.69	822151.30	32.5	37.55	88.83	62.48	27.16	72.01	23,73	14.64	184.16	127,07	21.91
TA-12 TA-12	[38,35]	833847.69 833847.69	822151.30 822151.30	35.65 38.8	40.7	86.95	62.13	27.00	70.30	23.33	14.43	166.98	119.05	19.91
TA-12	[38,35]	833847.69	822151.30	41.95	47	86.93	62.10	26.98	70,28	23,32	14,41	166.55	117.40	19.38
TA-13	[38,35]	833866.19	N22135.93 822135.93	29,35 32,5	34.4 37.55	88.83	62.50	27.17	72.02	23.74	14.65	185.20	126,48	22.19
TA-13 TA-13	[38,35]	833866.19 833866.19	822135.93	35.65	40.7	86.96	62.48	27.16	72.01	23.73	14.64	167.60	125.32	21.81
TA-13	[38,35]	833866.19	822135.93	38.8	43.85	X6.94	62.11	26.99	70.29	23,32	14.42	167.17	117.50	19.55
TA-13 TB-01	[38,35]	833866.19 833861.54	822135.93 822130.31	41.95 29.35	47 34.4	86.93 88.85	62.09	26.98	70.27	23,31	14,41	166.86 185.24	117.42 126.06	19.32
TB-01	[38,35]	833861.54	N22130.31	32.5	37.55	88.83	62.47	27.15	72.00	23,73	14.64	185.08	125,44	21.80
TB-01	[38,35]	833861,54	822130.31	35.65	40,7	86.96	62.12	27.00	70,30	23,32	14.42	167.74	119.05	19,82
TB-01 TB-01	[38,35]	833861.54 833861.54	822130.31 822130.31	38.8 41.95	43.85	86.94 86.93	62.11	26.99	70.28	23.32	14.42	167.28	117.51	19.32
TB-02	[38,35]	833876.25	822118.01	29.35	34,4	88.84	62.49	27.16	72.02	23.73	14,65	185,47	126.46	22,09
TB-02	[38,35]	833876,25	822118.01	32.5	37.55	88.83	62.47	27.15	72,00	23,73	14.64	185.25	125.08	21.73
TB-02 TB-02	[38,35]	833876.25 833876.25	822118:01 822118:01	35.65	40,7	86.96 86.94	62.12	26.99	70,30	23.32	14.42	168.44	119.39	19.76
TB-02	[38,35]	833876.25	822118.01	41.95	47	86.93	62.00	26.98	70.27	23,31	14.41	167.26	116.74	19.27
TB-03 TB-03	[38,35]	833618.53 833618.53	822095.91 822095.91	29,35 32,5	34.4 37.55	88.86	62.59	27.21	72.03 72.01	23.82	14.69	185.79 185.46	128.80	23,40
TB-03	[38,35]	833618.53	822095.91	35.65	40.7	86.96	62.20	27.03	70.30	23.38	14.45	169.13	120.92	20.69
TB-03	[38,35]	833618.53	N22095.91	38.8	43.85	86.95	62.17	27.01	70.29	23,37	14.44	168.36	119.50	20.27
TB-03 TB-04	[38,35]	833618.53 833624.49	822095.91 822078.96	41.95 29.35	47 34.4	86.93 88.86	62.15	27.00	70,27	23,36	14,43	167.81	118,26	19.92
TB-04	[38,35]	833624,49	¥22078.96	32.5	37.55	88.83	62.56	27.19	72.01	23.79	14.67	185.62	127.17	22,77
TB-04 TB-04	[38,35]	833624,49	822078.96 822078.96	35.65	43.85	86.96 86.94	62.20	27.02	70,30	23,38	14.45	169.76 168.82	119.14	20.63
TB-04	[38,35]	833624,49	822078.96	41.95	47	86.93	62.15	27.00	70.27	23,35	14.43	168.14	115.05	19.87
TB-05	[38,35]	833630,77	822060.43	29.35	34,4	88.86	62.59	27.20	72,03	23.81	14,68	186,27	127,69	23.23
TB-05 TB-05	[38,35]	833630.77 833630.77	822060.43 822060.43	32.5 35.66	37.55 40.7	88.83	62.56	27.19	72.01	23,79	14.67	185,87	125.87	22,70
TB-05	[38,35]	833630,77	822060.43	38.8	43,85	86.94	62.17	27.01	70,28	23.36	14,44	169,68	117.99	20.17
TB-05 TB-06	[38,35]	833630.77 833638.16	822060.43 822039,43	41.95 29.35	47 34.4	86.93 88.86	62.15	27.00	70.27	23.35	14.42	168.78	117.61	19.82
TB-06	[38,35]	833638.16	822039.43	32.5	37.55	88.84	62.56	27.18	72.01	23.78	14.67	186.20	125,80	22,63
TB-06	[38,35]	833638.16	822039.43	35.65	40.7	86.96	62.19	27.02	70,30	23,37	14,45	172.31	119,13	20.51
TB-06 TB-06	[38,35]	833638.16 833638.16	822039,43 822039,43	38.8 41.95	43.85	86.94 86.93	62.17 62.15	27.01	70.29	23.36	14.43	170.60 169.62	119.07	20.12 19.78
TB-07	[38,35]	833619.68	822033.12	29.35	34.4	88.86	62.59	27.20	72.04	23,80	14.68	186.70	128.55	23.16
TB-07 TB-07	[38,35]	833619.68 833619.68	822033.12 822033.12	32.5 35.65	37.55 40.7	88.84	62.56	27.18	72.01	23,78	14.67	186.25 172.50	125.94	22.65
TB-07	[38,35]	833619.68	822033.12 822033.12	38.8	43,85	86.94	62.17	27.01	70,28	23,36	14,43	172.00	119,15	20.53
TB-07	[38,35]	833619.68	W22033.12	41,95	47	86.93	62.15	26.99	70.27	23.35	14.42	169.81	117.47	19.79
TB-08 TB-08	[38,35]	833602,12 833602,12	822026.90 822026.90	29.35 32.5	34,4 37.55	88.86 88.83	62.59 62.56	27.20	72.03	23,80 23,78	14.68	186,72 186,28	128,10 126,06	23.17
TB-08	[38,35]	833602.12	\$22026.90	35,65	40.7	86.96	62.20	27.02	70.30	23,37	14.45	172.60	119.68	20.54
TB-08	[38,35]	833602.12 833602.12	822026.90	38.8 41.95	43,85	86.94 86.92	62.17 62.15	27.01	70.28	23.36	14.43	171.12	118.63	20.14
TB-08 TB-09	[38,35]	833594.66	822026.90 822048.19	29,35	34,4	88.86	62.15	26.99	70.27	23.35	14.42	186.41	128.74	23.25
TB-09	[38,35]	833594,66	822048.19	32.5	37.55	88.83	62.56	27.19	72,01	23,79	14.67	186.00	127.43	22,73
TB-09 TB-09	[38,35]	833594.66 833594.66	822048.19 822048.19	35.65	43.85	86.96 86.94	62.20	27.02	70.30	23,57	14.45	171.21	119.18	20.60
TB-09	[38,35]	833594,66	822048.19	41.95	47	86.92	62.15	27.00	70.27	23.35	14.42	169.00	116.80	19.85
TB-10	[38,35]	833587,75	822068.18	29.35	34.4	88.85	62.59	27.21	72.03	23.81	14.69	186.32	128.17	23.34
TB-10 TB-10	[38,35]	833587.75 833587.75	822068.18 822068.18	32.5 35.65	37.55 40.7	88.83 86.96	62.56 62.20	27.19	70.30	23.79	14.67	185.88	127.27	22.80
TB-10	[38,35]	833587.75	822068.18	38.8	43.85	86.94	62.17	27.01	70,28	23,37	14,44	169,34	118.46	20.26
TB-10 TB-11	[38,35]	833587.75 833582.49	822068.18 822083.39	41.95 29.35	47 34,4	86,93 88,85	62.15	27.20	70.27 72.03	23.36	14.43	168.49	117,42 127,98	19.90
TB-11	[38,35]	833582,49	822083.39 822083.39	32.5	37.55	88.83	62.56	27.19	72.01	23.82	14.69	185.83	127.98	22.87
TB-11	[38,35]	833582.49	822083.39	35.65	40.7	86.96	62.20	27.03	70.30	23.38	14.45	170.22	120.61	20.73
TB-11 TB-11	[38,35]	833582.49 833582.49	822083.39 822083.39	38.8	43,85	86.94 86.93	62.18	27.01	70,28	23.37	14,44	169.09	119.16	19.95
TB-12	[38,35]	833600.51	N22089.65	29,35	34.4	88,85	62.60	27,21	72.03	23.82	14.69	186.02	128.85	23,42
TB-12	[38,35]	833600,51	822089.65	32.5	37,55	88.83	62.56	27.19	72.01	23,80	14,67	185,62	127.04	22.86
TB-12 TB-12	[38,35]	833600.51 833600.51	822089.65 822089.65	35.65	40.7	86.96 86.94	62.20	27.03	70.30	23,38	14.45	169,58 168,66	120.34	20.71
TB-12	[38,35]	833600,51	822089.65	41.95	47	86.93	62.16	27.00	70,27	23,36	14,43	168,00	117.97	19.93
BC-01	[38,35]	833618,53	822095.91 822095.91	1.5	6.55	92.04	63.65	27.76	74,94	24,79	15.35	197.77	154.67	34,70
BC-01 BC-01	[38,35]	833618.53 833618.53	822095.91 822095.91	11.6	13.05 16.65	91.86	63.48	27.69	74.77	24.71	15.28	196.03	150.17	31.55
BC-01	[38,35]	833618.53	822095.91	15.2	20.25	91.64	63.27	27.59	74.57	24.58	15.19	192.90	145.82	30.26

Assessment Point	PATH Grid	Easting (m)	Northing (m)	Level (mAG)	Level (mPD)	Daily 1st Maximum RSP	Daily 10th Maximum RSP	Annual RSP	Daily 1st Maximum FSP	Daily 36th Maximum FSP	Annual FSP	Hourty 1st Maximum NO2	Hourly 19th Maximum NO2	Annual NO2
	Crite	ria (AQO)					100	50		50	35		200	40
BC-01	[38,35]	833618.53	822095,91	18.8	23.85	88,98	62.76	27.30	72.14	23.92	14.77	188,16	134,71	25,97
BC-01	[38,35]	83361N.53	822095.91	22.4	27.45	88.92	62.69	27.26	72.09	23.88	14.74	187.07	132.21	24.96
BC-01	[38,35]	833618.53	822095.91	26	31,05	88.88	62.64	27.23	72,06	23.84	14,71	186.29	130,20	24,09
BC-01 BC-01	[38,35]	833618,53 833618,53	822095.91 822095.91	30.5 35	35.55 40.05	88.85 88.82	62.58	27.20	72.02	23.81	14,68	185.66 185.28	128,38	23,19
BC-02	[38,35]	833624.49	R22078.96	1.5	6.55	91.91	63.51	27.70	74.82	24.73	15.29	195.67	152.00	33.13
BC-02	[38,35]	833624,49	822078.96	-8	13.05	91.81	63.42	27.66	74.73	24,67	15,25	194.61	149.90	32,00
BC-02 BC-02	[38,35]	833624,49 833624,49	822078.96 822078.96	15.2	16.65 20.25	91.72	63.34	27.62	74.65	24.62	15.22	193.61	148,44	30.99
BC-02	[38,35]	833624,49	822078.96	18.8	23.85	88.98	62.74	27.29	72.15	23.91	14,77	188.73	134,44	25.75
BC-02	[38,35]	833624.49	M22078.96	22,4	27.45	88.93	62.68	27,26	72.10	23.87	14.74	187.22	132.66	24.81
BC-02 BC-02	[38,35]	833624,49 833624,49	822078.96 822078.96	30.5	31,05	88.89 88.85	62.63	27.23	72.06	23.84	14.71	186,50 185,84	130,97	23.98
BC-02	[38,35]	833624,49	\$22078.96	35	40.05	88.82	62.54	27.17	72.00	23,78	14.66	185.41	126.30	22.39
BC-03	[38,35]	833630.77	822060.43	1.5	6.55	91.83	63.43	27.66	74.75	24.68	15.26	195.00	150.40	32.17
BC-03	(38,35)	833630,77 833630,77	822060,43 822060,43	8	13.05 16.65	91.76	63.37	27.63	74.68	24.64	15.23 15.20	194,21	149,10 146,51	31.33
BC-03 BC-03	[38,35]	833630,77	822060.43	15.2	20.25	91.63	63.26	27.57	74.57	24.55	15.17	192.57	144.03	29.60
BC-03	[38,35]	833630,77	822060,43	18.8	23,85	88.98	62.74	27.28	72.15	23,90	14.76	188.33	133,40	- 25.53
BC-03	[38,35]	833630.77	N22060.43	22.4	27,45	88.93	62.68	27.25	72.10	23.86	14.73	187,51	131.62	24.66
BC-03 BC-03	[38,35]	833630,77 833630,77	822060,43 822060,43	26 30.5	31,05 35,55	88.89 88.85	62.63 62.58	27.23	72.06	23.83	14,71	186.81	130.08 126.52	23.88
BC-03	[38,35]	833630.77	822060.43	35	40.05	88.82	62.53	27.17	72.00	23.78	14.66	185.62	125.42	22.33
BC-04	[38,35]	833638.16	822039.43	13	6.55	91.78	63.38	27.64	74,70	24.65	15.23	195,38	148.29	31.51
BC-04 BC-04	[38,35]	833638.16 833638.16	822039.43 822039.43	8	13.05 16.65	91.73	63.34	27.61	74.65	24.61	15.21	194,66	147.75	30.81
BC-04	[38,35]	833638.16	822039.43	15.2	20.25	91.62	63.25	27.56	74.56	24.53	15.16	193,11	142.31	29.31
BC-04	[38,35]	833638.16	822039.43	18.8	23.85	88.98	62.72	27,28	72.15	23,88	14,75	188.88	132.13	25.33
BC-04 BC-04	[38,35]	833638.16 833638.16	822039,43 822039,43	22.4	27:45 31.05	88.93	62.67	27.25	72.10	23.85	14.73	188.03 187.27	130.67	24.52
BC-04	[38,35]	833638.16	822039.43	30.5	35.55	88.85	62.58	27.19	72.03	23,79	14.68	186.49	126.26	22.95
BC-04	[38,35]	833638.16	822039,43	35	40.05	88.82	62.53	27.17	72.00	23.77	14.65	185.90	124.41	22.27
BC-05	[38,35]	833619.68	822033.12	1.5	6.55	91.78	63.37	27.63	74.70	24.63	15.23	194,85	149.83	31.43
BC-05 BC-05	[38,35]	833619.68 833619.68	822033.12 822033.12	8	13.05 16.65	91.73 91.68	63.33	27.61 27.58	74.65	24.60	15.21	194.23 193.61	148.72	30.74
BC-05	[38,35]	833619.68	822033.12	15.2	20.25	91.63	63.25	27,56	74.56	24.53	15.16	192.88	143.01	29.27
BC-05	[38,35]	833619.68	822033.12	18.8	23,85	88.98	62.72	27.28	72.15	23,88	14.75	188.74	132.39	25,30
BC-05 BC-05	[38,35]	833619.68 833619.68	822033.12 822033.12	22.4 26	27.45 31.05	88.94 88.89	62.67	27,25	72.10	23.85	14.72	187.98	130.57	24.51
BC-05	[38,35]	833619.68	822033.12	30.5	35.55	88.85	62.58	27.19	72.03	23,79	14.68	186.53	127.23	22.97
BC-05	[38,35]	833619.68	822033.12	35	40.05	88.82	62.53	27.17	72.00	23.77	14.65	185,95	124.09	22.29
BC-06 BC-06	[38,35]	833602,12 833602,12	822026.90 822026.90	1.5	6.55	91.78	63.36	27.63	74.70	24.62 24.59	15.23	194,47	149.28	31.45
BC-06	[38,35]	833602.12	N22026.90	11.6	16.65	91.68	63.30	27.58	74.61	24.56	15.18	193.36	145.90	30.04
BC-06	[38,35]	833602.12	822026,90	15.2	20.25	91.63	63.26	27,55	74.56	24.52	15.16	192.70	141,97	29.25
BC-06 BC-06	[38,35]	833602.12 833602.12	822026.90 822026.90	18.8	23.85	88.98 88.94	62.72	27.27	72.15	23.88	14.75	188.64	132.56	25.29
BC-06	[38,35]	833602.12	822026.90	26	31,05	88.89	62.63	27,22	72.06	23.82	14.70	187.27	129,97	23.78
BC-06	[38,35]	833602.12	822026.90	30.5	35.55	88.85	62.58	27.19	72.03	23,79	14.68	186.55	127.14	22.97
BC-06	[38,35]	833602.12 833594.66	¥22026.90	35 13	40.05 6.55	88.82 91.83	62.54	27.17	71.99	23.77	15.25	185.99 194.56	124.33	22.29
BC-07 BC-07	[38,35]	833594.66	822048.19 822048.19	8	13.05	91.83	63,37	27.62	74.69	24,63	15.23	193,90	149,61	31.20
BC-07	[38,35]	833594.66	822048.19	11.6	16.65	91.70	63.33	27.60	74.63	24.58	15.20	193.26	147.79	30.40
BC-07	[38,35]	833594.66	822048.19	15.2	20.25	91.64	63.27	27.56	74.57	24,54	15.17	192.51	144,32	29.51
BC-07 BC-07	[38,35]	833594.66	822048.19 822048.19	22.4	23.85	88.99 88.93	62.73 62.68	27.28	72.15	23,89	14.76	188.38	133.75	25.48
BC-07	[38,35]	833594.66	822048.19	26	31,05	88.39	62.63	27,23	72.06	23.83	14.70	186.95	130,33	23,88
BC-07	[38,35]	833594.66	822048.19	30.5	35.55	88,85	62.58	27.20	72.02	23,80	14.68	186.25	128.30	23.05
BC-07 BC-08	[38,35]	833594.66 833587.75	822048.19 822068.18	35 1.5	6.55	88.81 91.92	62,54 63,53	27.17	71.99	23.78	14.66	185.73	152.56	22.36
BC-08	[38,35]	833587.75	822068.18	- 8	13.05	91.92	63.44	27.65	74.73	24.64	15.25	195.07	150.27	31.88
BC-08	[38,35]	833587.75	822068.18	11.6	16.65	91.73	63.36	27,61	74.65	24.60	15.21	194.14	147.97	30.88
BC-08 BC-08	[38,35]	833587.75 833587.75	822068.18 822068.18	15.2	20.25	91.65 88.98	63.28	27.58	74.58 72.15	24,56 23,90	15.18	193.09	146.04	29.83
BC-08	[38,35]	833587.75	822068.18 822068.18	22.4	27:45	88.93	62.69	27.26	72.10	23,87	14.73	187.73	132.50	24.79
BC-08	[38,35]	833587.75	822068.18	26	31.05	88.89	62.63	27,23	72.06	23.84	14,71	186,92	130.75	23.99
BC-08	[38,35]	833587.75 833587.75	822068.18	30.5	35.55	88.84	62.58	27.20	72.02	23,80	14.68	186.14	127.81	23.14
BC-08 BC-09	[38,35]	833587.75	822068.18 822083.39	35 13	40.05 6.55	92.05	63.67	27,18	71.99	23.78	14.66	185.61	125.78	22.42 34.39
BC-09	[38,35]	833582.49	822083,39	. 8	13.05	91.87	63,49	27.68	74.78	24.67	15.27	197.43	150.43	32.65
BC-09	[38,35]	833582.49	#22083.39 #22002.20	11.6	16,65	91.74	63,38	27.63	74.67	24.62	15.23	195.88	147.86	31.35
BC-09 BC-09	[38,35]	833582.49 833582.49	822083.39 822083.39	15.2	20.25	91.64 88,98	63.28	27,59	74.57	24,57	15.19	194,22 189,32	145.91 134.69	30.12 25.89
BC-09	[38,35]	833582.49	822083.39 822083.39	22.4	27.45	88.92	62.70	27.26	72.09	23.67	14.74	188.02	132.23	24.93
BC-09	[38,35]	833582.49	822083.39	26	31.05	88.88	62.64	27.23	72,06	23.84	14.71	187,00	130.26	24,10
BC-09 BC-09	[38,35]	833582.49 833582.49	822083.39 822083.39	30.5 35	35.55 40.05	88.84 88.81	62.59	27.20	72.02	23.81	14.68	186.11 185.55	127.58 125.81	23.22
BC-10	[38,35]	833582.49	822089,65	1.5	6.55	92.04	63.66	27.75	74.94	24.76	15.34	198.27	154.85	34.48
BC-10	[38,35]	-833600.51	822089.65	- 8	13.05	91.87	63.49	27.69	74,78	24.69	15.28	196.62	150.52	32.74
BC-10	[38,35]	833600.51	822089.65 922090.65	11.6	16.65	91.74	63.37	27.64	74.66	24.63	15.23	195.10	148,14	31.43
BC-10 BC-10	[38,35]	833600,51 833600,51	822089.65 822089.65	15.2	20.25	91.64 88.98	63.28	27.59	74.57	24,58	15,19	193.51	145.87	30.18
BC-10	[38,35]	833600.51	N22089.65	22,4	27.45	88.92	62.69	27.26	72.09	23.87	14.74	187.51	132.20	24.95
BC-10	[38,35]	833600,51	822089,65	26	31.05	88.88	62.64	27.23	72,06	23.84	14.71	186,62	130.24	24,10
BC-10 BC-10	[38,35]	833600.51 833600.51	822089.65 822089.65	30.5	35.55 40.05	88.85 88.82	62.58	27.20	72.02	23.78	14.68	185.86	128.44	23.21

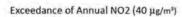
APPENDIX 4-6

Summary of Annual Averaged NO₂ Concentration (Air Quality)

				Ann	ual Average	ed NO ₂ Con	centration	(μg/m³) at d	ifferent Height	37
	Assessment Point	mAG	1.5	6.35	10.85	14.5	18	21.5		
		mPD	6.55	11.4	15.9	19.55	23.05	26.55		
	AP-01		37,95	33.15						
	AP-02		39.33	33.57						
	AP-03		43,92	33.31						
	AP-04		41.98	33.37						
=	AP-05		41.34	33.27						
Podium	AP-06		37.13	33.21	30.11	28.41	24.10	23.25		0
po	AP-07		39.63	33.75	29.69	27.97	23.80	23.08		
4	AP-08		37.44	33.63	30.19	28.44	24.15	23.33		
V	AP-09		37.38	33.66	30.33	28.60	24.30	23.46		
Site	AP-10		37.87	33.92	30.49	28.75	24.45	23.59		
S	AP-11		35.83	33.62	30.93	29.12	24.67	23.70		
	AP-12		35.05	33.29	31.01	29.32	24.86	23.84		170
	AP-13		34.40	32.91	30.73	29.06	24.62	23.63		
	AP-14		34.70	33.05	30.72	28.99	24.54	23.57		
	AP-15		35.21	33.13	30,50	28.73	24.32	23.40		

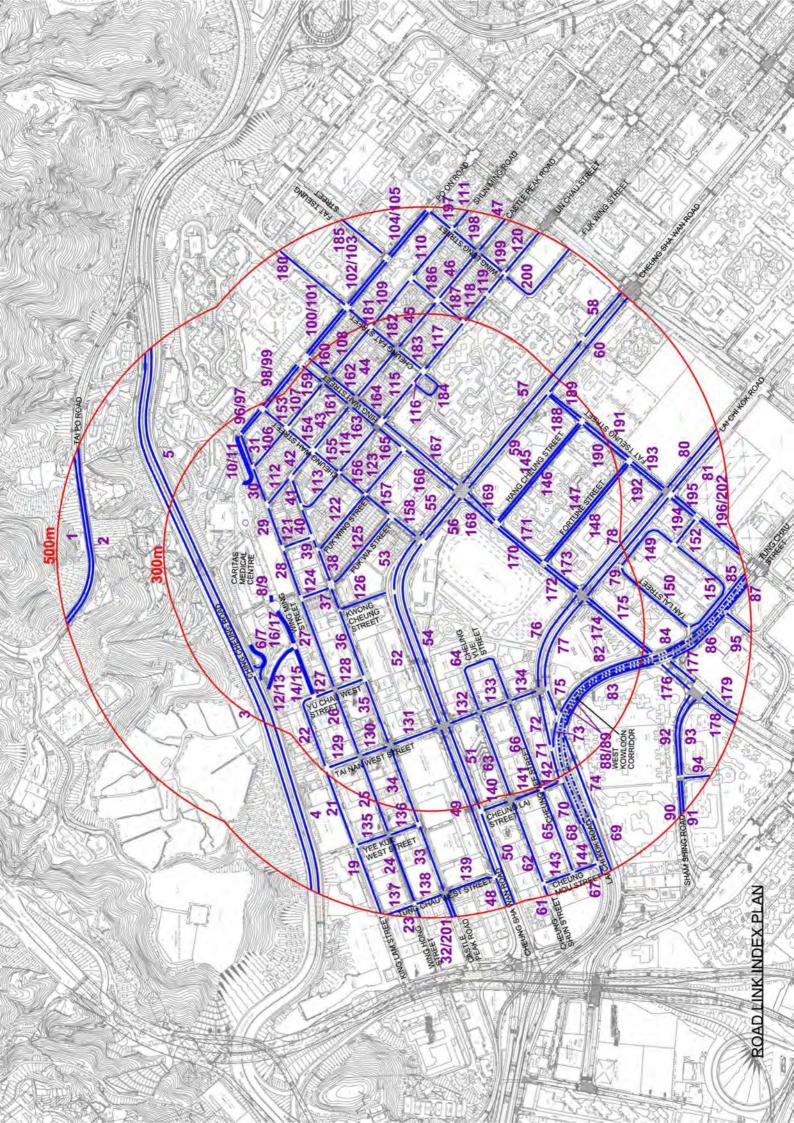
				Ann	ual Average	d NO ₂ Con	centration (µg/i	n³) at different	t Height	
	Assessment Point	mAG	29.35	32.5	35.65	38.8	41.95			
		mPD	34.4	37.55	40.7	43.85	47			
	TA-01		22.00	21.65	19.69	19.43	19.22			
	TA-02		21.97	21.64	19.69	19.44	19.22			
	TA-03		21.97	21.65	19.69	19.44	19.23			
V	TA-04		22.04	21.71	19.75	19.49	19.27			
Tower	TA-05		22.12	21.77	19.80	19.54	19.32			
3	TA-06		22.01	21.66	19.70	19.45	19.23			
ř	TA-07		21.98	21.65	19.70	19.45	19.23	- 11		
A	TA-08		22.12	21.77	19.80	19.54	19.31			
Site	TA-09		22.19	21.82	19.85	19.58	19.35			
Si	TA-10		22.27	21.89	19.90	19.62	19.38		- 1	
	TA-11		22.28	21.89	19.90	19.62	19.38		-1	
	TA-12		22.32	21.91	19.91	19.62	19.38			
	TA-13		22.19	21.81	19.82	19.55	19.32			
	TB-01		22.17	21.80	19.82	19.55	19.32			
	TB-02		22.09	21.73	19.76	19.50	19.27			
	TB-03		23.40	22.84	20.69	20.27	19.92			
8	TB-04		23.31	22.77	20.63	20.22	19.87	- 11		
Tower	TB-05		23.23	22.70	20.57	20.17	19.82			
ō	TB-06		23.15	22.63	20.51	20.12	19.78	14		
	TB-07		23.16	22.65	20.53	20.14	19.79			
A	TB-08		23.17	22.66	20.54	20.14	19.80			
Site	TB-09		23.25	22.73	20.60	20.20	19.85			
٠,	TB-10		23.34	22.80	20.67	20,26	19.90			
	TB-11		23.43	22.87	20.73	20.31	19.95			
	TB-12		23.42	22.86	20.71	20.30	19.93			

				Ann	ual Average	d NO ₂ Con	centration	$(\mu g/m^3)$ at	different H	eight	
	Assessment Point	mAG	1.5	8	11.6	15.2	18.8	22.4	26	30.5	35
		mPD	6.55	13.05	16.65	20.25	23.85	27.45	31.05	35.55	40.05
-	BC-01		34.70	32.91	31.55	30.26	25.97	24.96	24.09	23.19	22.45
Complex	BC-02		33.13	32.00	30.99	29.92	25.75	24.81	23.98	23.10	22.39
ď	BC-03		32.17	31.33	30.52	29.60	25.53	24.66	23.88	23.03	22.33
ō	BC-04		31.51	30.81	30.11	29.31	25.33	24.52	23.77	22.95	22.27
	BC-05		31.43	30.74	30.06	29.27	25.30	24.51	23.78	22.97	22.29
9/10	BC-06		31.45	30.73	30.04	29.25	25.29	24.50	23.78	22.97	22.29
	BC-07		32.05	31.20	30.40	29.51	25.48	24.64	23.88	23.05	22.36
8	BC-08		33.02	31.88	30.88	29.83	25.70	24.79	23.99	23.14	22.42
Site	BC-09		34,39	32,65	31.35	30,12	25,89	24.93	24,10	23.22	22.49
01	BC-10		34.48	32.74	31.43	30.18	25.93	24.95	24.10	23.21	22.48



APPENDIX 5-1

Predicted Traffic Flow at Peak Hour in Year 2049



Predicted Traffic Flow at Peak Hours of Year 2049

Road ID	Road	Direction	At grade	Speed Limit	AM	Peak	PM	Peak	Within 300i
20.2	77.00	Santan	/ Flyover	(km/hr)	Traffic	% Heavy	Traffic	% Heavy	Boundary
3	Ching Cheung Road	EB	At grade	70	5400	32	4550	35	N
4	Ching Cheung Road	WB	At grade	70	4800	31	5200	29	N
6	Ching Cheung Road	WB EB	At grade	70 50	4750 50	31	5200	29	N Y
7	Access Road of Caritas Medical Centre Access Road of Caritas Medical Centre	WB	At grade At grade	50	18	40	50	4	Y
8	Access Road of Caritas Medical Centre Access Road of Caritas Medical Centre	EB	At grade	20	100	6	50	5	Y
9	Access Road of Caritas Medical Centre Access Road of Caritas Medical Centre	WB	At grade	20	50	16	50	0	Y
10	Access Road of Caritas Medical Centre	EB	At grade	50	200	12	200	12	Y
11	Access Road of Caritas Medical Centre	WB	At grade	50	150	17	100	17	Y
12	Access Road to St. Raphael's Catholic Cemetery	NB	At grade	50	13	25	11	27	Y
13	Access Road to St. Raphael's Catholic Cemetery	SB	At grade	50	10	41	21	43	Y
14	Wing Ming Street	EB	At grade	50	100	9	50	19	Y
15	Wing Ming Street	WB	At grade	:50	50	28	50	13	Y
16	Wing Ming Street	EB	At grade	50	100	- 8	50	15	Y
17	Wing Ming Street	WB	At grade	50	50	26	50	6	Y
21	King Lam Street	WB	At grade	.50	250	28	150	27	Y
22	King Lam Street	EB	At grade	- 50	200	30	250	28	Y
25	Wing Hong Street	WB	At grade	50	200	29	500	27	Y
26	Wing Hong Street	WB	At grade	50	200	37	350	29	Y
27	Wing Hong Street	WB	At grade	50	350	30	450	28	Y
28	Wing Hong Street	WB	At grade	50	150	28	300	27	Y
29	Wing Hong Street	WB	At grade	50	150	37	100	34	Y
30	Wing Hong Street	WB	At grade	50	300	30	450	27	Y
31	Wing Hong Street	WB	At grade	50	100	40	150	32	Y
34	Castle Peak Road	EB	At grade	50	800	29	1150	27	Y
35	Castle Peak Road	EB	At grade	50	1350	30	1200	27	Y
36	Castle Peak Road	EB	At grade	50	1550	29	1600	27	Y
37	Castle Peak Road	EB	At grade	50	1250	38	1150	30	Y
38	Castle Peak Road	EB	At grade	50	1250	40	1200	26	Y
39	Castle Peak Road	EB	At grade	50	950	42	850	29	Y
40	Castle Peak Road	EB	At grade	50	850	42	700	28	Y
41	Castle Peak Road	EB	At grade	50	1000	42	800	29	Y
42	Castle Peak Road	EB	At grade	50	1150	42	1250	29	Y
43	Castle Peak Road	EB EB	At grade	50	700 850	47	900	34 28	Y
44	Castle Peak Road Castle Peak Road	EB	At grade	50	600	42	700	29	Y
49	Cheung Sha Wan Road	EB	At grade At grade	50	2500	38	1650	35	Y
51	Cheung Sha Wan Road	WB	At grade	50	2350	43	2250	35	Y
52	Cheung Sha Wan Road	EB	At grade	50	1600	42	1600	35	Y
53	Cheung Sha Wan Road	EB	At grade	50	1850	44	2000	38	Y
54	Cheung Sha Wan Road	WB	At grade	50	1950	- 46	2050	43	Y
55	Cheung Sha Wan Road	EB	At grade	50	2200	43	2050	35	Y
56	Cheung Sha Wan Road	WB	At grade	50	1150	49	1200	44	Ŷ
57	Cheung Sha Wan Road	EB	At grade	50	1550	29	1250	23	Y
59	Cheung Sha Wan Road	WB	At grade	50	900	32	1150	27	Y
60	Cheung Sha Wan Road	WB	At grade	50	850	47	1050	44	Y
63	Cheung Shun Street	EB	At grade	50	150	28	250	27	Y
64	Cheung Yue Street	EB	At grade	50	150	28	150	27	Y
66	Cheung Yee Street	WB	At grade	50	250	28	350	26	Y
71	Lai Chi Kok Rond	EB	At grade	50	1900	36	1800	32	Y
72	Lai Chi Kok Road	EB	At grade	50	850	29	950	25	Y
73	Lai Chi Kok Road	EB	At grade	50	1050	31	850	28	Y
74	Lai Chi Kok Road	WB	At grade	50	1000	31	1000	29	Y
75	Lai Chi Kok Road	WB	At grade	.50	700	28	600	26	Y
76	Lai Chi Kok Road	EB	At grade	-50	650	31	600	31	Y
77	Lai Chi Kok Road	WB	At grade	-50	1350	29	1300	30	Y
78	Lai Chi Kok Road	EB	At grade	:50	700	34	550	32	Y
79	Lai Chi Kok Road	WB	At grade	50	1100	28	950	30	Y
82	Tung Chau Street	EB	At grade	50	950	37	900	33	Y
83	Tung Chau Street	WB	At grade	50	400	30	300	30	Y
88	West Kowloon Corridor	EB	Flyover	70	3600	26	3600	12	Y
89	West Kowloon Corridor	WB	Flyover	70	2650	25	3450	12	Y
96	Po On Road	NB	At grade	50	100	24	100	25	N.
97	Po On Road	SB	At grade	50	50	42	50	31	N
98	Po On Road	NB	At grade	50	50	25	50	25	N
99	Po On Road	SB	At grade	50	250	42	200	28	N V
106	Shun Ming Road	NB	At grade	50	250	25	300	25	Y
107	Shun Ming Road	NB	At grade	50	200	26	100	25	Y
108	Shun Ming Road	NB	At grade	50	250	26	150	25	Y
109	Shun Ming Road	NB	At grade	50	250	25	100	24	Y
112	Kwong Shing Street	SB	At grade	50	150	42	100	28 25	Y
113	Un Chau Street	NB NB	At grade	50	150 800	26	700	25	
114	Un Chau Street Un Chau Street	NB NB	At grade	50	700	39	700	31	Y
116	Un Chau Street	NB NB	At grade	50	750	27	700	27	Y
110	On Chan Sirect	NB	At grade	.50	700	28	650	27	Y

Predicted Traffic Flow at Peak Hours of Year 2049

Road ID	Road	Direction	At grade	Speed Limit	AM	Peak	PM	Peak	Within 300r Assessmen
200.525		S.WALSAN	/ Flyover	(km/hr)	Traffic	% Heavy	Traffic	% Heavy	Boundary
118	Un Chau Street	NB	At grade	50	700	28	800	27	Y
121	Tsap Fai Street	NB	At grade	50	100	35	200	42	Y
122	Fuk Wing Street	SB	At grade	50	400	36	500	23	Y
123	Fuk Wing Street	SB	At grade	50	250	16	300	18	Y
124	Fuk Wa Street	NB	At grade	50	200	35	150	41	Y
125	Fuk Wa Street	NB	At grade	50	200	38	200	18	Y
126	Kwong Cheung Street	SB	At grade	50	250	28	400	27	Y
127	Yu Chau West Street	SB	At grade	50	150	27	250	31	Y
128	Yu Chau West Street	SB	At grade	50	200	26	350	30	Y
129	Tai Nan West Street	NB	At grade	50	600	25	550	30	Y
130	Tai Nan West Street	NB	At grade	50	800	25	750	30	Y
131	Tai Nan West Street	NB	At grade	50	1300	26	750	27	Y
132	Tai Nan West Street	NB	At grade	50	800	36	950	26	Y
133	Tai Nan West Street	NB	At grade	50	700	36	800	26	Y
134	Tai Nan West Street	NB	At grade	50	750	24	1050	22	Y
145	Hang Cheung Street	SB	At grade	.50	50	33	200	13	Y
146	Hang Cheung Street	NB	At grade	- 50	24	35	21	9	Y
147	Fortune Street	SB	At grade	50	100	30	50	7	Y
148	Fortune Street	NB	At grade	.50	50	29	100	15	Y
149	Tan Lai Street	SB	At grade	50	50	24	50	31	Y
150	Tan Lai Street	NB	At grade	50	50	24	50	31	Y
153	Cheung Wah Street	NB	At grade	50	300	25	200	18	Y
154	Cheung Wah Street	NB	At grade	50	300	25	300	18	Y
155	Cheung Wah Street	SB	At grade	50	250	25	200	18	Y
156	Cheung Wah Street	SB	At grade	50	800	27	700	21	Y
157	Cheung Wah Street	SB	At grade	50	1400	32	950	23	Y
158	Cheung Wah Street	SB	At grade	50	1200	33	900	25	Y
159	Hing Wah Street	NB	At grade	50	50	28	100	30	Y
160	Hing Wah Street	SB	At grade	50	250	32	150	27	Y
161	Hing Wah Street	NB	At grade	50	400	28	350	29	Y
162	Hing Wah Street	SB	At grade	50	500	32	400	25	Y
163	Hing Wah Street	NB	At grade	.50	550	30	650	24	Y
164	Hing Wah Street	SB	At grade	50	400	31	350	27	Y
165	Hing Wah Street	NB	At grade	50	400	28	400	27	Y
166	Hing Wah Street	NB	At grade	50	800	19	750	13	Y
167	Hing Wah Street	SB	At grade	-50	650	39	600	33	Y
168	Hing Wah Street	NB	At grade	50	350	14	350	10	Y
169	Hing Wah Street	SB	At grade	50	800	12	950.	9	Y
170	Hing Wah Street	NB	At grade	50	350	26	400	28	Y
171	Hing Wah Street	SB	At grade	.50	700	35	750	24	Y
172	Hing Wah Street	NB	At grade	50	500	26	450	27	Y
173	Hing Wah Street	SB	At grade	50	700	35	750	24	Y
174	Hing Wah Street	NB	At grade	50	700	29	550	30	Y
175	Hing Wah Street	SB	At grade	50	550	33	650	27	Y
181	Cheung Fat Street	NB	At grade	50	50	27	50	29	Y
182	Cheung Fat Street	NB	At grade	50	100	28	50	28	Y
183	Cheung Fat Street	SB	At grade	50	50	31	50	28	Y
184	Un Chau Street	NB	At grade	50	50	34	50	14	Y
187	Fat Tseung Street	NB	At grade	50	250	30	150	31	Y
188	Fat Tseung Street	NB	At grade	50	50	26	50	29	Y
189	Fat Tseung Street	SB	At grade	50	150	32	200	27	Y
190	Fat Tseung Street	NB	At grade	50	50	29	50	29	Y
191	Fat Tseing Street	SB	At grade	50	150	32	200	27	Ŷ

APPENDIX 5-2

Traffic Noise Assessment Results (Base Scenario)

	I
cade	
- by fa	
(Zone)	
A (Low	
Tower	

	7	13-3	100	80	(0)	100	les.	7	1	1	7	7	1	10	10	9	10	10	9	10		10	5	in		5	
		Z TAL-1	E.	7	7	1	7	7	7	7	7	7		7	3		7	-		-	*	7	2	-		^	
		TAL-13-2	78	38	78	78	业	11	11	11	11	11	11	36	35	3/2	38	20	36	R	73	K	75	75		22	2
		TAL-13-1	22	加	78	11	11	11	11	11	11	76	76	76	20	76	20	72	75	75	75	2	75	75		22	18
		TAL-12-2	11	11	11	77	11	11	11	76	22	76	36	76	76.	22	75	於	75	22	此	75	35	74		24	11
		TAL-12-1	77	77	11	77	11	22	76	76	75	76	22	76	75	75	75	75	75	75	35	75.	杜	74		74	11
		TAL-11-2	7.6	77	77	. 11	77	75	76	75	76	The	7.6	76	75	75	75	75	75	75	75	74	7.5	7.6		7.6	11
		TAL-11-1	75	35	76	76	76	75	76	76	20	76	76	75	75	22	75	75	23	75	7.4	74	74	74		22	16
		TAL-10-2	74	76	76	76	75	76	76	布	3/2	76	75	75	75	75	75	75	75.	75	74	74	批	74		74	16
		TAL-10-1	7.3	75	九	76	76	24	7.6	76	2/2	76	75	75	75	75	. 75	75	75	75	74	花	74	7.4		73	76
		TAL-09-2	77	74	市	92	76	理	St.	那	76	75	75	75	2	12	3	松	35	74	200	花	2	20		22	92
		TAL-09-1	11	73	. 75	75	76	76.	34	75	75	75	75	75	75	75	75	7.4	7.4	74	74	7.4	14	74		7.7	76
		TAL-08-5	200	72	74	75	75	75	75	75	75	75	75	75	75	75	74	74	74	74	7.4	74	74	74		70	75
		TAL-08-4	69	3.1	73	74	75	77	75	75	75	75	75	- 75	74	74	74	74	74	74	34	74	24	73		69	75
		TAL-08-3	89	20	77	7.3	74	75	22	35	75	75	7.8	74	女	7.4	74	74	74	74	74	73	73	73		88	75
		TAL-08-2	95	57	28	99	19	63	64	2	99	99	99	99	99	99	99	99	99	99	99	- 65	99	99		95	99
		TAL-08-1	- 51	53	55	88	09	62	63	63	64	64	64	64	64	63	64	64	64	99	64	99	64	64		51	64
		TAL-07-3	95	52	55	58	65	99	09	9	09	61	19	19	19	19	19	19	19	19	19	19	19	61		9	19
	(A)	TAL-07-2	98	25	55	88	65	65	65	99	09	9	09	09	9	09	99	09	09	99	99	09	9	09		98	09
	Predited Noise level, dB(A)	TAL-07-1	47	49	51	53	X.	95	95	23	57	25	25	- 23	25	57	23	88	58	88	58	58	88	58		47	85
	Predited No	TAL-06-5	48	20	25	7	55	95	95	26	25	25	23	57	57	57	25	85	28	88	28	28	88	28		22	28
	1	TAL-06-4	95	57	58	88	59	09	09	09	09	09	09	99	09	09	09	09	61	19	19	19	19	61		36	19
		2 TAL-06-3	09	19	25	59	99	9	99	99	99	99	99	99	99	99	99	9	99	99	99	99	59	9		9	99
		1 TAL-06-2	20	20	20	20	20	20	20	69	69	69	69	69	88	89	89	89	89	88	68	67	19	19		67	20
		4 TAL-06-1	89	69	69	69	38	89	89	89	89	19	29	19	29	19	19	19	99	99	99	99	99	98		99	69
		-3 TAL-05-4	8	99	19	19	99	99	99	98	99	99	99	99	65	99	99	2	35	2	25	25	3	2		2	
	200	-2 TAL-05-3	76	75	75	75	75	74	74	74	74	74	74	7.8	73	73	73	73	73	73	7.3	73	72	7.2	П		76
		TAL-04-2 TAL-05-1 TAL-05-2	26		75	75	75	75	24	74		74	7.9	74		73	73	73	73	73	73		72	7.5		- 22	Н
		1-2 TAL-05	76		75	75	75	75	74			74	74	7.6		73			73	H			72	72	Н	72	_
		4-1 TAL-O	76		75	73		. 75	25			H	73			7.6		73		8			13	72			91
		3-2 TAL-04-1	176			75	75	12	-	74		.74	74	74		74		13				73	17	7.1	Н	73	
		3-1 TAL-03-2	9/		15	75.	73	75.	75			74	7.4	74	H	74	74	73		73		73	73	73	Н		16
	200	TAL-02-1 TAL-02-2 TAL-02-3 TAL-03-1	94	Į.		75	75	75		75	1	74	74	74		対		74	73			73	73	73	Н	73 73	_
		32-2 TAL-0	37. 76			376	75		25				1 74	74		74							3 73	3 73			
,		02-1 TAL-	32 1		5 76	90 5	75 75	75 75		75 75		H	5 .24	14 74		12 12			_			73 73		3 73	Н	13	Н
2			11 11	2		36	J. Je						5 75	5 74	П								3 73	13		-	
1		31-2 TAL-	17 77	77 76		76 76	76 76	76. 76	75 75	75 75	75 75	75 75	75 75	75 75			74 74	74 74		74 74		74. 73	73 73	73 73	Н	73 73	17 77
-		TAL-01-1 TAL-01-2 TAL-01-3	77 37		7	77 76	77 76			77 77			75 77		76 75								74 75	74 7		74 7	7 3
יסוגרו ע (בסוג בסוגר) של וחלחתר	tion	-				7						H									35					7	1
	Elevation	(mPD)	F 34.1		H		Н	7	F 53	5	-		Н	H	F 71.9	H	Н		F 84.5	Ĺ	Н	H	F 97.1	300.25		min	max
2	-	1004	1/1	2/5	3/8	4/15	5/6	5/F	7/8	8/5	9/6	10/1	11/1	12/	13/	14/	15/	16/	17/	18/	19/6	30/1	777	22/			L

Tower A (High Zone) - by façade

	4-12-4	K	35	75	於	2	74	40	建	74	74	74	74.	- 2	22
	12-3 1 AM														
	12-2 TAH-1	K	2	73	K	74	74	74	7	74	74	74	74	74	3. 75
	ITAH	K.	34	74	74	74	72	74	74	74	74	74	7.3	73	75
	1-2 TAH-12-	段	24	74	74	7.4	74	74	74	73	73	73	73	73	花
	11-1 TAH-11-2	74	74	74	74	74	74	74	73	73	73	73	73	73	74
	10-2 TAH-1	74	7.8	74	74	74	74	73	73	7.3	7.3	E	73	73	74
	10-1 TAH-1	74	7.8	74	74	7.	*	73	73	73	73	73	73	. 73	だ
	09-3 TAH-1	74	74	故	74	74	73	73	73	73	73	-73	73	. 73	74
	6-09-2 TAH-0	74	34	74	74	73		73	73	73	7.3	73	73	.73	74
	9-1 TAM-0	74	果	72	既	73	73	73	73	73	73	73	73	73	花
	B-S TAH-O	74	74	74	73	73	73	73	73	73	73	73	73	73	7.4
	L4 TAH-OF	74	73	73	73	73	73	73	73	73	73	H	73	73	74
	1-3 TAH-08-4	73	78	73	73	73	73	73	73	73	78	73	72	72	73.
Į	L2 TAH-08-	73	73	73	73	73	73	73	73	73	7.5	77	72	77	73
	1.1 TAH-08-2	65	99	99	65	59	99	65	65	99	99	99	99	65	99
	-3 TAH-08-1	99	64	95	99	54	64	64	29	54	64	3	64	64	99
	-2 TAH-07-3	61	61	61	61	-61	19	19	61	19	61	19	61	19	19
18(A)	-1 TAH-07-2	8	9	09	9	09	61	61	61	61	61	19	19	99	61
toise level, o	-5 TAH-07-	28	88	65	65	65	65	89	65	65	65	93	99	28	09
Predited 2	4 TAH-06-5	85	28	88	65	65	65	89	89	65	65	65	9	28	09
	-06-3 TAH-05-	19	61	61	61	19	61	61	19	61	19	19	61	61	61
	TAH	99	99		99	99	99		99	59	99	59	99	99	99
	36-1 TAH-06-2	19	19	. 67	19	19	19	99	9	99	99	99	99	99	29
į	TAH	99	99	99	65	99	99	65	65	99	99	99	99	68	99
	F3 TAH-05-4	2	15	63	63	63	63	63	63	63	63	63	63	63	23
	F-2 TAH-05-3	7.2	72	7.5	7.7	7.5	7.7	7.3	7.1	11	14	77	71	77	72
ļ	F.1 TAH-05-2	72	77	72	72	72	72	7.7	72	71	71	71	71	71	12
	L2 TAH-05-	72	.72	72	72	72	72	72	72	7.1	71	.71	71	71	72
	4-1 TAH-08	77	77	77	77	77	72	72	.72	7.2	11	110	7.1	11	72
	8-2 TAH-G	7.2	3.2	72	72	72	72	7.2	72	72	7.2	72	11	71	77
	3-1 TAH-03-2	72	72	72	7.2	72	72	72	72	72	72	7.1	7.1	71	72
	2-3 TAH-03-1	73	72	77	72	77	72	72	72	72	77	72	71	11	73
	2-2 TAH-02-3	73	32	7.5	72	7.2	72	72	77	72	77	7.1	7.1	11	73
	2-1 TAH-02-2	73	73	72	72	72	72	72	72	72	72	72	22	77	7.3
	1-3 TAH-02-1	73	73	73	72	72	72	72	72	72	72	72	72	72	73
	1-2 TAH-01-	73	7.8	73	7.5	7.8	72	7.2	.72	72	72	72	72	72	7.3
	-1 TAH-01-2	73	73.	73	22	73	73	73	77	72	72	22	72	72	7.3
	TAH-01-1	74	74	12	74	74	74	34	73.	73	73	73	73	73	74
Bevation	(mPO)	103.4	106.55	109.7	112.85	116	119.15	122.3	125.45	128.6	131.75	134.9	138.05	min	max
- Element	FIGOR	23/F	24/F	25/F	26/F	3//2	28/F	39/F	30/1	31/F	32/5	33/F	34/F		
			_	_	_	-	7						1	1	

TB-13-1 TB-13-2 TB-12-3	79	78 79 7	78 78 7	78 78 2	77 78 7	77 78 7	77 78 7	77 77	TT TT	TI TI	76 77 7	76 77 3	76 77 7	76 76 7	76 76 7		76 76 7	75 75 7	75 76 7	75 76 7		75 75 7	75 75 7	75 75 7	75 75 7	74 75 7	74 75 75	74 75	78 75 7	74 75 7	74 74 7	74 74 74	74 74
TB-11-2 T	۰	78	7.8	11	22	77	11	77	94	76.	76	76	16	36	76	2	. 75	75	北	. 25	75	75	75	龙	74	74.	7.4	74	74	7.4	74	7.4	3.0
TR.11.1	-	17	11	11	22	. 17.	76	76	3/2	76	76	76	75	75	. 75	75	75	75	75	74	74	.74.	74	74	74	74	74	74	73	73	73	73	7.8
3.1 TR.10.2	-		11	77		76	76	2/2	36	76	76	75	75		75			75		74			74			74	73	73	73	73	. 73	73	78
TB-09-3 TB-10-1	۰	76 TE	76 76	76 75	76 76	16 76	76 76	76 76	75 76	75 75	75 75	75. 75	75 75	75 75	75 75	九 花	74 74	74 74	74 74	74 44	74 74	74 74	74 74	73 74	73 73	73. 73	73 73	73 73	73 73	73 73	73 73	73 73	71
TB-09-2 TB	н	75	76	7.6	76	76	7.6	75	75	75	75	75	75	75	74	74	74	74	74	7.8	74	74	73	73	7.3	73	73	73	73	73	7.3	7.3	7.8
T6-06-1	-	74	75	75	26	76	Z.	75	72	X	75	75	75	75	74	74	7.0	74	74	7.8	140	74	74	7.3	73	7.8	73.	7.8	7.8	7.3	73	73	3.6
T8-06-3	-	30	7.1	73	73	73	73	73	73	73	73	73	73	32	77	22	72	72	7.5	72	72	77	7.1	- 73	71	72	71	73	7.1	71	71	71	3.6
1 TR-08-2	₽	20	72	73	74	74	74	世	74	74	74	74	74	艾	-73	. 73	73	73	73	73	73	73	73	72	72	72	72	72	72	11	72	72	23
3.3 76.06.1	۰		71	72	73	74	74	74	74	74	73	73	73	73	7.3	73	7.8	73	73			7.2	72				22	7.2	72	72	72	7.1	7.1
TB-07-2 TB-03-3	₽	55 47	55 48	56 49	56 51	57 53			58 56		52 65		85 09	65 19		25 60		62 60	62 61			52 61	62 61	52 61	52 61	62 61	62 61	62 61	62 61	62 61	19 23	62 61	19 (29
TR-07-1 TR-0	-	56 5	1	H	5 95		57 5	57 5	-	7	58 8		2.5		9 09					62. 6	1			61 6			61 6	61 6	61 6	61 6	61 6	61 6	9 13
1	-	23	23	57	57	57	25	88	28	88	65	65	65	60	09	19	61	61	29	62	62	62	62	61	61	61	61	61	19	19	61	61	19
LOG-1 TR-OG-4 TB-OG	-57	57	57	88	58	58	88	. 65	65	89	09	9	09	19	. 61	62	62	62	62	62	63	63	63	62	- 62	29	62	62	62	62	62	62	62
E	-	99	09	19	19	29	29	63	63	29	99	99	99	59	99	95	99	99	99	99	99	99	99	99	99	99	99	99	99	99	99	99	39
1 TB-06-2	٠	69	69	89	69	69	69	69	69	69	69	69	69	89	89	89	89	89	89	89	29	69	19	19	19	19	67	19	29	19	99	89	99
T8-05-4 T8-06-1	٠		99 65	61 66	2 66	63. 67	61 67	64 67	64 67	64 67		64 67	19 19	19 19	64 67	H	99 19	63 66	99 69	63 66		63 66	63 65	63 65	63 65		63 65	63 65		62 65	62 65	62 65	39 09
8.8	9	75 5	75 5	75. 6	75 6	35 6	74 6	74 6	74 6	74 6	74 6	74 6	73 6	73 6	73 6	73 / 67	7.8	73	73	7.2	72 6	72 6	72 6	72 6	72 6	72 6	72 6	7.2	71. 6	71 6	75 6	71. 6	34
T8-05.2 TB-0	36	75	75	75	75	75	K	74	74	裁	74	74	73	73	73	73	73	73	7.5	72	7.2	72	72	-72	72	72	72	7.2	77	7.1	71	71	3.6
TR-05-1	75 76	75	75	75	74.	74	74	74	74	73	73	73	73	73	72	72	. 72	72	72	72	72	71	71	7.1	71	71	71	71	71	71	71	71.	14
TR-06.2	12	75	52	72	75	74	74	H	H			73	73					-	72	H								7.1	. 71	71	. 73	77	7
L2 TB-04.1	-	75	Н	Н	74	L	L	Ц		73	73	Ц	7.3		ш		ш	Ц	72	ш			ш		Ц	ш	71	71	7.1	7.1	71	T.	71
TR-01-1 TR-01-2		75 75		Н	H	Н	74 74	74 74	H	74 73		Н	73 73	Н			Н		72 72								71 71	71 71		71 71	71 71	71 71	71 31
T8-02-3 T8-0		75. 7		H	H					74 3	Į.	73 7	7.3			H			73 7						-	-		71 7	72 7	71 7	71 7	71 71	71 7
		76	H	Н	Н	Н	H	74	74	74		H	73	73	73	73	-73	72	22	72	72	77	72	-72	72	7.5	72	71	7.1	7.5	72	7.1	22
TR-02-1 TR-02-2	32	76	75	75	72	75	75	世	74	74	74	74	74	13	73	73	73	73	73	72	72	72	77	72	72	72	72	. 22	7.1	71	71	7.5	12
TR-01-3	26	16	94	- 16		- 75	75.	75	74	74			7.4	Н	7.8	Н			73	Н			Н				72	7.2	7.5	72	7.1	71	71
.1 TB-01-2	75 25	施	2	76	於	が	H	73	H			24		H	H	H	H		73	H		H	H	H	H	H	H	72	H	72	72	22	34
												75 77			П				8 76	Ц							Ц	Ц		45 74		75 74	24
Floor (mPC	34.1	Н	3/F 40.4	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	Н	29/F 122.3	Н	128.6	Н	H

Predicted Traffic Noise Level, dB(A) - (a) Base Scenario

Tower A (Low Zone) - by flat

Floor	Elevation						Predite	ed Noise level, dB(A)						
Libor	(mPO)	TAL-01	TAL-02	TAL-03	TAL-04	TAL-05	TAL-06	TAL-07	TAL-08	TAL-09	TAL-10	TAL-11	TAL-12	TAI-13
1/F	34.1	78	.72	76	76	.76	70	50	70	72	74	. 76	. 77	78
2/F	37.25	78	76	76	76	.75	70	52	π	. 24	76	77	27	78
3/F	40.4	78	76	76	75	75	70	55	74	76	76	77	77	78
4/F	43.55	77	76	75	75	75	70	58	75	76	76	77	77	78
5/F	46.7	27.	76	.75	75	75	70	59	75	76	76.	77	77	78
6/F	49.85	T	75	75.	75	75	70	60	75	76	76	76	77	77
7/F	53	77	75	75	75	74	70	60	75	76	76	76	77	77
8/F	56.15	77.	75	75	74	74	69	60	75	76	76	76	76	77
9/F	59.3	76	75_	75	. 74	74	69	60	_75	76	76	76_	76	77
10/F	62.45	76	75	74	74	74	69	61	75	75	76	76	76	77
11/F	65.6	76	75	74	74	74	69	61		75	75	76	76	77
12/F	68.75	76	74	74	. 74	. 74	69	61	75	75	75	76	.76	76
13/F	71.9	76	74	74	74.	74	68	61	.75	75	- 75	-75	76	76
14/F	75.05	76	74	74	74	73	68	61	75	75	75	75	75	76
15/F	78.2	75	74	74	74	73	68	61	74	75	75	75	75	76
16/F	81.35	75	.74	74	73	73	68	61	.74	75	75	75	75	76
17/F	84.5	75	74	73	73.	73	68	61	74	75	75.	75	75	76
18/F	87.65	75	73	73	. 73	73	68	61	74	74	75	. 75	75	76
19/F	90.8	75	73	73	73	79	68	61	74	74	74	75	75	75
20/F	93.95	75	73	7.5	73	73	67	61	74	74	74.	74	75	75.
21/F	97.1	74	73	73	. 73	72	67	61	74	74	74	. 74	75	75
22/F	100.25	74	73	73.	73	72	67	61	74	74	74	74	74	75
	nin	74	73	73	73	72	67	50	70	72	74	74	74	75
	nax	78	72	26	76	76	70	61	75	76	76	77	77	78

Tower A (High Zone) - by flat

	Elevation						Predit	ed Noise level, dB(A)					
Floor	(mPD)	TAH-01	TAH-02	TAH-03	TAH-04	TAH-05	TAH-06	TAH-07	TAH-08	TAN-09	TAH-10	TAH-11	TAH-12
23/F	103.4	74	- 73	73	72	72	67	61	74	24	74	74	75
24/F	106.55	74	73	72	72	72	67	61	73	74	74	74	75
25/F	109.7	74	71	- 72	72	72	67	61	- 73	74	74	74	75
26/F	112.85	74	72	72	72	72	67	61	73	74	74	74	75.
27/F	115	74	72	72	.72	72	67	61	73	73	74	74.	75
28/F	119.15	74	72	72	72	72	67	61	73	73	74	74	74-
29/F	122.3	74	72	72	72	72	66	61	73	73	73	74	74
30/F	125.45	73	72	72	72	72	66.	61	73	73	73	73	74,
31/F	128.6	73	72	22	72	71	66	61	73	73	73	73	74
32/F	131.75	73	72	22	72	71	66	61	71	73	73	73	74
33/F	134.9	73	72	72	71	71	66	61	73	73	.73	73	74
34/F	138,05	78	72	71	71	71	66	61	-73	73	73	73	74.
	min	73	72	71	71	71	66	61	73	73	. 73	73	74
	TIES.	74	73	73	72	72	67	61	74	74	7.4	74	75.

Tower B - by flat

Floor	Devation						Predited Noise level, dB(/				The same of		
Floor	(mPO)	TB-01	T8-02	TB-03	TB-04	TB-05	TB-06	18-07	TB-08	TB-09	TB-10	T8-11	TB-12
1/F	34.1	79	76	76	75	76	69	56	67	74	77	78	.79
2/F	37.25	79	76	75	75	75	69	56	70	76	77	76	79
3/F	40.4	79	76	75	75	75	69	36	72	76	77	78	79
4/F	43.55	72	75	75	75	75	68	56	. 73	76	77	77	78
5/F	46.7	78	75	75	75	.75	69	56	74	76	77	- 77	78
6/F	49.85	78	75	74	74	75	69	57	74	76	76	- 77	78
7/F	53	78	75	74	74	75	69	57	78	76	76	77	78
8/F	56.15	TI	74	74	74	74	69	58	74	76	76	77	78
9/4	59.3	77	74	74	74	74	69	58	74	75	76	76	77.
10/F	62.45	77	74	74	74	74	69	58	74	75	76	76	77
11/F	65.6	77	-74	73	73	74	69	59	74	75	76	76	77
12/F	68.75	77	74	73	73	74	69	59	74	75	75	76	77.
13/F	71.9	77	74	73	73	73	69	60	74	75	75	76	77
14/F	75.05	76	71	73	73	73	68	61	74	75	75	76	27
15/F	78.2	76	73	73	72	73	68	61	73	75	75	76	76
16/F	81.35	76	73	72	72	73	68	62	73	74.	75	75	76
17/F	84.5	76	73	72	72	73	68	62	73	74	75	75	76
18/F	87.65	.76	73	72	72	.73	68	62	73	74	75	75	.76
19/F	90.8	76	73	72	72	72	68	62	73	74	74	75	76
20/F	93,95	76	72	72	72	72	68	62	73	74	74	75	76
21/F	97.1	75	72	72	72	72	67	62	73	74	74	75	76
22/F	100.25	75	72	72	.72	72	67	62	73	74	74	75	76
23/F	103.4	75	72	72	71	77	67	62	73	74	74	75	75
24/F	106.55	75		.71	71	72	67	62	72	73	78	74	75
25/F	109.7	75	72	71	71	72	67	62	72	73	74	74	73
26/F	112.85	75	72	71	71	72	67	62	72	73	74	74	75
27/F	116	75	72	71	71	72	67	62	72	73	73	74	75
28/F	119.15	75	72	71	71	72	67	62	72	73	73	.74	73
29/F	122.3	74	71	71	71	72	67	62	72	73	73	74	75
30/F	125.45	74	71	71	71	n	67	62	72	73	73	74	.75
31/F		74	71	71	71	71	66	62	72	71	73	74	75
32/F	131.75	74	71	71	71	71	66	62	72	73	73	74	74
33/F		74	71	71	71	71	66	62	72	73	73	. 74	.74
34/F	138.05	74	71	71	71	71	66	62	72	73	73	71	74
	min	74	71	71	71	71	66	56	67	73	73	73	74
	max	. 73	76	76.	75	76	69	62	7.6	76	77	28	79

APPENDIX 5-3

Proposed Mitigation Measures & Traffic Noise Assessment Results (Mitigated Scenario - With Windows)

Proposed Noise Mitigation

Tower A (Low Zone) - by façade

	Elevation		,,,,		_															Predited Nois	se level diff	A)															_		
Floor	(mPD)	TAL-01-1	TAL-01-2	TAL-01-3	TAL-02-1	TAL-02-2	TAL-02-1	TAL-03-1	TAL-03-2	TAL-04-1	TAL-04-2	TAL-05-1	TAL-05-2	TAL-05-1	TAL-05-4	TAL-06-1	TAL-06-2	TAL-06-3		TAL-06-5			TAL-07-3	TAL-08-1	TAL-08-2	TAL-08-3	TAL-08-4	TAL-08-5	TA1-09-1	TAL-09-2	TAL-10-1	TAL-10-2	TAL-11-1	TAL-11-2	TAL-12-1	TAI-12-2	TAL-13-1	1 TAL-13-2	TAL-13-3
1/F	34.1	AW	AW	AW	AW	AW.	AW	AW	AW	AW	AW	AW.	AW	AW	-		-	-	-	-	-	-			-	4W	AW	AW	AW	AW	AW	AW.	AW	AW	AW	AW	AW	.RW	AW.
2/9	37.25	AW	AW	AW	500	696	AW	AW	AW	AW	AW	AM	AW	AW/	-	-	-	-	-	-	-	-	-	- 64	-	AW	AMP.	AW	AW										
3/F	40.4	AW	AW	AW	AW	AW	AW	aw	AW	AW	AW	AW	AW	AW	-	-	-	-	-	-		-	-		-	AW	AW												
4/6	43.55	AW	AW	AW	AW	AW	AW	400	AW	AW	aw	AVV	AW	AW	-	-	-	-	-	-		_	-		-	AW	AW	AW	AW	AW	AW	68	AW	AW	AW	AW	AW	AVA.	AW
5/F	46.7	AW	584	AW	499	494	AW	AW.	AW	AW	AW	AM	AM	AM/			-	-	-	- 14		_	-	- 44	-	AW	AW.	AW	8000										
6/F	49.85	ANA	AW	AW	AW	AW	AME	AW:	AW	AW	AW	AW	AW	AW	-	-		-	-		- 44	-	-	-	-	AW	AW	AWI	AW	AW	AM	BIM.	AM	AW	AW	AW:	AW	AW	AW
7/F	53	AW	AW	AW	AW	AW	Alle	5W	AW	AW	AW	AW	AW	AW	-	-	-	-	-		-	-	-	-	-	AW	AM	AW	AW										
8/F	56.15	AW	AW	AW	AW	AW	AW	AW	AW	AW	Ave	AM	AW	AW		-		1	-	-	-		-		-	AW	406	AW	AW										
9/F	59.3	ANN	AW	490	AW	898	AM	AW	AW	AME	aw	AIM	AWA	AME	-	-		-	-		-	-	-		-	AW	AMA:	AW	AW	AW	AW	AMI	AW	AME	AW	AVAC	AMC	AW	AW
10/F	62.45	ANN	AM	AW	AW	AW	Auto	AVAI	AW	AW	AW	AW	AMI	ANA/	-	-	-	-	-	-	-	-	-	-	-	AW	AM	AVA	AW	AW	AW	AVAIL	AMI	AW	AW	AW	AW	AW	AW
11/F	65.6	Ann	AW	STATE OF THE PERSON NAMED IN	Aller	ANN	Aust	No.	400	AW	Ann.	ANA	AW	AW	-	-		1	-	-	-	-	-	-	-	400	Aug	ANA	AUG	510	AW	ALLEY	ANN	AW	AW	Avec	AW	AW	410
12/9	68.75	ANU	AUG	AME	AND	AME	AW	- ATAV	AW	AW	2000	aw	AW	AW	-	-	-	-	-		-		-	-	-	AW	ALM	200	AW	400									
13/F	71.9	AVE:	Alai	AVA	AW	AW	AM	AW	AM	AW	Alde	AUA/	AW	ANT.	-	-	-	-		-			-	-	-	AM	AM	AW	AW	AW	AVAI	AVAIL.	800	Atas	AME	AW	ANY	AW	AM
14/F	75.05	A110	200	ALLEY	200	AW	Aut	ALC:	AW	110	mile:	AVE.	AVE	AW	-	-	-	-	-	-		-	-	-	-	AM	4147	- 200	AUU	500	ATAY	AUG.	ANI	600	AVE	AIR	AW	AW.	2100
15/F	79.0	ANN	AUG.	5162	AME	8385	AUA	AMI:	0182	ANN	Augu	Alas	AME	AM		-	-	-	-	-		-	-	- 12	-	AM	ALAZ	850	0.00	AW.	-8160	8181	8387	8100	0.00	A101	P180	8:00	200
16/F	81.35	AVA/	Aiki	AM	AW	AW	Auto	EM:	AVAV	AW	AW	AMA	AW	AW	-		-	-	-	-		-	-	- 10	-	AM	AMA	AMI	AW	AW	AVAIL	AVAIL	AM	AME	AW:	AW	AME	AW	AM
17/F	84.5	ANN	AW	AUG	A160	Allei	AW	N/40	AW	AW	Alle	Alai	ANN	ANN			-	-	-	-		-	-	-	-	ANG	AUG	aw	AW	AW	AW	AW	AVE	AW	2161	0.00	AW	88	AM
18/F	87.65	ASS	500	AW	4.00	AW	AW	AW	AW	AW	200	AW	AW	AW	-		-	-	-	-	-	-	-		-	AW	ALAP:	AW	AW										
19/F	90.8	AVAIL	AM	AW	AW	AW	AME	AVAIL	AW	AW	AW	ANN	ANN	8500		-	-	- "	-	-0			-			ANA	AMA	AVAI	AM	AW.	AIM	ANN	ANN	AM	ANN	AM	ANN	AVAIL	ANN
20/F	93.95	AME	AM	AME	AMI	AW	AW	NW:	AW	AVE	ANN	Allei	ANN	AW	-	-	-	-	-	-	-	-	-	-	-	AM	ANIC	AW	AW	AUN	AND	AUG.	ANN	AME	AMI	AIM	ANN	AW	AM
	97.1	AW	AW	AVA	AW	AW.	AW	_	_	-	-	-	-	-	-	_	_	-	AW	AVAIL	400	-0.00	AW	AVE	AND:	200	AW	400	AW	AW	AW	AW							
21/F	100.25	ANN	Ave	- NYF	AVV	AW	2000	AW	AM	AW.	.000	May	ANY	WAY.	- 11	- 7		-	- "	-			- 0	- 1	- 11	AVE	ACMA:	AW	AW.	- NW	NW.	ANN.	ANY	N.A.	ALVE .	AW-	AW		AW
un	100.25	AW	-AW	AW	AW	AW	AW	AW	AW	WW	AW	AW	HWV	400		-	-	-	-	100					-	AW	MY	HW	AW	HW.	M.W	100	HW.	AW	1999	2.00	MAN	AW	HW

Tower A (High Zone) - by façade

Plane	Elevation												4					1 1	P	redited Nois	se level, dB	A)																	
Floor	(mPD)	TAH-01-1	TAH-01-2	TAH-01-3	TAH-02-1	TAH-02-2	TAH-02-3	TAH-03-1	TAH-03-2	TAH-04-1	TAH-04-2	TAH-05-1	TAH-05-2	TAH-05-3	TAH-05-4	TAH-06-1	TAH-06-2	TAH-06-3	TAH-05-4	TAH-06-5	TAH-07-1	TAH-07-2	TAH-07-3	TAH-08-1	TAH-08-2	TAH-08-3	TAH-08-4	TAH-08-5	TAH-09-1	TAH-09-2	TAH-09-3	TAH-10-1	TAH-10-2	TAH-11-1	TAH-11-2	TAH-12-1	TAH-12-2	E TAH-12-7	TAH-12-4
23/F	103.4	AW	AW	AW	AW	AW -	AW	AW	AW	AW	AW	AW!	AW	AW	100	740	- 14	44			dar	-		Ni .	-	AW	AW	AW	AW	AW	AW	- AW	AW	AW	AW	AW	AW	AW	AW
24/F	106.55	AW	AW	AW	AW	AW-	AW.	AW	PT .	- 77		-	.+	777	200	-		-	-	AW.	AW	AW	.AW	AW	AW	AW	AW.	AW	AW	- AW	AW	AW	AW-						
25/F	109.7	AW	AW	AW	AW	AW	AW	AW:	AW	AW	AW	AW	AW	AW	**	-0	-	**	in	rie.	**	**		**	in	AW	AW.	AW	AW:	AW	AW	AW	AW						
26/F	112.85	AW	AW	AW	AW-	AW	AW.	AW	AW.	AW	AW	AW -	AW-	AW	ma.	- 100	be		-	10.0	- 140	-	100	44	- 10	AW	AW	AW	AW	AW	AW	AW:	AW-	AW	AW	AW	AW	AW	AW
27/F	116	AW	AW	AW.	AW	AW.	AW.	.AW	AW	AW	AW	AW	AW	AW	-			-	*	-	-	-	-	-	-	AW.	AW	AW	AW	AW	AW	AW.	AW.	AW	AW	AW	AW	AW	AW.
28/F	119.15	AW	AW	aw	AW	AW	AW	.AW	AW	AW	AW	AW.	AW	AW		-	312	- 11		- 10	- m, -	-			- 14	AW	AW-	AW	AW-	W.	AW	AW-							
29/F	122.3	:AW	AW	-AW	AW	AW	-AW-	AW-	AW	AW	AW	AW:	AW:	AW		- 20		-		940		-	- >-			AW	AW:	AW	AW	AW	AW	AW	AW:	AW	AW:	AW	AW	AW	AW
30/F	125.45	AW	AW	AW	AW	AW	AW/	#W	AW-	AW	AW	AW.	AW	AW	-	-	-	+4	in i	-	-	-	100	- 44	-	AW	AW	AW	.AW	AW	AW	AW.	AW	AW	AW	AW-	AW	AW	AW
31/F	128.6	AW	AW	AW:	AW	AW.	AW	AW.	AW.	AW.	AW	AW.	AW	AW	-	. 0	-	111	TH.	- m	97			77		AW.	AW:	AW	AW	AW	AW-	AW	AW	AW	AW	-ww	AW	AW	AW-
32/F	131.75	AW	AW	- AW	AW	AW	AW	AW	AW	-AW	AW	AW	AW	AW	**	-	-	-	-	100		-	~	-	-	- AW-	AW	AW	- AW	AW.	AW	AW:	AW:	AW	AW	AW	AW	AW	- AW
33/F	134.9	AW	AW	AW	AW	AW.	AW	#W-	AW.	AW	AW	AW	AW	AW	84		- 14	44	- 11	-	-	-	100	-	-	AW	AW	AW	AW	W.W	AW	MAC	AW						
34/F	138.05	AW	AW	AW	AW	AW.	AW	AW	AW.	WA	AW	AW	AW	AW		. 7	. 75			100				-	-	AW	AW	AW	3.00	AW	AW.	AW	AW	AW	AW	W.	XW	RA	AW

Floor	Elevation																	Predite	ed Noise leve	f, dB(A)						da										
PHOOF	(mPO)	TB-01-1	TB-01-2	TB-01-3	TB-02-1	TB-02-2	TB-02-3	TB-03-1	TB-03-2	TB-04-1	TB-04-2	TB-05-1	TB-05-2	TB-05-3	TB-05-4	TB-06-1	T8-06-2	T8-06-3	TB-06-4	TB-06-5	TB-07-1	TB-07-2	TB-07-3	TB-08-1	T8-08-2	TB-08-3	TB-09-1	TB-09-2	TB-09-3	TB-10-1	TB-10-2	TB-11-1	TB-11-2	TB-12-1	T8-12-2	TB-12-3
1/F	34.1	AW	AW	AW	AW	AW	AW	:AW:	.AW	AW	AW	WA.	AW	AW	-	ú.	- 14	An		les:	-	94		AW:	AW	AW	AWF	AW	AW	AW	AW	AW.	AW	AW	AW:	AW
2/F	37.25	AW	AW -	AW	-	-	- 22	4+	+	147	~	-	-	AW	AW	AW	AW.	AW																		
3/F	40.4	AW	AW	WW.	AW	(Are)	W	. 44		-	. I par	- New 1	-	-	AW	AW.	AW	AW	AW																	
4/F	43.55	AW	WA	AW	AW.	AW	AW	- 44		- >+		- 14	***	***	-	+	AW	AW	AW	AW.	AW															
5/F	46.7	AW	AW	AW	AW	AW	AW-	AW		141	- 44	- 44	+		146			AW	AW	AW	AW	AW	WAW	AW												
6/F	49.85	AW	AW	AW	AW	AW	AW	.NW	490	AW	AW:	AW	AW.	NW	My;	140	ja .	- in	~	196	144.	- 100	-	AW	AW	AW:	AW	aw.	AW	WW.						
7/F	53	ASV	AW	AW	AW	AW	AW	AW-	AW	AW	AW	AW	AW	AW	**	*	-	94		-		-	-	WW	AW	AW	AW	AW	WA	AW						
8/F	56.15	AW	AW	AW	AW	AW	AW.	WA	.AW	AW	AW	AW	AW	AW	Table 1	'w-	44	.44	-	· W	the.	- 1	-	AW	AW	AW	AW	- AW	AW	-AW	AW	AW	AW.	AW	AW	AW
9/4	59.3	AW	AW .	AW.	AW	AW	AW.	NW-	AW	AW	AW	AW.	AW.	AW	-	-	14.		-	-	-	-	-	AW	AW	AW	AW/	AW	AW	AW	#W	AW	AW.	AWI	AW:	AW
10/F	62.45	AW	AW-	AW	AW.	AW.	AW	- 44		-			-			-	AW	AW	AW	AW	-AW	AW	AW	AW	AW	AW	AW	AW-	AW							
11/F	65.6	AW	AW.	AW.	AW	AW:	AW.	WA	AW.	WA	AW	AW	AW	AW	44	144	- Au	An.	44	34	44		-	AW	AW.	AW.										
12/F	68.75	AW	AW	AW	AW	AW.	AW.	AW-	AW	AW	AW	AW	AW	AW	-	- 2		-	-	-	-	-	1	AW	AVP	AW.	-AW/	#W	:AW	AW	AW	AW.	AW	AWK	AW:	AW
13/F	71.9	AW	AW	AW.	AW	AW.	AW	AW	AW	AW.	AW	AW.	AW	AW	- 44	- 9	- 14	-	- 10	- 00			-	AW												
14/F	75.05	AW	AW.	AW.	AW	AW.	AW.	AW.	AW	.AW	AW	AW	AW.	AW	-	- 11	-	-	-	- 14	-		-	AW	WW	AW	AW	AW	AW	AW						
15/F	78.2	AW	AW	AW	AW:	AW.	AW.	AW	AW-	AW	AW	AW	AW	-AW	- i-c	-	144	-	-	200	da	-	-	AW	-AW	AW.	AW	- AW	.AW	AW:						
16/F	81.35	AW	AW.	NW.	- WA	AW	AW	AW	AW	- NW	AW	AW.	W.	AW	19	- 17	je.	- 11	in .		10	-	-	AW.	AW	AW	AW	.AW	AW	AW	AW	AW	AW	AW:	AW	AW
17/F	84.5	AW	AW	AW.	AW	AW	AW.	AW	AW	AW	AW	AW.	AW	AW	- Sect	- 94	- 10	- 6		796	- W-			AW	AW	AW	AW	AW:	AW							
18/F	87.65	AW	AW	AW	WA	AW	AW	AW	AW.	AW	W.	AW	AW	AW		- 2	- 14	-	in	166	1.00	-	-	AW	AWC	AW	AW:	.AW	AW							
19/F	90.8	AW	AW .	AW	AW	ww.	AW.	AW	AW	AW	AW	AW	- MW	AW	-	-	-	**		-	-	-	-	WW	AW	AW-	AW	AW	AW	AW	AW	AW	WW	AW:	AW	AW
20/F	93.95	-AW	AW		141	- 14		-	196		-	-	AW																							
21/F	97.1	AW	:AW	AW	AW	AW		- 11)÷	46	ja.	Ter.	44			AW	WA	AW.	AW.	AW	AW.															
22/F	100.25	AW	AW	AW	AW	- AW	AW	AW	AW	AW	AW	AW	AW	AW	-			+	-	-	-	-	-	-AW	AW	AW	AW.	AW								
23/F	103.4	AW	AW	AW	AW	AW	AW.	AW	AW	AW	AW	W	AW	AW		- N 1	- 14	- 6-	-	100	100	-	Jec. 1	AW	AW.	AW.	AW	AW	AW							
24/F	106.55	ASM	AW			36	**	- 14		- 10	-	-	AW	AW	AW	AW.	AW	AW	AW	:AW	AW	AW	AW	AW	AW											
25/F	109.7	AW	1,4	- H		-					~	-AW	AW	AW	AW!	AW																				
26/F	112.85	ASV	AW	NW	AW	AW	ZQAF.	AW	AW	AW	AW.	AW	AW	AW	100	PF.	. (10	÷-		196	144.	- 100	-	J/W	AW	AW.	AW	AW	6W							
27/F	116	AW	WW.	AW	AW	AW	.00	*)÷	**	**			-	+	AW	AW	AW	AW:	AW	AW	AW	AW	AW	AW	W.	AW	AW								
28/F	119.15	AW	AW:	AW	AW	AW	AW	1947	a.i	-14	44	-	- 14	144	-	-	AW.	AW	AW	AW:	AW	AW-	AW													
29/F	122.3	AW	AW	AW	AW	AW	AW	RW:	AW	AW	AW	AW	AW	AW	-		74	-	-	-		-	-	AW												
30/F	125.45	AW	AW:	1.44	- 0	-	-	**	-	**	-	-	AW	V.M.	AW	AW																				
31/F	128.6	AW	AW	AW	AW-	AW	100	94	Air	- Am	- 44	34	44	-	-	-AW-	AW	AW	AW-	AW	AW	AW	AW	AW:	AW	AW	AW	AW								
32/F	131.75	AW	AW	'AW	4W	AW	AW	AW	AW-	AW	AW	AW	AW	AW	**		- 14		-		**		**	AW	AW	AW	AW:	AW	AW	AW	AW	AW.	AW	AW	AW	- AW-
33/F	134,9	AW	AW	AW.	AW	AW	-AW	AW	-AW-	AW	AW	AW	AW	AW	.00	9	- 10			- 0	44.	.00	- 64	AW	AW	AW	W.	AW	AW	AW.	AW	AW	AW	AW	AW	AW
34/F	138.05	AW	AW	-AW-	AW-	AW	AW	-AW	AW	- AW	AW	AW	AW	AW	**	**	-			- **	**		***	-AW-	AW	AW-	- AW:-	AW								

Noise Correction from the Mitigation, dB(A)

Tower A (Low Zone) - by façade

	Elevation			•			3000						1								F		Predited No	ise level, di	(A)											10000						
Floor			-1 TAL	-01-2	TAL-01-3	TAL-02-1	TAL-02-2	TAL-03	2-3 TAL-	13-1	TAL-03-2	TAL-04-1	TAL-04-3	TAL-05	-1 TAL-05-2	TAL-0	-3 TAL-	5-4 TA	L-06-1	TAL-06-2	TAL-06-3	TAL-06-4	TAL-06-5	TAL-07-1	TAL-07-2	TAL-07-3	TAL-08-1	TAL-08-3	TAL-08-3	TAL-08-4	TAL-08-5	TAL-09-1	TAL-09-2	TAL-10-1	TAL-10-2	TAL-11-1	TAL-11-2	TAL-12-1	TAL-12-2	TAL-13-1	TAL-13-7	TAL-13-7
1/F	34.1	-5		-5	-5	- 8-	- 5	- 8	- 4		- 5	-5	- 6	- 8	- 5	- 5	0		0	0	0	0	0	0	0	0	0	0	-5	- 5	-5	-5	- 5	- 45	- 8	-5	-5	- 4	- 8	- 15	-5	-5
2/F	37.25	-5		5	-5	- 6	-5 -	-6	- 4		-5	-6	-6	-5	-5	-5	- 0		0	0	0	0	0	. 0	0	0	.0	0	-5	-5	-5	-5	- 6	- 45	- 6	-8	- 46	-5	-5	- 6	-5	-5
3/F	40.4	-5		4	-5.	-5	-5	-5	- 4		-5	-5	- 8	- 5	-5	- 6	0		0	0	0	0	0	0	.0	0	0	0	- 5	- 6	-5	-5	5.	-5	- 5	-5.	-6	-5	-5	- 8	-5	- 5
4/F	43.55	-5		5	5	- 6	-5	-5	- 4		- 6	- 5	-5	- 5	-5	- 5	- 0		0	0	0	0	0	0	0	0	0	0	- 5	- 5	-5	-8	- 5	-5	- 6	-5.	- 6	- 6	- 5	- 6	-5	- 5
5/F	46.7	-5		5	-5	-6.	-5	-5	- 4		-5	15		-5	- 5	- 5	0		0	0	0	0	0	0	0	0	0	0	- 5	- 5	- 5	-5	-5	- 15	- 6.	-5	-6	-5	-5-	- 6	-5	- 5
6/F	49.85	- 6		5.	- 5	-5	-8	- 5	- 4		-5	-6	- 4	- 6	-5	- 5	- 0		0	0	0	0	0	0	0	.0	0	0	- 5	- 6	-5	-5.	- 6.	- 6	- 6.	-5	-15	-5	-5	à	- 4	- 5
7/4	53	-5		5	- 5	- 5	-5	- 6	-		- 6	- 6	15	- 5	- 5	-8	- 0		0	0	0	0	0	. 0	0	0	0	0	- 5	- 6	-5	- 5	- 5	-5	- 5	- 6	-9	-5	- 5	- 6	-5	5
8/F	56.15	-5		-5	-5	-5	-5	-5	- 4		-5	- 6	-5	-5	-5	-5	0		0	0	0	0	0	0	0	0	0	0	-5	- 6	-5	-5	-5-	-15	- 5	-5	-6	-5	-5	-5	-5	-5
9/F	59.3	-5		5	-5	-5	-5	-5	- 3		-5	- 6	- 6	-5	-5	- 5	0		0	0	0	0	. 0	0	0	0	0	0	-5	- 6	-9	-5	- 6	- 5	- 5	-5	-5	-5	-5	- 8	- 3	-5
10/F	62.45	-5		5	-5	-5	- 5	- 5	- 4		- 5	- 6	- 4	-5	-5.	-5	0		0	0	0	0	0	0	0	0	0	0	-5	-5	-5	-5	-5-	-3-	-5	-8	-4	-5	- 5	- 4	-3	-5
11/F	65.6	-5		-5	-5-	-5	-5	-5	- 4		-5	- 6	- 6-	- 5	- 5	- 5	- 0		0	0	0	0	0	0	0	0	0	0	- 5	- 5	-3	-5	-5	46	- 6	-5	- 4	- 5	-5	-6	-5	- 5
12/F	68.75	-5		6	- 5	-5	-5	-5	- 4		-5	- 6	- 5	- 3	- 5	- 6	- 0		0	0	0	0	0	0	0	0	0	0	-5	- 5	5	-5	- 5	-5	- 5	-5	-4	-5	-5	8	-3	-5
13/F	71.9	-5		5	- 5	-5	- 5	-5.	- 4		-5	- 4	- 4	- 5	- 5	-5	0		0	0	0	0	0	0	0	0	. 0	0	-5	- 6	-5	-5	- 5	-5	- 5	-5	-5	-5	-5	4	-4	-5
14/F	75.05	-5		5	5	- 5	- 3	- 5	- 4		- 5.	5	- 5	- 5	-5	- 5	0		0	0	0	0	0	. 0	0	0	0	0	-5	- 6	- 5	- 5	8	- 3	ě	-5	- 6	- 5	- 5	- 5	-3	-5
15/F	78.2	- 5		5	5	- 5	- 6	5			. 5	15	. 5	- 5.	5		. 0		0	0	0	0	0	0	0	0	0	. 0	5.	- 8	- 8	. 5	- 5	- 5	- 8	5	5	- 5	- 5	- 5	- 3	5
16/F	81.35	-5		5	- 5	-6	- 5	- 5.	- 4		-5	-5.	- 6	-5	- 8	- 5	0		0	0	0	0	0	0	0	0	0	0	-5	-8-	- 5	- 5	-5	-5	- 5	-5.	-4:	-5.	-5	- 16-	-3	-5
17/F	84.5	-5.		5	8	- 5	- 8	- 8	- 6		- 5	- 5	- 5	- 5	- 5	- 5	0		0	0	0	0	0	0	0	0	0	0	-5	- 6	-5	- 5	- 5	15	- 8	- 5	-6	-5	- 5	- 15	-3	-5
18/F	87.65	-5		5	- 5	- 5	- 5	-5	- 4		- 5	-5	- 5	-5	- 5	- 5	0		0	0	0	0	0	0	0	.0	0	0	- 5	- 5	-5	-5	5	-5	- 5	-5	-5	-5	- 5	- 6	3	- 5
19/F	90.8	-9		5	-5	- 6	-5	-8	- 4		- 5	- 6	15	- 4	- 8	-6	- 0		0	0	0	. 0	0	0	0	0	0	0	-5	-6	-9	- 6	- 5	-45	- 6	- 8	15	- 6	- 5	- 15	- 4	-5
20/F	93.95	- 5		5	- 5	- 3	- 5	- 8	- 6		-5	5.	- 8	-5	- 5	- 6	- 0		0	0	0	0	0	0.	0	0	0	0	- 5	- 6	-5	- 5	5.	- 6	- 5	-6	- 6	-5	- 5	8	- 3	-5
21/F	97.1	-5		5	-5	-5.	-5	-5	- 4		-6	15	-5	-5	- 5	- 5	0		0	0	0	0	0	0	0	0	0	0	- 5	- 6	-5	-5	- 5	-5	- 6	-5	-5	-5	- 5	- 15	- 3	- 5
22/F	100.25	-5		4	-5	-4-	- 5	-5	- 4		-5	-	5	-5	-5	-5	- 0		0	0	0	0	0	0	0	0	. 0	0	-5	-6	-5	-5	-5	-6	- 6	-5	-6	-5	-5	- 6	-5	5

Tower A (High Zone) - by façade

Plane	Elevation				7								-			-7				Predited No	ise level, dB	(A)															7		
Floor	(mPD)	TAH-01-	1 TAH-01-	TAH-01-3	TAH-02-1	TAH-02-2	TAH-02-3	TAH-03-1	TAH-03-2	TAH-04-1	TAH-04-2	TAH-05-1	TAH-05-2	TAH-05-3	TAH-05-	TAH-06-	TAH-06-	2 TAH-06-	TAH-05-	TAH-06-5	TAH-07-1	TAH-07-2	TAH-07-3	TAH-08-1	TAH-08-2	TAH-08-3	TAH-08-4	TAH-08-5	TAH-09-1	TAH-09-2	TAH-09-3	TAH-10-1	TAH-10-2	TAH-11-1	TAH-11-2	TAH-12-1	TAH-12-2	TAH-12-	3 TAH-12-4
23/F	103.4	-6	- 5	-5	-5	-5	- 6	- 4	- 5	-5	- 8	-5	- 8	- 6	0	0	0	0	0	0	0	0	0	0	0	-5	- 6	-5	- 8	5	-5	- 6	-5	-4	-5	-5	- 18	- 3	-5
24/F	106.55	-5	- 5	5	- 5	- 5	- 5	- 5	- 5	- 5.	- 5	-5	- 5	-5	0	0	0	0	0	0	0	0	0	0	0	- 5	- 6	-5	- 5	8	- 6	å	- 5	- 6	-5	- 5	- 8	-3	- 5
25/F	109.7	- 6	- 5	5	- 5	- 6	- 8	-6	- 5.	15	.5	- 6	- 6	- 6	0	0	0	0	0	0	0	0	0	0	0	- 5	- 5	- 5.	- 5	å	- 6	- 6	- 4	-5.	-5	-5.	6	- 3	- 5
26/F	112.85	-6	- 5	-	- 6	- 6	-8	-5	-5	- 16	- 1	- 4	-5	-6.	0	.0	0	0	. 0	0	0	0	0	0	0	- 6	-6	-6	- 5	- 8	-6	- 6	- 8	- 4	-5	- 5	- 6	-4	- 5
27/F	116	- 6	- 5	S	-5	-5	-6	-5	- 5.	- 5	- 15	-5	- 5	- 6	.0	0	0	0	0	0	0.	.0	0	0	0	-5	- 6	-5	- 5	8.	- 6.	- 5	-6	- 4	-5	- 5.	- 6	-3	-5
28/F	119.15	-5	- 5	5	-6	-5	-5	-5	- 8	- 5	-35	-5	- 5	-5	0	0	0	0	0	0	0	0	0	0	0	- 5	- 5	-5	-5	5	-5	- 5	-5	-5	-5	- 8	- 6	-5	- 5
29/F	122.3	-5	- 5	-5	-6-	-5	-8	-6	-5	16	-6	- 4	-8	- 6	0	0	0	0	0	0	0	0	.0	0	0	-5	- 6	-5	- 6	-3-	45	- 6	-8	16	-6	-6	- 6	-3	- 5
30/F	125.45	-5	- 6.	-5-	- 5	- 6	-6	-5	-5	16.	- 15	- 5	-6	- 4	0	0	0	0	0	0	0	0	0	0	0	1-5	- 8	-5	-5	6.	- 6	- 8	-6	-6	-5	-5	- 16	- 3	-5
31/F	128.6	-5	- 5	-5-	-5	- 8.	-5	- 6	- 5	-5	-5	- 6	-5	-5	. 0	0	0	0	0	.0	0	0	0	0	0	-5-	-8	5	-5	- 5	- 5	- 6	-5	-5	- 6 -	- 15	-15	- 3	- 5
32/F	131.75	-5	- 5	-5	1.0	-6	-6	- 5	- 5	151	- 6	- 6	-5	- 6	0	0	0	0	0	0	0	-0	.0	0	0	-5	-6	-5	-5	-5	-15	- 6	-6	- 46	-5	- 5	- 6	15	-5
33/F	134.9	-6	- 6	5	- a	- 4	-6	-6	-5:	-6	- 16	- 8	-5	-6	0	0	0	0	0	0	0	0	0	0	0	- 6	- 8	-5	-6	-3	- 4	8	-5	- 4	-6	-6	- 8	- 4	-5
34/F	138.05	-5	- 4	-5	-5	- 5	- 6	-5	-5	- 5	- 6	- 5	- 5	-5	0	0	. 0	- 0	0	0	0	0	0	0	0	- 5	- 8	-5	- 5	- 5	-5	- 6	- 5	- 6	- 5	-5	15	- 3	- 5

Floor	Elevation						A series				A				A Server				ed Noise lev						Acres 1	And the same			Value of					d		
PIOUR	(mPD)	TB-01-1	TB-01-2	TB-01-3	TB-02-1	TB-02-2	TB-02-3	TB-03-1	TB-03-2	TB-04-1	T8-04-2	TB-05-1	TB-05-2	TB-05-3	TB-05-4	TB-06-1	T8-06-2	T8-06-3	TB-06-4	TB-06-5	TB-07-1	TB-07-2	TB-02-3	TB-08-1	TB-08-2	TB-08-3	TB-09-1	TB-09-2	TB-09-3	TB-10-1	TB-10-2	TB-11-1	TB-11-2	TB-12-1	T8-12-2	TB-12-3
1/F	34.1	-5	- 6	-5	-6.	- 5	-5	-6	- 5	- 6	-5	- 6	-5	- 8	0	0	0	0	0	0	0	0	0	- 6	- 6	- 5	- 4	-4	- 5	- 5	-8	-6	-5	4	-6	-5
2/F	37.25	- 4	- 4	-1	-5	-5	- 6	-5	- 5	- 4	- 6	-5	-5	-5	0	0	0	0	0	0	0	0	0	- 4	- 4	-5	- 4	-8	-5	- 4	-6	-5	- 5	-9-	-5	-5
3/F	40.4	-5	-5	- 5	-5	- 5	- 5	-5	-5	-5	- 3	-5	-5	-5	0	0	0	0	0	0	0	0	0	- (5	5	- 6	- 5	-5	- 5	- 5	- 15	- 5	-5	-5	-5	- 5
4/F	43,55	-4	- 5	- 5	-5	- 6	-5	-6	- 6	- 5	- 5	- 6	- 5	- 6	0	0	0	0	0	0	0	0	0	-5	- 4	- 5	- 5	-5	-5	- 4	- 45	- 6	-5	- 15	-5	-5
5/F	46.7	-6	- 5	- 5	-5	-5	-6	-5	-5	- 5	15	-6	- 5	-5	0	0	0	0	0	0	0	0	0	- 3	-5	- 5	8	-5	-5	- 5	16	- 6	- 6	145	-5	-5
6/F	49.85	- 5	- 5	5	-9-	- 6	-5	-5	- 5	15.	- (5-	-5	- 5	- 5	0	0	0	0	0	0	0	0	0	- 15	- 6	- 5	- 5	-5	- 5	5-	-15	- 8	- 5	- 5	-5	- 5
7/F	53	-5	-5	-5	-5	-5	-5	-5	-5	5	-5	15	-5	-5	0	.0	0	0	0	0	0	0	0	-3	- 5	- 5	- 4	-5	-5	-5	-5	- 5	-5	4	-5	-5
8/F	56.15	-5	- 6	-9	-5	-5	-5	-5	- 5	- 5	15	- 5	- 15	4 -	0	0	0.	0	0	0	0	0	0	-6	- 6	- 5	- 6	5	-5	8	-45	- 6	-5	-5	-5	-5-
9/4	59.3	- 4	- 8	-8	-5	- 8	- 8	- 3	-5.	- 5	- 15	-5	-5	- 6	0	0	0	0	0	0	0	0	0	-3-	-5	-8	- 6	-4	- 8		-8	- 8	- 8	- 6	- 5	-5
10/F	62.45	-5	- 5	5	- 5	- 5	5	-5	-5	5	- 5	-5	- 5	-5	0	0	0	0	0	0	0	0	0	- 35	- 5	- 5	- 5	-5	-5	- 5	-5.	- 5	-5	- 5	-5	- 5
11/F	65.6	-5	-6	-5	8.	- 6	-6:	- 6	- 5	6.	- 6	- 6	- 5	- 6	0	0	0	0	0	0	0	0	0	- 6	- 4	- 6	. 6	-6.	- 5	-5	-48	- 6	-6	-6	- 6	- 5
12/F	68.75	-5	- 6	-5	- 6	16	-6	-4	-5	- 6	- 15	-5	-5	- 4	0	0	0	0	0	0	0	0	0	-3	-5	-5	- 6	-5	-5	- 5	- 4	- 6	- 6	-4-	-5	-5
13/F	71.9	-5	- 5	-5	-5	-5	-5	-5	-5	- 15	- 6	-5	- 5	ă	0	0	0	0	0	0	0	0	0	-5	- 5	- 5	- 8	-5	-5	-5.	-5	-5	-5	-5	-5	-5
14/F	75.05	- 6	- 5	-5	4	- 6	-5	- 6	-6	161	- 15	- 5	- 5	- 4	0	0	0	0	0	0	0	0	0	- 6	- 6	- 6	- 6	- 5	- 6	-6:	- 9	- 6	-6	-2-	- 6	. 5
15/F	78.2	-5	- 6	5	- 6	- 5	-5	-5	- 5	-5	-3.	-5.	-5	- 4	0	0	0	0	0	0	0	0	0	-5.	- 5	-5	- 6	-5	-5.	-6.	- 5.	- 6	5	-1-	-5	-5
16/F	81.35	-6	- 6	S	- 6	- 6	-5	-6	-6	- 5	15	-5-	-6	- 6	0	0	0	0	0	0	0	0	0	15	-6	-6	- 6	-5	-5	- 6	15	- 6	- 5	- 6	-5	-5
17/F	84.5	- 5	- 6	-5	- 5	- 6	-5	- 5	- 5	- 6	- 5	-3-	- 5	- 5	0	0	0	0	0	0	0	0	0	-5	- 4	- 5	- 5	- 4	-5	- 4	-5	- 4	-5	-5	-5	-5
18/F	87.65	- 6	5	- 5	- 5	- 5	- 5	-5	5	- 5	- 3.	-5	- 5	- 5	0	0	0	0	0	. 0	0	0	0	-8	- 8	-5	- 6	-5	-5	- 5	-5	- 6	-5	-5	-5	5
19/F	90.8	- 4	- 6	- 5	- 6	- 6	- 9	- 6	- 5	- 6	- 5	- 6	-6	-8	0	0	0	0	0	0	0	0	0	-5	- 4	-5	- 4	-9	-5	- 6.	-5	- 8	-6	- 4	-3	-5
20/F	93.95	-5	- 5	-5-	- 8	-5	-5	-5	-5-	-5	-5	-5	-5	-5	0	0	0	0	0	0	0	0	0	-5	-5	- 5	- 4	-5	-5	- 5	-15	- 5	-5	-3	-5	-5-
21/F	97.1	- 5	- 6	- 5	- 8	- 6	-5	-5	- 5	- 16	35	-5	-5	- 6	0	0	0	0	0	0	0	0	0	- 5	- 6	5	6	- 5	- 5	- 5	18	- 6	-6	-8	-5	-5
22/F	100.25	- 5	- 5	-5	-5	-5	- 6	-5	-5	- 5	- 6	-5	- 4	- 6	0	0	0	0	0	0	0	0	0	-6	- 4	- 5	- 4	- 6	-5	- 4	-6	- 5	-6	- 4	-5	-5
23/F	103.4	-5	- 5	-5-	-5	-5	-5	-5	-5	-5	-5	- 5	-5	-5	0	0	0	0	0	0	0	0	0	-5-	- 5	- 5	-5	-5	-5	-5-	-5	- 5	- 5	-5	-5	-5
24/F	106.55	-5	- 6	5	- 2	- 6	-5	-8	- 6	- 5	4.	-5	-5	- 6	0	0	0	0	0	0	0	0	0	- 6	- 4	- 5	- 5	- 2	-5	- 5	- 15	- 6	-5	-5	-5	- 5
25/F	109.7	- 4	- 5	-5	-5	-5	-6	- 5	- 5	- 5		-5	- 6	- 6	0	0	0	0	0	0	0	0	0	. 4	- 5	-5	- 6	-6	- 5	- 6	-45	- 6	-6	-4	- 6	-5
26/F	112.85	- 5	- 5	-5-	-5	- 5	-5	-5	- 5	- 5	-3-	-3	-5	-5	0	0	0	0	.0	0	0	0	0	- 3	-8-	- 5	- 5	- 5	- 5	- 5.	- 3	- 6	-5	-5	-5	- 5
27/F	116	- 5	- 5	5	- 5	-5	-5	-5	- 5	- 5	.5	- 5	-5	- 5	0	0	0	0	0	0	0	0	0	-5	- 6	- 5	- 5	- 5	- 5	- 5	15	- 6	-5	-5	-5	-5
28/F	119.15	-5	- 5	-5	-6	-6	-6.	. 5	- 5	- 15	3-	- 5	-5	- 8	0	0	0	0	0	- 0	0	0	0	- 4	- 9	-5	- 6	-5	- 5	- 6	-5	- 6	-6	-4	-5	-5
29/F	122.3	-5	- 6	-5	- 5	4	-3.	-5	- 5	- 6	- 3	-5	- 5	- 4	0	0	0	0	0	0	0	0	0	-3-	-5	-5	-8	-5	- 5	- 6.	-5	- 5	-5	-6	-5	- 5
30/F	125.45	-5	-5	5	-5	- 5	-5	-5	- 5	- 5	-5	-5	-5	- 5	0	0	0	0	0	.0	0	0	0	-5	- 5	- 5	- 5	-5	-5	- 5	-5	- 5	-5	-5	-5	-5
31/F	128.6	- 6	- 5	-5:	- 6	-6	-6	-6	-5	- 4	-5	- 4	-5	- 8	0	0	0	0	0	0	0	0	0	-6	4	- 5	- 6	-5	-5	-5	-6	- 6	-5	-4-	-5	-5
32/F	131.75	-3	- 5	-5	-5	-5	-5	-5	-5	- 3	- 5	- 5	- 3	- 4	0	0	0	0	0	0	0	0	0	5	-5	- 5	- 5	-5	-5	-5	-6	-5	-5	-5	-5	-5
33/F	134.9	-5	- 5	-5	-5	-5	-5	-5	-5	-5	5	-5	- 5	-5	0	0	0	0	0	0	0	0	0	-5	-5-	- 5	- 8	-5	-5	-5-	-5-	- 5	-5	-5	-5	-5-
34/F	138.05	-3	-4	-5-	-5-	-5	-5	-5	-5	- 5	- 5	- 5	-5	-5	0	0	0	0	0	0	0	0	0	-5	- 5	- 5	- 6	-5	-5	-5-	5	- 6	5	- 4	5	-5

ID	Description	Corre	ction
240	Normal Windows	0	68
AW:	Acquatus: Mindows	.5	- 46

Predicted Traffic Noise Level, dB(A) - (b) Mitigated Scenario: Acoustic Windows

Tower A (Low Zone) - by façade

Stere	Elevation						A. A. A.											Marie V		Predited No	isé level, dis	A)																	100
Floor	(mPD)	TAL-01-1	TAL-01-2	TAL-01-3	TAL-02-1	TAL-02-2	TAL-02-3	TAL-03-1	TAL-03-2	TAL-04-1	TAL-04-2	TAL-05-1	TAL-05-2	TAL-05-3	TAL-05-4	TAL-06-1	TA1-06-2	TAL-06-3	TAL-06-4	TAL-06-5	TAL-07-1	TAL-07-2	TAL-07-3	TAL-08-1	TAL-08-2	TAL-08-3	TAL-08-4	TAL-08-5	TAL-09-1	TAL-09-2	TAL-10-1	TAL-10-2	TAL-11-1	TAL-21-2	TAL-12-1	TAL-12-2	TAL-13-1	TAL-13-2	TAL-13-3
1/F	34.1	- 79	72	72	- 72	71	71	71	71	71	71	71	71	71	66	68	70	-60-	56	45	47	50	50	51	56	63	64	65	66	67	68	69	70	71	- 32	72	73	73	73
2/F	37.25	- 22	72.	7.1	71	71	.71	71	71	71	71.	70	70	70	66	69	70	61	57	50	49	52	52	53	57	65	66	67	68	(3)	70	71	.71	72	31	72	73	71	- 73
3/F	40.4	- 11-	72	71.	TI	71.	-71	71	71	70	70	70	70	70	67	69	70	64	58	52	- 51	55	-22	55	58	67	.68	69	70	71	71	71	71.	72	72	72	73.	73	73
A/F	45.55	-n	71	71	71	71	71	70	70	70	70	70	70	70	67	69	70	65	59	- 54	53	58	58	- 58	60	68	69	70	70	71	71	71	71	72	72	72	72	73	73
5/F	46.7	72	71	71	71	70	70	70	70	70	70	70	70	70	- 66	68	70	65	59	55	54	59	59	60	61	69	70	70	21	71	71	71	71	72	72	72	72	73	23
6/F	49.85	72	71.	71.	70	70	70	70	70	70	70	70	70	69	66	68	70	65	60	56	56	59	60	62	63	70	70	70	n	71	73.	71	71	71	72	72	72	72	72
7/F	53	- 72 -	71	70	70	70	70	70	70	70	70	69	69	69	66	68	70	66	60	56	- 56	59	60	63	64	70	70	70	- 71	71	71	71	71	71	71	72	72	72	72
8/F	56.15	72	71	70	70	70	70	70	70	63	69	69	69	65	66	68	68	66	60	56	57	60	60	63	64	70	70	70	70	71	71.	71	71	71.	71	71	72	72	72
9/F	59.3	71	70	70	70	70	70	70	69	69	69	69	69	63	65	68	68	66	60	. 57	57	60	60	64	65	70	70	70	70	71	71	71	71	71	71	71	72	72	72
10/9	62.45	- 0	70	70	70	70	69	69	69	69	69	69	69	69	65	67	69	66	60	57	57	60	61	64	65	70	. 70	70	70	70	71	71	71	71	71	71	71	72	72
11/F	65.6	-71	70	70	70	69	69	69	69	69	69	69	69	69	65	67	69	-66	60	57	57	60	61	64	65	69	70	70	70	70	70	70	71	71	- 71	71	71	72	72
12/9	68.75	71	70	70	60	69	69	69	69	69	69	69	69	68	65	67	69	66	60	57	57	60	61	6.4	65	69	70	70	70	70	70	70	70	71	71	7.1	71	71	71
13/F	71.9	- 71	70	69	69	69	69	69	69	69	69	60	68	68	65	67	68	66	60	57	57	60	61	64	65	69	69	70	70	70	70	70	70	70	70	75	71	73	71
14/F	75,05	n-	70	69	69	69	69	69	69	69	69	68	68	68	65	67	68	66	60	57	57	60	61	63	65	69	69	70	70	70	70	70	70	70	70	70	71	71	71
15/F	78.2	70	69	69	69	69	69	69	69	69	- 68	68	- 68	- 68	65	67	83	66	60	57	57	60	61	64	65	69	69	69	70	70	70	70	70	70	70	70	73	71	71
16/F	81.35	70	69	69	69	69	69	69	68	68	.68	88	68	68	64	67	68	65	60	58	58	60	61	64	65-	69	69	69	69	70	70	70	70	70	70	70	70	71	71
17/F	84.5	70	69	69	69	69	68	68	68	58	68	68	68	68	- 64	66	- 68	65	61	58	58	60	61	64	65	69	69	69	69	70	70	70	70	70	70	70	70	71	71
18/F	87,65	70	- 69	69	- 68	68	68	68	68	68	68	68	68	68	64	66	- 68	65	61	58	58	60	61	64	65	69	69	69	6.9	69	70	70	70	70	70	70	70	71	71
19/F	90.8	70	69	68	- 68	68	68	68	68	68	68	68	68	68	64	66	68	65	61	58	58	60	61	64	65	69	69	69	69	(c)	69	69	69	70	70	70	70	70	70
20/F	93.95	70	69	68	68	68	68	68	68	58.	68	68	68	58	64	66	67	65	61	58	58	60	61	64	65	68	69	69	69	60	69	69	69	69	70	70	70	70	70
21/F	97.1	69	- 68	68	- 68	68	- 68	-68	68	- 68	68	67	67	67	64	- 66	67	65	61	58	58	60	61	64	65	68	69	69	69	69	69	69	60	69	69	70	70	- 70	70
22/F	100.25	69	- 48	68	- 68	. 68	68	:68	68	- 68	67	67	67	67	64	66	67	65	61	58	58	60	61	64	65	68	68	69	69	(0)	69	. 69	69	68	69	6/9	70	70	70
	in	69	68	68	68	68	68	68	68	68	67	67	67	67	64	66	67	60	36	45	47	50	50	51	56	63	64	65	66	67	68	69	69	69	69	69	70	70	70
- 0	lax.	73	2	72	12	25-	72	71	- 31	73.	71	71	71	71	67	69	70	- 66	61	58	58	60	61	64	65	70	70	70	- 71	7).	71	71	71	- 72	72	72	73	73	21

Tower A (High Zone) - by façade

****	Elevation											V							P	edited No.	e level, dill	A)																	
Floor	(mPD)	TAH-01-1	TAH-01-2	TAH-01-3	TAH-02-1	TAH-02-2	TAH-02-3	TAH-03-1	TAH-03-2	TAH-04-1	TAH-04-I	TAH-05-1	TAH-05-2	TAH-05-3	TAH-05-4	TAH-06-1	TAH-06-2	TAH-06-3	TAH-05-4	TAH-06-5	TAH-67-1	TAH-07-2	TAH-07-3	TAH-08-1	TAH-05-2	TAH-08-3	TAH-08-4	TAH-08-5	TAH-09-1	TAH-09-2	TAH-05-3	TAH-10-1	TAH-10-2	TAH-11-1	TAH-11-2	TAH-12-1	TAH-12-2	TAH-12-3	TAH-12-4
23/F	103.4	69	-68	68	- 68	68	- 68	68	67	67	67	67	67	67	64	66	67	65	61	- 58	- 38	60	61	64	65	68	68	69	69	60	69	69	69	69	69	69	70	70	70
24/F	106.55	69	- 68	68	68	- 68	67	67	67	67	67	67	67	67	64	66	67	65	61	58	58	60	61	64	65	68	68	68	69	69	69	69	69	69	69	69	69	70	70
25/F	109.7	69	68	68	- 68	67	67	67	67	67	67	67	67	67	63	65	67	65	61	50	59	60	61	64	65	68	68	68	69	69	69	69	69	69	69	69	69	70	70
26/F	112.85	69	68	68	67	67	67	67	67	67	67	67	67	67	63	65	67	65	61	59	59	60	61	64	65	68	68	68	- 68	69	69	69	69	68	60	69	69	70	70
27/F	116	69	68	68	67	67	67	67	67	57	67	67	67	67	63	65.	67	65	61	59	59	60	61	64	65	68	68	68	68	68	68	69	69	69	69	69	69	679	70
28/F	119.15	69	68	67	- 67	67	67	67	67	67	67	67	67	67	63	- 65	67	- 65	61	59	- 59	61	- 61	64	65	68	68	68	68	- 68	68	68	69	69	69	69	69	69	69
29/F	122.3	69	68	67	67	67	67	67	67	67	67	67	67	67	63	65	66	65	61	59	59	61	61	64	65	68	68	68	68	68	68	. 68	68	68	69	69	69	69	69
30/F	125.45		67	67	67	67	67	67	67	67	67	67	67	- 66	68	65.	66	65	61	59	59	61	61.	64	65	68	- 68	68	68	68	68	- 68	68	68	. 33	60	f2)	69	69
31/F	128.6	68	67	67	67	67	67	67	67	67	67	66	66	- 66	63	65	66	65	61	59	- 59	61	61	64	65	68	68	68	68	68	68	- 68	68	68	68	68	69	69	69
32/F	131.75	- 68	67	67	67	67	67	67	67	67	66	66	66	66	63	65	66	65	61	59	59	61	61	64	65	67	68	68	68	68	68	-83	68	88	88	68	69	69	69
33/F	134.9	- 68	67	67	67	67	67	67	66	166	66	66-	66	66	63	65	66.	65	61	59	60	61	61	64	65-	67	68	68	68	68	68	-68	68	88	33	68	69	69	69
34/F	138.05	68	- 67	67	.67	67	- 56	- 66	- 66	66	- 66	- 66	66	66	63	- 65	- 66	65	61	60	60	61	61	64	65	67	67	-68	- 68	68	68	- 68	- 68	- 68	- 68	68	68	69	69
																																						0 -	
- 1	nin	68	67	67	67	67	66	66	66	66	66	- 66	66	65	63	65	66.	65	61	.58	38	60	61.	64	65	67	67	68	68	68	68	68	68	68	68	68	68	69	69
-	188	69	68	6-8	- 68	68	68	68	67	67	67	67	67	67	64	66	67	65	61	60	60	61	61	64	65	68	68	69	69	69	69	69	69	69	69	69	70	70	70

	loor.	Devation									S	A							Predite	ed Noise lev	H, dB(A)																
Total Tota	1000	(mPO)	TB-01-1	TB-01-2	TB-01-3	T8-02-1	TB-02-2	TB-02-1	T8-03-1	TB-03-2	18-04-1	T8-04-2	TB-05-1	18-05-2	TB-05-3	TB-05-4	TB-06-1	T8-06-2	T8-06-3	TB-06-4	TB-06-5	TB-07-1	TB-07-2	18-07-9	T6-06-1	T8-08-2	TB-08-3	TB-09-1	TB-09-2	TB-09-3	TB-10-1	TB-10-2	TB-11-1	18-11-2	TB-12-1	TB-12-2	18-
T	/F	34.1	34 -	- 71	71	71	- 71 -	71	71	70	70	70	70	7.1	71	56	66	69	39	57	56	- 36	55	46	- 61	62	62	- 66	67	69	70	72	72	- 71	73.	74	7
Y 48.55 77 11 70 7	T I	37.25	74	-71	71	71	71	70	70	70	70	70	70	70	70	58	66	69	60	. 57	57	56	55	47	63	65	65	69	70	71	71	972	72	71	73	74	1
7	ΑF.	40.4	74	- 23	71	75	70	70	70	70	70	70	70	70	70	59	66	69	60	57	57	56	-55	48	66	67	66	70	72	71	71	72	72	7.5	78	73	
T 49.55; 72 70 70 70 70 70 70 70 70 70 70 70 70 70	F	43.55	73	- 71	71	70	70	70	70	70	70	70	70	70	70	61	66	61	61	58	57	56	56	49	67	68	68	70	71	71	71	72	72	72	73	73	
T 531 71 77 70 70 69 66 66 66 66 66 66 66 66 66 66 66 66	F	46.7	71	70	70	70	70	70	70	70	- 69	70	69	70	70	63	66	69	61	58	57	56	56	- 51	68	69	68	71	71	71	71	72	72	-72	772	73	
7 59.15 72 70 70 60 69 60 69 60 69 69 69 69 69 69 69 69 69 69 69 69 69	1	49.85	73	70	70	70	70	70	69	69	59	-69	69	70	70	63	67	60	62	58	57	57	57	53	69	69	68	71	71	71	71	71	72	72	72	73	
T \$1.1 \$7. \$7. \$7. \$7. \$7. \$7. \$7. \$7. \$7. \$7.	F	53	73	70	70	70	70	69	69	69	65	69	69	70	63	64	67	69	62	58	58	57	.57	- 54	69	60	68	70	71	71	71	71	71	72	72	73	
R C 4.45 72 69 69 69 69 69 68 69 68 80 68 68 68 68 68 68 68 68 68 68 68 68 68	F	56.15	72	70	70	69	69	69	69	69	59	69	69	69	69	64	67	68	63	59	- 51	57	58	55	69	69	68	70	70	71	71	71	71	72	72	72	
7	F	59.3	72	70	69	69	69	69	69	69	63	69	69	69	69	64	67	60	63	59	38	58	58	56	69	69	68	70	70	70	71	71	71	71	n	72	
T	VF.	62.45	72	69	69	69	69	69	69	68	68	69	68	69	69	64	67	65	64	59	58	58	58	56	69	69	68	70	70	70	70	71	71	71	72	72	
## 71.9 71.9 72. 69 69 69 69 69 69 68 58 68 68 68 68 68 68 68 68 68 68 68 68 68	/F	65.6	72	69	69	69	69	69	68	68	68	68	68	69	69	64	67	63	64	60	55	. 58	59	57	68	69	68	70	70	70	70	71	71	. 71	71.	72	
N 75.05 13 69 69 65 68 67 75 75 78 88 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 69 79 79 79 79 79 79 79 79 79 79 7	/F	68.75	72	69	69	69	69	- 68	68	68	58	68	68	69	69	64	67	68	65	60	59	59	59	58	68	69	68	70	70	70	70	70	73	71	71	72	
F 74.7 11 68 68 68 68 68 68 67 57 67 58 68 66 65 68 68 67 70	/F	71.9	77	69	69	69	68	.68	68	68	58	68	68	68	68	- 64	67	63	65	60	59	59	60	58:	68	69	68	70	70	70	70	70	70	71	71	72	
## 31.55 71 65 65 65 65 65 65 65 6	19	75.05	- 71	69	69	68	68	68	- 68	68	68	.68	68	68	68	64	67	68	65	61	60	60	61	59	6.8	69	67	70	70	70	.70	70	70	31	71	71	Т
## 44.5 12 68 68 68 68 67 67 67 67	F	78.7	The second	68	68.	- 88	68	68	68	67	67	67	67	68	68	64	67	68	65	61	60	60	61	60	68	- 68	67	69	69	70	70	70	70	71	71	TI	
7	Ŧ	81.35	- 71	68	68	- 68	68	58	67	67	57	67	67	68	68	64	66	68	66	62	61	61	62	60	68	68	67	69	69	69	70	70	70	70	71	73	
T 93.5 12 68 68 68 67 67 67 67 67 67 67 67 67 67 67 67 67	F	84.5	71	- 68	68	68	68	67	67	67	67	67	67	. 68	68	64	66	68	66	62	61	61	62	60	6.8	68	67	69	69	69	(9)	70	70	70	71	71	Т
7 91.55 11 05 68 67 67 67 67 67 67 67 67 67 67 67 67 67	7	87.65	TI	68	K9.	- 68	67	67	67	67	57	67	67	68	68	63	66	68	- 66	62	61	61	62	60	5.N	68	67	69	69	69	69	70	70	70	70	71	
7 97.1 79 65 67 67 67 67 67 67 67 68 66 66 66 66 66 67 67 67 68 67 67 68 68 68 68 68 69 69 79 79 79 79 79 79 79 79 79 79 79 79 79	Ψ.	90.8	71	68	68	- 68	67	67	67	67	67	57	67	67	67	63	66	68	66	62	62	61	62	61	68	- 88	67	69	69	69	69	60	70	70	70	-71	Т
## 19025 70 68 67 67 67 67 67 67 68 66 66 66 66 67 67 67 68 68 68 68 68 68 68 68 68 68 68 68 68	Œ.	93.95	71	- 68	68	67	67	67	67	67	67	67	67	67	67	63	66	68	66	62	62	62	62	61	6.8	68	67	69	69	69	69	69	69	70	70	71	Т
## 1914 70 67 67 67 67 67 67 67 67 67 67 67 67 67	/F	97.1	.70	68	67	67	67	67	67	67	66	67	67	67	67	63	66	67	66	63	62	62	67	61	67	68	67	69	69	69	69	69	69	70	70	71	
7 105.55 70 67 67 67 67 67 67 67 67 67 67 67 67 67	F .	100.25	70	48	67	67	67	67	67	66	56	- 67	66	67	67	63	- 66	67	66	63	62	62	62	61	67	- 68	67	69	69	69	60	69	69	70	79	70	
(7) 1100.7 70 67 67 67 67 67 67 67 67 67 68 66 66 57 67 67 67 67 67 67 68 68 68 69 59 59 70 70 70 (7) 112.8 70 67 67 67 67 66 68 68 66 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 66 66 66 67 67 67 67 67 67 67 67 67 67 67 66 66 66 66 67 67 63 65 66 67 67 67 66 68 68 66 67 67 63 65 67 66 66 68 68 69 70	/F		70	67		67	67	67	67	66	66	-66	66	67	67	63	65	67	66	63	62	61	62	61	67	- 68	66	69	68	69	69	69	69	70	70	70	I
7 1125 70 67 67 67 67 67 68 68 68 68 69 69 70 70 61 65 70 61 65 66 66 66 67 67 67 67 68 68 68 68 69 70 70 70 70 70 70 70 70 70 70 70 70 70	/F	106.55	70	67	67	67	67	67	66	66	66	- (6	66	67	67	63	65	67	66	62	61	61	62	61	67	67	66	68	68	68	(3)	69	69	69	70	70	
7 116 79 67 67 67 67 66 66 66 66 66 66 66 66 66	/F	109.7	70	67	67	67	67	66	66	66	66	- 66	66	67	67	63	65	67	66	62	61	61	62	61	67	67	66	68	68	68	68	69	69	69	70	70	
7 11315 70 87 87 87 87 88 88 88	15	112.85	70	67	67	67	67	66	66	66	66	- 66	66	67	67	63	65	57	66	62	51	61	62	61	67	67	66	- 68	68	68	58	69	69	69	69	70	1
## 1223 69 67 67 66 66 66 66 66 66 66 66 66 66 66	/ F	116	70	67	67	67	66	66	66	66	66	16	66	67	67	63	65	67	66	62	61	61	62	61	67	67	66	68	68	68	68	68	69	60	69	70	Г
T 115.45 69 67 67 66 66 66 66 66 66 66 66 66 66 66	/F	119.15	70	67	67	67	66	66	- 56	66	66	66	66	67	67	63	65	67	66	67	61	61.	63	61	67	67	66	68	68	68	- 68	68	69	69	69	70	1
7 1386 69 67 66 66 66 66 66 66 66 66 66 66 66 66	VF	122.3	69	67	67	66	66	66	66	66	66	- 66	66	67	66	62.	65	67	66	62	61	61	62.	61.	67	67	66	68	68	68	58	68	- 68	69	69	70	
7 131.75 199 67 66 66 66 66 66 66 66 66 66 66 66 66	VF .	125.45	69	67	67	66	66	.66	66	66	66	66	66	66	66	62	65	67	66	62	61	61	62	61	67	67	66	- 68	68	68	.68	- 68	68	69	69	70	
7 1349 59 66 56 66 66 66 66 66 66 66 66 66 66 66	14	128.6	69	67	66	66	66	66	66	66	66	- 66	66	66	66	62	65	66	65	62	61	61	62	61	67	67	66	68	68	68	58	68	68	69	69	69	Т
	/F	131.75	169	67	66	66	- 66	96	65	66	66	16	66	- 66	- 66	62	65	66	65	62	65	61	62	61	66	67	- 66	- 68	68	68	68	68	- 68	199	69	69	
9 138.05 69 66 66 66 66 66 66 66 66 66 66 66 66	VF:			- 66	65	66	66	66	- 66	66	66	- 66	66	66	66	62	65	65	65	62	61	61	62	61	66	67	66	68	68	68	68	68	- 68	69	69	69	\mathbf{I}
	y#	138.05	69	- 66	66	66	66	- 66	66	66	66	16	66	66	66	62	64	66	65	62	61	61	62	61	66	67	65	68	67	67	68	68	68	68	69	69	
	- 9	iin	69	66	66	66	66	- 66	- 66	66	- 66	- 66	66	66	66	56	64	- 66	59	57	56	56	- 55	46	61	62	62	66	67	67	- 68	68	68	68	69	69	I
	6	18.5	2.0	71	71	799	779	1774	27	70	70	70	70	77	71	2.6	67	679	66		67	27.	275.	2.5	2.00	65	6.00	. 799	77	277	71	77	77	71	. 77	34	4

Predicted Traffic Noise Level, dB(A) - (b) Mitigated Scenario: Acoustic Windows

Tower A (Low Zone) - by flat

	Elevation	Prodited Notice level, d8(A)												
1400k	(mPD)	TAU-01	TAL-02	TAL-03	TAL-04	TALOS	TAL-06	TAL-07	TAL-08	TAL-09	TAL-10	TAL-11	TAL-1Z	TAI-13
1/F	34.1	- 78	72	- 11	71	71	70	50	65	67	69	71	72	73
2/F	37.25		21	21	71	70	70	52	67	69	71.	72	72	я
3/F	40.4	73	71	TI II	70.	70	70	55	69	71	n	72	n n	7)
√F	45.55	72	71	70	70	70	70	58	70	71	71	72	- 11	73
/F	46.7	72	31	70	70	70	20	59	70	n	71	72	- 11	73
/F	49.85	TE	70	70	70	70	70	60	70	71	71.	71	(11)	72
/F	53	72	70	70	70	fi)	70	60	70	71	73	71	- 11	- 72
Æ	56.15	72	70	70	68	69	69	60	70	11	n	71	71	72
/F	59.3	TI .	70	70	69	69	60	60	70	.71	71	71	71	72
0/#	62.45	71	70	69	68	69	69	61	.70	70	71	71	п	72
JF.	65.6	71	70	69	10	69	69	61	70	70	70	71	71	72
1/5	68.75	71.	69	69	69	69	69	61	70	70	70	71	71	71
J/F	71.9	71	69	69	60	69	68	61	70	70	70	70	71	71
4/F	75.05	.7%	69	69	59	68	68	61	70	70	70	70	70	71
/F	78.2	70	69	69	65	68	68	61	69	70	70	70	70	71
E/F	81.35	70	69	69	68	68	68	61	69	70	70	70	70	71
7/4	84.5	70	69	68	58.	68	68	61	60	70	70	70	70	- 71
VF-	87.65	70	68	68	68	68	68	61	60	- 69	70	70	70	71
9/F	90.8	70	68	68	68	68	68	61	60	65	69	70	70	70
0/F	93.95	70	68	68	68.	68	67	61	69	69	69	(6)	70	70
1/F	97.1	69	68	68	- 68	62	67	63	60	- 69	69	69	70	70
2/F	100.25	63	:68	68	68	67	67	61	69	69	69	69	69	20
	nin	69	68	68	58	67	67	50	65	67	69	69	69	70
- 10	nax	78	72	73	71	71	20	61	70	71	71	72	22	73

Tower A (High Zone) - by flat

Hoor	Elevation	Predited Native level, dB(A)												
HOSF	(mPD)	7AH-01	TAH-02	TAH-03	TAH-04	TAH-05	TAH-06	TAH-07	TAH-08	TAN-09	TAH-10	TAH-11	TAH-12	
3/F	103.4	69	68	68	67	67	67	61	69	60	69	69	70	
1/6	106.55	69	- 68	67.	67	67	67	61	68	60	69	69	70	
/F	109.7	69	68	67	67	67	67	61	68	69	69	69	70	
14	112.85	69	67	67	67	67	67	61	68	69	(9)	69	70	
/F	116	69	- 67	67	67	67	67	61	68	68	69	69	70	
14	119.15	69	67	67	67	67	67	61	68	68	60	69	69	
T-	122.3	69	67	67	67	67	66	61	68	68	68	69	69	
/F	125.45	- 68	67	67.	67	67	66	61	- 68	68	68	- 88	69	
/F	128.6	- 68	67	67	67	66	66	61	68	68	66	68	69	
/F	131.75	68	67	67	67	66	66	61	- 68	68	66	88	69	
/F	134.9	68	67	67	66	66	66	61	68	68	68	68	69	
/F	138.05	68	67	66	56	66	66	61	68	68	66	68	69	
	min	68	67	66	66	66	- 66	61	68	68	68	68	69	
	max	69	- 68	68	67	67	67	61	69	69	69	69	70	

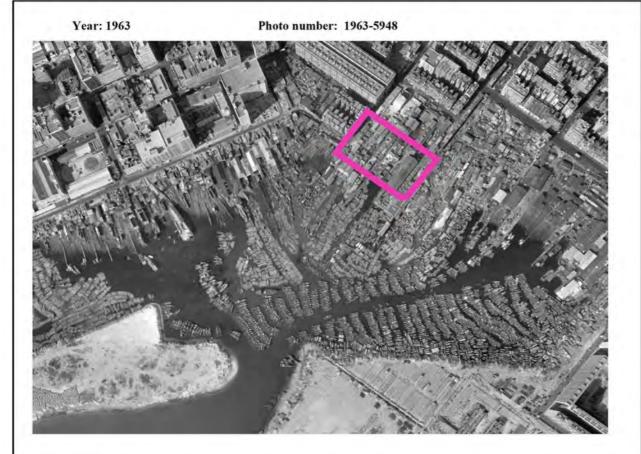
Tower B - by flat

Floor	Elevation	Predited Rolls I level, dB(A)											
1000	(mPO)	TB-01	T8-02	TB-03	TB-04	TB-05	TB-06	18-07	18-08	TB-09	TB-10	18-11	T8-12
1/F	34.1	70	71	71	.70	71	69	56	62	. 69	72	23	74
2/1	37.25	.34	74	70	70	70	69	56	65	71	72	73	.79
3/F	40.4	- 14	71	70	70	70	69	36	67	71	72	23	- 11
4/F	43.55	Th	70	70	70	70	68	56	68	71	72	72	- 71
5/F	46.7	23	70	70	70	70	60	56	69	71	72	72	
6/1	49.85	TI.	70	69	18	70	69	\$7	69	71	71	77	13
7/4	53	77	70	69	65	70	69	57	69	71	71	72	:73-
8/F	56.15	72	(4)	69	68	69	69	58	69	71	71	72	71.
9/F	59.3	71	69	- 69	65	69	69	58	- 69	70	71	71	72
10/F	62.45	72	69	69	69	69	69	58	69	70	71	71	-72
11/F	63.6	22	69	68	68	69	69	59	69	70	71	71	72
12/F	68.75	71	69	- 88	SI .	69	69	59	69	70	70	71	71
	71.9	72	69	- 68	68	68	69	60	69	70	70	71	72
14/F	75.05	71	68	.68	68	68	68	61	69	70	70	71	- 1
15/F	78.2	73	68	68	67	68	68	61	88	70	70	T).	T
16/F	81.35	71	- 68	67	67	68	68	62	68	69	70	70	- 11
17/F	84.5	73		67	67	68	68	62	68	69	70	70	- 11
18/9	87.65	-71	68	67	67	.68	68	62	68	69	70	70	TI.
19/F	90.8	71	68	67	67	67	68	62	- 68	69	69	70	- 71
20/F	93.95	71	67	67	67	67	- 68	62	68	69	69	70	75
21/9	97.1	70	67	67	67	67	67	62	- 68	69	69	70	.71
22/F	100.25	70	67	67	67	67	67	63	68	69	69	70	71.
23/F	103.4	70	67	67	66	67	67	62	68	69	69	70	70
24/F	106.55	70	67	66	66	67	67	62	67	68	69	69	70
25/F	109.7	70	67	66	66	67	67	67	67	68	69	69	70
26/7	112.85	70	-67	66	56	67	67	62	67	68	69	109	70
27/9	116	- 70	67	66	66	67	67	62	67	68	. 68	69	30
28/F	119.15	70	67	66	66	67	67	62	. 67	88	68	(6)	70
29/7	122.3	69	66	66	66	67	67	62	67	58	68	60	70
30/F	125.45	69	66	66	(6	66	67	62	67	68	68	69	70
31/7	128.6	69	66	66	66	66	66	62	67	68	68	68	70
12/F	131.75	- 10	66	- tió	86	56	68	62	67	- 68	68	63	69
33/F	134.9	69	66	66	66	66	66	62	67	- 68	68	69	69
34/F	138.05	.69	66	66	66	66	66	62	67	68	68	- 68	69
	min -	- 69	66	- 66	66	66	66	56	62	- 68	- 68	68	69
	max	78	71	71	70	25	60	62	49	71	22	70	74

APPENDIX 7-1

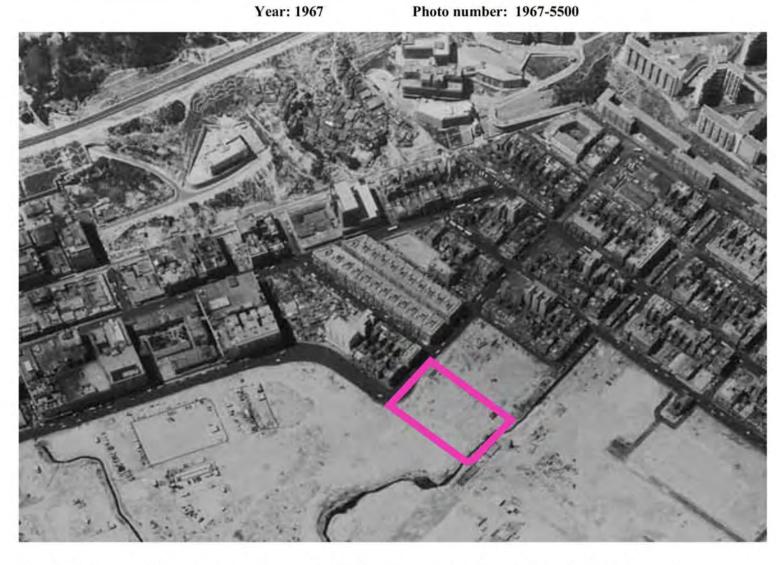
Historical Aerial Photos







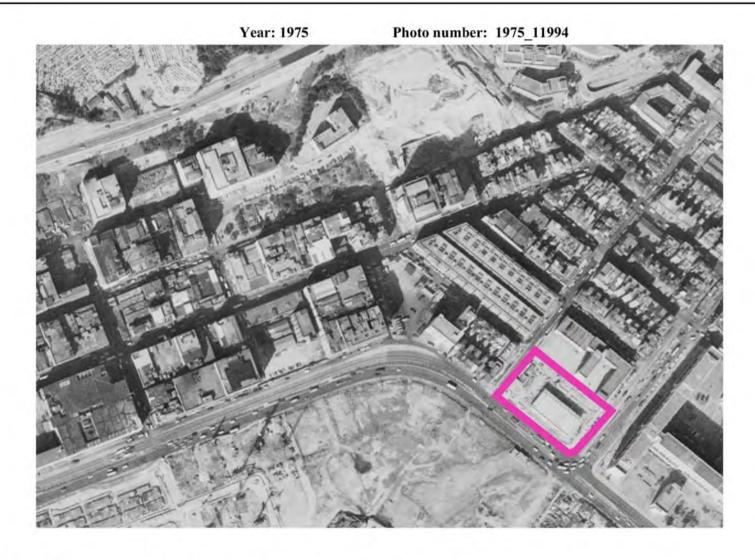
<u>Description:</u> (Top) Aerial view of Cheung Sha Wan. The reclamation of the land at the Site was completed, while the reclamation works of the bay was still in progress. Buildings and temporary structures are also developed in the vicinity of the Site and the coastal area. (Bottom) Temporary structures assumed to be squatter structures are recorded in the site.



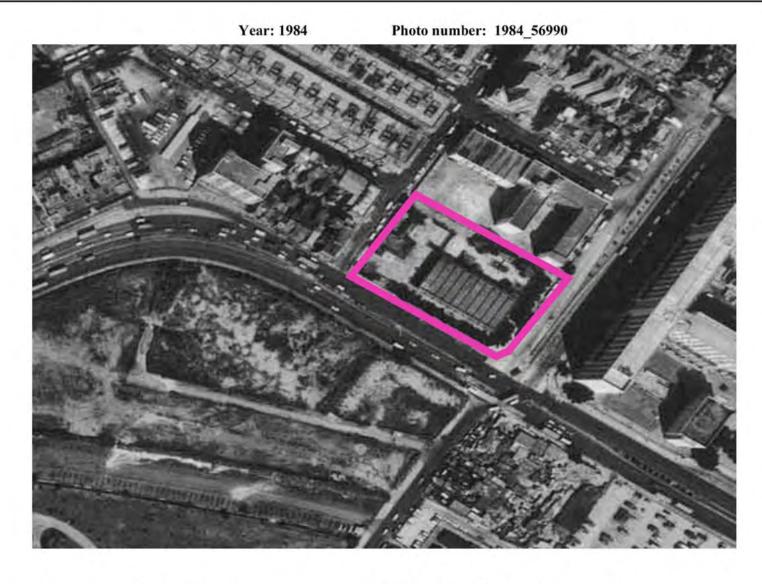
Description: Temporary structures at the Site have been removed, and barren land are observed.



<u>Description:</u> Temporary structures are observed and the land is assumed to be used open area storage of construction materials as piping materials are observed.



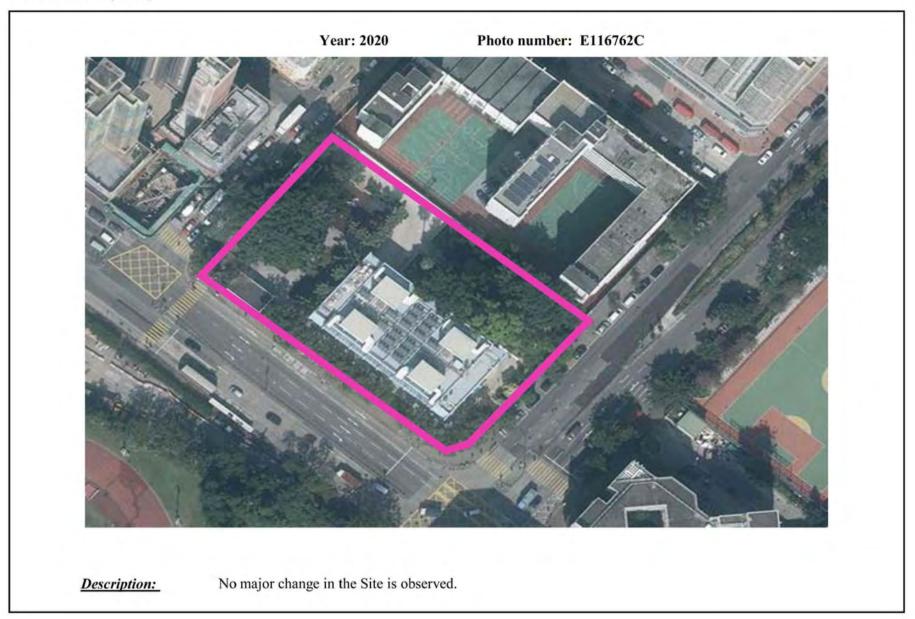
Description: The building for the existing Cheung Sha Wan Sports Centre was erected.



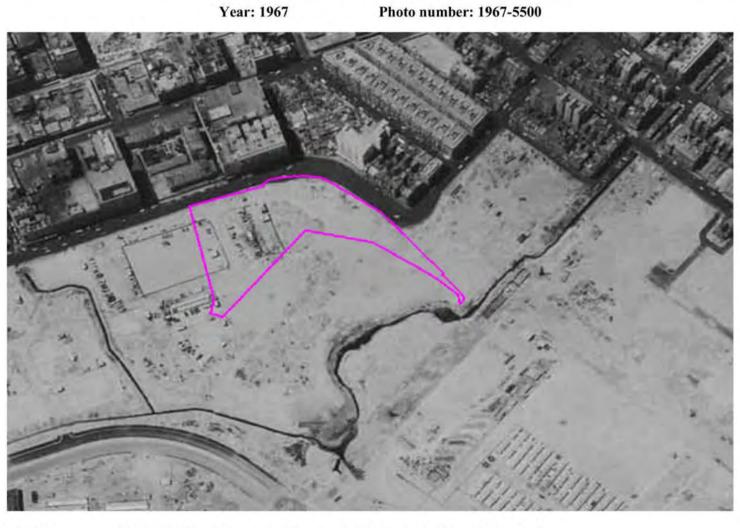
Description: No significant change is observed for the building. Some shrubs were grown on the site.



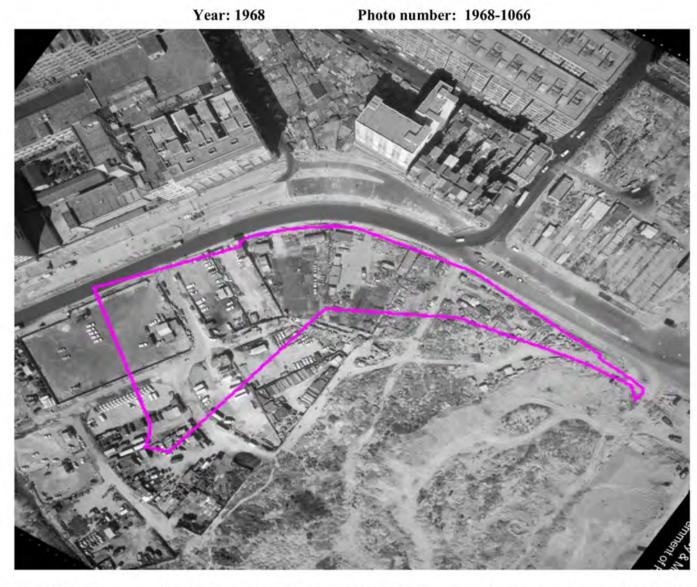
Appendix 7-1 Aerial Photos (Site A)



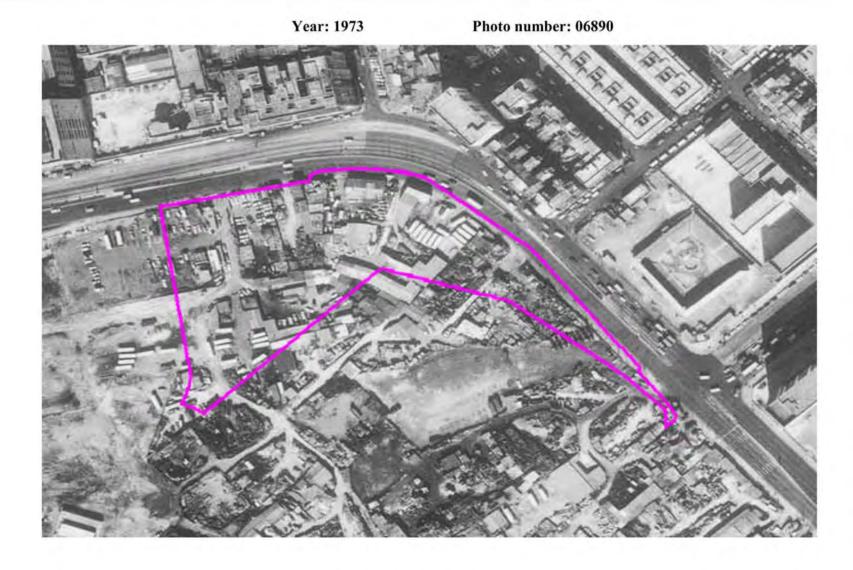




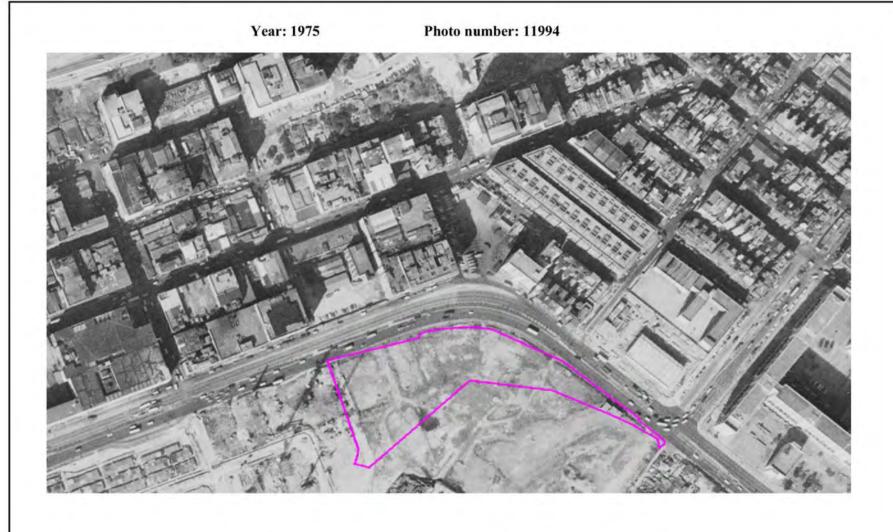
Description: The land of the Site was reclaimed and vehicles in the Site are observed.



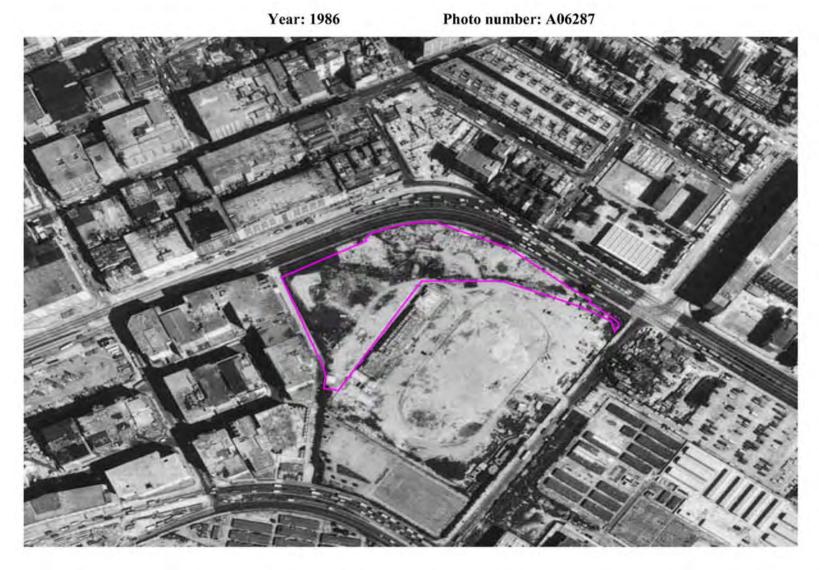
<u>Description:</u> The Site was generally paved. More vehicles and some open area storage of construction materials are recorded in the site.



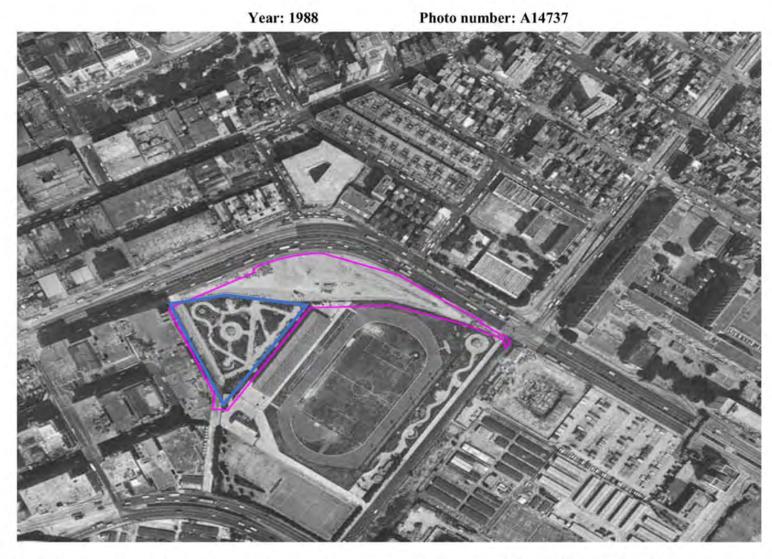
Description: No significant change was recorded.



Description: The temporary structures and vehicles were removed.

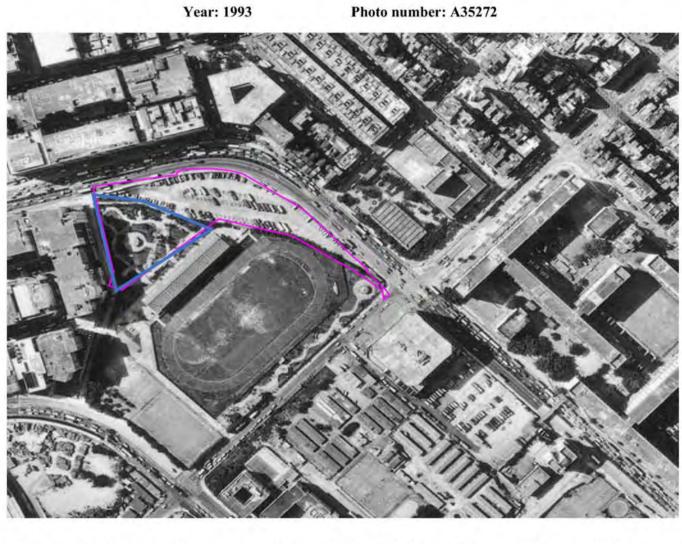


Description: Apart from some shrubs that were being grown on the Site, no major change in the Site are observed, while the existing Sham Shui Po Sports Ground near the Site was under construction and the development in the surrounding areas was also in progress.

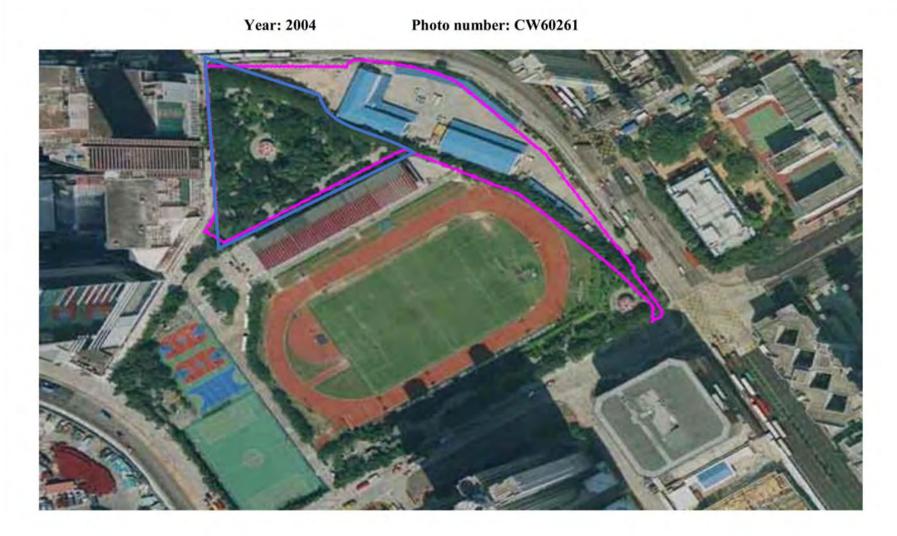


Description:

In the southwest of the Site, the construction of the existing Cheung Sha Wan Path Sitting-out Area (Blue) was substantially completed and the area was fully paved apart from the landscaped areas, while the remaining area of the Site remained unchanged. The construction of Sham Shui Po Sports Ground was completed.



<u>Description:</u> No significant change was recorded in the Cheung Sha Wan Path Sitting-out Area, while the remaining area of the site was occupied by vehicles.



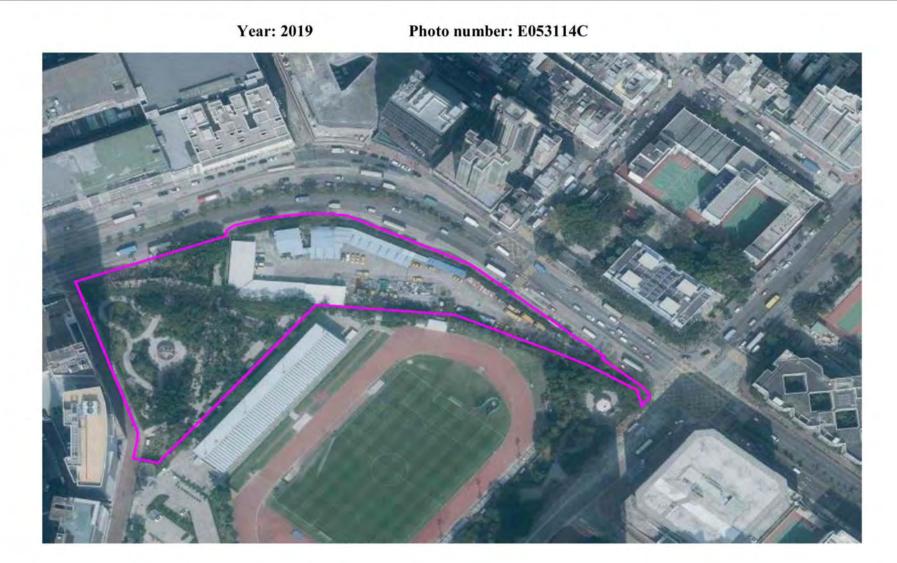
Description:

The northern boundary of the Cheung Sha Wan Path Sitting-out Area was extended. The remaining area of the Site was fully paved and was occupied by temporary structures, assumed to be site offices, and vehicles.

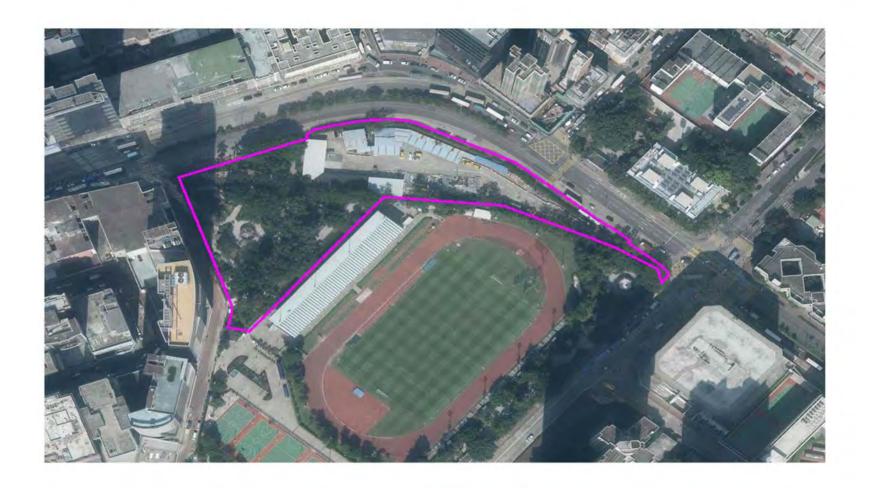


Description:

More temporary structures and vehicles were also recorded in the site. Open area storage of construction materials (yellow) are also observed.



<u>Description:</u> More temporary structures and vehicles were recorded in the site.



Year: 2020 Photo number: E116762C

Description: No significant change is observed.

APPENDIX 7-2

Correspondent from EPD and FSD regarding for Land Contamination Enquires

Fwd: Request for Records of Chemical Waste Producers and Chemic...

Subject: Request for Records of Chemical Waste Producers and Chemical Spillage / Leakage Incidents at Sham Shui Po Study Area

Date:Mon, 26 Jul 2021 11:05:02 +0800

From:joescmok@epd.gov.hk
To:info@cinotech.com.hk

CC:wyiu@epd.gov.hk, karinhwwong@epd.gov.hk

Dear Mr Colman Wong,

I refer to the letter signed by KS LEE of Cinotech Consultants Limited dated 14 July 2021 to us for the captioned request.

- 2. A registry of Chemical Waste Producers in the concerned area is available in the Territory Control Office of the Environmental Protection Department. Please contact our Mr Eric FUNG at 2835 1027 for making an appointment to view the records.
- 3. This office has no record of previous chemical spillage / leakage incident for the concerned area. You may check with other relevant department(s) for such information as appropriate.

Best regards
Joe MOK
E(RW)51 / EPD

Tel.: 2417 6673

1 of 1 20-Aug-21, 1:10 PM

消防處 香港九龍尖沙咀東部康莊道1號 消防處總部大廈



FIRE SERVICES DEPARTMENT FIRE SERVICES HEADQUARTERS BUILDING, No.1 Hong Chong Road, Tsim Sha Tsui East, Kowloon, Hong Kong.

本處檔號 OUR REF.

(85) in FSD GR 6-5/4 R Pt. 35

來函檔號 YOUR REF. :

CCL/IA19021/SSPAA1/ks210714a

電子郵件 E-mail

hkfsdeng@hkfsd.gov.hk

圖文傳真 FAX NO.

2739 5879

奮 話 TEL NO.

2733 7741

3 August 2021

CINOTECH Consultants Limited Room 1710, 17/F, Technology Park, 18 On Lai Street, Shatin, N.T.

(Attn: Mr. K S LEE, Technical Director)

Dear Mr. LEE,

Environmental Assessment for Proposed Urban Renewal Authority Development Scheme at Sham Shui Po Request for Information of Dangerous Goods & Incident Records

I refer to your letter of 14.7.2021 regarding the captioned request and reply below in response to your questions:-

Please be advised that neither records of dangerous goods license, fire incidents nor incidents of spillage / leakage of dangerous goods were found in connection with the given conditions of your request at the subject location.

If you have further questions, please feel free to contact the undersigned.

Yours'sincerely,

for Director of Fire Services

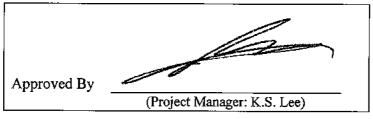
Appendix 7

Air Ventilation Assessment (AVA) Report

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Air Ventilation Assessment Report (v2.0)

Sep 2021



REMARKS:

The information supplied and contained within this report is, to the best of our knowledge, correct at the time of printing.

CINOTECH accepts no responsibility for changes made to this report by third parties.

CINOTECH CONSULTANTS LIMITED

Room 1710, Technology Park 18 On Lai Street Shatin, NT, Hong Kong Tel: (852) 2151 2083 Fax: (852) 3107 1388

Email: info@cinotech.com.hk

Prepared by	Colman Wong	Colman	23 September 2021
Checked by	Karina Chan		23 September 2021

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1 INTRODUCTION

1.1 Project Background

- 1.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Sha Wan Road / Lai Chi Kok Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO).
- 1.1.2 The Scheme consists of two sites. Site A of the Scheme is broadly bounded by Hing Wah Street to the southeast, Cheung Sha Wan Road to the southwest, Cheung Wah Street to the northwest, and Cheung Sha Wan Catholic Secondary School to the northeast. Site B of the Scheme broadly bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground to the southeast. (Figure 1-1). The site areas of the Site A & Site B are 5,197m² and 13,857m² respectively, subject to site survey and detailed design. According to the *Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37*, Site A is currently zoned for "Government, Institution or Community (G/IC)" with maximum building height of 1 storey and "Open Space (O)". Site B is currently zoned for "Government, Institution or Community (G/IC)" with maximum building height of 1 storey, "Open Space (O)", and shown as "Road". (Figure 1-2).
- 1.1.3 The Scheme is proposed to rezone the Site A into "R(A)" with height restriction of 140mPD with commercial uses always permitted on the lowest two floors of the building. The Scheme is also proposed to rezone the west portion of Site B into G/IC of 95mPD and the rest of Site B into Open Space.
- 1.1.4 Given the Scheme propose zoning with relaxation of maximum building height up to 140mPD, an Air Ventilation Assessment (AVA) would be prepared to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.5 Cinotech Consultants Limited was commissioned by URA to carry out an Air Ventilation Assessment (AVA) to assess and envisage any potential/adverse air ventilation impact on the implementation of the Scheme as compared to the OZP-compliance notional redevelopment and to recommend mitigation measures when necessary. The AVA study for the assessment area would be conducted in accordance with the recommendations of "Feasibility Study for Establishment of Air Ventilation Assessment System Final Report" by Planning Department in 2005, and "Technical Circular No. 1/06 on Air Ventilation Assessments" by HPLB & ETWB in 2006 (Technical Circular). As there is a planned concurrent URA project within the assessment area, the air ventilation performance of the planned development (SSP-017) shall also be included in this assessment (Figure 1-4).
- 1.1.6 In the event that the proposed "Good Design Features" explained in Sections 1.2.3-1.2.5 below in this AVA report are not adopted in the future design scheme or no other alternative and equivalent design features to be agreed with Planning Department, further AVA study would be conducted by the project proponent for demonstrating that the performance of any future development would not be worse than the scheme adopted in this report.

1.2 The Scheme (SSP-018)

1.2.1 The Scheme involves demolition of existing Cheung Sha Wan Sports Centre (620 Cheung Sha Wan Road); and clearance of existing facilities in Cheung Sha Wan Path Sitting-Out Area, the garden portion of Sham Shui Po Sports Ground, as well as some temporary structures along Cheung Sha Wan Road (Land Lot: GLA-TNK 1723).

- 1.2.2 The notional layout plan of the proposed development is shown in Figures 1-2 & 1-3. The notional design of the Scheme is subject to change in the detailed design stage upon CE in C's approval of the draft DSP. Under current notional design of the Scheme, it proposes to develop two residential towers (Towers A & B) on top of 5-storey podia at Site A which would incorporate GIC/commercial/retail, private clubhouse facilities and podium garden, a basement carpark; and an about 18-storey block with G/IC facilities at Site B which would incorporate a basement carpark.
- 1.2.3 A maximum building height of 140mPD is proposed for the Site A. In order to provide a large (partially decked) open area which can enhance the air ventilation of pedestrian level, a ~20m setback from Cheung Wah Street and >10m setback from Cheung Sha Wan Road for the western portion of the podium of Site A has been considered in the early stage.
- 1.2.4 A G/IC block with maximum building height of 95mPD is proposed for the Site B. In order to reduce the potential impact to the local ventilation, the G/IC block is proposed to be built near the western boundary of Site B, in order to provide a large continuous open space in the core region of Site B.
- 1.2.5 The ~20m setback from Cheung Wah Street for Site A should not only enhance the air ventilation performant of the open area for Site A, instead, it should also facilitate the ventilation in downwind area under SW wind, which is the major prevailing wind direction in summer. The positioning of the G/IC Block in Site B maximises the flow penetration of Site B, by providing large open area for connecting the nearby air pathways, e.g. Hing Wah Street, Cheung Sha Wan Road, Cheung Wah Street & Sham Shui Po Sports Ground. Although the G/IC Block may potentially reduce the ventilation performant near the G/IC Block, it is anticipated that the benefit from the continuous open area will overcome its drawback.

1.3 Planned Redevelopment Project (SSP-017)

- 1.3.1 As stated in the Planning Report of the DSP submission, a street block at Kim Shin Lane / Fuk Wa Street (namely SSP-017) comprising 90 building blocks of age over 60 with no lifts is identify as a site with imminent redevelopment needs. However, SSP-017 is undesirable for redevelopment because its existing plot ratio is as high as 8.12, hence, the residual plot ratio is 0.88 only. Multiple sub-divided units are also identified. Although SSP-017 has all the quality to demand for redevelopment, its redevelopment potential is low. In this respect, a wider area for planning opportunities have to be explored.
- 1.3.2 Under a "planning-led" approach in urban renewal works in recent years, URA has identified part of Sham Shui Po as Sham Shui Po Action Area 1 (SSPAA1) for holistic planning of urban renewal works. SSP-018 comprises Sites A and B, both Government land opposite each other across Cheung Sha Wan Road is identified for redevelopment to formulate a comprehensive land-use restructuring together with SSP-017 to create more planning gains at district level. The proposed residential use at Site A of SSP-018 will be able to sustain the proposed redevelopment of SSP-017.
- 1.3.3 As SSP-017 and SSP-018 are interrelated and are commenced on the same day, the AVA will also consider the cumulative impact of SSP-017 and SSP-018 redevelopment. It is noted that SSP-017 conforms to the existing planning control, it will be implemented under Section 26 of the Urban Renewal Authority Ordinance (URAO) separately; it does not form part of this DSP.

- 1.3.4 Similar to the Scheme (SSP-018), the development of SSP-017 is still in early stage thus no detailed designed is available, URA planned to development 2 residential towers of 120mPD each with separated podium. The location and the latest notion block plan of the SSP-017 is illustrated in Figures 1-4 & 1-5.
- 1.3.5 URA intends to incorporate air ventilation friendly designs into SSP-017. Similar to Site A of SSP-018, in order to provide a large open area via ground floor setbacks which can enhance the air ventilation of pedestrian level, a ~20m setback from Cheung Wah Street has been considered. Besides, the podiums are 2m 9m setback from site boundary in south, west and north. Moreover, a new 15m SW-NE pedestrian pathway will be provided in the middle of the site. Although the new buildings will be much taller than the existing buildings, it is anticipated that the benefit from the smaller footprint and the air ventilation friendly designs will overcome its drawback.

1.4 The Baseline Scheme

- 1.4.1 For the Scheme, a Baseline Scheme fulfilling the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37, has been used to represent the intended air ventilation performance as permitted in the current OZP. The zonings of OZP No. S/K5/37 are illustrated in Figure 1-6 for reference. Two 1 storey buildings of 12m tall under existing "G/IC" zone within the boundary of SSP-018 Sites A and B are adopted in the Baseline Scheme to reflect the possible redevelopment.
- 1.4.2 For the SSP-017 Site, as it is not part of the current DSP, the existing building configuration, i.e. two rows of tenement buildings, has been adopted in Baseline Scheme to reflect the cumulative impact before and after redevelopment. The notional layout of the Baseline Scheme is shown in Figure 1-7.

1.5 Design Consideration of the Scheme (SSP-018)

- 1.5.1 Despite the structures in the Baseline Scheme is much shorter and occupy much less area, their orientation are not optimised for air ventilation, especially for the wind pathways of the major prevailing wind direction under summer (SW wind).
- 1.5.2 Although the wind pathways will not be completely blocked in the Scheme as there are large open space in both the Sham Shui Po Sport Ground and Site B for the wind pathways, the ventilation performance in the pedestrian level of downstream region should be adversely affected under SW wind.
- 1.5.3 On the other hand, the buildings of the Scheme are not expected to affect the major wind pathway. Moreover, local ventilation enhancement design such as podium setback will be incorporated into the Scheme. The western portion of podium in Site A will setback from the Cheung Wah Street and Cheung Sha Wan Road to provide a wider open space at grade as stated in Section 1.2.
- 1.5.4 The layouts of the two schemes are illustrated in Figures 1-8. Simplified 3D models of the two Schemes are illustrated in Figures 3-7a, 3-7b & 3-7c. The air ventilation related design feature of the Baseline Scheme and the Scheme, including the Planned Project (SSP-017), are summarised in Table 1-1.

Table 1-1 Summary of the Baseline Scheme and Proposed Scheme

	SSP-017 (Planned Project)	SSP-018 (Current Scheme)
Building Height (Baseline Scheme)	30mAG	12mAG
Building Height (Proposed Scheme)	140mPD (~135mAG)	Site A: 140mPD (~135mAG) Site B: 95mPD (~90mAG)
Air Ventilation Consideration	The podium will be setback from Cheung Wah Street (20m), Fuk Wa Street (5m), Fuk Wing Stret (2m or 9m), & Castle Peak Road (7m) to provide a wider open space and pedestrian pathway at grade. A new 15m SW-NE pedestrian pathway will be provided in the middle of the site.	Site A: The western portion of podium will be setback from the Cheung Wah Street (~20m) and Cheung Sha Wan Road (>10m) to provide a wider open space at grade. Site B: The G/IC building will be located near the west boundary to minimized the potential effect to the local ventilation. The rest of the Site B is open area connecting the nearby wind pathways.

1.6 The Surrounding Environment

1.6.1 The Scheme (SSP-018) and Planned Project (SSP-017) are located in a developed urban area, with a mix of old tenement buildings, newer high-rise residential buildings, industrial buildings. In the south of the Scheme, there is a large open area (Sham Shui Po Sport Ground). Make use of the natural wind from the Sham Shui Po Sport Ground is a key consideration for providing good ventilation at pedestrian level under S-SW wind.

1.7 Objective

- 1.7.1 The objective of this AVA study is to demonstrate that the air ventilation impact on the surrounding area at the pedestrian level of the Scheme will not worsen, if not better, than the Baseline Scheme, which has adopted the requirement as listed in the *Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37*, by qualitatively comparing the two schemes. This comparison is conducted using the Velocity Ratio (VR) computed by Computational Fluid Dynamics (CFD) models for the two schemes.
- 1.7.2 It should be noted that the Scheme is a notional design and subject to change at detailed design stage. The results and conclusion in this report is used to compare the air ventilation performance between feasible design under the planning permission of the current OZP and the proposed design under the proposed planning parameters of the Scheme.

2 ASSESSMENT METHODOLOGY

2.1 Introduction

- 2.1.1 The selection and evaluation of the wind availability data for the upstream wind conditions are described in this section. The following sources of wind data have been reviewed for this AVA study as follows:
 - · Measurement from Hong Kong Observatory (HKO) weather station.
 - Measurement from Wind Tunnel Test in Experimental Site Wind Availability Study¹.
 - Simulated results from Meso-Scale Model Regional Atmospheric System (RAMS)² in Planning Department website.

2.2 Selection of Wind Data Source

- 2.2.1 Simulated result of RAMS from Planning Department website is adopted in this AVA study. The reason for the selection of this wind data source is explained in the following paragraphs.
- 2.2.2 HKO weather stations provided reliable wind data in Hong Kong. The closest HKO weather station to the Site is Sham Shui Po Automatic Weather Station which is located approximately 1.4km away from the Site. The next closest HKO weather stations are in Kowloon City and King's Park which are both more than 3 km away. Since the measurement location of HKO weather station is often at low height or a few meters above roof top, the wind at the weather station is inevitably affected by nearby developments or topography. Its data should be applied with caution specifically when the station is not very close to the Site.
- 2.2.3 The measurement level of the wind data from the Sham Shui Po Automatic Weather Station is 11 mPD which is far lower than the proposed building of the Scheme (140mPD) and considering that the weather station is located within urban area, it should only be adopted when no other alternatives are preferred. However, the Waglan Island Automatic Weather Station is located in an undisturbed area and its measured wind data can describe the overall wind condition for Hong Kong well. Therefore, the wind data from Waglan Island Automatic Weather Station is often adopted in AVA study.
- 2.2.4 A series of experimental site wind availability studies for various regions in Hong Kong using wind tunnel experiment have been conducted and some of the reports are available to public. The closest location can be found in "Experimental Site Wind Availability Data for Mong Kok Investigation Report WWTF007-2007". As the site of this development is approximately 1 km away from its study area. The wind data from WWTF003-2007 should only be adopted when no other alternatives are available.
- 2.2.5 In order to provide a comprehensive set of standardized and reasonably representative site wind availability data for both qualitative and quantitative AVA, a consultancy study was commissioned by the Planning Department. The study adopted meso-scale model RAMS to simulated 10-year wind climate at horizontal resolution of 0.5km x 0.5km, covering the whole Hong Kong. Three levels of nested domains with realistic boundary conditions were adopted to provide reasonable approaching wind condition to the finest level of nesting. To refine the model results, the wind data from various wind stations have been used in RAMS.

¹ https://www.pland.gov.hk/pland en/info serv/site wind/index.html

https://www.pland.gov.hk/pland en/info serv/site wind/site wind/index.html

- 2.2.6 When comparing the RAMS to the wind tunnel experiments in the experimental site wind availability studies, the RAMS have the following advantage:
 - RAMS covers a much larger upwind area, with terrain height and land surface type, compare to those wind tunnel experiments;
 - RAMS considers the atmospheric stability where those wind tunnel experiments do not consider thermal effect;
 - RAMS provides wind data for every single grid at various elevation, unlike those wind tunnel experiments that can only provide data at predetermined locations, and HKO's measurements that only provide surface data.
- 2.2.7 Reference can be made to an AVA study (Project ref. AVR/G/136; Public Housing Development at North West Kowloon Reclamation Site 1 (East)) which is available from the Air Ventilation Assessment Register³ in Planning Department website. The AVA study (AVG/G/136) is centred at the land slot surrounded by Lai Chi Kok Road, Tonkin Street and Tung Chau Street, which is around 400m south-east from the Scheme. In the study, wind data from grid [76,46] at 500m in RAMS had been adopted.
- 2.2.8 Considering that the grids from RAMS can cover every part of Hong Kong and the advantages of the RAMS over those wind tunnel experiments, the data of grid [76,46] from RAMS is best suited for this AVA study.

2.3 Adopted Wind Conditions

- 2.3.1 The wind speed and the vertical wind profiles of grid [76,46] from RAMS⁴ have been adopted in order to provide a realistic flow condition.
- 2.3.2 The wind direction at 500m elevation have been adopted in the analysis of general wind condition of the site, while the vertical wind profiles are adopted as the inlet boundary conditions of the numerical analysis.
- 2.3.3 It should be noted that the wind profiles from RAMS are grouped into four range of wind directions, therefore, all wind directions within the same 90-degree segment share the same profiles. The boundary layer height is assumed to be 500m, thus the flow velocity at 500m is the free stream flow velocity and the flow above 500m is uniform.
- 2.3.4 The wind rose at 500m elevation of grid [76,46] and the wind profile from RAMS are illustrated in Figures 2-1a and 2-1b. The top 80% of wind directions, which has been assessed in this study, are presented in the Table 2-1 & Table 2-2. Detailed occurrence probability for each wind direction and wind speed at 500m elevation are listed in Appendix 2-1. The adopted wind profile from 10-500m were extracted from the wind profile curve provided by PlanD (Figure 2-1b). The wind profiles for different wind direction, in term of ratio to the free stream flow velocity at different heights, are summarised in Table 2-3.
- 2.3.5 Under annual condition, the major wind direction is East. For around 60% of the time, the wind comes from NE, ENE, E, ESE, or SE (45-135 deg). Around 18% of the wind comes from S, SSW, or SW (180-225deg). The occurrence chance for the rest of wind directions are all below 5% each.

³ https://www.pland.gov.hk/pland en/info serv/ava register/government.html

⁴ https://www.pland.gov.hk/pland en/info serv/site wind/site wind/index.html

- 2.3.6 Under summer condition, the major wind direction shifted to South-Western. For around 48% of the time, the wind comes from S, SSW, SW, or WSW (180-247.5 deg). Around 34% of the wind comes from E, ESE, SE, or SSE (90-157.5 deg). The occurrence chance for the rest of wind directions are all below 6% each.
- 2.3.7 Generally, the major wind direction of concern is the east direction for the whole year and the south-western direction for summer. A good designer should have considered those two major wind directions to reduce the impact of air ventilation to the surrounding area.

Table 2-1 Occurrence Probability for Each Wind Directions and the Average Wind Speed at 500m Elevation (Annual)

Wind Speed at 500m Elevation (Annual)

Wind Direction	Wind Direction (degree)	Occurrence Probability at 500m elevation
E	90	21.8%
ENE	67.5	12.4%
ESE	112.5	12.4%
NE	45	7.6%
SW	225	6.8%
SSW	202.5	6.7%
SE	135	6.5%
SSE	157.5	4.9%
S	180	4.5%
Sum		83.6%

Table 2-2 Occurrence Probability for Each Wind Directions and The Average

Wind Speed at 500m Elevation (Summer)

Wind Direction	Wind Direction (degree)	Occurrence Probability at 500m elevation
SW	225	16.9%
SSW	202.5	14.2%
ESE	112.5	9.7%
S	180	9.2%
E	90	8.3%
SSE	157.5	8.2%
SE	135	7.6%
WSW	247.5	7.6%
Sum		81.7%

Table 2-3 Vertical Wind Profiles for different Wind Directions

Heights (m)	for diff		eed (m/s) tions (degree from	North)
neiguis (iii)	22.5- 112.4°	112.5-202.4°	202.5-292.4°	292.5-22.4°
10	3.58	2.11	2.20	2.87
50	3.88	2.25	2.39	3.10
100	4.33	2.55	2.73	3.85
150	4.86	2.82	3.03	4.17
200	5.44	3.12	3.28	4.29
250	5.92	3.46	3.46	4.13
300	6.31	3.97	3.62	3.97
350	6.67	4.45	3.76	3.85
400	6.95	4.91	3.88	3.88
450	7.22	5.32	4.06	3.94
500 and above	7.32	5.62	4.22	3.97

3 ASSESSMENT METHODOLOGY

3.1 Assessment Tool

3.1.1 The microclimate around the Site for the two Schemes have been assessed by Computational Fluid Dynamics (CFD). Commercial CFD software, Ansys Fluent, has been utilized for calculating the local wind speed. The model solves the algebraic equations by applying the conservation laws of physics to finite volumes of space and time. Realisable k-epsilon with wall model is adopted to handle the flow turbulence.

3.2 Assessment Area and Surround Area

3.2.1 According to the Technical Circular, the Assessment Area of the Scheme should include the Scheme's surrounding up to a perpendicular distance H from the Scheme boundary, H being the height of the tallest building on site. Surrounding Area of up to a perpendicular distance of 2H from the DSP boundary must be included. Since no building is higher than the proposed Tower T1 135mAG (140 mPD) within 135m from the Scheme boundary, areas of not less than 135m and 300m from the Scheme boundary are adopted as the Assessment Area and Surrounding Area, respectively. The Assessment Area and Surrounding Area are illustrated in Figure 3-1.

3.3 Test Points

- 3.3.1 146 perimeter test points (P001-P144) have been used to examine the air ventilation around the Site A (P001-P030), Site B (P031-P104) and SSP-017 (P105-P144). The perimeter test points are evenly spread, with around 10m separation, along the boundary of the Sites. As only locations that exist in both Baseline Scheme and Proposed Scheme should be chosen for a fair comparison, the perimeter test points have been provided surrounding the building structure of Baseline Scenario when necessary. The locations of the perimeter test points are illustrated in Figure 3-2.
- 3.3.2 384 overall test points (O001-O384) have been used to examine the air ventilation of the local area. Overall test points are evenly spread on road surface within the Assessment Area, with around 25m separation, on all roads within the Assessment Area (O001-O275). For very wide roads, i.e. part of Cheung Sha Wan Road and Hing Wah Street, 2 rows of overall test points with at least 15m separation have been provided to balance the weighting of each test point. Besides the roads, overall test points are also placed at open areas where there are frequent access (O276-O384). Test points with 25m separation have been applied for very large open area, i.e. Sham Shui Po Sports Ground and football field. For other open area, the separation is down to 15m due to the limited area. The locations of the perimeter test points are illustrated in **Figure 3-3**.
- 3.3.3 The ventilation performance between the Baseline Scheme and Proposed Scheme in the neighbourhood, including the effectiveness of the design considerations stated in Sections 1.3 & 1.5, can be quantified using the predicted wind speed at the perimeter test points and overall test points. However, the ventilation performance at the open areas within the Scheme is not covered. Therefore, 81 special test points (D01-D81) are provided at the open areas of the Scheme, with ~10m separation at Site A (D01-D19), 15m separation at Site B (D20-D61) and ~10m separation at SSP-017 (D62-D81). The locations of the special test points within the proposed development of the Scheme are illustrated in Figure 3-4.
- 3.3.4 In order to examine the localised ventilation, the spatial averaged VRs have been broken into individual focus zones for 31 road sections, 8 open areas and 5 additional zones within the

Sites for demonstrating the localised ventilation performance. The focus areas are illustrated in Figures 3-5a, 3-5b & 3-5c and listed in Table 3-1.

3.3.5 The vertical locations of all test points are 2mAG.

Table 3-1 List of Focus Areas

	Road Se	ections			
R001	Hing Wah Street (O001 - O012)	R017	Castle Peak Road (O161 - O182)		
R002	Hing Wah Street (O013 - O027)	R018	Cheung Yue Street (O183 - O191)		
R003	Cheung Wah Street (O028 - O035)	R019	Un Chau Street (O192 - O196)		
R004	Cheung Sha Wan Path (O036 - O044)	R020	Cheung Fat Street (O197 - O199)		
R005	Kwong Cheung Street (O045 - O048)	R021	Hing Wah Street (O200 - O205)		
R006	Tai Nan West Street (O049 - O060)	R022	Cheung Wah Street (O206 - O208)		
R007	Lai Chi Kok Road (O061 - O069)	R023	Tsap Fai Street (O209 - O211)		
R008	Fortune Street (O070 - O073)	R024	Fuk Wa Street (O212 - O214)		
R009	Hang Cheung Street (O074 - O079)	R025	Yu Chau West Street (O215 - O220)		
R010	Cheung Sha Wan Road (O080 - O091)	R026	Tai Nan West Street (O221 - O226)		
R011	Cheung Sha Wan Road (O092 - O108)	R027	Castle Peak Road (O227 - O239)		
R012	Cheung Sha Wan Road (O109 - O130)	R028	Kwong Shing Street (O240 - O241)		
R013	Fuk Wa Street (O131 - O137)	R029	Wing Hong Street (O242 - O262)		
R014	Fuk Wing Street (O138 - O142)	R030	Wing Ming Street (O263 - O270)		
R015	Fuk Wing Street (O143 - O147)	R031	King Lam Street (O271 - O275)		
R016	Un Chau Street (O148 - O160)		***************************************		
	Open .	Area	Assessment of the second		
Z001	Sham Shui Po Sports Ground (O276 - O328)	Z005	Un Chau Estate (O354 - O355)		
Z002	Hang Chun Court (O329 - O337)	Z006	Hing Wah Street Playground (O356 - O370)		
Z003	S.K.H. Kei Fook Primary School – Middle (O338 - O343)	Z007	Cheung Sha Wan Catholic Secondary School (O371 - O376)		
Z004	S.K.H. Kei Fook Primary School – West (O344 - O353)	Z008	Wing Hong Street Rest Garden (O377 - O384)		
	Open Area - Within	Scheme Bou	ndary		
A001	Site A – Setback Areas in West (A001 - A014)	A004	SSP-017 - Setback Area in West (A062 - A076)		
A002	Site A – North-East Area (A015 - A019)	A005	SSP-017 - SW/NE pedestrian pathway (A077 - A081)		
A003	Site B – Open Area (A020 - A061)				

3.4 Assessed Parameters

3.4.1 According to the Technical Circular, Wind Velocity Ratio (VR) should be used as an indicator of wind performance for the AVA. It is defined as

$$VR = V_P/V_g$$

Where V_g is the wind velocity at the top of boundary layer (at 500m in this AVA) and V_P is the wind velocity at pedestrian level (2m above ground or slab).

- 3.4.2 To quantitatively assess the air ventilation for the Site and in the surrounding area, two spatial averaged values, namely Site Air Ventilation Assessment (SVR) and Local Air Ventilation Assessment (LVR) will be used.
- 3.4.3 SVR is the average (weighted by the occurrence probability of the wind directions) of the VRs along the Site boundary (i.e. P001-P144), to quantify the air ventilation of the Site. LVR is the average of the VRs for the whole assessment area (average of all perimeter and overall test points), for quantify the air ventilation of the local region.
- 3.4.4 It should be noted that the VRs (also SVRs and LVRs) should only be compared between the Baseline Scheme and the Proposed Scheme of the study which have applied identical setting for each parameter, and should not be directly compared with on-site measurement and/or wind tunnel experiment.

3.4.5 Averaged VRs for smaller focus areas (e.g. a street section or open area) will also be presented to examine the effect of the building design to air ventilation of individual regions within the Assessment Area.

3.5 Studied Scenarios

- 3.5.1 Two scenarios were considered in this study. The first scenario is based on the design of the Baseline Scheme. The other scenario is based on the Proposed Scheme. The results of the scenarios will be compared to draw the conclusion.
- 3.5.2 In both scenarios, all buildings in the surrounding area and the terrain are included. The terrain information of the surrounding is extracted from Digital Terrain Model (DTM)⁵ of Hong Kong provided by Lands Department and illustrated in **Figure 3-6a**. The buildings (and flyovers) included in the CFD are illustrated in **Figures 3-6b & 3-6c**.
- 3.5.3 The difference between the two scenarios are the buildings within the Site A, Site B and Site for SSP-017, which are shown in Figures 1-2, 1-7 & 1-8. For Site A, the Baseline Scheme have a single 12mPD building, while the Proposed Scheme consist of two 140mPD residential towers (Towers A & B) on top of 6-storey podia. For Site B, the Baseline Scheme have a single 12mPD building, while the Proposed Scheme consist of a 95mPD block with G/IC facilities. For the Site of SSP-017, the Baseline Scheme have two rows of 30m tenement buildings, while the Proposed Scheme consist of 2 residential towers of 120mPD each with separated podium.
- 3.5.4 The simplified 3D model of the development (SSP-018) adopted in both scenarios are illustrated in Figures 3-7a & 3-7b for Baseline Scheme and Proposed Scheme, respectively. The simplified 3D model of the development adopted in SSP-017 Site is illustrated in Figure 3-7c.
- 3.5.5 Both scenarios share the identical boundary conditions and other modelling parameters to have a fair comparison focused on the design between the Proposed Scheme and Baseline Scheme only. The details models' setting will be explained in later paragraphs.

3.6 Computational Domain and Boundary Condition

- 3.6.1 The global domain size is 4000m (length) x 4000m (width) x 2500m (height) centred at 833700m (E), 822100m (N). The Terrain and buildings within the surrounding area have been included in the model. The distance between the side boundaries of the domain and the buildings are more than 5 times the adopted highest building. The Blockage ratio is less than 3% for all wind directions. **Figure 3-8** shows the computation domain of the Proposed Scheme as an example.
- 3.6.2 The computation domain has been discretized by triangle and tetrahedral meshes for 2D surfaces and 3D volumes, respectively. The 2D triangle meshes on the surface of buildings and flyovers are mostly in the range of 0.8m 6m. The 2D triangle meshes on the ground are mostly in the range of 0.8m 20m. The 3D tetrahedral meshes with size of 0.8m 80m were used in the discretization of the computation domain. In order to resolve the near ground flow velocity, as the data sampling point is 2m above ground, 6 prism layers with a total thickness of 3.0m were applied on the Ground and building surfaces. The different in size of

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⁵ Lands Department - Digital Terrain Model (DTM) - https://data.gov.hk/en-data/dataset/hk-landsd-openmap-5m-grid-dtm

neighbourhood grids, also called grid expansion ratio, are less than 30% for the whole domain. Generally, smaller grids were placed near the building surfaces and ground in order to resolve the near surface flow properly. The meshes adopted in the model are illustrated in Figures 3-9 & 3-10.

3.7 Model Setting

- 3.7.1 The Realisable k-epsilon model has been used in this study as it can provide better results than the standard k-epsilon model. Wall functions are applied on the solid boundaries, i.e. ground and building facades, to account for the turbulence, generated by flow over surfaces.
- 3.7.2 SIMPLE algorithm is adopted to handle the velocity-pressure coupling.
- 3.7.3 Convergence criterion of <1.0E-3 is adopted to control when the iteration will stop. A summary of the model setting can be found in **Table 3-2**.

Table 3-2 Summary of Model Settings

C. Phone	Pre-processing	Ansys Fluent Mesh	
Software	Processing	Ansys Fluent CFD	
Domain Size	4000m x 4000m x 2500m (W	idth x Length x Height)	
Assessment Area	>=1H area		
Surrounding Area	>=2H area		
	Inflow boundary	Velocity Inlet with velocity profiles as listed in Table 2-3	
Boundary Conditions	Outflow Boundary	Pressure Outlet	
	Ground and Building Surfaces No Slip Condition with Wall Fu		
Grid Expansion Ratio	< 30%		
Blockage Ratio	< 3%		
Prismatic layer	6 prism layers with a total thickn	ess of 3.0m (0.5m each)	
Turbulence Model	Realisable k-ɛ turbulence model		
Solving algorithms	SIMPLE algorithm for momentum and pressure coupling		
Convergence criteria	<1.0E-3		

3.8 List of Models

3.8.1 The wind environment of the site has been discussed in Section 2.3. The top 80% wind directions for both annual and summer condition has been adopted in this study (Table 2-1 & Table 2-2). As most of the wind directions in annual and summer are overlapped, only 10 wind directions thus 20 models are required for the two scenarios (Table 3-3).

Table 3-3 List of Wind Conditions Included in the AVA Study

Wind 1	Direction	Occurrence Probability (Annual)	Occurrence Probability (Summer)
NE	45	7.6%	
ENE	67.5	12.4%	
E	90	21.8%	8.3%
ESE	112.5	12.4%	9.7%
SE	135	6.5%	7.6%
SSE	157.5	4.9%	8.2%
S	180	4.5%	9.2%
SSW	202.5	6.7%	14.2%
SW	225	6.8%	16.9%
WSW	247.5		7.6%
Total		83.6%	81.7%

4 ASSESSMENT RESULTS

4.1 Model Results - Spatial Averaged Velocity Ratios

- 4.1.1 Baseline Scenario and Proposed Scenario (for Baseline Scheme and Proposed Scheme respectively) each with 10 wind directions, as stated in Table 3-3 have been conducted based on the methodology mentioned in Section 3. A summary of the predicted spatial averaged VRs of the test points are presented in Table 4-1 including the average SVR for all perimeter test points (P Points) and the average LVR for all perimeter and overall test points (P & O Points). The averaged VRs of each focus areas (Figures 3-5a, 3-5b & 3-5c) are also presented in Table 4-1.
- 4.1.2 The detailed simulated VRs at individual test points are listed in Appendix 4-1. The bar charts for the comparison between the 2 scenarios are also illustrated in Appendix 4-1. The contours and vectors of VRs at 2m above ground are illustrated in Figures 4-1a to 4-1j and Figures 4-2a to 4-2j, for the assessment area and 4km domain, respectively. The contours of annual/summer weighted averaged VRs are illustrated in Figures 4-3a & 4-3b, respectively.

Overall Spatial and Wind Directions Averaged VRs

- 4.1.3 The SVR and LVR are used for quantifying the change in air ventilation performance of the sites and local area in this study. It should be noted that the SVR and LVR in this study is only valid for comparison between different scheme of the current study, but not applicable for comparing different studies.
- 4.1.4 Generally, the SVR and LVR are higher in summer condition than that in the annual condition. This is largely due to the open area provided by Site B, the Sham Shui Po Sports Ground (Z001) and the wind pathway provided by the Cheung Sha Wan Road Section (R012) are more favourable for S to WSW wind (180-247.5 deg).
- 4.1.5 The overall SVR are 0.098 and 0.115 for Baseline Scheme and Proposed Scheme respectively, under annual wind condition. During summer, the SVRs are 0.121 and 0.143 for Baseline Scheme and Proposed Scheme respectively. The SVR of the Proposed Scheme as a whole are better than that of the Baseline Scheme with improvement of SVR 0.018 & 0.022 for Annual and Summer respectively.
- 4.1.6 The SVR for Site A are 0.076 and 0.103 for Baseline Scheme and Proposed Scheme respectively, under annual wind condition. During summer, the SVRs are 0.105 and 0.140 for Baseline Scheme and Proposed Scheme respectively. The SVR of the Proposed Scheme as a whole are better than that of the Baseline Scheme with improvement of SVR 0.026 & 0.035 for Annual and Summer respectively.
- 4.1.7 The SVR for Site B are 0.115 and 0.125 for Baseline Scheme and Proposed Scheme respectively, under annual wind condition. During summer, the SVRs are 0.141 and 0.161 for Baseline Scheme and Proposed Scheme respectively. The SVR of the Proposed Scheme as a whole are better than that of the Baseline Scheme with improvement of SVR 0.010 & 0.020 for Annual and Summer respectively.
- 4.1.8 The SVR for SSP-017's Site are 0.082 and 0.108 for Baseline Scheme and Proposed Scheme respectively, under annual wind condition. During summer, the SVRs are 0.095 and 0.111 for Baseline Scheme and Proposed Scheme respectively. The SVR of the Proposed Scheme

- as a whole are better than that of the Baseline Scheme with improvement of SVR 0.025 & 0.016 for Annual and Summer respectively.
- 4.1.9 The LVR are 0.112 and 0.117 for Baseline Scheme and Proposed Scheme respectively, under annual wind condition. During summer, the LVRs are 0.130 and 0.137 for Baseline Scheme and Proposed Scheme respectively. the LVR of the Proposed Scheme are better than that of the Baseline Scheme with smaller improvement of SVR 0.004 & 0.008 for Annual and Summer respectively.
- 4.1.10 The increases in SVR for each Site under Proposed Scheme implies that ventilation consideration incorporated in the design are effective in general. The slightly increases in LVR implies that the Proposed Scheme is not adversely affecting the pedestrian level's ventilation in average.

Table 4-1 Summary of Spatial Averaged Velocity Ratios

T	est Points for the Subject Site and Assessment Area	Bas	Baseline		Proposed	
		Annual	Summer	Annual	Summe	
	Overall					
Site Air	Ventilation Assessment (SVR) (All P Points)	0.098	0.121	0.115	0.143	
-Site A	(P001 - P030)	0.076	0.105	0.103	0.140	
-Site B	(P031 - P104)	0.115	0.141	0.125	0.161	
-SSP-0	17 (P105 - P144)	0.082	0.095	0.108	0.111	
Local A	ir Ventilation Assessment (LVR) (All P & O Points)	0.112	0.130	0.117	0.137	
	Road Sections					
R001	Hing Wah Street (O001 - O012)	0.114	0.143	0.107	0.142	
R002	Hing Wah Street (O013 - O027)	0.122	0.127	0.132	0.149	
R003	Cheung Wah Street (O028 - O035)	0.095	0.112	0.116	0.143	
R004	Cheung Sha Wan Path (O036 - O044)	0.159	0.157	0.139	0.140	
R005	Kwong Cheung Street (O045 - O048)	0.099	0.123	0.116	0.159	
R006	Tai Nan West Street (O049 - O060)	0.156	0.185	0.146	0.175	
R007	Lai Chi Kok Road (O061 - O069)	0.182	0.169	0.178	0.165	
R008	Fortune Street (O070 - O073)	0.122	0.145	0.109	0.143	
R009	Hang Cheung Street (O074 - O079)	0.115	0.132	0.118	0.132	
R010	Cheung Sha Wan Road (O080 - O091)	0.148	0.183	0.153	0.191	
R011	Cheung Sha Wan Road (O092 - O108)	0.088	0.160	0.114	0.181	
R012	Cheung Sha Wan Road (O109 - O130)	0.184	0.271	0.169	0.270	
R013	Fuk Wa Street (O131 - O137)	0.096	0.098	0.096	0.090	
R014	Fuk Wing Street (O138 - O142)	0.137	0.129	0.142	0.133	
R015	Fuk Wing Street (O143 - O147)	0.072	0.078	0.132	0.141	
R016	Un Chau Street (O148 - O160)	0.148	0.114	0.149	0.121	
R017	Castle Peak Road (O161 - O182)	0.108	0.124	0.111	0.124	
R018	Cheung Yue Street (O183 - O191)	0.109	0.109	0.105	0.109	
R019	Un Chau Street (O192 - O196)	0.138	0.108	0.129	0.090	
R020	Cheung Fat Street (O197 - O199)	0.117	0.097	0.114	0.090	
R021	Hing Wah Street (O200 - O205)	0.116	0.112	0.117	0.110	
R022	Cheung Wah Street (O206 - O208)	0.081	0.075	0.093	0.101	
R023	Tsap Fai Street (O209 - O211)	0.068	0.057	0.072	0.067	
R024	Fuk Wa Street (O212 - O214)	0.086	0.079	0.078	0.073	
R025	Yu Chau West Street (O215 - O220)	0.084	0.076	0.075	0.069	
R026	Tai Nan West Street (O221 - O226)	0.097	0.116	0.088	0.115	
R027	Castle Peak Road (O227 - O239)	0.147	0.114	0.152	0.122	
R028	Kwong Shing Street (O240 - O241)	0.064	0.065	0.073	0.058	
R029	Wing Hong Street (O242 - O262)	0.096	0.106	0.096	0.115	
R030	Wing Ming Street (O263 - O270)	0.101	0.091	0.096	0.084	
R031	King Lam Street (O271 - O275)	0.085	0.125	0.092	0.141	
	Open Area					
Z001	Sham Shui Po Sports Ground (O276 - O328)	0.127	0.153	0.115	0.145	
Z002	Hang Chun Court (O329 - O337)	0.096	0.141	0.094	0.138	

Т	est Points for the Subject Site and Assessment Area	Baseline		Proposed	
		Annual	Summer	Annual	Summer
Z003	S.K.H. Kei Fook Primary School – Middle (O338 - O343)	0.119	0.076	0.119	0.077
Z004	S.K.H. Kei Fook Primary School - West (O344 - O353)	0.100	0.116	0.092	0.110
Z005	Un Chau Estate (O354 - O355)	0.089	0.072	0.088	0.072
Z006	Hing Wah Street Playground (O356 - O370)	0.072	0.078	0.077	0.082
Z007	Cheung Sha Wan Catholic Secondary School (O371 - O376)	0.048	0.055	0.052	0.062
Z008	Wing Hong Street Rest Garden (O377 - O384)	0.087	0.077	0.082	0.074
	Open Area - Within Scheme B	oundary			
A001	Site A – Setback Areas in West (D001 - D014)	0.072	0.103	0.104	0.123
A002	Site A - North-East Area (D015 - D019)	0.051	0.049	0.076	0.107
A003	Site B - Open Area (D020 - D061)	0.109	0.113	0.090	0.110
A004	SSP-017 - Setback Area in West (D062 - D076)	0.072	0.071	0.092	0.092
A005	SSP-017 - SW/NE pedestrian pathway (D077 - D081)	0.046	0.067	0.065	0.057

4.2 Localised Spatial and Wind Directions Averaged VRs (Road Section)

- 4.2.1 For road sections (R001-R031), the change in averaged VRs are in the range of -0.020 to 0.060 under annual condition and in the range of -0.018 to 0.063 under summer condition.
- 4.2.2 It should be note that although the average VRs for road sections can give general picture of the ventilation performance, the density of the test points are not sufficient to capture the small but sharply change flow, e.g. flow concentration near building corner. Therefore, only significant changes in averaged VRs are presented in this section to give a general idea of the improvement (or drawback) due to the Proposed Scheme to the surrounding.
- 4.2.3 The road sections with noticeable improvement (VR different >= 0.015 in both annual and summer condition) are Cheung Wah Street Section (R003), Cheung Sha Wan Road Section (R011), & Fuk Wing Street Section (R015). Two out of 3 road sections (R003 & R015) are experiencing lower than average (i.e. LVR) ventilation performance in Baseline Scenario. In the Proposed Scenario, their ventilation performance shapely improve and sometimes higher than the average level. The improvements at R003 & R011 are mainly due to the refined building footprints and the open areas provided in Site A & SSP-017's Site. The poor placement of building partially blocking wind pathways in Baseline Scenario is also related but unlikely the major reason. The improvement in R015 is the result of the building setback and the new at-grade NW-NE pedestrian pathway at the middle of the SSP-017's Site.
- 4.2.4 The road section with noticeable reduction (VR different <= -0.015 in both annual and summer condition) is Cheung Sha Wan Path (R004) only. It is worth pointing out that the reduction in ventilation performance of R004 is not only due to the blockage of the proposed G/IC Block in Site B, but also due to the less obstructed core region of Site B. For example, under E wind in Baseline Scenario (Figure 4-1c), the wind entering the core of Site B is partially blocked by the 12m building in Site B leads to re-circulation, making it hard for the air to penetrate Site B from south and reach the downstream air pathway (R012) under Baseline Scenario. In comparison, the western portion of Site B and R004 are easier to penetrating (relatively less air resistance) under this case. In the Proposed Scenario, the wind in the core of Site B is no longer blocked thus the western portion of Site B and R004 are less attractive (relatively more air resistance). Nevertheless, the averaged VRs of R004 are

higher than the LVRs in both annual and summer conditions, making it a reasonable tradeoff for improving the poor ventilated areas (R003 & R015).

4.3 Localised Spatial and Wind Directions Averaged VRs (Open Area)

- 4.3.1 Compare to the road sections, the changes in averaged VRs for open areas (Z001-Z008) are relatively small, which is in the range of -0.012 to 0.005 under annual condition; and in the range of -0.008 to 0.007 under summer condition.
- 4.3.2 The only noticeable change (averaged VRS either <= -0.010 or >= 0.010) is identified at Sham Shui Po Sports Ground (Z001) with 0.012 reduction under annual condition. Considering the averaged VRs in the Proposed Scenario (0.115 in annual and 0.145 in summer), it is slightly lower than LVR under annual condition (- 0.002) and slightly higher than LVR (+ 0.008) under summer condition. No adverse air ventilation impact is anticipated.

4.4 Localised Spatial and Wind Directions Averaged VRs (Open Area – Sites)

- 4.4.1 For open area within Site A (A001 & A002), noticeable improvement in ventilation (VR different > 0.020) are identified. The improvement in A001 is strongly related with the improvement in Cheung Wah Street (R003), which is the result of the combined effect of the refined building footprints and the open areas provided in Site A & SSP-017's Site. For A002, although the Baseline Scenario provide more space in Site A, the space in between the building in Site A and the Cheung Sha Wan Catholic Secondary School (Z007) are forming a wake region (slow and recirculating flow region), especially under SSE & S winds (157.5-180 deg) (Figures 4-1f & 4-1g). On the other hand, the proposed building in the Site A under Proposed Scenario is not forming wake region under the same wind directions, despite having narrower space, resulting in higher averaged wind speed and VRs.
- 4.4.2 For open area within Site B (A003), reduction in ventilation performance are identified. Noticeable reduction is only identified in annual condition, which is dominated by ENE-ESE wind (157.5-202.5 deg). Under E wind (Figure 4-1c), the proposed G/IC Block is blocking the flow from entering the western portion of Site B.
- 4.4.3 For the open are within SSP-017 (A004 & A005), the averaged VRs are 0.092 & 0.065 under annual condition; 0.092 & 0.057 under summer condition. No results for Baseline Scenario are available as those open areas in Proposed Scheme are mostly occupied in Baseline Scenario. Therefore, reference has been made to the open area in Site A (A001 & A002) under Baseline Scenario for comparison. Compare to the A001 in Baseline Scenario, the averaged VRs of A004 is higher by 0.020 under annual condition and lower by 0.011 under summer condition. Compare to the A002 in Baseline Scenario, the averaged VRs of A005 is higher by 0.014 under annual condition and higher by 0.009 under summer condition. Although this is not a fair quantitative comparison, it shows the averaged VRs of open area in SSP-017 in the Proposed Scenario are in the same ballpark of that in Site A under Baseline Scenario, which should be within reasonable range which no adverse impact is anticipated.

4.5 Effectiveness of the Design Consideration

4.5.1 The design considerations of the Scheme and SSP-017 are stated in Sections 1.3 & 1.5. From the increased SVR and LVR in the Proposed Scenario, it is known that the design of the SSP-017 & SSP-018 are favourable for air ventilation at the Sites' boundaries and in the assessment area in average.

- 4.5.2 For localised region, the ventilation of Cheung Wah Street Section (R003) is benefited from building setback of Site A and Site of SSP-017; the Cheung Sha Wan Road Section (R011) is benefited from the better building deposition in Site A & Site B; the Fuk Wing Street Section (R015) is benefited from the new open area in SSP-017.
- 4.5.3 However, it is inevitable that some region will be adversely affected. By the cautious notional design, notable adverse effect is only limited to Cheung Sha Wan Path (R004), and its ventilation is above average even in the Proposed Scenario. Therefore, no insurmountable adverse impact is anticipated from the current notional design.

5 CONCLUSIONS

- 5.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Sha Wan Road / Lai Chi Kok Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). An Air Ventilation Assessment (AVA) has been conducted in accordance with the recommendations of "Feasibility Study for Establishment of Air Ventilation Assessment System Final Report" by Planning Department, and "Technical Circular No. 1/06 on Air Ventilation Assessments" by HPLB & ETWB to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration. A planned concurrent URA project (SSP-017) within the assessment area, which is not part of this DSP, is also included in the current assessment.
- 5.1.2 The microclimate around the Site for the two scenarios, i.e. the Baseline Scheme (i.e. OZP-compliance development) and the Proposed Schemes (the proposed development of the draft DSP), have been assessed by Computational Fluid Dynamics (CFD) using well proven CFD code. The model settings have been compared to previous studies to ensure the reliability of the model results.
- 5.1.3 The models result suggested that the averaged air ventilation performance of the Proposed Scheme is better than that of the Baseline Scheme in both annual and summer conditions in average.
- 5.1.4 The most significant improvement compare to the Baseline Scheme can be found along the Site Boundary, and the Cheung Wah Street Section (R003), Cheung Sha Wan Road Section (R011), and Fuk Wing Street Section (R015). Their improvements are mainly due to the refined building footprints, the open area provided as well as the better building disposition of the Sites. Although noticeable deterioration has been identified in Cheung Sha Wan Path (R004), the averaged VRs of R004 are higher than the LVRs in both annual and summer conditions, making a reasonable trade-off for improving the poor ventilated areas (R003 & R015).
- 5.1.5 In the event that the Proposed Scheme in this AVA report, including building disposition and setback, are not adopted in the future design scheme or no other alternative and equivalent design features to be agreed with Planning Department, further AVA study would be conducted by the project proponent in accordance with the joint Housing Planning and Lands Bureau Environment, Transport and Works Bureau Technical Circular No. 1/06 on Air Ventilation Assessments (or its latest version) for demonstrating that the performance of any future development would not be worse than the scheme adopted in this report.

APPENDIX 2-1

Wind Data at grid [76,46] form RAMS

Occurrence Probability at 500m elevation (Annual)

e_01299	Wind_direction	N	NNE	NE	ENE	E	ESE	SE	SSE	S	ssw	sw	wsw	w	WNW	NW	NNW
V_infinity(m/s)	Sum	0.018	0.043	0.076	0.124	0.218	0.124	0.065	0.049	0.045	0.067	0.068	0.033	0.027	0.015	0.014	0.012
00_to_01	0.027	0.001	0.002	0.002	0.002	0.004	0.002	0.002	0.001	0.001	0.001	0.001	0.001	0.003	0.001	0.001	0.001
01_to_02	0.064	0.003	0.005	0.006	0.007	0.008	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.004	0.002	0.002	0.003
02_to_03	0.088	0.004	0.005	0.008	0.01	0.012	0.005	0.004	0.004	0.005	0.005	0.006	0.005	0.006	0.002	0.003	0.003
03_to_04	0.101	0.003	0.004	0.008	0.013	0.017	0.006	0.006	0.007	0.006	0.006	0.008	0.006	0.005	0.003	0.002	0.002
04_to_05	0.11	0.002	0.004	0.008	0.016	0.021	0.009	0.006	0.006	0.007	0.008	0.008	0.005	0.004	0.002	0.002	0.001
05_to_06	0.115	0.001	0.003	0.008	0.016	0.025	0.014	0.008	0.007	0.006	0.009	0.009	0.004	0.002	0.002	0.001	0.001
06_to_07	0.108	0.001	0.003	0.007	0.015	0.026	0.015	800.0	0.006	0.004	0.007	0.008	0.003	0.001	0.001	0.001	0
07_to_08	0.098	0.001	0.003	0.006	0.013	0.023	0.017	0.007	0.005	0.005	0.007	0.007	0.002	0.001	0.001	0.001	0
08_to_09	0.084	0.001	0.003	0.006	0.011	0.023	0.014	0.006	0.003	0.003	0.006	0.006	0.001	0	0	0	0
09_to_10	0.064	0	0.002	0.005	0.008	0.018	0.011	0.005	0.002	0.002	0.005	0.003	0.001	0	0	0	0
10_to_11	0.047	0	0.002	0.004	0.005	0.014	0.009	0.003	0.002	0.001	0.004	0.003	0.001	0	0	0	0
11_to_12	0.032	0	0.002	0.002	0.002	0.009	0.007	0.002	0.001	0	0.002	0.003	0	0	0	0	0
12_to_13	0.021	0	0.001	0.002	0.002	0.006	0.004	0.001	0.001	0	0.001	0.001	0	0	0	0	0
13_to_14	0.014	0	0.001	0.001	0.001	0.004	0.003	0.001	0	0	0.001	0.001	0	0	0	0	0
14_to_15	0.009	0	0.001	0.001	0.001	0.002	0.002	0	0	0	0	0	0	0	0	0	0
15_to_16	0.005	0	0.001	0.001	0.001	0.002	0.001	0	0	0	0	0	0	0	0	0	0
16_to_17	0.004	0	0.001	0	0	0.001	0.001	0	0	0	0	0	0	0	0	0	0
17_to_18	0.002	0	0	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0
18_to_19	0.002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19_to_20	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20_to_21	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21_to_22	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22_to_23	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23_to_24	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Occurrence Probability at 500m elevation (Summer)

e_01299	Wind_direction	N	NNE	NE	ENE	E	ESE	SE	SSE	S	ssw	sw	wsw	w	WNW	NW	NNW
V_infinity(m/s)	Sum	0.009	0.01	0.015	0.028	0.083	0.097	0.076	0.082	0.092	0.142	0.169	0.076	0.053	0.03	0.022	0.012
00_to_01	0.02	0.001	0.001	0.001	0.001	0.002	0.001	0.002	0.001	0.002	0.001	0.001	0.001	0.003	0.001	0.001	0.001
01_to_02	0.058	0.002	0.002	0.002	0.003	0.003	0.004	0.004	0.005	0.005	0.006	0.005	0.005	0.006	0.002	0.002	0.002
02_to_03	0.094	0.003	0.002	0.003	0.003	0.004	0.005	0.006	0.007	0.009	0.009	0.014	0.01	0.011	0.003	0.003	0.002
03_to_04	0.114	0.001	0.001	0.001	0.002	0.006	0.004	0.008	0.011	0.011	0.013	0.019	0.014	0.01	0.006	0.004	0.002
04_to_05	0.116	0.001	0	0.001	0.003	0.007	0.007	800.0	0.011	0.011	0.015	0.02	0.013	0.008	0.005	0.004	0.001
05_to_06	0.116	0.001	0	0.001	0.003	0.009	0.011	0.008	0.01	0.012	0.018	0.022	0.01	0.006	0.004	0.002	0.001
06_to_07	0.101	0.001	0	0	0.001	0.009	0.011	0.007	0.009	0.01	0.015	0.021	0.007	0.003	0.003	0.003	0.001
07_to_08	0.094	0	0	0.001	0.001	0.008	0.013	0.008	0.008	0.011	0.015	0.017	0.005	0.002	0.002	0.001	0
08_to_09	0.076	0	0.001	0	0.002	0.009	0.009	0.006	0.006	0.008	0.012	0.015	0.004	0.001	0.001	0.001	0
09_to_10	0.055	0	0.001	0	0.001	0.005	0.008	0.005	0.004	0.005	0.011	0.009	0.003	0.001	0.001	0.001	0
10_to_11	0.045	0	0.001	0.001	0.001	0.005	0.006	0.004	0.004	0.002	0.01	0.008	0.002	0.001	0	0	0
11_to_12	0.034	0	0	0.001	0.001	0.004	0.005	0.002	0.003	0.001	0.007	0.007	0.001	0.001	0	0	0
12_to_13	0.024	0	0	0.001	0.001	0.003	0.004	0.002	0.002	0.001	0.004	0.004	0.001	0	0	0	0
13_to_14	0.017	0	0	0.001	0.001	0.001	0.003	0.002	0.001	0.001	0.003	0.003	0.001	0	0	0	0
14_to_15	0.012	0	0	0	0.001	0.002	0.003	0.001	0	0.001	0.002	0.001	0.001	0	0	0	0
15_to_16	0.007	0	0	0	0	0.003	0.001	0	0	0.001	0	0.001	0	0	0	0	0
16_to_17	0.005	0	0	0	0	0.001	0.001	0	0	0.001	0	0	0	0	0	0	0
17_to_18	0.003	0	0	0	0	0.001	0	0	0	0.001	0	0	0	0	0	0	0
18_to_19	0.002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19_to_20	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20_to_21	0.001	0	0	0	0	0	0.001	0	0	0	0	0	0	0	0	0	0
21_to_22	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22_to_23	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23_to_24	0.001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

APPENDIX 4-1

Detailed Simulated Results

Wind Velocity Ratio, Base Case

Wind	Velocit	y Ratio,	Base Case													
Tes Point			Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 55W	225 SW	247.5 WSW	Sum	Average	Average
			Probability (Annual)	7.6%	12.4%	21.8%	12.4%	5.5%	4.9%	4.5%	6.7%	5.8%	MSM	83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)	110,00		8.3%	9.7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	1.000	12 annically
P001	833906.48	822110.14		0.078	0.137	0.139	0.154	0.092	0.063	0.088	0.060	0.053	0.113		0.111	0.090
P002	833900,24	822102.33		0.088	0.129	0.119	0.135	0.072	0.054	0.107	0.056	0.070	0.083		0.103	0.084
P003	833894.00	822094.52		0.030	0.111	0.095	0.106	0.062	0.044	0.114	0.078	0.066	0.104	\vdash	0.089	0.082
P004 P005	833890.92 833884.53	822084.84 822077,14		0.133	0.152	0.110	0.140	0.070	0.064	0.181	0.156	0.097	0.159		0.123	0.123
P006	833874.36	822071.19		0.127	0.124	0.033	0.098	0.052	0.049	0.055	0.102	0.192	0.247		0.087	0.111
P007	833864.49	822068.98		0.080	0.098	0.026	0.056	0.062	0.101	0.160	0.056	0.283	0.269		0.084	0.137
P008	833854.52	822072.47		0.030	0.058	0.033	0.037	0.040	0.131	0.220	0.042	0.301	0.246		0.076	0.142
P009	833846,90	822078.91		0,015	0,025	0,028	0.054	0.027	0,114	0,204	0,067	0.284	0.237		0.069	0,139
P010 P011	833839.86	822084.83	-	0.015	0.022	0.022	0.055	0.035	0.111	0.197	0.060	0.284	0.254	-	0.066	0.138
P011	833831.48 833823.50	822091,12 822098.43		0.027	0.025	0.021	0.050	0.028	0.118	0.193	0.108	0.299	0.283	\vdash	0.080	0.164
P013	833819.20	822105.01		0.049	0.085	0.024	0.053	0,028	0,100	0.138	0.241	0,263	0.254		0.088	0.157
P014	833813,78	822113,32		0.029	0.081	0,009	0,050	0,044	0,069	0,092	0,231	0.276	0,294		0.078	0.153
P015	833806.08	822119.70		0.017	0.075	0.019	0.053	0.044	0.045	0,069	0.202	0.263	0.289		0.073	0.141
P016	833799.61	822125.07		0.022	0.068	0.036	0.058	0.045	0.045	0.051	0.214	0.255	0.269	_	0.077	0.140
P017	833806.02 833812.47	822132.74 822140.39		0.016	0.064	0.031	0.056	0.078	0.043	0.028	0.253	0.057	0.044	$\overline{}$	0.062	0.084
P019	833818.91	822148.04		0.023	0.056	0.036	0.029	0.121	0.125	0.046	0.226	0.057	0.069		0.066	0.094
P020	833825.35	822155.68		0.054	0.083	0.053	0.011	0.125	0.148	0.047	0.205	0.062	0.110	-	0.075	0.097
P021	833831.80	822163.33		0.103	0.101	0.077	0.026	0.119	0.157	0.122	0.189	0.062	0.131		0.093	0.109
P022	833836.66	822168.33		0.103	0.087	0.087	0.030	0.104	0.152	0.166	0.211	0.047	0.129		0.096	0.115
P023	833844.35	822161.93		0,104	0.036	0,073	0,014	0,070	0.073	0.132	0,108	0,064	0,034	\vdash	0.067	0.073
P024	833852.03 833859.71	822155.53 822149.12	-	0.081	0.025	0.054	0.042	0.086	0.086	0.079	0.208	0.108	0.057	\vdash	0.073	0.100
P025	833867.39	822143.12		0.070	0.037	0.066	0.051	0.058	0.062	0.089	0.041	0.033	0.060		0.055	0.051
P027	833875.07	822136.32		0.057	0,049	0,050	0.049	0.051	0.021	0,050	0.022	0.046	0.084		0.046	0.044
P028	833882.75	822129.92		0.057	0.058	0.042	0.063	0.051	0.016	0.040	0.014	0.061	0.085		0.047	0.046
P029	833890.44	822123.51		0.053	0.055	0.050	0.064	0.049	0.019	0.052	0.031	0.053	0.081		0.050	0.049
P030 P031	833898.12 833851.44	822117.11 822040.71	-	0.029	0.044	0.028	0.042	0.036	0.020	0.048	0.032	0.061	0.060		0.037	0.042
P031	833846.06	822032,53		0.155	0.119	0.070	0.129	0.203	0.215	0,179	0.055	0.129	0.217		0.122	0,140
P033	833840.32	822041.06		0.132	0.116	0.064	0.115	0.179	0.176	0.133	0.111	0.101	0.211		0.112	0.129
P034	833832.12	822046.78		0.089	0.110	0.072	0.098	0.176	0.179	0.140	0.180	0.095	0.194		0.111	0.138
P035	833823.92	822052.51		0.051	0.098	0.073	0.091	0.161	0.182	0.146	0.216	0.085	0.158		0.107	0.138
P036	833815.73	822058.23	-	0,030	0.087	0.071	0.086	0.139	0.184	0.153	0.229	0.079	0.128	\vdash	0.101	0.134
P037 P038	833806.62 833797.51	822062.36 822066.50		0.027	0.080	0.065	0.085	0.110	0.177	0.146	0.233	0.064	0.108	$\overline{}$	0.095	0.125
P039	833788.41	822070.63		0.030	0.083	0.047	0.088	0.070	0.169	0.125	0.210	0.035	0.116		0.083	0.107
P040	833779.30	822074.76		0.042	0.086	0.046	0.089	0.066	0.159	0.101	0.185	0.030	0.132		0.079	0.099
P041	833770.19	822078.90		0,040	0.087	0.052	0.090	0.061	0.146	0,074	0,152	0,025	0.146		0.075	0.090
P042	833761.09	822083.03		0.038	0.079	0.057	0.088	0.046	0.127	0.043	0.120	0,023	0.161		0.068	0.079
P043	833750.74	822085.73		0.034	0.066	0.061	0.087	0.078	0.090	0.050	0.105	0.027	0.168	\vdash	0.066	0.078
P044 P045	633740.78 833730,81	822086.56 822087.38		0.032	0,059	0.067	0.086	0.130	0.057	0.079	0.100	0.035	0.169	\vdash	0.070	0.084
P046	833720.85	822088.21		0.036	0.051	0.068	0.076	0,103	0.106	0.138	0,104	0.049	0.155		0.074	0.094
P047	833710.88	822089.03		0.054	0.048	0.058	0.066	0.060	0.060	0.086	0.118	0.055	0.135		0.064	0.079
P048	833700.91	822089,86		0.114	0.047	0.062	0.057	0.068	0.042	0.052	0.116	0.056	0.110		0.066	0.071
P049	833690.95	822090.68 822083.21		0.153	0.052	0.143	0.053	0.052	0.052	0.064	0.125	0.053	0.113	-	0.092	0.081
P050 P051	833684.22 833677.77	822085.21		0.157	0.058	0.185	0.029	0.044	0.055	0,070	0,169	0,076	0.160		0.106	0.100
P052	833671.33	822067.91		0.157	0.078	0.213	0.012	0.036	0.068	0.087	0.189	0.069	0.061		0.115	0.096
P053	833664.89	822060.26		0.157	0.078	0.219	0.022	0.034	0.067	0.095	0.198	0.067	0.037		0.119	0.097
P054	833658.45	822052.62		0,154	0.079	0,225	0.031	0.041	0,062	0,103	0.204	0.064	0.027		0.123	0.099
P055	833652.00 833645.56	822044.97		0.148	0,079	0.231	0,032	0.055	0.057	0,120	0.206	0.059	0.048		0.126	0,104
P056 P057	833639.12	822037.32 822029.67		0.140	0.079	0.234	0.035	0.056	0.058	0.125	0.203	0.055	0.061	-	0.126	0.105
P058	833632.67	822022.03		0.124	0.084	0,226	0.098	0.093	0.051	0.096	0.192	0.050	0.055		0.132	0,108
P059	833626,22	822014.39		0.148	0.093	0.207	0.163	0.215	0.166	0.141	0.190	0,051	0,042		0.159	0.140
P060	833619.77	822006.74	-	0.223	0.094	0.192	0.203	0.284	0.264	0.298	0.191	0.053	0.033		0.188	0.177
P061	833611.41	822001.06		0.216	0.084	0.173	0.223	0.268	0.271	0.316	0.186	0.047	0.039	-	0.183	0.178
P062 P063	833602.43 833604.44	822002.93 822013.68		0.178	0.074	0.125	0.248	0.267	0.294	0.346	0.174	0.043	0.026		0.171	0.177
P064	833598.77	822022.34		0.167	0.075	0.121	0.244	0.283	0.327	0.392	0.106	0.028	0.040		0.167	0.172
P065	B33595.43	822031.77		0.146	0.073	0.123	0.214	0.251	0.298	0.352	0.056	0.011	0.069		0.149	0.149
P066	833592.10	822041.20		0.115	0.078	0.139	0.200	0.232	0.279	0.321	0.020	0.007	0.095		0.142	0,137
P067 P068	833588.77 833585.44	822050.63		0.089	0.086	0.151	0.195	0.223	0.269	0.297	0.024	0.025	0.115	\vdash	0.142	0.140
P068	833585.44	822060.05 822069.48		0.129	0.094	0.169	0.195	0.218	0.261	0.274	0.053	0.043	0.125		0.154	0.147
P070	833578.78	822078.91		0.071	0.118	0.229	0.194	0.213	0.245	0.190	0.070	0.059	0.107		0.164	0.146
P071	833575.53	822088.37		0.063	0.137	0.246	0.202	0.225	0.248	0.169	0.069	0.059	0.085		0.172	0.146
P072	833576.05	822098.37		0.113	0.151	0,253	0,209	0,235	0.254	0,155	0.142	0.130	0.140		0.193	0.180
P073	833581.96	822106.63		0.138	0.136	0.248	0.184	0.208	0.225	0.151	0.326	0.312	0.315		0.213	0,256
P075	833591.37 833600.78	822110.01 822113.40		0.128	0.116	0.244	0.150	0.185	0.190	0.134	0.309	0.311	0.316		0.197	0.241
P076	833610.19	822116.78		0.114	0.094	0.236	0.085	0.159	0.131	0.117	0.307	0.342	0.349		0,174	0,231
P077	833619.60	822120.16		0.107	0.085	0.212	0.052	0.144	0.104	0,106	0.309	0,358	0.364		0.162	0,225
P078	833629.01	822123.54		0.097	0.078	0.200	0.037	0.131	0.080	0.094	0.305	0.366	0.370		0.152	0.219
P079	833638.42	822126.92		0.087	0.071	0.187	0.029	0.117	0.049	0.073	0.296	0.371	0.372		0.141	0.209
P080 P081	833647.06 833656.06	822133.14 822137.54		0.076	0.064	0.171	0.038	0.098	0.031	0.058	0.293	0.381	0.377	\vdash	0.134	0.205
P082	833665,90	822139.90		0.042	0.059	0.150	0.029	0.044	0.056	0.059	0.201	0.302	0.268		0.106	0.157
P083	833673.66	822146.21		0.088	0.050	0.110	0.029	0.014	0.090	0.068	0.257	0.399	0.370		0.111	0.194
P084	833683.40	822148.45		0.094	0.018	0.036	0.019	0.019	0.104	0.073	0.202	0.355	0.352		0,080	0.168
P085	833693.40	822148.18		0,082	0,009	0,051	0,019	0.025	0.123	0,065	0.089	0,244	0.283		0.064	0.122
P086	833703.38	822147.62		0.105	0.010	0.059	0,035	0.030	0.142	0.038	0.062	0.231	0.272		0.068	0.115
P087 P088	833712.77 833722.15	822144.13 822140.28		0.105	0.009	0.070	0.047	0.029	0.146	0.073	0.037	0.212	0.253	\vdash	0.071	0.112
P089	833730.70	822136.10		0.044	0.017	0.077	0.065	0.032	0.140	0.118	0.037	0.229	0.266		0.073	0.129
P090	833739.69	822131.73		0,021	0,024	0.068	0.074	0,035	0.141	0.166	0.068	0,240	0.280		0.079	0.139
P091	833748.73	822127.25		0.030	0.014	0.045	0.082	0.033	0.145	0.175	0.086	0.251	0.297		0.077	0.146
P092	833757.74	822122.93		0.036	0.011	0.016	0.087	0.030	0.151	0.177	0.108	0.276	0.323		0.074	0.156
				0.035	0.022	0.014	0.081	0.023	0.152	0.179	0.111	0.294	0.344		0.075	0.161
P093	833766.11	822118.19	-	0.033	0.020	0.035	0.040	0.000	0.475	0.174	0.000	0.303	0.744		D.Dec	15.5.55
P093 P094 P095	833766.11 833773.72 833780.92	822118.19 822111.90 822105.74		0.022	0.029	0.025	0.049	0.009	0.126	0.171	0.066	0,283	0.341		0.066	0.143

Wind Velocity Ratio, Base Case

Wilson W	willu	velocit	y Katio,	Base Case													
Part				Wind direction (Degree)	45 NE	67.5	90	112.5	135	157.5	180	202.5	225 SW	247.5	Sum	Average	Average
March Marc														WSW	83.6%	The contract of the contract o	(Summer)
March Marc			Northing (m)											7.6%			
																	0.135
																	0.138
Page																	0.140
																	0.143
PAGE MINISTA MINISTAL MIN															-		0.145
1985 1985 1995																	0.147
																	0.140
																	0.136
																	0.124
11 131520 1227528																	0.132
111 131124 121125 100																	0.106
111 15190-7																	0,106
131 1319-10 1329-10 1329-10 1319 1318 1318 1319 1329 1319																	0.099
11.1 13179-19 12271-12 10.00										_							0.125
Fig. 1977 1977 1977 1979											-						0.130
111 18377-197 12722-157 1001 1077 0.18 1096 0.187 0.15 0.248 0.097 0.115 0.1																	0,131
																	0.130
																	0,144
1211 13171-02 12171-12 13171-02 12171-12 13171-02 13																	0.142
Fig. 19378-13 19229-15 19																	0.132
\$1,000 \$																	0.129
Fig. 12 Fig.																	0.123
\$1931.1.93 \$2722.4.63 \$0.0056 \$0.0066 \$0.0066 \$0.0072 \$0.072 \$0.073 \$0.0073 \$0.0073 \$0.0072 \$0.0085																	0.111
																	0.095
\$1727.2 \$1771.2 \$177																	0.101
\$1.00 \$1.0	P127	633712.40	822286.84		0.047	0.027	0.116	0.063	0.100	0.057	0.049	0.122	0.034	0.135		0.075	0.081
\$1,000 \$																	0.075
1931 18379-0.00 19220-0.88																	0.073
\$1379.06 \$22720.08 0.066 0.067 0.068 0.069 0.056 0.075 0.075 0.088 0.055 0.067 0.055 0.067 0.055 0.067 0.055 0.067 0.055 0.067 0.055 0.067 0.055 0.067 0.055 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.055 0.057 0.057 0.057 0.057 0.057 0.057 0.057 0.055 0.057																	0.056
																	0.063
\$1916 \$18776.71 \$2222672 0.077			822299.96														0.061
1916 181791-0.																	0.070
Fig.																	0.075
1918 81816678 822246.04 0.109 0.081 0.018 0.012 0.099 0.031 0.122 0.000 0.087 0.088																	0.070
Pi40 Si3822.15 Si3225.25 Si3255.25 O.112 O.074 O.069 O.023 O.075 O.019 O.075 O.017 O.014 O.067 O.075 O.076 O.014 O.076 O.075 O.076 O.077 O																	0.067
Pilar 18389384 183292845 183292485 0.012	P139	833814.46	822261.64		0.111	0.078	0.052	0.018	0.085	0.023	0.111	0.063	0.048	0.108		0.061	0.061
PIAS \$183873 \$21224.24 \$0.109 \$0.064 \$0.072 \$0.074 \$0.065 \$0.075 \$0.072 \$0.143 \$0.084 \$0.075 \$0.074 \$0.085 \$0.075 \$0.075 \$0.085 \$0.075 \$0.085 \$0.075 \$0.085																	0.051
P144 \$33845.22 \$2225.66 0.009																	0.043
P144 3388529 32222667 0.09																	0.049
0.003 0.003 0.004 0.005 0.005 0.0074 0.009 0.010 0.004 0.167 0.000 0.045 0.009 0.003 0.003 0.003 0.005 0.0																	0.057
DOOS 133710.59 231856.06 D.151 D.059 D.059 D.072 D.118 D.076 D.076 D.069 D.076 D.076 D.076 D.076 D.089 D.000 D.077 D.151 D.076 D.089 D.000 D.075 D.151 D.077 D.151 D.075	0001	833688.64	821827.88			0.222		0.204	0.291	0.161	0.118	0.246	0.206			0.214	0.206
DOM \$33737.00 \$21855.14 DOM									-								0.114
0.000 \$33939.32 \$21994.23 0.133 0.007 0.134 0.018 0.116 0.155 0.158 0.285 0.225 0.194 0.110 0.000 0.000 \$33978.52 \$21942.41 0.152 0.030 0.093 0.093 0.093 0.093 0.027 0.255 0.266 0.102 0.007 0.008 0.00																	0.106
0.000 0.0000 0.																	0.171
0.0006 833801.66 821961.48 0.142 0.010 0.050 0.066 0.055 0.068 0.122 0.265 0.117 0.232 0.058 0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.000000 0.0000000 0.00000000															1		0.182
0.009 835817.81 831980.58 0.189 0.020 0.118 0.061 0.042 0.117 0.077 0.238 0.113 0.232 0.105 0.1001 0.118 0.238 0.188 0.198 0.020 0.038 0.038 0.035 0.045 0.172 0.075 0.235 0.102 0.0101 0.038888.89 0.03986.60 0.02077.71 0.118 0.038 0.048 0.037 0.039 0.075 0.235 0.068 0.075 0.021 0.001 0.	0007		821942.41		0.152	0,030	0.093	0.056	0.045	0.062	0.059	0.299	0.214	0.296		0.102	0.157
Color Colo																	0.138
OO11 833890.10 \$22018.75 O.200 O.080 O.049 O.147 O.038 O.045 O.037 O.099 O.075 O.235 O.086 O.0012 S3866.64 S22070.77 O.152 O.150 O.056 O.160 O.156 O.157 O.156 O.157 O.156 O.157 O.156 O.156 O.156 O.156 O.156 O.156 O.156 O.156 O.157 O.156 O.157 O.156 O.156 O.156 O.156 O.156 O.156 O.157 O.156																	0,132
COLID \$33985.00 \$22070.77 COLID CO																	0.089
COLID COLID CO																	0.183
O015 83393.30 83208.87 O128 O.146 O.124 O.137 O.105 O.090 O.071 O.160 O.158 O.221 O.129 O.100 O.166 O.196 O.119 O.100 O.166 O.196 O.119 O.100 O.160 O.185 O.100 O.196 O.119 O.100 O.175 O.123 O.123 O.125 O.104 O.100 O.073 O.167 O.100 O.196 O.119 O.100 O.175 O.185 O.187 O.185	0013		822056.66		0.160	0.136	0.062	0.134	0.090	0.090	0.170	0.112	0.207	0.221		0.118	0.142
OOID 833999.61 821216.88 O.079 O.137 O.123 O.135 O.104 O.100 O.073 O.167 O.100 O.196 O.119 O.1017 O.1018 S.35972.19 822146.60 O.104 O.024 O.148 O.119 O.123 O.117 O.085 O.187 O.079 O.204 O.122 O.1018 O.1024 O.104 O.024 O.148 O.119 O.123 O.117 O.085 O.187 O.079 O.204 O.122 O.10019 O.083 O.181 O.103 O.087 O.084 O.092 O.202 O.093 O.137 O.116 O.116 O.103 O.087 O.084 O.092 O.202 O.093 O.137 O.116 O.10019 O.084 O.092 O.093 O.137 O.116 O.10019 O.084 O.092 O.093 O.087 O.084 O.092 O.093 O.137 O.116 O.116 O.10019 O.084 O.092 O.093 O.137 O.116 O.116 O.115 O.10019 O.084 O.092 O.093 O.137 O.116 O.116 O.116 O.116 O.115 O.025 O.073 O.078 O.126 O.094 O.131 O.125 O.138 O.10019 O.188 O.10019 O.189 O.091 O.189 O.091 O.189 O.091 O.189 O.091 O.189 O.091 O.199 O.091 O.											-		+				0.132
CODIT \$33955.91 \$22127.63 C.0.95 C.0.94 C.1.12 C.1.14 C.1.11 C.1.13 C.0.73 C.1.86 C.0.75 C.1.82 C.1.97 C.1.04 C.1.17 C.1.18 C.0.73 C.1.82 C.1.87 C.0.75 C.1.82 C.1.87 C.1.8									-								0.137
Coll						_									-		0.119
O2020 834004.02 822184.83 0.136 0.184 0.166 0.115 0.025 0.073 0.078 0.126 0.094 0.131 0.135 0.021 0.021 0.02384.10 822099.37 0.169 0.166 0.116 0.152 0.098 0.078 0.163 0.170 0.131 0.205 0.138 0.1002 0.0238 0.0238 0.024 0.0248 0.024					_								-				0.130
OO21 833894.10 822079.37 0.169 0.166 0.116 0.152 0.098 0.078 0.183 0.170 0.131 0.205 0.138 0.1 OO22 833910.40 8220998.32 0.112 0.160 0.137 0.160 0.114 0.086 0.116 0.131 0.024 0.133 0.1 0024 833996.70 82215.23 0.015 0.028 0.984 0.092 0.103 0.105 0.118 0.069 0.118 0.004 0.086 0.166 0.119 0.010 0.004 0.004 0.004 0.004 0.004 0.004 0.008 0.018 0.018 0.018 0.018 0.019 0.004 0.004 0.008 0.004 0.009 0.013 0.007 0.006 0.007 0.006 0.003 0.004 0.009 0.012 0.008 0.004 0.009 0.012 0.008 0.004 0.009 0.023 0.004 0.009 0.0234 0.000 0.009 0.0234																	0.124
CO22 833910.40 822098.32 CO112 CO160 CO137 CO160 CO114 CO.80 CO137 CO127 CO103 CO174 CO133 CO133 CO137 CO127 CO138 CO137 CO138																	0.118
CO23 833926.70 822117.28 CO.991 CO.135 CO.127 CO.140 CO.112 CO.86 CO.116 CO.131 CO.88 CO.196 CO.179 CO.101 CO.202 CO.203																	0.141
O024 833943.00 822136.23 O.115 O.098 O.084 O.092 O.103 O.105 O.117 O.182 O.066 O.179 O.101 O.10025 833995.29 822155.20 O.122 O.136 O.207 O.158 O.207 O.158 O.128 O.112 O.214 O.108 O.189 O.159 O.150 O.026 O.33975.40 822174.31 O.097 O.096 O.103 O.065 O.095 O.083 O.073 O.233 O.081 O.199 O.101 O.101 O.101 O.102 O.027 S33991.52 S22193.42 O.115 O.149 O.105 O.075 O.044 O.070 O.059 O.234 O.060 O.176 O.105 O.036 O.038 O.038 O.038 O.038 O.038 O.045 O.028 O.028 O.028 O.028 O.028 O.028 O.028 O.026 O.028 O.046 O.028 O.046 O.028 O.045 O.028 O.038 O.045 O.028 O.038 O.045 O.028 O.038 O.039 O.038 O.038 O.039 O.																	0.127
O025 833959.29 822155.20 O.122 O.136 O.207 O.158 O.138 O.128 O.112 O.214 O.108 O.189 O.159 O.159 O.206 B.33975.40 B.22174.31 O.097 O.096 O.103 O.065 O.095 O.083 O.073 O.233 O.081 O.196 O.101 O.101 O.102 O.228 O.229 O.224 O.128 O.027 O.2393991.52 B.22195.42 O.113 O.149 O.105 O.075 O.044 O.070 O.059 O.234 O.060 O.176 O.105 O.105 O.028 O.228 O.228 O.026 O.028 O.026 O.028 O.026 O.028 O.026 O.028 O.026 O.028											-				7		0.115
O027 833991.52 822193.42 0.115 0.149 0.105 0.075 0.044 0.070 0.059 0.234 0.060 0.176 0.105 0.05 0028 833795.28 822131.96 0.021 0.058 0.028 0.064 0.063 0.068 0.028 0.175 0.075 0.0 0030 833826.98 822170.63 0.009 0.099 0.082 0.036 0.135 0.138 0.079 0.018 0.055 0.0 0031 833826.98 822170.63 0.007 0.062 0.080 0.085 0.166 0.170 0.165 0.097 0.117 0.100 0.0 0031 833826.88 822189.96 0.047 0.062 0.080 0.085 0.106 0.170 0.163 0.151 0.101 0.100 0.094 0.0 0033 833874.53 822209.29 0.035 0.093 0.076 0.070 0.081 0.162 0.227 0.090 0.138 0.081 <td>0025</td> <td>833959.29</td> <td>822155.20</td> <td></td> <td>0.122</td> <td>0.136</td> <td>0.207</td> <td>0.158</td> <td>0.138</td> <td>0.128</td> <td>0.112</td> <td>0.214</td> <td>0.108</td> <td>0.189</td> <td>1</td> <td>0.159</td> <td>0.155</td>	0025	833959.29	822155.20		0.122	0.136	0.207	0.158	0.138	0.128	0.112	0.214	0.108	0.189	1	0.159	0.155
O028 833795.28 822131.96 0.021 0.058 0.045 0.064 0.063 0.068 0.028 0.234 0.168 0.175 0.075 0.1 O029 833811.13 822151.29 0.028 0.026 0.028 0.040 0.123 0.113 0.038 0.138 0.079 0.018 0.055 0.0 O030 833826.98 822170.63 0.109 0.099 0.082 0.036 0.135 0.129 0.165 0.097 0.117 0.100 0.090 0.031 833824.83 822189.96 0.047 0.062 0.085 0.106 0.170 0.163 0.151 0.101 0.100 0.094 0.0 0.035 0.093 0.076 0.070 0.081 0.162 0.227 0.090 0.138 0.081 0.094 0.1 0.034 833893.83 822247.96 0.093 0.076 0.081 0.167 0.223 0.138 0.081 0.099 0.121 0.0 0.0 0.035 83399																	0.119
OO29 833811.13 822151.29 0.028 0.026 0.028 0.040 0.123 0.113 0.038 0.079 0.018 0.055 0.030 OG30 833826.98 822170.63 0.109 0.099 0.082 0.036 0.185 0.129 0.165 0.097 0.117 0.100 0.03 OG31 833842.83 822189.96 0.047 0.062 0.080 0.085 0.106 0.170 0.163 0.151 0.101 0.100 0.034 OG32 833858.68 822209.99 0.035 0.093 0.076 0.070 0.081 0.162 0.227 0.090 0.138 0.081 0.094 0.0 OG34 833896.28 822228.63 0.090 0.098 0.118 0.118 0.127 0.167 0.223 0.138 0.081 0.090 O34 833890.83 822227.96 0.142 0.127 0.084 0.070 0.093 0.127 0.183 0.089 0.090 0.21																	0.107
O300 833826-98 822170.63 0.109 0.099 0.082 0.036 0.135 0.185 0.129 0.165 0.097 0.117 0.100 0.33 0031 833824_28 822189.96 0.047 0.062 0.080 0.085 0.106 0.170 0.163 0.151 0.101 0.100 0.094 0.3 0032 833884.68 822209.29 0.035 0.093 0.076 0.070 0.081 0.162 0.227 0.090 0.138 0.081 0.094 0.3 0033 833874.53 822228.63 0.090 0.098 0.118 0.118 0.127 0.167 0.223 0.138 0.089 0.090 0.211 0.1 0.034 833890.38 822247.96 0.142 0.127 0.084 0.070 0.093 0.142 0.196 0.093 0.105 0.045 0.106 0.3 0036 833578.83 821900.02 0.141 0.119 0.138 0.078 0.219 0.16																	0.120
031 833842.83 822189.96 0.047 0.062 0.080 0.085 0.106 0.170 0.163 0.151 0.101 0.100 0.094 0.3 0032 833858.68 822209.29 0.035 0.093 0.076 0.070 0.081 0.162 0.227 0.090 0.138 0.081 0.094 0.1 0034 833874.53 822228.63 0.090 0.098 0.118 0.118 0.127 0.167 0.223 0.138 0.089 0.090 0.121 0.1 0034 833890.38 822247.96 0.142 0.127 0.084 0.070 0.093 0.142 0.125 0.045 0.045 0.106 0.045 0.045 0.106 0.035 833906.23 822267.29 0.141 0.119 0.138 0.091 0.077 0.104 0.135 0.081 0.124 0.103 0.116 0.3 0035 833578.89 821994.58 0.246 0.118 0.158 0.159 0.16																	0.118
CO33 833874.53 822228.63 CO90 CO.98 CO.118 CO.118 CO.127 CO.167 CO.223 CO.138 CO.89 CO.99 CO.121 CO.121 CO.121 CO.121 CO.121 CO.122 CO.124 CO.127 CO.124 CO.127 CO.124 CO.125 CO.124 CO.125 CO.124 CO.125 CO.124 CO.125 CO	0031	833842.83	822189.96		0.047	0.062	0.080	0.085	0.106	0.170	0.163	0.151	0.101	0.100		0.094	0.120
0034 833890.38 822247.96 0.142 0.127 0.084 0.070 0.093 0.142 0.105 0.045 0.045 0.106 0.1 0035 833906.23 822267.29 0.141 0.119 0.138 0.091 0.077 0.104 0.135 0.081 0.124 0.103 0.116 0.3 0036 833578.89 821900.02 0.204 0.128 0.078 0.219 0.167 0.088 0.127 0.085 0.231 0.167 0.0 0037 833583.56 821924.58 0.264 0.118 0.158 0.219 0.167 0.088 0.127 0.085 0.231 0.167 0.0 0038 833588.23 821949.14 0.204 0.112 0.070 0.203 0.181 0.224 0.299 0.147 0.088 0.060 0.141 0.3 0039 833598.75 821998.26 0.160 0.068 0.086 0.246 0.249 0.274 0.321 0.171																	0.117
0035 833906.23 822267.29 0.141 0.119 0.138 0.091 0.077 0.104 0.135 0.081 0.124 0.103 0.116 0.13 0036 833578.89 821900.02 0.290 0.140 0.228 0.078 0.219 0.167 0.088 0.127 0.085 0.231 0.167 0.037 833588.59 821924.58 0.264 0.118 0.158 0.130 0.213 0.254 0.196 0.139 0.038 0.054 0.118 0.158 0.130 0.213 0.254 0.196 0.139 0.038 0.054 0.118 0.158 0.130 0.213 0.254 0.196 0.139 0.038 0.060 0.141 0.158 0.038 833598.29 821973.70 0.165 0.130 0.037 0.252 0.218 0.258 0.269 0.176 0.276 0.304 0.164 0.3 0041 833599.75 821998.26 0.160 0.688 0.086 0.246									-		-						0.130
036 833578.89 821900.02 0.290 0.140 0.228 0.078 0.219 0.167 0.088 0.127 0.085 0.231 0.167 0.030 0337 833583.56 821924.58 0.264 0.118 0.158 0.130 0.254 0.136 0.139 0.038 0.054 0.158 0.3 0038 833583.23 821949.14 0.204 0.112 0.070 0.203 0.181 0.224 0.209 0.147 0.088 0.060 0.141 0.0 039 833592.90 821973.70 0.165 0.130 0.037 0.252 0.218 0.258 0.269 0.176 0.276 0.304 0.164 0.0 0404 833597.57 821998.26 0.160 0.068 0.086 0.246 0.240 0.274 0.321 0.171 0.036 0.020 0.152 0.1 0041 833599.77 82198.26 0.167 0.075 0.124 0.239 0.280 0.323																	0.104
0037 833583.56 821924.58 0.264 0.118 0.158 0.130 0.213 0.254 0.196 0.139 0.038 0.054 0.158 0.158 0038 833588.23 821949.14 0.204 0.112 0.070 0.203 0.181 0.224 0.209 0.147 0.088 0.060 0.141 0.1 0039 833592.90 821973.70 0.165 0.130 0.037 0.252 0.218 0.259 0.169 0.76 0.304 0.164 0.2 0040 833592.78 821998.26 0.160 0.068 0.086 0.246 0.240 0.274 0.321 0.171 0.036 0.020 0.152 0.1 0041 833598.79 822023.72 0.167 0.075 0.124 0.239 0.280 0.323 0.387 0.100 0.044 0.166 0.0 0042 833598.77 822047.33 0.102 0.084 0.150 0.198 0.228 0.274 0.306 <td></td> <td>0.141</td>																	0.141
0339 833592.90 821973.70 0.165 0.130 0.037 0.252 0.218 0.258 0.269 0.176 0.276 0.304 0.164 0.7 0040 833597.57 821998.26 0.160 0.068 0.086 0.246 0.240 0.274 0.321 0.171 0.036 0.020 0.152 0.1 0041 833599.77 822023.72 0.167 0.075 0.124 0.239 0.280 0.323 0.387 0.100 0.026 0.044 0.166 0.1 0042 833590.77 822047.33 0.102 0.084 0.150 0.198 0.228 0.274 0.366 0.017 0.017 0.108 0.143 0.0 0043 833592.55 822070.94 0.083 0.105 0.205 0.191 0.213 0.249 0.221 0.063 0.053 0.157 0.1 0044 833574.33 822094.95 0.090 0.149 0.250 0.209 0.234 0.253											_						0.136
O040 833597.57 821998.26 0.160 0.068 0.086 0.246 0.240 0.274 0.321 0.171 0.036 0.020 0.152 0.152 OO41 833598.99 822023.72 0.167 0.075 0.124 0.239 0.280 0.323 0.387 0.100 0.044 0.166 0.3 C042 833590.77 822047.33 0.084 0.150 0.198 0.228 0.274 0.306 0.017 0.018 0.143 0.3 O043 833582.55 822070.94 0.083 0.105 0.205 0.191 0.213 0.249 0.221 0.063 0.053 0.120 0.157 0.13 O044 833582.05 822190.77 0.090 0.149 0.250 0.209 0.234 0.253 0.164 0.066 0.059 0.073 0.179 0.1 O045 833682.05 822190.77 0.181 0.028 0.107 0.149 0.188 0.201 0.134 0.192 </td <td></td> <td>0.143</td>																	0.143
O041 833598.99 822023.72 0.167 0.075 0.124 0.239 0.280 0.323 0.387 0.100 0.026 0.044 0.166 0.1 O042 833590.77 822047.33 0.102 0.084 0.150 0.198 0.228 0.274 0.306 0.017 0.017 0.108 0.143 0.1 O043 833592.55 822070.94 0.083 0.105 0.205 0.191 0.213 0.249 0.221 0.063 0.053 0.157 0.1 O044 833574.33 822094.55 0.090 0.149 0.250 0.209 0.234 0.253 0.164 0.066 0.059 0.073 0.179 0.1 O045 833682.05 822190.77 0.181 0.028 0.107 0.149 0.188 0.201 0.134 0.192 0.165 0.146 0.133 0.1 O046 833673.60 822214.34 0.158 0.038 0.064 0.134 0.141 0.107																	0.226
O042 833590.77 822047.33 0.102 0.084 0.150 0.198 0.228 0.274 0.306 0.017 0.018 0.143 0.13 O043 833582.55 822070.94 0.083 0.105 0.205 0.191 0.213 0.249 0.221 0.063 0.053 0.120 0.157 0.1 O044 833574.33 822094.55 0.090 0.149 0.250 0.209 0.234 0.253 0.164 0.066 0.059 0.073 0.179 0.1 O045 833673.60 8222190.77 0.181 0.028 0.107 0.149 0.188 0.201 0.184 0.059 0.165 0.146 0.053 0.146 0.064 0.134 0.114 0.147 0.098 0.170 0.141 0.129 0.165 0.146 0.133 0.1 O046 833673.60 822219.388 0.094 0.053 0.045 0.114 0.110 0.103 0.065 0.147 0.164 0.064 <td></td> <td>0.163</td>																	0.163
0043 833582.55 822070.94 0.083 0.105 0.205 0.191 0.213 0.249 0.221 0.063 0.053 0.120 0.157 0.1 0044 833574.33 822094.55 0.090 0.149 0.250 0.209 0.234 0.253 0.164 0.066 0.059 0.073 0.179 0.1 0045 833673.60 822219.077 0.181 0.028 0.107 0.149 0.188 0.201 0.134 0.192 0.165 0.146 0.133 0.1 0046 833673.60 822214.34 0.158 0.383 0.064 0.134 0.141 0.147 0.098 0.170 0.141 0.152 0.164 0.088 0.1 0047 833665.14 822237.88 0.094 0.053 0.045 0.114 0.110 0.103 0.065 0.162 0.147 0.164 0.088 0.1																	0.170
O044 ## 33574.33 ## 82293.58 0.090 0.149 0.250 0.209 0.234 0.253 0.164 0.066 0.059 0.073 0.179 0.3 O045 ## 833682.05 ## 822190.77 0.181 0.028 0.107 0.149 0.188 0.201 0.134 0.192 0.165 0.146 0.133 0.3 O046 ## 833673.60 ## 82214.34 0.158 0.038 0.064 0.134 0.141 0.147 0.098 0.170 0.141 0.152 0.106 0.3 O047 ## 833665.14 ## 822237.88 0.094 0.053 0.045 0.114 0.110 0.103 0.065 0.162 0.147 0.164 0.088 0.3					_						-						0.146
O045 833682.05 822190.77 0.181 0.028 0.107 0.149 0.188 0.201 0.134 0.192 0.165 0.146 0.133 0.3 O046 833673.60 822214.34 0.158 0.038 0.064 0.134 0.141 0.147 0.098 0.170 0.141 0.152 0.106 0.3 O047 833665.14 822237.88 0.094 0.053 0.045 0.114 0.100 0.103 0.065 0.162 0.147 0.164 0.088 0.3				A											-		0.146
O047 833665.14 822237.88 0.094 0.053 0.045 0.114 0.110 0.103 0.065 0.162 0.147 0.164 0.088 0.1		833682.05	822190.77			0.028	0.107	0.149		0.201			0.165	0.146		0.133	0,162
					_	_					_	_		_			0.134
	0047	833665.14 833656.27	822237.88 822261.04		0.094	0.053	0.045	0.114	0.110	0.103	0.065	0.162	0.147	0.164		0.088	0.120

	vinu	Velocity Ratio,		ar.	63.5	00	1425	125	irac	100	2025	1 225	242.5			
Dec.		Tes Point	Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 5SW	225 SW	247.5 WSW	5um	Average	Average
STATESTON STAT	in	Fasting (m) Northing (m)	Probability (Annual)												(Annual)	(Summer)
0.000 0.00	72.4		Probability (Summer)		200									81.7%		10000
Description	_											_			0.216	0.245
SEARCH S															0.237	0.190
Control Cont															0.146	0.191
Description															0.128	0.200
Company															0.113	0.127
Compose Compose Co	_														0.093	0.106
			1												0.229	0,281
Company Comp															0.089	0.114
Control Cont	0059														0.127	0.139
Concess Conc															0.093	0.111
DOME BINDALES 231847															0.269	0.238
Compose SENSICIA SIJENSIS SIJENSIS COMPOSE SIJENSIS SIJENSIS SIJENSIS COMPOSE SIJENSIS SIJENSIS SIJENSIS COMPOSE SIJENSIS SI															0.191	0.137
DOME BISSTY, RE BISSS-56 CLIPS															0.171	0.151
0.000 0.00	0065	833601.27 821876.72	1:		0.206		0.186	0.206			0.036				0.155	0.147
0.000 0.00			1												0.167	0.155
0.0000 0															0.119	0.118
COPT B3790-79 B21924-75 COPT														-	0.182	0.206
Control															0.132	0,158
															0.112	0.122
0.075 0.07															0.138	0.173
0076 0338747 031916.77 0.068 0.062 0.058 0.110 0.118 0.047 0.055 0.158															0.106	0.129
														1	0.118	0.140
0.0797 0.0786.02 0.2194.049 0.097 0.067 0.067 0.043 0.008 0.022 0.190 0.018 0.008 0.023 0.008 0.023 0.008 0.023 0.008 0.023 0.008 0.023 0.008 0.023 0.008 0.008 0.023 0.008 0.008 0.023 0.008 0.															0.093	0,128
COURT \$3392.02 \$21945.89 COURT															0.070	0.104
COSE 333974, 621943,69 COSE															0.113	0.138
COSE 339958-94 821996-75 COSE															0.098	0.122
COMPAN C															0.092	0.119
COMPAN C															0.162	0.197
COSE \$33885,34 \$2204.21			J. T.												0.200	0.216
Confect Conf			1												0.183	0.215
COSS \$33970.62 \$31977.70 \$0.160 \$0.197 \$0.180 \$0.055 \$0.145 \$0.129 \$0.255 \$0.165 \$0.185 \$0.165 \$0.187 \$0.088 \$33992.78 \$20204.73 \$0.208 \$0.041 \$0.145 \$0.120 \$0.225 \$0.291 \$0.310 \$0.355 \$0.161 \$0.197 \$0.099 \$33919.718 \$20200.595 \$0.161 \$0.197 \$0.009 \$33919.118 \$20200.595 \$0.161 \$0.099 \$0.018 \$0.119 \$0.114 \$0.125 \$0.226 \$0.226 \$0.226 \$0.119 \$0.159 \$0.348 \$0.0091 \$0.00															0.159	0.218
Cornel C			1												0.175	0.199
COSP 833915.11 822000.95 COSP															0.199	0,233
COP21 833895.99 822086.28 COP22 CO200 CO69 CO63 CO207 CO242 CO200 CO244 CO207 CO244 CO207 CO208 CO244 CO207 CO208 CO244 CO207 CO208	0089	833932.78 822004.73				0,145	0.120	0.226	0.228	0.204	0.119	0,159	0.248		0.145	0.173
0.0029 83353.22 822049.51 0.132 0.119 0.005 0.114 0.201 0.255 0.228 0.076 0.106 0.204 0.0033 83353.39 82205.52 0.006 0.076 0.070 0.060 0.068 0.124 0.211 0.227 0.116 0.181 0.004 0.004 0.004 0.004 0.005															0.139	0.183
0099 833833.90 822065.25 0.026 0.070 0.060 0.069 0.124 0.124 0.124 0.022 0.176 0.181 0.134 0.094 0.083 0.083 0.084 0.083 0.085 0.086 0.088 0.124 0.021 0.160 0.020 0.161 0.255 0.255 0.066 0.877 0.880 0.127 0.026 0.087 0.082 0.085 0.086 0.087 0.087 0.085 0.086 0.087 0.087 0.087 0.085 0.086 0.087 0.085 0.086 0.087 0.085 0.085 0.086 0.087 0.085															0.113	0.181
COMPS 83381A39 82200.088 O.024 O.043 O.043 O.045 O.046 O.188 O.213 O.206 O.114 O.194															0.101	0.152
OO96 833775.48 832112.73 O.026 O.037 O.032 O.046 O.012 O.126 O.174 O.073 O.301 O.352			1												0.088	0.156
COSP 833754.94 822126.43 COSP															0.084	0.157
COSS 83173.40 822140.31 0.038 0.038 0.099 0.056 0.047 0.139 0.127 0.082 0.328 0.399 0.059 0.059 0.042 0.140 0.066 0.048 0.311 0.320 0.009 0.051 0.021 0.042 0.042 0.040 0.069 0.058 0.311 0.320 0.010 0.33846.35 822062.10 0.011 0.011 0.011 0.022 0.090 0.099 0.153 0.204 0.069 0.255 0.238 0.010 0.33822.21 822094.42 0.013 0.026 0.021 0.047 0.044 0.150 0.188 0.162 0.309 0.259 0.008 83282.21 822094.42 0.013 0.026 0.021 0.047 0.044 0.150 0.188 0.162 0.309 0.259 0.008 0.03822.21 0.0383805.84 822110.23 0.053 0.068 0.059 0.066 0.067 0.064 0.055 0.068 0.055 0.068 0.067 0.065 0.065															0.071	0.150
COSP 833704.92 822150.52 0.088 0.019 0.052 0.042 0.042 0.140 0.066 0.098 0.351 0.320															0.078	0.160
COLON \$33863.55 \$22062.10 COLON COLO															0.078	0.144
COLOR \$333825.21 \$32094.42 0.013 0.026 0.021 0.047 0.014 0.130 0.198 0.162 0.309 0.289 0.103 833805.84 \$22110.23 0.018 0.080 0.011 0.049 0.029 0.096 0.152 0.183 0.332 0.338 0.014 833785.64 \$22124.96 0.034 0.050 0.063 0.067 0.041 0.116 0.095 0.189 0.402 0.414 0.005 833785.65 322140.48 0.077 0.022 0.065 0.040 0.060 0.096 0.042 0.200 0.418 0.418 0.005 0.033746.17 322155.62 0.057 0.046 0.035 0.028 0.076 0.072 0.078 0.079 0															0.101	0.149
Color			1												0.070	0.142
Old 833765,68 822124,96 O.034 O.050 O.053 O.067 O.041 O.116 O.095 O.189 O.402 O.414 O.05 O.053 O.065 O.040 O.060 O.066 O.042 O.000 O.418 O.418 O.418 O.077 O.025 O.085 O.040 O.066 O.066 O.066 O.078 O.079 O.418 O.418 O.079 O.046 O.053 O.026 O.076 O.077 O.078 O.174 O.386 O.379 O.076 O.077 O.086 O.078 O.078 O.078 O.078 O.078 O.078 O.078 O.078 O.078 O.079 O.088 O.079 O.088 O.021 O.066 O.066 O.069 O.088 O.028 O.066 O.099 O.088 O.028 O.066 O.099 O.088 O.028 O.066 O.099 O.088 O.028 O.088 O.021 O.047 O.091 O.131 O.166 O.340 O.266 O.086 O.086 O.086 O.088 O.021 O.047 O.091 O.131 O.166 O.340 O.266 O.086 O.088															0.075	0.163
O105 833766.05 822140.48 O.077 O.022 O.065 O.040 O.060 O.066 O.042 O.200 O.418 O.418 O.066 O.066 O.033 O.078					-							-			0.081	0,168
O106 833746.17 822155.62 O.057 O.046 O.053 O.028 O.076 O.072 O.078 O.174 O.386 O.379 O107 835723.15 822188.33 O.073 O.046 O.038 O.020 O.066 O.099 O.098 O.088 O.148 O.318 O.288 O108 833700.02 822152.19 O.115 O.029 O.038 O.021 O.047 O.091 O.131 O.166 O.340 O.266 O109 833664.88 822149.89 O.066 O.066 O.056 O.044 O.055 O.076 O.089 O.044 O.070 O.380 O110 833664.88 822149.89 O.066 O.056 O.056 O.044 O.055 O.076 O.080 O.283 O.414 O.382 O111 83364.28 822143.66 O.077 O.062 O.062 O.066 O.064 O.096 O.033 O.099 O.332 O.430 O.423 O112 833617.67 822133.44 O.114 O.074 O.194 O.055 O.076 O.080 O.067 O.378 O.437 O.443 O113 833594.06 822152.22 O.151 O.095 O.217 O.094 O.131 O.104 O.048 O.431 O114 833570.45 82216.99 O.202 O.140 O.209 O.182 O.191 O.104 O.104 O.433 O115 833546.84 822100.77 O.230 O.109 O.070 O.091 O.090 O.094 O.131 O.104 O.432 O116 833532.23 82120.075 O.230 O.109 O.090 O.064 O.194 O.120 O.228 O.151 O.044 O117 83349.62 822092.33 O.284 O.112 O.134 O.104 O.235 O.157 O.201 O.531 O.429 O.380 O118 833456.04 822008.10 O.333 O.135 O.163 O.141 O.140 O.228 O.151 O.445 O.404 O117 833496.02 822084.10 O.303 O.135 O.163 O.141 O.243 O.174 O.203 O.524 O.404 O.331 O118 833456.01 822084.10 O.303 O.135 O.163 O.141 O.243 O.174 O.203 O.524 O.404 O.331 O119 833656.67 822177.18 O.069 O.060 O.061 O.060 O.066															0.096	0.191
Color															0.090	0,177
O109 833684.50 822152.29 O.115 O.029 O.038 O.023 O.026 O.105 O.085 O.244 O.407 O.380	0107									0,098	0.148	0,318		-	0.080	0.152
O110 83364.88 822149.89 O.066 O.056 O.147 O.044 O.055 O.076 O.080 O.283 O.414 O.382															0.093	0.163
O111 833641.28 822141.66 0,072 0,062 0,166 0.064 0.096 0.033 0.069 0.332 0.430 0.423 O112 833617.67 822133.44 0.114 0.074 0.194 0.058 0.109 0.080 0.067 0.378 0.433 0.443 O113 833594.06 822125.22 0.151 0.095 0.217 0.094 0.131 0.130 0.110 0.408 0.431 0.437 O114 833570.45 822116.99 0.202 0.140 0.209 0.182 0.191 0.211 0.194 0.443 0.442 0.439 O115 833546.84 822108.77 0.230 0.109 0.070 0.091 0.194 0.120 0.260 0.476 0.443 0.423 O117 833496.28 8222092.33 0.284 0.112 0.134 0.104 0.235 0.157 0.201 0.531 0.449 0.380 O118 833496.21 822084.0 <															0.093	0.191
O112 833617.67 322133.44 0.114 0.074 0.194 0.058 0.109 0.080 0.067 0.378 0.437 0.443 0113 83359.0.65 822125.22 0.151 0.095 0.217 0.094 0.131 0.130 0.110 0.408 0.431 0.437 0114 833570.45 822116.99 0.202 0.140 0.209 0.182 0.191 0.211 0.194 0.443 0.442 0.439 0115 833546.84 822108.77 0.230 0.109 0.070 0.091 0.194 0.120 0.260 0.476 0.443 0.423 0116 833523.23 822100.55 0.261 0.093 0.995 0.064 0.210 0.120 0.228 0.511 0.404 0.303 0.135 0.163 0.141 0.243 0.177 0.201 0.521 0.404 0.331 0.148 0.104 0.235 0.157 0.201 0.523 0.324 0.404 0.331 0.			1									-			0.143	0.231
0114 833570.45 822116.99 0.202 0.140 0.209 0.182 0.191 0.211 0.194 0.443 0.442 0.439 0115 833546.84 822100.77 0.230 0.109 0.070 0.991 0.194 0.120 0.260 0.476 0.433 0.423 0116 833523.23 822100.55 0.261 0.093 0.095 0.064 0.210 0.120 0.228 0.511 0.445 0.404 0117 833499.62 822092.33 0.284 0.112 0.134 0.104 0.235 0.157 0.201 0.531 0.429 0.380 0118 833476.01 822084.10 0.333 0.135 0.163 0.141 0.243 0.174 0.203 0.524 0.404 0.331 0119 833452.40 822075.88 0.315 0.148 0.179 0.157 0.238 0.176 0.217 0.474 0.367 0.258 0121 833660.27 822164.97 <															0.163	0,249
O115 833546.84 822108.77 0.230 0.109 0.070 0.091 0.194 0.120 0.260 0.476 0.443 0.423 O116 833552.23 822100.55 0.261 0.093 0.995 0.064 0.210 0.120 0.228 0.511 0.445 0.404 O117 833496.02 822092.33 0.284 0.112 0.134 0.104 0.235 0.157 0.201 0.531 0.429 0.380 O118 833476.01 822084.10 0.303 0.135 0.163 0.141 0.243 0.174 0.203 0.524 0.404 0.331 O119 833452.40 822075.88 0.315 0.148 0.179 0.157 0.238 0.176 0.217 0.474 0.367 0.258 0120 833660.27 822177.18 0.069 0.048 0.153 0.044 0.104 0.066 0.166 0.244 0.415 0.340 0121 833660.27 822156.74 <															0.190	0.271
O116 833523.23 822100.55 O.261 O.093 O.095 O.064 O.210 O.120 O.228 O.511 O.445 O.404															0.230	0.313
0117 833499.62 822092.33 0.284 0.112 0.134 0.104 0.235 0.157 0.201 0.531 0.429 0.380 0118 833476.01 822084.10 0.303 0.135 0.163 0.141 0.243 0.174 0.203 0.524 0.404 0.331 0119 833452.40 822075.88 0.315 0.148 0.179 0.157 0.238 0.176 0.217 0.474 0.367 0.258 0120 833676.62 822177.18 0.069 0.048 0.153 0.044 0.104 0.066 0.166 0.244 0.415 0.340 0121 833660.27 822164.97 0.051 0.052 0.142 0.050 0.090 0.033 0.126 0.290 0.455 0.409 0122 833650.67 822156.74 0.056 0.052 0.151 0.098 0.087 0.068 0.095 0.324 0.466 0.443 0123 833583.65 822140.30 <	_														0.179	0.291
O118 833476.01 822084.10 0.303 0.135 0.163 0.141 0.243 0.174 0.203 0.524 0.404 0.331 O119 833452.40 822075.88 0.315 0.148 0.179 0.157 0.238 0.176 0.217 0.474 0.367 0.258 O121 833660.27 822177.18 0.069 0.048 0.153 0.044 0.104 0.066 0.166 0.244 0.415 0.340 O121 833660.27 822164.97 0.051 0.052 0.142 0.050 0.090 0.033 0.126 0.290 0.455 0.409 O122 833636.67 822144.97 0.056 0.052 0.151 0.098 0.087 0.068 0.095 0.324 0.466 0.443 0123 833613.06 822144.52 0.093 0.049 0.159 0.108 0.062 0.064 0.034 0.554 0.466 0.443 0124 833558.45 822142.030													-		0.208	0,303
O120 833676.62 822177.18 0.069 0.048 0.153 0.044 0.104 0.066 0.244 0.415 0.340 O121 833660.27 822164.97 0.051 0.052 0.142 0.050 0.090 0.033 0.126 0.290 0.455 0.409 O122 83366.67 822155.74 0.056 0.052 0.151 0.098 0.087 0.068 0.095 0.324 0.466 0.443 O123 8335613.06 822148.52 0.093 0.049 0.139 0.108 0.062 0.064 0.034 0.354 0.466 0.451 O124 833589.45 822140.30 0.134 0.061 0.160 0.092 0.068 0.065 0.085 0.366 0.453 0.437 O125 833565.84 822132.07 0.197 0.105 0.147 0.135 0.141 0.146 0.189 0.374 0.436 0.412 O127 833518.62 822115.63 0.242 <	_	833476.01 822084.10					_				0.524	_			0.226	0.302
O121 833660.27 822164.97 0.051 0.052 0.142 0.050 0.090 0.033 0.126 0.290 0.455 0.409 0122 833636.67 822156.74 0.056 0.052 0.151 0.098 0.087 0.068 0.095 0.324 0.466 0.443 0123 833513.06 822148.52 0.093 0.049 0.159 0.108 0.062 0.064 0.034 0.354 0.466 0.451 0124 833589.45 822140.30 0.134 0.061 0.160 0.092 0.068 0.065 0.365 0.354 0.437 0125 833565.84 822132.07 0.197 0.105 0.147 0.135 0.141 0.146 0.189 0.374 0.436 0.412 0126 833542.23 822123.85 0.242 0.157 0.131 0.186 0.241 0.243 0.269 0.384 0.419 0.391 0127 833495.01 822107.40 0.249 <												-			0.229	0.284
0122 833636.67 822156.74 0.056 0.052 0.151 0.098 0.087 0.068 0.095 0.324 0.466 0.443 0123 833613.06 822148.52 0.093 0.049 0.159 0.108 0.062 0.064 0.034 0.554 0.466 0.451 0124 833589.45 822140.30 0.134 0.061 0.160 0.092 0.068 0.065 0.085 0.366 0.453 0.437 0125 833565.84 822132.07 0.197 0.105 0.147 0.135 0.141 0.146 0.189 0.374 0.436 0.412 0126 833542.23 822115.63 0.242 0.157 0.131 0.186 0.241 0.243 0.269 0.384 0.419 0.391 0127 833545.01 822107.40 0.254 0.163 0.144 0.177 0.275 0.259 0.276 0.399 0.402 0.383 0129 833471.40 822099.18 <															0.134	0.216
0123 833613.06 822148.52 0.093 0.049 0.159 0.108 0.062 0.064 0.034 0.354 0.466 0.451 0124 833589.45 822140.30 0.134 0.061 0.160 0.092 0.068 0.065 0.085 0.366 0.453 0.437 0125 833596.84 822132.07 0.197 0.105 0.147 0.135 0.141 0.146 0.189 0.374 0.436 0.412 0126 833542.23 822123.85 0.242 0.157 0.131 0.186 0.241 0.243 0.269 0.384 0.419 0.391 0127 833518.62 822115.63 0.254 0.163 0.144 0.177 0.259 0.259 0.384 0.419 0.383 0128 833495.01 822107.40 0.249 0.162 0.167 0.177 0.289 0.259 0.261 0.405 0.389 0.390 0129 83347.40 822099.18 0.267 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.133</td><td>0,229</td></t<>															0.133	0,229
0124 833589,45 822140,30 0.134 0.061 0.160 0.092 0.068 0.065 0.085 0.366 0.453 0.437 0125 833568,84 822132,07 0.197 0.105 0.147 0.135 0.141 0.146 0.189 0.374 0.436 0.412 0126 833542,23 822123,85 0.242 0.157 0.131 0.186 0.241 0.249 0.269 0.384 0.419 0.391 0127 833518,62 822115,63 0.254 0.163 0.144 0.177 0.259 0.259 0.269 0.384 0.419 0.391 0128 833495,01 822107,40 0.249 0.162 0.167 0.177 0.289 0.259 0.261 0.405 0.389 0.390 0129 833471,40 822099,18 0.267 0.168 0.187 0.186 0.292 0.259 0.255 0.418 0.435 0.380 0130 833487,79 822090,96 <															0.150	0.245
0126 833542.23 822123.85 0.242 0.157 0.131 0.186 0.241 0.243 0.269 0.384 0.419 0.391 0127 833518.62 822115.63 0.254 0.163 0.144 0.177 0.275 0.259 0.276 0.399 0.402 0.383 0128 833495.01 822107.40 0.249 0.162 0.167 0.177 0.289 0.259 0.251 0.405 0.389 0.390 0129 833471.40 822099.18 0.267 0.168 0.187 0.186 0.292 0.259 0.255 0.418 0.435 0.380 0130 833447.79 822090.96 0.282 0.171 0.195 0.192 0.291 0.255 0.249 0.450 0.440 0.354 0131 83388.29 82180.88 0.107 0.087 0.104 0.057 0.169 0.117 0.055 0.49 0.410 0.071 0132 833798.99 822196.77	0124	833589.45 822140.30		0.134	0.061	0.160	0.092	0.068	0.065	0.085	0.366	0.453	0.437		0.156	0.247
0127 833518.62 822115.63 0.254 0.163 0.144 0.177 0.275 0.259 0.276 0.399 0.402 0.383 0128 833495.01 822107.40 0.249 0.162 0.167 0.177 0.289 0.259 0.261 0.405 0.389 0.390 0129 833471.40 822099.18 0.267 0.168 0.187 0.186 0.292 0.255 0.218 0.435 0.380 0130 83347.79 822090.96 0.282 0.171 0.195 0.192 0.291 0.255 0.249 0.450 0.440 0.354 0131 833818.29 822180.88 0.107 0.087 0.104 0.057 0.106 0.148 0.169 0.117 0.038 0.54 0132 833798.99 822196.77 0.054 0.031 0.038 0.128 0.091 0.140 0.201 0.211 0.005 0.029 0133 833779.70 822212.67 0.031 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.187</td><td>0.273</td></td<>															0.187	0.273
O128 833495.01 822107.40 0.249 0.162 0.167 0.177 0.289 0.259 0.261 0.405 0.389 0.390 0129 833471.40 822099.18 0.267 0.168 0.187 0.186 0.292 0.259 0.255 0.418 0.435 0.380 0130 833447.79 822090.96 0.282 0.171 0.195 0.192 0.291 0.255 0.249 0.450 0.440 0.354 0131 833818.29 822180.88 0.107 0.087 0.104 0.051 0.148 0.169 0.117 0.038 0.054 0132 833798.99 822196.77 0.054 0.038 0.128 0.091 0.140 0.201 0.211 0.105 0.037 0.029 0133 833779.70 822212.67 0.031 0.038 0.137 0.097 0.129 0.205 0.225 0.119 0.091 0.077															0.219	0.302
O129 833471.40 822099.18 0.267 0.168 0.187 0.186 0.292 0.259 0.255 0.418 0.435 0.380 O130 833447.79 822099.96 0.282 0.171 0.195 0.192 0.291 0.255 0.249 0.450 0.440 0.354 O131 833818.29 822180.88 0.107 0.087 0.104 0.057 0.148 0.169 0.117 0.038 0.054 O132 833798.99 822126.77 0.054 0.038 0.128 0.091 0.140 0.201 0.211 0.105 0.037 0.029 O133 833779.70 822212.67 0.031 0.038 0.137 0.097 0.129 0.205 0.225 0.119 0.091 0.077															0.227	0.306
0130 833447.79 822090.96 0.282 0.171 0.195 0.192 0.291 0.255 0.249 0.450 0.440 0.354 0131 833818.29 822180.88 0.107 0.087 0.104 0.057 0.106 0.148 0.169 0.117 0.038 0.054 0132 833798.99 822196.77 0.054 0.038 0.128 0.091 0.140 0.201 0.211 0.105 0.037 0.029 0133 833779.70 822212.67 0.031 0.038 0.137 0.097 0.129 0.205 0.225 0.119 0.091 0.077															0.232	0.307
O132 833798.99 822196.77 0.054 0.038 0.128 0.091 0.140 0.201 0.211 0.105 0.037 0.029 O133 833779.70 822212.67 0.031 0.038 0.137 0.097 0.129 0.205 0.225 0.119 0.091 0.077															0.253	0.326
O133 833779.70 822212.67 0.031 0.038 0.137 0.097 0.129 0.205 0.225 0.119 0.091 0.097															0.097	0.094
															0.103	0,109
	O133	833779.70 822212.67 833760.40 822228.57		0.031	0.038	0.137	0,097	0.129	0.205	0.225	0.119	0,091	0.077		0.110	0.130
0.134 833760.40 822228.57 0.026 0.057 0.141 0.076 0.097 0.195 0.229 0.074 0.040 0.050 0.055 0.135 833741.11 822244.46 0.015 0.084 0.150 0.055 0.113 0.206 0.235 0.032 0.035 0.035															0.100	0.103
0136 833721.81 822260.36 0.048 0.093 0.134 0.022 0.072 0.180 0.209 0.021 0.032 0.041															0.088	0.079
O137 833702.52 822276.26 0.048 0.032 0.096 0.053 0.072 0.143 0.135 0.049 0.061 0.051	0137	833702.52 822276.26		0.048	0.032	0.096	0.053	0.072	0.143	0.135	0.049	0.061	0.051		0.072	0.078
O138 833949.25 822153.86 0.109 0.138 0.217 0.166 0.131 0.115 0.099 0.178 0.127 0.122														1	0.158	0.145
0139 833930.31 822170.04 0.058 0.102 0.254 0.195 0.132 0.078 0.058 0.116 0.068 0.043												_			0.148	0.114
0140 B33911.51 822185.72 0.111 0.066 0.210 0.182 0.136 0.072 0.062 0.164 0.081 0.091 0141 833892.39 822202.46 0.117 0.031 0.154 0.153 0.122 0.044 0.069 0.175 0.118 0.156															0.139	0.124
0.142 0.33697.379 0.2222.40															0.117	0.138
0143 833855.40 822235.72 0.103 0.037 0.111 0.098 0.131 0.029 0.075 0.096 0.027 0.160															0.084	0.084
0144 833836.08 822251.59 0.107 0.058 0.109 0.080 0.127 0.042 0.075 0.060 0.034 0.121	0144	833836.08 822251.59		0.107	0.058	0.109	0.080	0.127	0.042	0.075	0.060	0.034	0.121		0.083	0.074

	vvina	Velocity Ratio,		AE	cre	1 00	112.5	125	1575	180	2025	225	247.5			
		Tes Point	Wind direction (Degree) Wind direction	45 NE	67.5 ENE	90 E		135 SE	157.5 SSE		202.5 55W	225 SW	247.5 WSW	Sum	Average	Average
March Marc	ID	Easting (m) Northing (m)			12.4%		12.4%	6,5%	4.9%	4.5%	6.7%	6.8%			(Annual)	(Summer)
1987 1987 1987 1988		The second secon	Probability (Summer)	0.100	0.000									81.7%	0.024	0.070
100 100	_					_						_	_			
Second S																
100 100	0148				0.261		0.122	0.125	0.124	0.128					0.204	0.169
Section Column					_		_									
STATE STAT																
STATE STAT																
1975 1976																
1985 1987	0154	833975.47 822219.16		0.131	0.160		0.159	0.126	0.097	0.032	0.129	0.156	0.146		0.163	0.137
1975 1975												_				
1975 1987-100 1977-100 1978 1979																
1915 1917-10, 1927-14, 1918 1919 1		The second secon														
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Cold					_					-						
1946 1937-1943					_											
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10 13 13 13 13 13 13 13	0165	833794.55 822319.81		0.105	0.122	0.048	0.078	0.048	0.066	0.095	0.039	0.124	0.031		0.077	0.071
1956 1957-145 1272-145 1959																
1999 1999																
1975 1985 1975																
Column C																
Column C	0171	833653.54 822268.68		0,088	0,054	0.157	0.098	0.035	0.047	0.129	0.170	0,145	0.179	5.00	0.109	0.126
1975 1975																
1975 1985 1922 1975																
Column C																
Column C																
0.1916 0.1914 0.192 0.193 0.193 0.193 0.193 0.195 0.	0177	833512.52 822217.55		0.186	0.152	0.196	0.296	0.260	0.223	0.218	0.234	0.202	0.228		0.215	0.230
1916 61814-15 22219-18																
1918 835416.51 822318.46																
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0232 834037.68 822248.19 0.199 0.093 0.209 0.118 0.094 0.159 0.067 0.215 0.172 0.081 0.155 0.148 0233 834018.66 822264.41 0.080 0.021 0.239 0.123 0.083 0.166 0.038 0.055 0.184 0.037 0.128 0.118 0234 833991.38 822280.02 0.104 0.060 0.198 0.114 0.072 0.166 0.038 0.055 0.032 0.116 0.092 0235 833979.88 822295.97 0.179 0.125 0.215 0.141 0.095 0.157 0.011 0.046 0.059 0.031 0.137 0.087 0236 833960.00 822311.88 0.154 0.103 0.174 0.121 0.085 0.146 0.034 0.025 0.051 0.019 0.115 0.075 0237 833942.31 822328.92 0.119 0.045 0.125 0.095 0.057																
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Wind	Velocit	y Ratio,	Base Case													
	Tes Point		Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 55W	225 SW	247.5 WSW	Sum	Average	Aumenin
			Probability (Annual)	7.6%	12.4%	21.8%	12.4%	5.5%	4.9%	4.5%	6.7%	5.8%	M2M	83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)			8.3%	9.7%	7,6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	- Francis	12 ministry
0241	833866.22	822391.65		0.078	0.101	0.033	0.042	0.040	0.092	0.036	0.056	0.115	0.046		0.061	0.063
0242	833851.35	822407,57		0.136	0.121	0.087	0.064	0.086	0.072	0.096	0.046	0.103	0.047		0,091	0.076
O243 O244	833827.89 833804.30	822398.95 822390.67		0.115	0.094	0.051	0.019	0.099	0.032	0.118	0.067	0.062	0.020		0.067	0.059
0245	833780.78	822382.18		0.109	0.082	0.025	0.029	0.051	0.032	0.123	0.075	0.076	0,074		0.054	0.056
0246	833757.33	822373.51		0.067	0.036	0.063	0.009	0.066	0.033	0.057	0.061	0.031	0.076		0.047	0.047
0247	833734.04	822364.43		0.049	0.024	0.054	0.020	0.067	0.039	0.079	0.075	0.014	0.097		0.044	0.052
0248	833710.59	822355.78		0.030	0.042	0.082	0.015	0.093	0.081	0.106	0.079	0.042	0.115		0.060	0.072
0249	833687.02 833663.42	822347.45 822339.18		0.132	0.119	0.084	0.037	0,104	0,109	0.113	0.104	0.109	0.146	_	0,095	0.100
0251	833639.95	822330.58		0.249	0.191	0.056	0.050	0.109	0.051	0.043	0.218	0.199	0.203		0.127	0.135
0252	833616.38	822322.23		0.242	0.177	0.047	0.069	0.090	0.086	0.113	0.261	0.234	0.213		0.129	0.156
O253	833593.28	822312.67		0.220	0.126	0,034	0.038	0,060	0,109	0.127	0,290	0,266	0,245		0.116	0.167
0254	833569,92	822303.77		0.177	0.135	0.080	0.021	0,033	0.124	0,133	0,233	0.212	0.231	\perp	0,113	0.147
0255	833546.38 833522.92	822295.35 822286.72		0.234	0.184	0.046	0.056	0.016	0.094	0.074	0.040	0.034	0.205	\vdash	0.086	0.064
0257	833499.46	822278.09		0.203	0.235	0.029	0.045	0.018	0.111	0.053	0.244	0.205	0.264		0.116	0.138
0258	833475.98	822269.49		0.210	0.141	0.021	0.024	0.016	0.088	0.055	0.254	0.216	0.270		0.096	0.136
0259	833452.58	822260.70		0.247	0.182	0.031	0.053	0.041	0.076	0,036	0.248	0.213	0.282		0.112	0,138
0260	833429.26	822251,69		0.287	0.206	0.051	0.148	0.074	0.016	0.009	0.229	0.197	0.290		0.133	0.140
OZ61 OZ62	833405.77 833381.89	822243.13 822234.73	-	0.265	0.181	0.048	0.187	0.068	0.063	0.028	0.114	0.135	0.281		0.122	0.117
O262 O263	833661.30	822392,32		0.200	0.083	0,063	0,033	0.022	0.030	0.050	0.222	0.266	0.302		0.050	0.050
0264	833639.45	822380.18		0.214	0.176	0.026	0.013	0.049	0.052	0.043	0.127	0.064	0.037		0.079	0.058
0265	833617.91	822367.49		0.249	0.220	0.037	0.084	0.091	0.116	0.033	0.061	0.041	0.040		0.101	0.060
0266	833594.76	822358.04		0.226	0.229	0.068	0.132	0.153	0.172	0.050	0.170	0.078	0.045		0.136	0.110
0267	833571.50	822348.88		0.194	0,085	0,081	0.123	0.108	0.134	0.087	0.078	0.102	0.097		0.105	0.100
O268 O269	833548.06 833524.81	822340.20 822331.01		0.114	0.101	0.101	0.145	0.136	0.145	0.075	0.149	0.150	0.057		0.120	0,125
0270	833501.49	822321.99		0.221	0.090	0.080	0.133	0.065	0.065	0.036	0.136	0.170	0.166		0.113	0.109
0271	533471.89	822335.41		0.079	0.137	0.034	0.091	0.060	0.094	0.009	0.162	0.051	0.243		0.078	0.092
0272	833448.29	822327.15		0,078	0.011	0.027	0,022	0,016	0,046	0,033	0,077	0.142	0,283	1	0.043	0.084
0273	833425.53	822318.81		0.023	0.059	0.024	0.017	0.011	0.037	0.059	0.204	0.224	0.328		0.060	0.128
O274 O275	833401.62 833378.55	822309.78 822301.33		0.192	0.177	0.019	0.021	0.021	0.020	0.027	0.293	0.240	0.329		0.099	0.143
0276	833677.38	821849.60		0.197	0.109	0.160	0.083	0.247	0.143	0.198	0.325	0.197	0.078		0.168	0.190
0277	833693.33	821868.85		0.192	0.051	0.070	0.065	0.166	0.131	0.150	0.257	0.211	0.188		0.119	0.166
0278	B33709.27	821888.11		0.167	0.053	0.074	0.042	0.155	0.133	0.125	0.212	0.218	0.238		0.110	0.158
0279	833725.22	821907.36		0.109	0.051	0.141	0.043	0.165	0.146	0.138	0.220	0.213	0.275		0.124	0,173
O280 O281	833741.17 833757.11	821926.61 821945.87	-	0.094	0.052	0.181	0.076	0.164	0.164	0.163	0.248	0.211	0.327	\vdash	0.143	0,195
0282	833773.06	821965.12		0.136	0.064	0.095	0.071	0.080	0.077	0.081	0.293	0,203	0.369		0.112	0.170
0283	833789.01	821984.38		0.141	0.076	0.064	0.074	0.044	0.074	0.073	0.304	0.168	0.345		0.101	0.155
0284	633804.95	822003.63		0.142	0.093	0.097	0.092	0.041	0.037	0.036	0.287	0.121	0.301		0.106	0.135
0285	833820.90	822022.88		0,139	0,110	0,103	0,110	0.055	0.050	0.035	0.237	0.073	0,257		0,106	0.118
O286 O287	833658.41 833674.35	821865.88 821885.13		0.220	0.091	0.165	0.108	0.190	0.139	0.203	0.231	0.109	0.264	\vdash	0.154	0.171
0288	833690.30	821904.38		0.205	0.055	0.116	0.029	0.202	0.151	0.188	0.281	0.151	0.303		0.136	0.182
0289	833706.25	821923.64		0.145	0.062	0.201	0.037	0.199	0.177	0.176	0.249	0.173	0.323		0.150	0.190
O290	833722.19	821942.89		0.066	0.071	0.196	0.079	0.204	0.192	0,186	0.243	0,193	0,341		0.152	0.202
0291	833738.14	821962.15		0.045	0.082	0.156	0.105	0.180	0.165	0.162	0.252	0.197	0.346		0.141	0.197
O292 O293	833754.09 833770.03	821981.40 822000.65	-	0.051	0.097	0.095	0.087	0.136	0.085	0.084	0.258	0.191	0.357	-	0.113	0.168
0294	833785.98	822019.91		0.051	0.116	0.039	0.076	0.063	0.031	0.042	0.277	0.126	0.347		0.099	0.137
0295	833801.93	822039.16		0.049	0,112	0.088	0.105	0,118	0.082	0.060	0.259	0.058	0.239		0.102	0.127
0296	B33639.43	821882.15		0.244	0.080	0.138	0.119	0.138	0.123	0.171	0.132	0.105	0.310		0.134	0.146
0297	833655.38	821901.41	-	0.247	0.030	0.165	0.093	0.180	0.150	0.218	0.186	0.084	0.302		0.140	0.162
0298	833671.33 833687.27	821920.66		0.238	0.047	0.211	0.047	0.200	0.177	0.231	0.241	0.100	0.306	\vdash	0.156	0,181
O299 O300	833703.22	821939.92 821959.17		0.192	0.062	0.202	0.070	0.218	0.209	0.210	0.244	0.082	0.254		0.152	0.178
0301	833719.17	821978.42		0.047	0.093	0.147	0.104	0.212	0.200	0.195	0.237	0.140	0.203		0.141	0.178
0302	833735.11	821997.68		0.044	0.106	0.077	0.097	0.172	0.156	0.160	0.233	0.166	0.206		0.118	0.163
0303	833751.06	822016.93		0.053	0,112	0,050	0.089	0.114	0.085	0.091	0.228	0.156	0.233		0.097	0.139
O304 O305	833767.01 833782.95	822036.18 822055.44		0.053	0.109	0.072	0.102	0.078	0.058	0.053	0.226	0.113	0.243		0.095	0.124
O306	833620.46	821898.43		0.260	0.066	0.165	0.103	0.099	0.115	0.070	0.060	0.041	0.265		0.132	0.124
0307	833636.40	821917.69		0,263	0.019	0.214	0.108	0.169	0.149	0,193	0.096	0,073	0.267		0.144	0.144
0308	833652.35	821936.94		0.261	0.029	0.227	0.089	0.185	0.173	0.240	0.144	0.127	0.244		0.160	0.169
0309	833668.30	821956.19		0.232	0.050	0.224	0.054	0.211	0.196	0.249	0.190	0.062	0.203		0.157	0.161
0310	833684.24	821975.45	-	0.130	0.071	0.196	0.064	0.232	0.210	0.233	0.222	0.027	0.103	_	0.146	0.150
0311	833700.19 833716.14	821994.70 822013.95		0.055	0.087	0,101	0.093	0.230	0.211	0.214	0.213	0.066	0.068		0.122	0.145
0313	833732.08	822033.21		0.047	0.098	0.053	0.089	0.158	0.141	0.160	0.189	0.137	0.102		0.102	0.134
0314	B33748.03	822052.46		0.051	0.094	0.076	0.101	0.081	0.074	0.102	0.171	0,101	0.149		0.091	0.111
0315	833763.98	822071.72		0.045	0.088	0.066	0.096	0.054	0.116	0.047	0.155	0.045	0.172		0.078	0.092
0316	833601.30 833617.25	821914.50		0.266	0,062	0.225	0.104	0.225	0.206	0.189	0.100	0.064	0.148		0.160	0.142
0317	833633.19	821933.75 821953.00		0.262	0.024	0.221	0.143	0.211	0.188	0.199	0.056	0.085	0.167	\vdash	0.156	0.143
0319	833649.14	821972.26		0.255	0.024	0.222	0.109	0.194	0.186	0.241	0.096	0.078	0.149		0.154	0.146
0320	833665.09	821991.51		0.081	0.046	0.115	0.096	0.205	0.191	0.231	0.118	0.066	0.119		0.113	0.132
0321	833681.03	822010.77		0,035	0,062	0,033	0.073	0.222	0.202	0.220	0.151	0.067	0.138		0.090	0.131
0322	833696.98	822030.02		0.031	0.069	0.047	0.060	0.222	0.202	0.204	0.141	0.092	0.142		0.093	0.133
O323	833712.93 833728.87	822049.27 822068.53		0.031	0.070	0.067	0.085	0.206	0.183	0.190	0.126	0.108	0.140	\vdash	0.099	0.133
0325	833598.23	821949.98		0.033	0.074	0.133	0.207	0.233	0.258	0.266	0.114	0,056	0.139		0.094	0.119
0326	833614.17	821969.23		0.238	0.079	0.181	0.205	0.238	0.228	0.270	0.152	0.192	0.236		0.185	0.206
0327	833630.12	821988.48		0.272	0.060	0.191	0.142	0.193	0.179	0.195	0.049	0.038	0.067		0.148	0.117
0328	833705.99	822080.08		0.045	0.055	0.050	0.039	0.053	0.041	0.050	0.096	0.086	0.151		0.055	0.073
0329	833853.65	821865.50		0.083	0.051	0.086	0.027	0.056	0.118	0.089	0.063	0.326	0.144		0.089	0.131
O330 O331	833840.40 833849.95	821873,52 821885.09		0,067	0,048	0,083	0.050	0.086	0.198	0,167	0.089	0,400	0.215		0.109	0.179
	833849.95	821895.09 821896.66		0.100	0.064	0.117	0.046	0.056	0.166	0.151	0.093	0.341	0.231		0.113	0.164
0332			-	-	0.024	0.060	0.044	0.106	0.215	0.183	0.052	0.317	0.158		0.092	0.153
O332	833829.02	821883,22		0.065											91972	
O333 O334	833829.02 833838.81	821894.58		0.083	0.046	0.083	0.075	0.063	0.197	0.185	0.064	0,327	0.189		0.105	0.160
0333	833829.02			+			_	0,063 0,037 0,040	0.197 0.108 0.130	0.185 0.141 0.121	0.064 0.108 0.135		0.189 0.205 0.102			0.160 0.169 0.105

Wind	Velocit	y Ratio,	Base Case													
	Tes Point		Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 5SW	225 SW	247.5 WSW	Sum	Average	
		Section 1	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6.5%	4.9%	4.5%	6.7%	5.8%	M2M	83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)			8.3%	9.7%	7,6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	W	12 minutes
0337	833828.51	821901.13		0.043	0.016	0.038	0.024	0.055	0.146	0,132	0.070	0.165	0.078		0.059	0.095
0338	833932.47	821892.35		0.258	0.165	0.232	0.199	0.284	0.175	0.109	0.055	0.052	0.042		0,185	0.128
O339 O340	833941.87 833951.27	821904.03 821915.72		0.213	0.143	0.181	0.082	0.050	0.090	0.076	0.044	0.012	0.049		0.118	0.065
0341	833919.84	821903.19		0.225	0.133	0.182	0.124	0.170	0.038	0,023	0.023	0,017	0.036		0.126	0.066
0342	833929.72	821914.47		0.189	0.105	0.175	0.122	0.123	0.063	0.074	0.043	0.005	0.035		0.118	0.070
0343	833939.60	821925.76		0.113	0.060	0.101	0.112	0.125	0.088	0.079	0.044	0.008	0.033		0.086	0.065
0344	833900.99	821917.58		0.123	0.093	0.117	0.042	0.078	0.026	0.062	0.063	0.123	0.067		0.088	0.076
O345 O346	833910,39 833919.79	821929,27 821940.96		0,131	0.088	0,109	0.067	0,115	0.049	0.080	0.055	0.175	0.106		0.098	0.099
0347	833929.19	821952.65		0.101	0.079	0.072	0.053	0.083	0.024	0.029	0.042	0.167	0.130		0.093	0.083
0348	833938.59	821964.34		0.108	0.093	0.045	0.065	0.101	0.168	0.162	0.232	0.155	0.142		0.103	0.142
0349	833890.50	821926.82		0.105	0.066	0,089	0.083	0.120	0,116	0.149	0.182	0,212	0,069		0.111	0.141
0350	833900.14	821938,31		0.081	0.033	0.147	0,069	0,119	0.145	0,177	0,183	0.159	0,062		0,116	0.139
0351	833909.78	821949.80		0.074	0.036	0.149	0.040	0.109	0.153	0.182	0.179	0.145	0.028		0.110	0.130
O352	833919.42 833929.07	821961.29 821972.79	-	0.065	0.091	0.116	0.100	0.089	0.158	0.189	0.270	0.109	0.029		0.110	0.119
0354	834031.20	822022.99		0.145	0.159	0.136	0.062	0.056	0.068	0.137	0.153	0.021	0.026		0.111	0.082
0355	834044.19	822038.46		0.072	0.067	0.085	0.032	0.037	0.107	0.114	0.098	0.010	0.029		0.067	0.061
0356	833968.40	822059.06		0.164	0.068	0.095	0.060	0.063	0.093	0.116	0.102	0.053	0.148		0.088	0.087
0357	833978.02 833987.63	822070.57 822082.09	-	0.178	0.044	0.032	0.013	0.023	0.049	0.127	0.101	0.039	0.136		0.056	0.064
0359	833997.25	822093.60		0.123	0.056	0,069	0.033	0.019	0.039	0.042	0.072	0.038	0.185		0.052	0.033
0360	834006.87	822105.11		0.037	0.025	0.072	0.049	0.038	0.041	0.058	0.084	0.060	0.158	-	0.053	0.069
0361	833959.48	822066.78		0.107	0.088	0.100	0.061	0.066	0.093	0.123	0.131	0.052	0.145		0.090	0.094
0362	833969.16	822078.24	1	0.131	0.089	0.049	0.033	0.036	0.068	0.099	0.118	0.029	0.127		0.067	0.068
0363	833978.84	822089,70		0.113	0,088	0,043	0.045	0.023	0.051	0.033	0.097	0.045	0.144		0.059	0.060
0364	833988.52 833998.20	822101.16 822112.62		0.058	0.072	0.075	0.062	0.039	0.059	0.032	0.089	0.065	0.158		0.065	0.072
0366	833947.28	822077.33		0.043	0.031	0.115	0.049	0.033	0.096	0.102	0.131	0.054	0.112		0.104	0.103
0367	833957.20	822088.58		0.088	0.126	0.095	0.093	0.072	0.094	0.073	0.158	0.071	0.103		0.099	0.097
0368	833967.11	822099.84		0.068	0.118	0.092	0,097	0,058	0.076	0,029	0.156	0,082	0.111	1 5	0.092	0.091
0369	833977.03	822111.09		0.050	0.094	0.097	0.096	0.044	0.048	0.023	0.159	0.080	0.116		0.085	0.088
O370 O371	833986.95 833898.29	822122:35 822137.37		0.068	0.034	0.047	0.037	0.016	0.015	0.047	0.171	0.082	0.098	-	0.054	0.073
0372	833908.77	822148.17		0.034	0.025	0.047	0.031	0.022	0.020	0.050	0.021	0.030	0.029		0.033	0.031
0373	833870.30	822151.60		0.035	0.033	0.067	0.049	0.057	0.049	0.077	0.101	0.025	0.046		0.055	0.059
0374	833880.63	822162,47		0.025	0.022	0.046	0.037	0.028	0.039	0.082	0.118	0.025	0.016		0,043	0.052
0375	833856.97	822161.59		0.021	0.015	0.046	0.058	0.060	0.082	0.060	0.189	0.087	0.068		0.060	0.089
D376	833867.44 833611.59	822172.33 822332,37	-	0.022	0.018	0.055	0.054	0.011	0.040	0.092	0.069	0.054	0.040		0.045	0.054
0378	833635.20	822340.59		0.225	0.157	0.060	0.107	0.134	0.063	0.030	0.133	0.124	0.117		0.112	0.101
D379	833658.54	822349.55		0.201	0.142	0.079	0.117	0.144	0.134	0.075	0.085	0.101	0.128		0.115	0.105
0380	633675.53	822355.49		0.111	0.082	0.046	0.071	0.075	0.071	0.101	0.063	0.055	0.103		0.070	0.070
0381	833668,22	822374.10		0,080	0,049	0,040	0.015	0,061	0.024	0.073	0.024	0,045	0.055		0.043	0.041
O382	833645.34 833622.17	822354.63 822354.63		0.194	0.150	0.056	0.079	0.111	0.126	0.030	0.087	0.092	0.047		0.098	0.080
0384	833605.61	822354.63		0.193	0.112	0.049	0.105	0.129	0.121	0.026	0.105	0.052	0.031		0.082	0.076
D001	833820.29	822111.30		0.047	0.083	0.016	0.048	0.043	0.069	0.065	0.249	0.213	0.235		0.076	0.135
D002	833812.49	822117.56		0.024	0.079	0.008	0.050	0.051	0.058	0,068	0.223	0.231	0.267		0.071	0.136
D003	833804.69	822123.81		0.017	0.072	0.026	0.055	0.052	0.035	0.045	0.217	0.210	0.226		0.070	0.125
D004	833826.88 833819.07	822125.08		0.043	0.077	0.009	0.037	0.056	0.082	0.066	0.207	0.138	0.212		0.064	0.110
D006	833811.27	822131.34		0.034	0.067	0.025	0.052	0.072	0.073	0.041	0.252	0.055	0.044		0.063	0.086
D007	833825.66	822132.61		0.036	0,075	0.021	0.034	0.086	0.104	0.074	0.259	0.042	0.055		0.066	0.092
D008	833817.85	822138.87		0.029	0.064	0.031	0.040	0.102	0.098	0.056	0.256	0.042	0.054		0.067	0.092
D009	833832.24	822140.14		0.048	0.079	0.049	0.017	0.093	0.106	0.042	0.251	0.042	0.080		0.071	0.091
D010	833824.43 833838.82	822146.39 822147.67		0.036	0.073	0.044	0.020	0.113	0.125	0.042	0.244	0.039	0.090		0.070	0.094
D011	833831.02	822153.92		0.080	0.092	0.063	0.009	0.092	0.136	0.071	0.219	0.054	0.121		0.079	0.095
D013	833845.40	822155.20		0.106	0.052	0.066	0.022	0.086	0.090	0.106	0.191	0.081	0.044		0.077	0.092
D014	833837.60	822161.45		0.112	0.092	0.080	0.020	0.095	0.122	0.136	0.176	0.043	0.111		0.087	0.097
D015	833899.34	822107.40	1	0.062	0,089	0.094	0.098	0.049	0.036	0.070	0.030	0.060	0.045		0.075	0.059
D016	833891.53 833883.73	822113.66 822119.91		0.029	0.035	0.036	0.045	0.042	0.010	0.032	0.025	0.054	0.067		0.036	0.039
D017	833875.93	822119.91		0.047	0.050	0.041	0.067	0.045	0.014	0.042	0.024	0.060	0.078		0.048	0.048
D019	833868.12	822132,42		0.066	0.048	0.056	0.051	0.049	0.027	0,076	0.030	0,053	0,075		0.051	0.051
D020	833614.22	822011.42		0.206	0.090	0.193	0.220	0.291	0.286	0.329	0.171	0.046	0.028		0.190	0.181
D021	833625.42	822023.08		0.169	0.094	0.226	0.169	0.225	0.146	0,107	0.171	0.048	0.040		0.163	0.134
D022	833610.74	822026.16	-	0.187	0.088	0.200	0.216	0.288	0.295	0.326	0.123	0.034	0.046		0.184	0.172
D023	833634.39 833643.45	822032.59 822044.01		0.160	0.083	0.238	0.106	0.117	0.035	0.093	0.185	0.050	0.047	-	0.141	0.109
D025	833653.10	822055.85		0.168	0.078	0.223	0.051	0.082	0.033	0.057	0.184	0.058	0.033	1 1	0.124	0.093
D026	833638.45	822059.59		0.184	0.088	0.233	0.108	0.158	0.075	0.064	0.129	0.038	0.053		0.140	0,101
D027	833662.47	822068.39		0.157	0.074	0.210	0.028	0.059	0.045	0.064	0.169	0.058	0.084		0.113	0.091
D028	833647.41 833632.58	822072.72		0.165	0.081	0.219	0.071	0.132	0.054	0.070	0.111	0.031	0.080		0.123	0.089
D029	833632.58	822075.81 822082.91		0.163	0.092	0.234	0.116	0.186	0.112	0.117	0.069	0.018	0.075		0.141	0.102
D031	833658.24	822085.88		0.140	0.070	0.197	0.024	0.097	0.029	0.036	0.095	0.037	0.068		0.100	0.069
D032	833643.46	822088.68		0.135	0.081	0,213	0.062	0.148	0.070	0.093	0.051	0.056	0.063		0.118	0.087
D033	833628.53	822090.95		0.129	0,092	0.232	0.104	0.184	0.119	0.135	0.046	0.077	0.097		0.140	0.113
D034	833818.77	822061.95		0.028	0.077	0.067	0.079	0.130	0.196	0.174	0.223	0.102	0.112		0.100	0.138
D035	833809.59 833799.96	822067.11 822072.88		0.025	0.068	0.059	0.077	0.100	0.194	0.172	0.227	0.087	0.083		0.093	0.129
D037	833770.99	822080.33		0.040	0.087	0.049	0.077	0.067	0.150	0.163	0.150	0,025	0.138		0.075	0.090
D038	833765.27	822090.10		0.035	0.074	0.038	0.079	0.053	0.146	0.086	0.108	0.047	0.120		0.066	0.082
D039	833751.16	822091.77		0.034	0.049	0.044	0,080	0.086	0.107	0.040	0.099	0.037	0.143		0.060	0.075
D040	833736.50	822092.92		0.039	0.045	0.058	0.080	0.129	0.059	0.066	0.098	0.036	0.135		0.065	0.078
D041	833721.74	822093.94		0.059	0.043	0.061	0.075	0.074	0.091	0.114	0.107	0.040	0.120		0.068	0.082
D042	833705.95 833688.13	822094.71 822096.51		0.120	0.041	0,052	0.067	0.068	0.043	0.058	0.106	0.038	0.106		0.063	0.080
D044	833673.32	822098.89		0.119	0.056	0.173	0.037	0.043	0.049	0.036	0.116	0.037	0.100		0.094	0.088
D045	833658.51	822101.28		0.114	0.066	0.183	0.022	0.096	0.028	0.031	0.107	0.152	0.112		0.103	0.097
	202412.00	822103.66		0.108	0.076	0.203	0.032	0.138	0.058	0.085	0.118	0.191	0.161		0.123	0.128
D046	833643.70				_		_		_		_	_		_		
D046 D047 D048	833643.70 833628.89 833614.39	822105.04 822102.19		0.105	0.086	0.219	0.067	0.162	0.104	0.126	0.153	0.223	0.213		0.145	0.163 0.164

	Tes Point		Wind direction (Degree)	45	67.5	90	112.5	135	157.5	180	202.5	225	247.5			
	res Point		Wind direction	NE	ENE	E	ESE	SE	SSE	5	SSW	SW	WsW	Sum	Average	Average
in		Northing (m)	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6,5%	4.9%	4.5%	6.7%	6.8%		83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)			8.3%	9.7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%		150000
D049	833599.89	822098.34	1.	0.114	0.111	0.252	0.158	0.207	0.199	0,128	0.119	0.132	0.162		0.171	0.161
D050	833585.40	822094.49		0.100	0.130	0.253	0.191	0.223	0.240	0.122	0.080	0.076	0.104		0,173	0.146
D051	833776.49	822095.36		0.043	0.083	0.022	0.070	0.059	0.162	0.156	0.107	0.117	0.082		0.073	0,100
D052	833761.81	822098.45		0.043	0.018	0.012	0.066	0.073	0.148	0.116	0.089	0.105	0.084		0.056	0.089
D053	833747.13	822101.53		0.057	0.020	0.014	0.067	0.092	0.115	0,081	0,106	0.113	0.079		0.058	0.088
D054	833732.45	822104.61	1	0.084	0.023	0.028	0.068	0.069	0.082	0.071	0.106	0.131	0.047		0.061	0.083
D055	833717.77	822107.70		0.106	0.020	0.032	0.066	0.036	0.085	0.093	0.070	0.156	0.112		0.062	0.088
D056	833703.09	822110.78		0.097	0.017	0.098	0.063	0.052	0.076	0.089	0.046	0.192	0.195		0.079	0,106
D057	833688,41	822113.86	1	0,087	0,042	0.117	0.056	0.039	0.071	0.076	0.132	0,232	0.261		0.094	0.133
D058	833673.73	822116.95		0.086	0.043	0.123	0.042	0.038	0.054	0.065	0.189	0.259	0.286		0.098	0.147
D059	833659.05	822120.03		0.090	0.061	0.164	0.020	0.084	0.029	0.049	0.197	0.279	0.279		0.112	0.153
D060	833644.37	822123.11		0.087	0.070	0.185	0.019	0.115	0.037	0.065	0.256	0.335	0.334		0.132	0.188
D061	833663.64	822132.67		0.058	0.059	0,155	0,016	0.057	0.029	0,066	0.195	0.279	0.265		0.105	0.149
D062	833825.69	822190.69		-	~	-	-	-	-		**	-	-		_	
D063	833832.10	822198.36		- 44	-		-	-	-	- 44	- 40	40	140			94
D064	833838.51	822206.04		0.067	0.021	0.095	0.068	0.098	0.063	0.144	0.085	0.032	0.025		0.072	0.073
D065	833844.92	822213.71			-	-	-	-	77	(Fr.	m.	m.	TP.		-	
D066	833851.33	822221.39	ė.		1 4 1	. A.	-		-		+-		-		- 2	H
D067	833817.23	822197.22		-	-	-	~	-	3-61	. Jan. 1			in the contract of the contrac		~	- ><
D068	833823.77	822204.78								-			-			- 4-
D069	833830.31	822212.35		0.052	0.020	0,100	0.086	0.087	0.062	0.160	0.049	0.030	0.009		0.072	0,068
D070	833836.85	822219.91		-	+	-	-	-	2-0	The state of	-	-	-		-	-
D071	833843.39	822227.48			-	-	-	-	-	-		-	-			-
D072	833835.66	822233.82		-	-		-			- 04	-					*
D073	833827.93	822240.17		-					* .		-		- 1			-
D074	833820.21	822246.51	1		-	-	-	***		(99)			i dec		-	-
D075	833812.48	822252.86	1.		-	-	-	-	-				-	1 5 7 7	-	- *
D076	833805.65	822257.88		-	-	-	-	_	-	-		-	-		-	-
D077	833772.09	822234.97		1 100		100		-		340		5			-	-
D078	833778.67	822242,50		1	in the same	-		-				3-0			-	-
D079	833785.26	822250,02		0.013	0.028	0.035	0.045	0.065	0.046	0.158	0.022	0.087	0.089		0.046	0.067
D080	833791.84	822257.55		-		-	-	-	-	***	+6	-	-			- 14
D081	833798.42	822265.08		- 44-	-	-	-	-		- 044	-46	- 40	- 46		-	24

WILL	velocit	y Katio,	Proposed Case													
	Tes Point		Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 5SW	225 SW	247.5 WSW	5um	Average	Average
			Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6.5%	4.9%	4.5%	6.7%	6.8%	Wave	83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)			8.3%	9.7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%		1500000
P001	833906.48	822110.14		0.074	0.114	0.114	0,162	0.042	0,149	0,114	0,158	0.047	0.126		0.112	0.111
P002	833900.24 833894.00	822102.33 822094.52		0.132	0.120	0.089	0.147	0.038	0.195	0.169	0.216	0.058	0.142		0.120	0.131
P003	833890.92	822094.52		0.111	0.137	0.077	0.142	0.054	0.154	0.122	0.205	0.041	0.187		0.110	0.119
P005	833884.53	822077.14		0.148	0.179	0.083	0.150	0.061	0.150	0,132	0.156	0.050	0.276		0.121	0.125
P006	833874.36	822071.19		0.139	0.176	0.078	0.155	0.077	0.176	0.148	0.106	0.112	0.278		0.124	0.135
P007	833864.49	822068.98		0.076	0.089	0.044	0.084	0.117	0.161	0.144	0.042	0.322	0.274		0.100	0.157
P008	833854.52 833846.90	822072.47		0.015	0.048	0.013	0.037	0.137	0.140	0.134	0.029	0.330	0.211		0.073	0.140
P009 P010	833839.86	822078.91 822084.83		0.027	0.054	0.011	0.039	0,126	0.149	0.144	0,064	0.333	0.230		0,078	0.150
P011	833831.48	822091.12		0.060	0.054	0.035	0.017	0.128	0.180	0.176	0.126	0.333	0.261		0.092	0.170
P012	833823.50	822098.43		0.031	0.050	0.047	0.008	0.128	0.182	0.180	0.159	0.352	0.295		0.095	0.184
P013	833819.20	822105.01		0.114	0.066	0.037	0,011	0.122	0,179	0.179	0.176	0,345	0,306		0.103	0.185
P014	833813,78	822113,32		0.188	0.153	0.116	0,048	0,143	0.214	0,221	0,216	0,321	0,325		0.156	0.211
P015	833806.08 833799.61	822119.70 822125.07		0.141	0.147	0.072	0.039	0.118	0.151	0.166	0.205	0.272	0.287		0.125	0.175
P017	833806.02	822132.74		0.093	0.132	0.036	0.016	0.123	0.134	0.136	0.248	0.026	0.053		0.086	0.099
P018	833812.47	822140.39		0.084	0.151	0.029	0.039	0.170	0.212	0.192	0.326	0.035	0.066		0.108	0.136
P019	833818.91	822148.04		0.092	0.158	0.046	0.037	0.206	0.263	0.237	0.388	0.056	0.041		0.129	0,164
P020	833825.35	822155.68		0.103	0.146	0.099	0.023	0.220	0.279	0.256	0.385	0.096	0.035		0.146	0.180
P021	833831.80 833836.66	822163.33 822168.33	-	0.084	0.123	0,101	0.060	0.211	0.272	0.227	0.336	0.044	0.052		0.136	0,162
P023	833844.35	822161.93		0.024	0.051	0,026	0,043	0.129	0.148	0.084	0.221	0,049	0.067		0.068	0.099
P024	833852.03	822155.53		0.075	0.079	0.059	0.030	0.035	0.111	0.168	0.225	0.087	0.161		0.082	0.115
P025	833859.71	822149.12		0.073	0.054	0.056	0.033	0.062	0.190	0.214	0.153	0.069	0.061		0.080	0.105
P026	833867.39	822142.72		0.079	0.064	0.054	0.035	0.090	0.237	0.257	0.094	0.090	0.083		0.086	0.113
P027 P028	833875.07 833882.75	822136.32 822129.92		0.067	0,068	0.026	0.048	0.078	0.223	0.227	0.054	0.103	0.131		0.074	0,106
P029	833890.44	822123.51		0.047	0.059	0.056	0.061	0.084	0.240	0.253	0.166	0.066	0.063		0.077	0.123
P030	833898.12	822117.11		0.079	0.045	0.038	0.040	0.093	0.182	0.206	0.194	0.035	0.046		0.077	0.104
P031	833851.44	822040.71		0.150	0.175	0.123	0.141	0.236	0.236	0.204	0.085	0.224	0.297		0.161	0,187
P032	833846,06	822032,53		0,152	0.175	0.106	0.140	0.172	0.205	0,171	0.053	0,199	0,313		0.143	0.163
P033	833840.32 833832.12	822041,06 822046.78		0.130	0.144	0.103	0.118	0.208	0.220	0.190	0.071	0.221	0.279		0.140	0.171
P034	833823.92	822052.51		0.053	0.075	0.068	0.053	0.208	0.208	0.187	0.142	0.224	0.194		0.109	0.172
P036	833815.73	822058.23		0,095	0,069	0.057	0.033	0.198	0.192	0.182	0.218	0,212	0.151		0.110	0.164
P037	833806.62	822062.36		0.151	0.094	0.060	0.026	0.180	0.185	0.178	0.232	0.192	0.137		0.116	0.157
P038	B33797.51	822066.50		0.077	0.076	0.082	0.023	0.148	0.174	0.170	0.221	0.179	0.117		0,106	0.148
P039 P040	833788.41	822070.63		0.056	0.028	0.073	0.026	0.109	0.180	0.180	0.171	0.190	0.125		0.090	0,139
P040	833779.30 833770.19	822074.76 822078.90		0.043	0.110	0.079	0.031	0.022	0.083	0.126	0.181	0.136	0.119		0.072	0,110
P042	833761.09	822083.03		0.037	0.106	0.080	0.043	0.082	0.073	0.106	0.167	0.098	0.105		0.084	0.099
P043	833750.74	822085.73		0.040	0.079	0.082	0.042	0.134	0.068	0.100	0.149	0.078	0.103		0.081	0.095
P044	633740.78	822086,56	1	0.042	0.055	0.079	0.036	0.170	0.077	0.105	0.143	0.060	0.096		0.078	0.094
P045	833730,81	822087.38		0,041	0,037	0,072	0,035	0,188	0,121	0.148	0,150	0.048	0.090		0.079	0.102
P046 P047	833720.85 833710.88	822088.21 822089.03		0.046	0.039	0.058	0.031	0.160	0.143	0.174	0.163	0.037	0.070		0.076	0.101
P048	833700.91	822089.86		0.126	0.067	0.056	0.026	0.090	0.068	0.081	0.198	0.020	0.074		0.002	0.079
P049	833690.95	822090.68		0.187	0.124	0.134	0.058	0.189	0.170	0.205	0.215	0.015	0.093		0.133	0.127
P050	833684.22	822083.21		0.180	0.132	0.143	0.070	0.230	0.215	0.252	0.225	0,017	0.051		0.147	0.141
P051	833677.77	822075.56		0.165	0.136	0.150	0.082	0.261	0.250	0.285	0.189	0.030	0.050		0.154	0.150
P052 P053	833671.33 833664.89	822067.91 822060.26		0.152	0.137	0.160	0.095	0.286	0.279	0.309	0.183	0.039	0.070		0.163	0.163
P054	833658.45	822052.62		0.107	0.138	0.179	0.117	0.310	0.311	0.330	0.178	0.053	0.098		0.173	0.180
P055	833652.00	822044.97		0.077	0,144	0.206	0.146	0.313	0.316	0,332	0.188	0.060	0.102	1	0.184	0.191
P056	B33645.56	822037.32		0.096	0.141	0.226	0.187	0.292	0.292	0.312	0.222	0.076	0.095		0.197	0.200
P057	833639.12	822029.67		0.120	0.108	0.196	0.169	0.213	0.207	0.220	0.231	0.083	0.069		0.169	0.169
P058 P059	833632.67 833626.22	822022,03 822014,39		0.077	0.083	0.167	0.156	0.153	0,138	0,143	0.186	0.075	0.044		0.135	0.132
P060	833619.77	822006.74		0.136	0.080	0.139	0.175	0.127	0.116	0.073	0.121	0.052	0.026		0.121	0.101
P061	833611.41	822001.06		0.141	0.078	0.129	0.191	0.119	0.126	0.089	0.088	0.027	0.032		0.117	0.094
P062	833602.43	822002.93		0.091	0.080	0.095	0.208	0.114	0.144	0.121	0.095	0.010	0.022		0.108	0.094
P063	833598.77	822013.68		0.088	0,082	0.103	0.189	0.114	0.142	0.110	0.101	0.025	0.025		0.108	0.095
P064 P065	833598.77 833595.43	822022.34 822031.77		0.097	0.117	0.094	0.227	0.192	0.227	0.214	0.144	0.063	0.057		0.141	0.144
P066	833592.10	822041.20		0.086	0.150	0.128	0.272	0.264	0.287	0.282	0.141	0.089	0.100		0.173	0.185
P067	833588.77	822050.63		0,086	0.153	0.191	0.267	0.275	0.285	0.285	0.116	0.105	0.117		0.191	0.190
P068	833585.44	822060.05		0.093	0.153	0.212	0.261	0.277	0.283	0.282	0.106	0.107	0.133		0.196	0.191
P069	833582.11	822069.48		0.093	0.147	0.223	0.242	0.260	0.271	0.269	0.086	0.097	0.146		0.190	0.182
P070 P071	833578.78 833575.53	822078.91 822088.37		0.071	0.143	0.238	0.226	0.245	0.257	0.263	0.082	0.084	0.161	-	0.185	0.176
P072	833576.05	822098.37		0.031	0.098	0,248	0.120	0.120	0.126	0.263	0.076	0.130	0.162	-	0.178	0.143
P073	833581.96	822106.63		0.122	0.046	0.053	0.060	0.119	0.111	0.071	0.295	0.316	0.320		0.110	0,189
P074	833591.37	822110.01		0.120	0.047	0.033	0.087	0.156	0.153	0.078	0.283	0.334	0.333		0.114	0.202
P075	833600.78	822113.40		0.124	0.057	0.038	0.104	0.172	0.175	0.059	0.291	0.357	0.352		0.124	0.214
P076	833610.19 833619.60	822116.78 822120.16		0.132	0.059	0.040	0.106	0.168	0.177	0.062	0.284	0.368	0.360		0.126	0.216
P077	833629.01	822120.16		0.145	0.052	0.034	0.097	0.156	0.171	0.146	0.271	0.377	0.366		0.123	0.217
P079	833638.42	822126.92		0.145	0.051	0.029	0.058	0.131	0.152	0.182	0.282	0.397	0.391		0.120	0.225
P080	833647.06	822133.14		0.140	0.051	0.047	0.037	0.123	0.142	0.196	0.294	0.415	0.411		0.124	0.232
P081	833656.06	822137.54		0.131	0,054	0,071	0.043	0.119	0.131	0.191	0.285	0,417	0.411		0.129	0.232
P082	833665,90	822139.90		0.120	0.058	0.081	0.057	0.120	0.119	0.178	0.264	0.408	0.400		0.129	0.226
P083	833673.66 833683.40	822146.21 822148.45		0.103	0.059	0.100	0.075	0.112	0.097	0.152	0.269	0.416	0.402		0.133	0.227
P085	833693.40	822148.45		0.084	0,069	0.100	0.089	0.092	0.087	0.131	0.230	0,390	0.372		0.126	0.208
P086	833703.38	822147.62		0.078	0.075	0.098	0.095	0.084	0.108	0.124	0.208	0,378	0.363		0.125	0.202
P087	833712.77	822144.13		0.083	0.081	0.096	0.097	0.088	0.121	0.130	0.178	0.363	0.359		0.124	0.196
POSS	833722.15	822140.28		0.091	0.081	0.094	0.098	0.104	0.133	0.138	0.137	0.347	0.357		0.122	0.189
P089	833730.70	822136.10		0.099	0.068	0.092	0.098	0.114	0.141	0.145	0.095	0.327	0.354		0.117	0.179
P090 P091	833739.69 833748.73	822131.73		0.100	0.050	0.088	0.096	0.114	0.148	0.148	0.069	0,307	0.352	-	0.110	0.171
P091 P092	833748.73 833757.74	822127.25 822122.93		0.085	0.034	0.083	0.092	0.098	0.158	0.155	0.070	0.287	0.348		0.102	0.165
P093	833766.11	822118.19		0.041	0.063	0.079	0.078	0.070	0.158	0.171	0.040	0.271	0.345		0.095	0.154
P094	833773.72	822111.90		0.035	0.094	0.082	0,068	0,072	0.155	0.173	0,034	0,247	0,329		0.095	0.146
mane	833780.92	822105.74		0.044	0.117	0.103	0.056	0.090	0.158	0.174	0.037	0.227	0.308		0.104	0.143
P095 P096	833783.82	822099.70		0.043	0.115	0.126	0.046	0.093	0.164	0.176	0.051	0.198	0.263		0,107	0.138

Wind	velocity	Ratio,	Proposed Case													
	Tes Point		Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 55W	225 SW	247.5 WSW	5um	Average	Average
	1		Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6.5%	4.9%	4.5%	6.7%	6.8%	Man	83.6%	(Annual)	(Summer)
ID	200000000000000000000000000000000000000	Northing (m)	Probability (Summer)	1000		8,3%	9,7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%		
P097	833790.30	822092.06		0.057	0.054	0.045	0.022	0.128	0.181	0.189	0.048	0.178	0.208		0.077	0.123
P098 P099	833798.07 833805.83	822085.76 822079.45		0.143	0.105	0.051	0.006	0.140	0.160	0.161	0.093	0.135	0.183		0.090	0.114
P100	833813.59	822073.45		0.139	0.096	0.079	0.014	0.137	0.163	0.176	0.220	0.196	0.084		0.121	0.151
P101	833821.67	822067.40		0.060	0.069	0.076	0.019	0.207	0.187	0,179	0.202	0.227	0.095		0.110	0.159
P102	833828.02	822058.82		0.040	0.046	0.076	0.041	0.220	0.194	0.182	0.177	0.234	0.152		0.108	0.166
P103	833835.80	822052.54		0.077	0.057	0.089	0.073	0.230	0.204	0.187	0.125	0.238	0.214		0.119	0.172
P104 P105	833843.58 833859.73	822046.26 822218.10		0.125	0.131	0.104	0.113	0.232	0.218	0.193	0.074	0,234	0.262		0.141	0,175
P105	833853.32	822210.43		0.123	0.104	0.067	0.078	0,153	0.181	0.131	0.287	0.116	0.053		0.120	0.145
P107	833846.97	822202.70		0.083	0.106	0.086	0.097	0.177	0.193	0.184	0.288	0.137	0.047		0.129	0.160
P108	833840.62	822194.97		0.035	0.104	0.090	0.101	0.182	0.209	0.215	0.283	0.142	0.062		0.129	0.168
P109	833834.27	822187.25		0,071	0.100	0,093	0.102	0,200	0.250	0.256	0.280	0.124	0,060		0.137	0.174
P110 P111	833827.92 833820.19	822179.52 822185.86		0.093	0.101	0.108	0.094	0.268	0.337	0,318	0.307	0.093	0.072		0.155	0.196
P112	833812.46	822192.20		0.101	0.050	0.041	0.070	0.103	0.130	0.091	0.032	0.095	0.070		0.070	0.079
P113	833804.73	822198.54		0.076	0.057	0.066	0.072	0.126	0.022	0.024	0.033	0.075	0.061		0.064	0.059
P114	833796.99	822204.88		0.044	0.056	0.099	0,103	0.069	0.018	0.013	0.069	0.046	0.045		0.070	0.057
P115	833789.26	822211.22		0.017	0.052	0.121	0.129	0.057	0.041	0.035	0.129	0.058	0.035		0.084	0.079
P116 P117	833781.53 833773.79	822217.57 822223.91		0.014	0.041	0.135	0.149	0.079	0.090	0.040	0.072	0.039	0.067		0.087	0.079
P118	833766.06	822230.25		0.079	0.062	0.149	0.158	0.053	0.036	0.034	0.105	0.103	0.171		0.111	0.103
P119	833758.33	822236.59		0,033	0.076	0,154	0,153	0.041	0.098	0.051	0,129	0,130	0.115		0.110	0,113
P120	833750.60	822242.93		0.062	0.047	0.166	0.162	0.087	0.040	0.010	0.112	0.130	0.108		0.109	0.106
P121	833742.86	822249.27		0.066	0.050	0.177	0.161	0.041	0.027	0.013	0.097	0.122	0.101		0.107	0.097
P122	833735.13	822255.61		0.083	0.046	0.182	0.155	0.034	0.037	0.020	0.081	0.121	0.092		0.107	0.094
P123	833727.40 833719.66	822261.95 822268.29		0.130	0,032	0.182	0.149	0.032	0.049	0.031	0.077	0.144	0.105		0.111	0,100
P125	833711.93	822274.63		0.110	0.092	0.149	0.129	0.032	0.077	0.031	0.035	0.136	0.098		0.117	0.093
P126	833704.20	822280.97		0.096	0.077	0.127	0.114	0.044	0.080	0.070	0.101	0.096	0.058		0.098	0.089
P127	833712.40	822286.84		0.103	0.087	0.064	0.060	0.068	0.076	0.072	0.137	0.080	0.067		0,079	0.082
P128	833721.80	822290.25		0,099	0.102	0.068	0.042	0,077	0.071	0,076	0.141	0,056	0.082		0.078	0.079
P129 P130	833731.20 833740.60	822293.66 822297.07		0.082	0.112	0.085	0.058	0.092	0.085	0.078	0.150	0.043	0.098		0.087	0.086
P130	833750.00	822300.48		0.042	0.117	0.127	0.083	0.103	0.128	0.109	0.153	0.100	0.111		0.110	0.118
P132	833759.40	822303.89		0.032	0.122	0.155	0.112	0.150	0.149	0.139	0.142	0.119	0.113		0.127	0.133
P133	833768.34	822299.96		0.056	0.097	0.163	0.124	0.150	0.149	0.136	0.075	0.114	0.093		0.123	0.121
P134	833776.02	822293.62		0.030	0.028	0.157	0.128	0.132	0.137	0.119	0.050	0.035	0.031		0,098	0.089
P135	833783.71 833791.40	822287.22		0.053	0.026	0.152	0.130	0.123	0.134	0.118	0.085	0.065	0.047		0.103	0.102
P137	833799.09	822280.83 822274.43		0.076	0.048	0,154	0.141	0.123	0.142	0.154	0.110	0.038	0.042		0.111	0.118
P138	833806.78	822268.04		0.079	0.059	0.154	0.145	0.109	0.143	0.172	0.101	0,067	0.064		0.117	0.114
P139	833814.46	822261.64		0.078	0.047	0.160	0.154	0.117	0.154	0.202	0.060	0.093	0.089		0.120	0.122
P140	833822.15	822255.25	-	0.093	0.026	0.166	0.163	0.130	0.168	0.222	0.032	0.115	0.103		0.124	0,129
P141	833829,84	822248.85		0,111	0,030	0,172	0,169	0,147	0,181	0,234	0.040	0,121	0.104		0,132	0.137
P142	833837.53 833845.22	822242.46 822236.06		0.126	0.064	0.163	0.159	0.162	0.175	0.232	0.058	0.120	0.100		0.137	0.138
P144	833852.90	822229.67		0.144	0.099	0.071	0.079	0.131	0.114	0.186	0.182	0.072	0.097		0.105	0.117
0001	833688.64	821827.88		0.059	0.244	0.208	0.227	0.301	0.151	0.109	0.244	0.193	0.199		0.203	0.204
0002	833704.79	821846.97		0.067	0.045	0.024	0.075	0.108	0,101	0,059	0.141	0.176	0,040		0.073	0.103
0003	833720.93	821866.06		0.094	0.041	0.051	0.080	0.116	0.082	0,056	0.142	0.156	0.135		0.081	0.110
0004	833737.08 833753.23	821885.14 821904.23		0.106	0.044	0.071	0.069	0.111	0.096	0.085	0.188	0.147	0.213	_	0.091	0.128
0006	833769.37	821923.32		0.115	0.052	0.079	0.072	0.090	0.095	0,079	0.281	0.202	0.326		0.105	0.164
0007	833785.52	821942.41		0.110	0,069	0.090	0.091	0,049	0.072	0.061	0.269	0.080	0.363	1	0.096	0.136
8000	833801.66	821961.49		0.101	0.080	0.077	0.088	0.056	0.095	0.104	0.232	0.074	0.353		0.094	0.133
0009	833817.81	821980.58	-	0.125	0.085	0.083	0.084	0.043	0.109	0.082	0.186	0.108	0.322		0.096	0.127
0010	833833.95 833850.10	821999.67 822018.75		0.149	0.108	0.028	0.099	0.050	0.056	0.040	0.120	0.135	0.330		0.081	0,109
0012	833866.40	822037.71	-	0.135	0.170	0.138	0.148	0.256	0.254	0.217	0.158	0.227	0.330		0.173	0.210
0013	833882.70	822056.66		0.179	0.183	0.073	0.139	0.083	0.095	0.082	0.092	0.255	0.328		0.128	0.150
0014	833907.00	822070.77		0.191	0.180	0.102	0.118	0.063	0.153	0.187	0.177	0.230	0.364		0.145	0.179
0015	833923.30	822089.72		0.141	0,158	0.137	0.131	0.102	0.123	0.175	0.158	0.229	0.352		0.147	0.179
O016	833939.61 833955.91	822108.68 822127.63		0.133	0.135	0.137	0.130	0.101	0.111	0.195	0.170	0.126	0.255		0.136	0.151
0018	833972.19	822146.60		0.111	0.078	0.154	0.100	0.134	0.085	0.232	0.200	0.102	0.165		0.131	0.148
0019	833988.31	822165.71		0.077	0.067	0.142	0.099	0,096	0.060	0.249	0.216	0.106	0,040		0.119	0.132
0020	834004.42	822184.83		0.100	0.189	0.155	0.101	0.049	0.091	0.239	0.210	0.044	0.156		0.135	0.128
0021	833894.10	822079.37		0.178	0.186	0.099	0.147	0.063	0.167	0.162	0.175	0.101	0.330		0.137	0.150
O022 O023	833910.40 833926.70	822098.32 822117.28		0.125	0.158	0.143	0.159	0.061	0.162	0.149	0.181	0.098	0.280		0.141	0.150
0024	833943.00	822136.23		0.140	0.122	0,108	0.086	0.093	0.130	0.262	0.200	0.070	0.242		0.116	0.140
0025	833959.29	822155.20		0.123	0.114	0.204	0.155	0.162	0.085	0.269	0.223	0.138	0.215		0.166	0,180
0026	B33975.40	822174.31		0.110	0.090	0.102	0.067	0.112	0.059	0.232	0.244	0.042	0.153		0.108	0.126
0027	833991.52	822193.42		0.087	0.159	0,101	0.070	0.100	0.073	0.223	0.241	0.066	0.116		0.117	0.127
O028	833795.28 833811.13	822131.96 822151.29		0.047	0.107	0.051	0.020	0.066	0.042	0.080	0.179	0.140	0.138		0.074	0,100
0030	833826.98	822170.63		0.033	0.112	0.119	0.045	0.212	0.307	0.235	0.310	0.052	0.061		0.110	0.174
0031	833842.83	822189.96		0.056	0.106	0.079	0.086	0.191	0.246	0.223	0.327	0.135	0.061		0.133	0.176
0032	833858.68	822209.29		0.115	0.094	0.052	0.069	0.163	0.196	0.119	0.291	0.113	0.067		0.111	0.142
0033	833874.53	822228.63	-	0.067	0,086	0,101	0.099	0.167	0,187	0.173	0.240	0,105	0.046		0.121	0.143
0034	833890.38	822247.96		0.098	0.113	0.085	0.064	0.131	0.157	0.177	0.219	0.075	0.028		0.110	0.120
O035	833906.23 833578.89	822267.29 821900.02		0.127	0.110	0.119	0.094	0.089	0.114	0.188	0.195	0.115	0.083		0.122	0.130
0037	833583.56	821924.58		0.176	0.029	0.075	0.140	0.208	0.210	0,096	0.072	0,034	0.048		0.106	0.099
0038	833588.23	821949.14		0.103	0.044	0.068	0.204	0.136	0.172	0.110	0.068	0.074	0.062		0.102	0,106
0039	833592.90	821973.70		0.081	0.100	0.120	0.245	0.171	0.200	0.170	0,094	0.276	0.294		0.154	0.197
0040	833597.57	821998.26		0.083	0.076	0.076	0.213	0.105	0.141	0.126	0.097	0.010	0.015		0.102	0.092
0041	833598.99	822023.72		0.103	0.121	0.095	0.231	0.202	0.236	0.222	0.145	0.067	0.060		0.145	0.149
0042	833590.77 833582.55	822047,38 822070.94		0.088	0.149	0.182	0.262	0.264	0.275	0.274	0.119	0.101	0.110		0.186	0.184
0044	833574.33	822094.55		0.092	0.132	0.232	0.181	0.183	0.195	0.282	0.084	0.094	0.148	-	0.164	0.177
0045	833682.05	822190.77		0.170	0.033	0.023	0.153	0.263	0.300	0.279	0.216	0.194	0.171		0.135	0.200
0046	833673.60	822214.34		0.183	0.049	0.027	0.141	0.206	0.271	0.217	0.187	0.125	0.149		0,120	0.162
	833665.14	822237.88		0.160	0.070	0.083	0.121	0.168	0.246	0.175	0.180	0.164	0.177		0.129	0.164
0047	833656.27	822261.04		0.087	0,052	0.032	0.077	0.103	0.203	0.124	0.103	0.121	0.103		0.080	0.109

			Proposed Case Wind direction (Degree)	45	67.5	90	112.5	135	157.5	180	202.5	225	247.5			
	Tes Point		Wind direction	NE	ENE	E	ESE	ŠE	SSE	5	SSW	SW	WSW	5um	Average	Average
ID	Easting (m)	Northing (m)	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6,5%	4.9%	4.5%	6.7%	6.8%		83.6%	(Annual)	(Summer)
0049	833500.99	821903.86	Probability (Summer)	0.200	0.237	8,3% 0.213	9,7%	0.267	0.296	9.2%	0.129	16.9% 0.288	7.6% 0.267	81.7%	0.237	0.250
0050	833492.37	821927.33		0.222	0.275	0.295	0.287	0.325	0.408	0.243	0.153	0.284	0.244	-	0.278	0.271
0051	833483.75	821950.80		0.122	0.168	0.187	0.224	0.228	0.264	0.135	0.126	0.134	0.198		0.179	0.177
0052	833475.14	821974.27		0.054	0.132	0.158	0.224	0.233	0.220	0.101	0.226	0.122	0.245		0.163	0.185
O053	833466.52 833457.93	821997.74 822021.22		0.044	0.108	0.068	0.206	0.189	0.162	0,036	0.224	0.220	0.404		0.130	0.191
0055	833449.35	822044.69		0.172	0.102	0.042	0.110	0.100	0.056	0.099	0.133	0.102	0.333		0.086	0.128
0056	833440.76	822068.17		0.240	0.095	0.084	0.157	0.181	0.160	0.139	0.440	0.287	0.174		0.171	0.228
0057	833432.17	822091.65		0,201	0,132	0.116	0,188	0.230	0.213	0,086	0.322	0,353	0,325		0,186	0,245
0058	833423.59	822115.13		0.082	0.043	0.021	0.083	0.060	0.038	0.061	0.200	0.175	0.095		0.072	0.108
0059	833415.00 833406.41	822138.61 822162.09		0.123	0.077	0.048	0.113	0.107	0.061	0.066	0.162	0.173	0.154		0.094	0.120
0061	833681.54	821817.30		0.065	0.319	0.023	0.059	0.077	0.031	0.079	0.266	0.188	0.134		0.058	0.237
0062	833662,17	821833.11		0.081	0.303	0,263	0,305	0,143	0,169	0.218	0,255	0.068	0.171		0.225	0.192
0063	833642.63	821848.71		0.103	0.277	0.243	0.271	0.056	0.112	0,112	0.092	0.066	0.245		0.184	0.138
0064	833622.52	821863.55		0.131	0.231	0.215	0.233	0.153	0.098	0.030	0.069	0.112	0.355		0.171	0.145
O065	833601.27 833577.88	821876.72 821885.56		0.164	0.200	0.167	0.193	0.200	0.149	0.055	0.050	0.107	0.370		0.157	0.145
0067	833553.62	821891.61		0.158	0.173	0.122	0.185	0.143	0.037	0.170	0.072	0.059	0.344		0.139	0.133
0068	833528.63	821891.21		0.164	0.150	0.123	0.219	0.143	0.155	0.281	0.038	0.166	0.329		0.154	0.171
0069	833503.70	821889.31		0.168	0.192	0.188	0.186	0.173	0.205	0.311	0.100	0.230	0.261		0.189	0.202
0070	833809.89	821828.55		0.054	0.016	0.047	0.191	0.274	0.290	0.328	0.114	0.057	0.055	-	0.118	0.156
0071	833790.74 833771.59	821844.62 821860.69		0.088	0.013	0.039	0,168	0.203	0,197	0.242	0.073	0,077	0.105		0.098	0.128
0073	833752.44	821876.76		0.086	0.013	0.089	0.101	0.054	0.057	0.074	0.223	0.164	0.050		0.091	0.118
0074	833921.77	821884.63		0.246	0.154	0.245	0.144	0.297	0.239	0.158	0.124	0.039	0.138		0.189	0.154
0075	833902.62	821900.70		0.054	0,055	0,110	0,160	0.301	0.147	0,036	0.036	0,146	0.199	h, 17	0.114	0.132
0076	833883.47	821916.77		0.083	0.066	0,101	0.105	0.135	0.083	0.115	0.106	0.152	0.228		0.102	0.128
0077	833864.32 833845.17	821932.84 821948.91		0.054	0.014	0.096	0.029	0.138	0.145	0.105	0.117	0.137	0.162		0.082	0.116
0079	833826.02	821948.91		0.084	0.047	0.179	0.053	0.038	0.191	0.154	0.091	0.208	0.200		0.095	0.146
0080	833977.41	821941.96		0.116	0.089	0,055	0.027	0,035	0.073	0,133	0,265	0.119	0,163		0.087	0.120
1300	833958.94	821956,75		0.035	0.097	0.100	0.024	0.067	0.140	0.169	0.285	0.061	0.190	1	0.098	0.132
0082	833940.69	821974.35		0.178	0.156	0.178	0.051	0.158	0.251	0.270	0.358	0.133	0.170	-	0.174	0.200
O083	833922.85 833904.56	821992.06 822007.36		0.218	0.128	0.197	0.103	0.259	0.293	0.296	0.340	0.140	0.123		0.197	0.219
0085	833885.34	822024.21		0.155	0.086	0.172	0.118	0.280	0.297	0.268	0.282	0.242	0.276		0.185	0.242
0086	833989.52	821957.37		0.179	0.178	0.149	0.046	0.097	0.085	0.140	0.311	0.091	0.154		0,141	0.141
0087	833970.62	821972.70		0.114	0,186	0.203	0.081	0.150	0.194	0.224	0,346	0.208	0.193		0.182	0.210
0088	833951.96	821988.58		0.205	0,088	0.208	0.114	0.253	0.281	0.293	0.345	0.193	0.255		0.198	0,243
0089	833932.78 833915.11	822004.73 822020.59		0.194	0.054	0.122	0.116	0.219	0.213	0.185	0.108	0,193	0,304	-	0.139	0.176
0091	833895.99	822036.28		0.120	0.032	0.063	0.066	0.226	0.231	0.182	0.178	0.273	0.235		0.119	0.132
0092	633853.32	822049.51		0.142	0.163	0.100	0.133	0.247	0.207	0.182	0.075	0.254	0,268		0.151	0.181
0093	833833.90	822065,25		0.041	0,052	0,069	0.028	0,221	0,189	0.176	0.151	0,260	0,125		0,105	0.161
0094	833814.39 833795.09	822080.88 822096.77		0.141	0.096	0.087	0.011	0.179	0.179	0.177	0.212	0.228	0.186		0.121	0.166
0095	833775.85	822112.73		0.039	0.104	0.081	0.038	0.152	0.156	0.201	0.042	0.245	0.339		0.098	0.151
0097	833754.94	822126.43		0.072	0.037	0.078	0.090	0.088	0.160	0.168	0.067	0.296	0.356		0.100	0.168
O098	833732.40	822140.31		0.089	0.069	0.084	0.099	0.113	0.152	0,152	0.115	0,340	0,358		0.117	0.187
0099	833704.92	822150.52		0.081	0.072	0.093	0.095	0.084	0.117	0.126	0.207	0,375	0.356		0.123	0.201
0100	833863.35 833844.65	822062.10		0.134	0.159	0.066	0.137	0.171	0.173	0.150	0.039	0.322	0.259		0.134	0.171
0102	833825.21	822078.70 822094.42		0.034	0.055	0.050	0.009	0.139	0.137	0.131	0.078	0.352	0.224		0.098	0.135
0103	833805.84	822110.23		0.182	0,153	0.141	0.048	0,150	0.194	0.206	0.197	0.403	0.381		0.166	0.230
0104	833785.64	822124.96		0.056	0.096	0.068	0.060	0.083	0.128	0.160	0.061	0.432	0.424		0.109	0.192
0105	833766.05	822140.48		0.036	0.061	0.044	0.073	0.107	0.181	0.183	0.135	0.416	0.424		0.108	0.211
O106	833746.17 833723.15	822155.62 822168.33		0.037	0.067	0.037	0.082	0.127	0,188	0.179	0.145	0.369	0.382		0.107	0.202
0108	833700.02	822176.18		0.061	0:034	0.058	0.086	0.110	0.175	0.137	0.171	0,329	0.270		0.105	0.182
0109	833684.50	822152.29		0.069	0.059	0.098	0.086	0.094	0.081	0.120	0.253	0.407	0.385		0.125	0.215
0110	833664.88	822149.89		0.104	0.049	0.097	0.075	0.104	0.097	0.155	0.296	0.434	0.417		0.134	0.236
0111	833641.28	822141.66		0.137	0,044	0,076	0.052	0.112	0.130	0.189	0.331	0,443	0.436		0.135	0.248
0112	833617.67 833594.06	822133.44 822125.22		0.154	0.054	0.057	0.067	0.158	0.173	0.180	0.362	0.444	0.443	-	0.144	0,262
0114	833570.45	822125.22		0.200	0.086	0.129	0.102	0.198	0.203	0.120	0.429	0.446	0.446		0.153	0.283
0115	833546.84	822108.77		0,205	0.105	0.044	0.134	0.238	0.218	0,079	0.470	0,450	0.438		0.175	0.289
0116	833523.23	822100.55		0.222	0.077	0.039	0.126	0.227	0.196	0.061	0.509	0.451	0.423		0.170	0.288
0117	833499.62	822092.33		0.242	0.084	0.074	0.145	0.224	0.189	0.085	0.529	0.436	0.403		0.186	0.294
0118	833476.01 833452.40	822084.10 822075.88		0.257	0.100	0.091	0.161	0.216	0.184	0.110	0.522	0.409	0.357		0.194	0.288
0120	833676.62	822177.18		0.261	0.024	0.057	0.167	0.204	0.180	0.082	0.477	0.362	0.261		0.100	0.197
0121	833660.27	822164.97		0.074	0.030	0.081	0.088	0.059	0.051	0.095	0.288	0.446	0.409		0.117	0,220
0122	833636.67	822156.74		0.103	0.024	0.090	0.107	0.092	0.101	0.171	0.307	0.460	0.434		0.137	0.249
0123	833613.06	822148.52		0.126	0.043	0.088	0.110	0.158	0.166	0.227	0.324	0.461	0.439		0.155	0.271
0124	833589.45	822140.30 822132.07		0.144	0.070	0.077	0.122	0.217	0.225	0.223	0.341	0.459	0.436		0.168	0.285
			-	0.187	0.093	0.134	0.173	0.276	0.233	0.203	0.373	0.426	0.404		0.179	0.301
O125 O126	833565.84 833542.23	822123.85			0.142	0.122	0.183	0.278	0.267	0.192	0.387	0.399	0.402		0.211	0.296
0125		822123.85 822115.63		0.215	With the		0.190	0.273	0.257	0.180	0.397	0.381	0.411		0.209	0.293
0125 0126 0127 0128	833542.23 833518.62 833495.01	822115.63 822107.40		0.209	0.136	0.125										
O125 O126 O127 O128 O129	833542.23 833518.62 833495.01 833471.40	822115.63 822107.40 822099.18		0.209	0.136	0.128	0,196	0.264	0,247	0.167	0.412	0,431	0.422		0.215	0.304
0125 0126 0127 0128 0129 0130	833542.23 833518.62 833495.01 833471.40 833447.79	822115.63 822107.40 822099.18 822090.96		0.209 0.224 0.235	0.136 0.134 0.132	0.128 0.123	0.196 0.202	0.253	0.247	0.167 0.130	0.412	0.431	0.390		0.215	0.304
0125 0126 0127 0128 0129 0130 0131	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29	822115.63 822107,40 822099.18 822090.96 822180.88	1	0.209 0.224 0.235 0.102	0.136 0.134 0.132 0.053	0.128 0.123 0.075	0.196 0.202 0.077	0.253	0.247 0.235 0.075	0.167 0.130 0.072	0.412 0.451 0.042	0.431 0.442 0.083	0.390		0.215 0.215 0.074	0.304 0.072
0125 0126 0127 0128 0129 0130	833542.23 833518.62 833495.01 833471.40 833447.79	822115.63 822107.40 822099.18 822090.96		0.209 0.224 0.235	0.136 0.134 0.132	0.128 0.123	0.196 0.202	0.253	0.247	0.167 0.130	0.412	0.431	0.390		0.215	0.304
0125 0126 0127 0128 0129 0130 0131 0132	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833798.99	822115.63 822107.40 822099.18 822090.96 822180.88 822196.77		0.209 0.224 0.235 0.102 0.072	0.136 0.134 0.132 0.053 0.068	0.128 0.123 0.075 0.073	0.196 0.202 0.077 0.070	0.253 0.099 0.109	0.247 0.235 0.075 0.027	0.167 0.130 0.072 0.017	0.412 0.451 0.042 0.022	0.431 0.442 0.083 0.061	0.390 0.057 0.060		0.215 0.215 0.074 0.064	0.304 0.072 0.052
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833798.99 833779.70 833760.40 833741.11	822115.63 822107.40 822099.18 822090.96 822180.88 822196.77 822212.67 822228.57 822244.46		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078	0.128 0.123 0.075 0.073 0.138 0.155 0.183	0.196 0.202 0.077 0.070 0.149 0.153 0.157	0.253 0.099 0.109 0.097 0.021 0.029	0.247 0.235 0.075 0.027 0.134 0.017 0.028	0.167 0.130 0.072 0.017 0.090 0.021 0.027	0.412 0.451 0.042 0.022 0.087 0.149 0.099	0.431 0.442 0.083 0.061 0.072 0.180 0.127	0.390 0.057 0.060 0.119 0.154 0.105		0.215 0.215 0.074 0.064 0.103 0.109 0.115	0.304 0.072 0.052 0.105 0.117 0.099
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833779.70 833760.40 833741.11 833721.81	82215.63 822107.40 822099.18 822090.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192	0,196 0,202 0,077 0,070 0,149 0,153 0,157 0,134	0.253 0.099 0.109 0.097 0.021 0.029 0.015	0,247 0.235 0.075 0.027 0.134 0.017 0.028 0.070	0,167 0,130 0,072 0,017 0,090 0,021 0,027 0,056	0.412 0.451 0.042 0.022 0.087 0.149 0.099	0.431 0.442 0.083 0.061 0.072 0.180 0.127 0.161	0.390 0.057 0.060 0.119 0.154 0.105 0.117		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116	0.304 0.072 0.052 0.105 0.117 0.099 0.108
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135 0136	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833798.99 833779.70 8337641.11 833721.81 833702.52	822115.63 822107.40 822099.18 822090.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36 822276.26		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096 0.150 0.090	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078 0.036	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192	0.196 0.202 0.077 0.070 0.149 0.153 0.157 0.134	0.253 0.099 0.109 0.097 0.021 0.029 0.015	0,247 0.235 0.075 0.027 0.134 0.017 0.028 0.070 0.049	0.167 0.130 0.072 0.017 0.090 0.021 0.027 0.056	0.412 0.451 0.042 0.022 0.087 0.149 0.099 0.079	0,431 0.442 0.083 0.061 0.072 0.180 0.127 0.161 0.108	0.390 0.057 0.060 0.119 0.154 0.105 0.117		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116	0.304 0.072 0.052 0.105 0.117 0.099 0.108 0.080
O125 O126 O127 O128 O129 O130 O131 O132 O133 O134 O135 O136 O137	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833798.99 833779.70 833760.40 833741.11 833721.81 833702.52	822115.63 822107.40 822099.18 822099.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36 822276.26		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096 0.150 0.090	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078 0.036 0.074	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192 0.140	0.196 0.202 0.077 0.070 0.149 0.153 0.157 0.134 0.106	0.253 0.099 0.109 0.097 0.021 0.029 0.015 0.032 0.152	0.247 0.235 0.075 0.027 0.134 0.017 0.028 0.070 0.049	0.167 0.130 0.072 0.017 0.090 0.021 0.027 0.056 0.072 0.236	0.412 0.451 0.042 0.022 0.087 0.149 0.099 0.079 0.052	0,431 0.442 0.083 0.061 0.072 0.180 0.127 0.161 0.108 0.133	0.390 0.057 0.060 0.119 0.154 0.105 0.117 0.062 0.187		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116 0.094	0.304 0.072 0.052 0.105 0.117 0.099 0.108 0.080 0.168
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135 0136	833542.23 833518.62 833495.01 833471.40 833447.79 833818.29 833798.99 833779.70 8337641.11 833721.81 833702.52	822115.63 822107.40 822099.18 822090.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36 822276.26		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096 0.150 0.090	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078 0.036	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192	0.196 0.202 0.077 0.070 0.149 0.153 0.157 0.134	0.253 0.099 0.109 0.097 0.021 0.029 0.015	0,247 0.235 0.075 0.027 0.134 0.017 0.028 0.070 0.049	0.167 0.130 0.072 0.017 0.090 0.021 0.027 0.056	0.412 0.451 0.042 0.022 0.087 0.149 0.099 0.079	0,431 0.442 0.083 0.061 0.072 0.180 0.127 0.161 0.108	0.390 0.057 0.060 0.119 0.154 0.105 0.117		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116	0.304 0.072 0.052 0.105 0.117 0.099 0.108 0.080
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135 0136 0137 0138	83542.23 835518.62 833495.01 833471.40 833447.79 833818.29 833779.70 833760.40 833741.11 833721.81 833702.52 833949.25 833949.25	822115.63 822107.40 822099.18 822090.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36 822276.26 822153.86		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096 0.150 0.090 0.096	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078 0.036 0.074 0.117	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192 0.140 0.212 0.236	0.196 0.202 0.077 0.070 0.149 0.153 0.157 0.134 0.106 0.163 0.198	0.253 0.099 0.109 0.097 0.021 0.029 0.015 0.032 0.152 0.146	0.247 0.235 0.075 0.027 0.134 0.017 0.028 0.070 0.049 0.062 0.096	0.167 0.130 0.072 0.017 0.090 0.021 0.027 0.056 0.072 0.236	0.412 0.451 0.042 0.022 0.087 0.149 0.099 0.079 0.052 0.201 0.083	0.431 0.442 0.083 0.061 0.072 0.180 0.127 0.161 0.108 0.133 0.096	0.390 0.057 0.060 0.119 0.154 0.105 0.117 0.062 0.187		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116 0.094 0.161	0.304 0.072 0.052 0.105 0.117 0.099 0.108 0.080 0.168
0125 0126 0127 0128 0129 0130 0131 0132 0133 0134 0135 0136 0137 0138 0139	83542.23 835518.62 833495.01 833471.40 833447.79 833818.29 833798.99 833799.70 833760.40 833741.11 833721.81 833702.52 833949.25 833949.25	822115.63 822107.40 822099.18 822099.96 822180.88 822196.77 822212.67 822228.57 822244.46 822260.36 822276.26 822276.26		0.209 0.224 0.235 0.102 0.072 0.047 0.069 0.096 0.150 0.090 0.096 0.099	0.136 0.134 0.132 0.053 0.068 0.055 0.064 0.078 0.036 0.074 0.117 0.067	0.128 0.123 0.075 0.073 0.138 0.155 0.183 0.192 0.140 0.212 0.236	0.196 0.202 0.077 0.070 0.149 0.153 0.157 0.134 0.106 0.163 0.198	0.253 0.099 0.109 0.097 0.021 0.029 0.015 0.032 0.152 0.146 0.150	0.247 0.235 0.075 0.027 0.134 0.017 0.028 0.070 0.049 0.062 0.096	0.167 0.130 0.072 0.017 0.090 0.021 0.027 0.056 0.072 0.236 0.149	0.412 0.451 0.042 0.022 0.087 0.149 0.099 0.079 0.052 0.201 0.083	0.431 0.442 0.083 0.061 0.072 0.180 0.127 0.161 0.108 0.133 0.096 0.058	0.390 0.057 0.060 0.119 0.154 0.105 0.117 0.062 0.187 0.045		0.215 0.215 0.074 0.064 0.103 0.109 0.115 0.116 0.094 0.149	0.304 0.072 0.052 0.105 0.117 0.099 0.108 0.080 0.168 0.126 0.124

0145 0146 0147 0148			Proposed Case Wind direction (Degree)	45	67.5	90	112.5	135	157.5	180	202.5	225	247.5			
0145 0146 0147 0148	Tes Point		Wind direction	NE	ENE	E	ESE	SE	SSE	5	SSW	SW	WsW	Sum	Average	Average
0145 0146 0147 0148	Easting (m)	Northing (m)	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	5,5%	4.9%	4.5%	6.7%	6.8%		83.6%	(Annual)	(Summer)
0146 0147 0148	100 T T T T T T T T T T T T T T T T T T	F-100	Probability (Summer)			8,3%	9,7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%		17
O147 O148	833816.77	822267.46		0.080	0.057	0.185	0.170	0.170	0.180	0.248	0.156	0.080	0.066		0.145	0.150
0148	833797.45 833778.14	822283.34		0.077	0:044	0.173	0.164	0.165	0.169	0.208	0.144	0.080	0.045		0.135	0.139
	834090.83	822299.21 822123.29		0.038	0.253	0.164	0.145	0.137	0.132	0.172	0.057	0.065	0.034		0.116	0.116
0149	834071.61	822139.27		0.302	0.286	0.357	0.155	0.134	0.140	0,125	0.156	0.060	0.139		0.229	0.148
0150	834052.38	822155.25		0.280	0.282	0.352	0.168	0.118	0.139	0.093	0.142	0.059	0.084		0.222	0.136
D151	834033.15	822171.23		0.201	0.241	0.270	0.138	0.074	0.118	0.043	0.106	0.056	0.141		0.173	0.111
0152	834013.92	822187.21		0.131	0.193	0.185	0.089	0.032	0.089	0.198	0.154	0.058	0.168		0.138	0.118
0153	833994.70	822203.18		0,081	0,140	0.144	0,066	0.076	0.074	0.190	0.220	0,092	0,133		0,121	0.128
0154	833975.47	822219.16	-	0.065	0.145	0.233	0.167	0.157	0.150	0.136	0.098	0.135	0.089		0.160	0.142
0155	833956.24 833937.01	822235.14 822251.12		0.044	0.118	0.219	0.158	0.167	0.142	0.135	0.097	0.107	0.030		0.147	0.128
0157	833937.68	822266.96		0.114	0.045	0.194	0.151	0.144	0.106	0.083	0.043	0.074	0,066		0.125	0.108
0158	833898,34	822282.81		0.043	0.016	0.167	0,130	0,139	0.107	0.062	0.037	0.123	0.023		0.103	0,097
0159	833879.00	822298.65		0.074	0.024	0.150	0.116	0.141	0.113	0,100	0.067	0.104	0.032		0.103	0.101
0160	833859.66	822314.49		0.071	0.015	0.135	0.115	0.144	0.119	0.099	0.069	0.078	0.059		0.096	0.097
0161	833891.02	822356.46		0.047	0.061	0.067	0.043	0.071	0.081	0.061	0.038	0.025	0.019		0.056	0.047
0162	833866.62	822346.88	1	0.058	0.058	0.018	0.016	0.026	0.040	0,065	0.033	0.073	0.023		0.038	0.040
O163 O164	833841.56 833818.06	822336.85 822328.33		0.106	0.028	0.083	0.078	0.093	0.078	0.057	0.052	0.079	0.058		0.073	0.071
0165	833794.55	822319.81		0.104	0.133	0.034	0.031	0.038	0.055	0.083	0.014	0.124	0.092		0.067	0.069
0166	833771.05	822311.28		0.043	0.102	0.099	0.090	0.100	0.095	0.113	0.139	0.134	0.117		0.100	0.115
0167	833747.55	822302.76		0,040	0.108	0.144	0,105	0,140	0,136	0.128	0.161	0,097	0.116		0.120	0.127
0168	833724.05	822294.24		0.088	0.101	0.100	0.063	0.103	0.077	0.097	0.157	0.037	0.092		0.092	0.089
0169	833700.54	822285.72		0.098	0.075	0.123	0.114	0.057	0.107	0.051	0.161	0.063	0.099		0.100	0.098
0170	833677.04	822277.20		0.116	0.090	0.061	0.046	0.066	0.072	0.067	0.183	0.086	0.141		0.081	0.095
0171	833653.54	822268.68		0.142	0,092	0,069	0,069	0.087	0.146	0.090	0.184	0.118	0.168		0.099	0.120
0172	833630.03	822260.16		0.156	0.096	0.077	0.056	0.077	0.064	0.066	0.207	0.159	0.214	-	0.100	0.124
0173	833606.53 833583.03	822251.63 822243.11		0.189	0.109	0.084	0.031	0.035	0.031	0.036	0.234	0.208	0.255		0.102	0.130
0174	833559.53	822234.59		0.182	0.098	0.104	0.085	0.079	0.073	0.104	0.240	0.236	0.260		0.122	0.156
0176	833536,02	822226.07		0.118	0.024	0.141	0.215	0,206	0.191	0.142	0.277	0,231	0,262		0.162	0.223
0177	833512.52	822217.55		0.192	0.149	0.173	0.272	0.234	0.203	0.147	0.244	0.197	0.217		0.199	0.212
0178	833489.02	822209.03		0.187	0.111	0.161	0.238	0.185	0.169	0.140	0.233	0.175	0.206		0.175	0.190
0179	833465.51	822200.51	1.	0.173	0.114	0.151	0.215	0.150	0.143	0.128	0.206	0.117	0.131		0.157	0.156
0180	833442.01	822191.98	i .	0,184	0,124	0,142	0,190	0.123	0.125	0,099	0.200	0.112	0.147		0.148	0.144
0181	833418.51	822183.46		0.172	0.119	0.120	0.149	0.091	0.105	0.053	0.179	0.100	0.154		0.125	0.121
0182	B33395.73	822175.47		0.184	0.126	0.105	0.131	0.081	0.100	0.048	0.171	0.193	0.224		0,126	0.140
O183	833494.09 833517.46	821958.10 821966.97		0.140	0.096	0.174	0.054	0.137	0.121	0.110	0.152	0.092	0.036		0.124	0,110
0185	833540.83	821975.85		0.187	0.123	0.212	0.110	0.173	0.156	0,151	0.059	0.090	0.023		0.153	0.121
0186	833564.20	821984.73		0.133	0.109	0.172	0.132	0.134	0.070	0.066	0.085	0.149	0.084		0.130	0.114
0187	833555.88	822008.30		0.146	0.048	0.186	0.021	0.038	0.019	0.068	0.141	0.085	0.088		0.098	0.085
0168	633547.55	822031.88		0.113	0.022	0.146	0.050	0.030	0.020	0.066	0.136	0.070	0.079		680.0	0.078
0189	833522.79	822032,20		0.039	0,005	0.047	0.065	0,058	0,034	0.079	0.202	0.165	0,044		0.067	0.103
0190	833499.37	822023.69	1	0.063	0.011	0.018	0.020	0.073	0.035	0.062	0.221	0.243	0.099		0.063	0.119
0191	833476.02	822014.76		0.134	0.019	0.037	0.036	0.077	0.014	0.057	0.230	0.263	0.217		0.080	0.138
O192 O193	834092.69 834076.69	822110.48 822091.28		0.166	0.203	0.195	0.075	0.100	0.115	0.143	0.139	0.039	0.216		0.144	0.118
0194	834061.01	822091.28		0.172	0.151	0.245	0.098	0.120	0.086	0.130	0.023	0.016	0.032		0.160	0.081
0195	834055.01	822106.10		0.266	0.074	0.110	0.083	0.055	0.060	0,056	0.102	0.037	0.160		0.098	0.079
0196	834071.23	822125.12		0.098	0.155	0.171	0.071	0.095	0.092	0.098	0.125	0.037	0.111		0.118	0.095
0197	834105.89	822119.29		0.086	0.124	0.112	0.030	0.035	0.045	0.074	0.075	0.041	0.102		0.078	0.062
0198	834121.82	822138.55		0.228	0.080	0.078	0,101	0.093	0.104	0.082	0.027	0.028	0.053		0.090	0.064
0199	834137.43	822158.08		0.258	0,156	0.166	0.186	0.177	0.222	0,174	0.132	0.101	0.036		0.172	0,144
0200	B34012.42	822196.28		0.078	0.112	0.114	0.035	0.045	0.045	0.229	0.211	0.047	0.124		0.098	0.108
0201	834028.88	822215.10	-	0.159	0.107	0.169	0.086	0.051	0.019	0.208	0.201	0.030	0.042		0.122	0.103
O202 O203	834045.22 833996.82	822234.02 822210.06		0.226	0.152	0.186	0.133	0.084	0.139	0.178	0.186	0.125	0.058		0,161	0.140
0204	834013.53	822228.65		0.118	0.110	0.035	0.068	0.054	0.035	0.185	0.222	0.048	0.083		0.084	0.097
0205	834030.03	822247.44		0.184	0.098	0.157	0.075	0.114	0.082	0.181	0.215	0.166	0.043		0.137	0.140
0206	833917.51	822281.83	1	0.131	0.105	0.108	0.085	0.126	0.105	0.189	0.161	0.092	0.067		0.115	0.118
0207	833931.03	822298.32	1.	0.125	0.106	0,030	0.022	0,065	0.069	0.167	0.138	0.121	0.083		0.077	0.094
0208	833945.00	822315.47		0.102	0.084	0.094	0.043	0.051	0.054	0.137	0.096	0.140	0.043		0.086	0.090
0209	833787.58	822327.31		0.120	0.182	0.055	0.044	0.074	0.080	0.088	0.118	0.103	0.091		0.092	0.086
O210 O211	833779.01 833771.18	822348.53 822369.01		0.075	0.126	0.076	0.054	0.092	0.078	0.039	0.059	0,070	0.032		0.077	0.063
0211	833693.07	822293.82		0.061	0.085	0.110	0.143	0.088	0.098	0,025	0.052	0.092	0.103		0.101	0.102
0213	833685.07	822315.42		0.032	0.076	0.027	0.134	0.038	0.059	0.055	0.030	0.032	0.013		0.059	0.053
0214	833677.37	822334.97		0.084	0.121	0.037	0.117	0.055	0.067	0.041	0.066	0.057	0.067		0.073	0.064
0215	833521.31	822229.48		0.110	0.121	0.090	0.146	0.137	0.130	0.105	0.137	0.131	0.137		0.118	0.128
0216	833514.08	822251.08		0.114	0,128	0,019	0,040	0,036	0.028	0,024	0.066	0,061	0,044	/	0.056	0,044
0217	833506.10	822272.25		0.173	0.197	0.008	0.039	0.055	0.056	0.061	0.076	0.076	0.099	1	0.076	0.061
0218	833496.89	822298.04		0.137	0.200	0.029	0.013	0.021	0.028	0.028	0.151	0.113	0.054		0.078	0.067
0219	833488.27	822321.50		0.141	0.077	0.048	0.076	0.043	0.045	0.031	0.068	0.066	0.044		0.067	0.056
D220	833483.05 833396.79	822335.87 822183.39		0.128	0.080	0.017	0.064	0.039	0.042	0.031	0.055	0.064	0.170		0.054	0.059
O220 O221	833388.48	822204.90	*·	0.054	0.035	0.037	0.012	0.009	0.008	0.031	0.105	0.099	0.069		0.041	0.056
0221	833380.97	822225.99		0.034	0.057	0.039	0.052	0.048	0.046	0.068	0.100	0.105	0.141		0.061	0.079
		822252.01		0.083	0.070	0.037	0.115	0.081	0.096	0.076	0.256	0.182	0.047		0.096	0.130
O221 O222	833371.73			0.061	0,056	0.017	0,120	0,099	0.081	0.056	0.201	0,167	0.027		0.081	0.112
O221 O222 O223 O224 O225	833362.73	822275.33			0.322	0.018	0.056	0.047	0.038	0.114	0.346	0.400	0.376		0.165	0.207
0221 0222 0223 0224 0225 0226	833362.73 833356.43	822295.67		0.353				0.181	0.215	0.166	0.147	0.119	0.036			
O221 O222 O223 O224 O225 O226 O227	833362.73 833356.43 834133.62	822295.67 822168.09		0.303	0.185	0.208	0.190								0,195	0.155
O221 O222 O223 O224 O225 O226 O227 O228	833362.73 833356.43 834133.62 834114.86	822295.67 822168.09 822184.62		0.303 0.318	0.185	0.257	0.187	0.164	0.191	0.142	0.143	0.125	0.076		0.207	0.156
O221 O222 O223 O224 O225 O226 O227 O228 O229	833362.73 833356.43 834133.62 834114.86 834095.37	822295.67 822168.09 822184.62 822200.27		0,303 0,318 0,309	0.185 0.200 0.198	0.257 0.277	0.187	0.164 0.185	0.191	0,142	0.143	0.125 0.124	0.076		0.207 0.215	0.156 0.161
O221 O222 O223 O224 O225 O226 O227 O228 O229 O230	833362.73 833356.43 834133.62 634114.86 834095.37 834076.20	822295.67 822168.09 822184.62 822200.27 822216.32		0.303 0.318 0.309 0.292	0.185 0.200 0.198 0.187	0.257 0.277 0.280	0.187 0.213 0.214	0.164 0.185 0.187	0.191 0.206 0.212	0,142 0,139 0,115	0.143 0.116 0.074	0.125 0.124 0.126	0.076 0.087 0.084		0.207 0.215 0.208	0.156 0.161 0.152
O221 O222 O223 O224 O225 O226 O227 O228 O229 O230 O231	833362.73 833356.43 834133.62 834114.86 834095.37 834076.20 834057.16	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52		0.303 0.318 0.309 0.292 0.266	0.185 0.200 0.198 0.187 0.169	0.257 0.277 0.280 0.258	0.187 0.213 0.214 0.198	0.164 0.185 0.187 0.166	0.191 0.206 0.212 0.204	0.142 0.139 0.115 0.085	0.143 0.116 0.074 0.072	0.125 0.124 0.126 0.130	0.076 0.087 0.084 0.073		0.207 0.215 0.208 0.192	0.156 0.161 0.152 0.142
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231	833362.73 833356.43 834133.62 834114.86 834095.37 834076.20 834057.16 834037.68	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 8222348.19		0.303 0.318 0.309 0.292 0.266 0.198	0.185 0.200 0.198 0.187 0.169 0.101	0.257 0.277 0.280 0.258 0.204	0.187 0.213 0.214 0.198 0.141	0.164 0.185 0.187 0.166 0.097	0.191 0.206 0.212 0.204 0.151	0.142 0.139 0.115 0.085 0.183	0.143 0.116 0.074 0.072 0.212	0.125 0.124 0.126 0.130 0.150	0.076 0.087 0.084 0.073 0.048		0.207 0.215 0.208 0.192 0.162	0.156 0.161 0.152 0.142 0.155
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231 0232	833362.73 833356.43 834133.62 834114.86 834095.37 834076.20 834057.16 834037.68 834018.66	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 822248.19 822264.41		0.303 0.318 0.309 0.292 0.266 0.198 0.098	0.185 0.200 0.198 0.187 0.169 0.101 0.017	0.257 0.277 0.280 0.258 0.204 0.233	0.187 0.213 0.214 0.198 0.141 0.140	0.164 0.185 0.187 0.166 0.097 0.114	0.191 0.206 0.212 0.204 0.151 0.150	0.142 0.139 0.115 0.085 0.183 0.067	0.143 0.116 0.074 0.072 0.212 0.044	0.125 0.124 0.126 0.130 0.150 0.178	0.076 0.087 0.084 0.073 0.048 0.062		0.207 0.215 0.208 0.192 0.162 0.132	0.156 0.161 0.152 0.142 0.155 0.124
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231 0232 0233 0234	833362.73 833356.43 834133.62 634114.86 834095.37 834076.20 834057.16 834037.68 834018.66 833999.13	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 8222348.19 822264.41 822280.02		0.303 0.318 0.309 0.292 0.266 0.198 0.098	0.185 0.200 0.198 0.187 0.169 0.101 0.017	0.257 0.277 0.280 0.258 0.204 0.233 0,202	0.187 0.213 0.214 0.198 0.141 0.140 0.124	0.164 0.185 0.187 0.166 0.097 0.114 0.101	0.191 0.206 0.212 0.204 0.151 0.150 0.124	0.142 0.139 0.115 0.085 0.183 0.067 0.071	0.143 0.116 0.074 0.072 0.212 0.044 0.087	0.125 0.124 0.126 0.130 0.150 0.178 0.083	0.076 0.087 0.084 0.073 0.048 0.062 0.061		0.207 0.215 0.208 0.192 0.162 0.132 0.123	0.156 0.161 0.152 0.142 0.155 0.124 0.103
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231 0232	833362.73 833356.43 834133.62 834114.86 834095.37 834076.20 834057.16 834037.68 834018.66	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 822248.19 822264.41		0.303 0.318 0.309 0.292 0.266 0.198 0.098	0.185 0.200 0.198 0.187 0.169 0.101 0.017	0.257 0.277 0.280 0.258 0.204 0.233	0.187 0.213 0.214 0.198 0.141 0.140	0.164 0.185 0.187 0.166 0.097 0.114	0.191 0.206 0.212 0.204 0.151 0.150	0.142 0.139 0.115 0.085 0.183 0.067	0.143 0.116 0.074 0.072 0.212 0.044	0.125 0.124 0.126 0.130 0.150 0.178	0.076 0.087 0.084 0.073 0.048 0.062		0.207 0.215 0.208 0.192 0.162 0.132	0.156 0.161 0.152 0.142 0.155 0.124
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231 0232 0233 0234 0235	833362.73 833356.43 834133.62 634114.86 834095.37 834076.20 834057.16 834037.68 834018.66 833999.13 833979.88	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 8222348.19 822264.41 822280.02 822295.97		0.303 0.318 0.309 0.292 0.266 0.198 0.098 0.117 0.178	0.185 0.200 0.198 0.187 0.169 0.101 0.017 0.059	0.257 0.277 0.280 0.258 0.204 0.233 0,202 0.217	0.187 0.213 0.214 0.198 0.141 0.140 0.124 0.148	0.164 0.185 0.187 0.166 0.097 0.114 0.101	0.191 0.206 0.212 0.204 0.151 0.150 0.124 0.135	0,142 0,139 0,115 0,085 0,183 0,067 0,071	0.143 0.116 0.074 0.072 0.212 0.044 0.087 0.091	0.125 0.124 0.126 0.130 0.150 0.178 0.083 0.061	0,076 0,087 0,084 0,073 0,048 0,062 0,061 0,047		0.207 0.215 0.208 0.192 0.162 0.132 0.123 0.147	0.156 0.161 0.152 0.142 0.155 0.124 0.103 0.105
0221 0222 0223 0224 0225 0226 0227 0228 0229 0230 0231 0232 0233 0233 0234 0235 0236	833362.73 833356.43 834133.62 634114.86 834095.37 834076.20 834057.16 834037.68 834037.68 834037.68 834037.68	822295.67 822168.09 822184.62 822200.27 822216.32 822232.52 822248.19 822264.41 822280.02 822295.97 822311.88		0.303 0.318 0.309 0.292 0.266 0.198 0.098 0.117 0.178 0.151	0:185 0:200 0:198 0:187 0:169 0:101 0:017 0:059 0:124 0:107	0.257 0.277 0.280 0.258 0.204 0.233 0.202 0.217 0.174	0.187 0.213 0.214 0.198 0.141 0.140 0.124 0.148 0.131	0.164 0.185 0.187 0.166 0.097 0.114 0.101 0.123 0.119	0.191 0.206 0.212 0.204 0.151 0.150 0.124 0.135	0.142 0.139 0.115 0.085 0.183 0.067 0.071 0.071	0.143 0.116 0.074 0.072 0.212 0.044 0.087 0.091	0.125 0.124 0.126 0.130 0.150 0.178 0.083 0.061	0.076 0.087 0.084 0.073 0.048 0.062 0.061 0.047		0.207 0.215 0.208 0.192 0.162 0.132 0.123 0.147 0.126	0.156 0.161 0.152 0.142 0.155 0.124 0.103 0.105 0.095

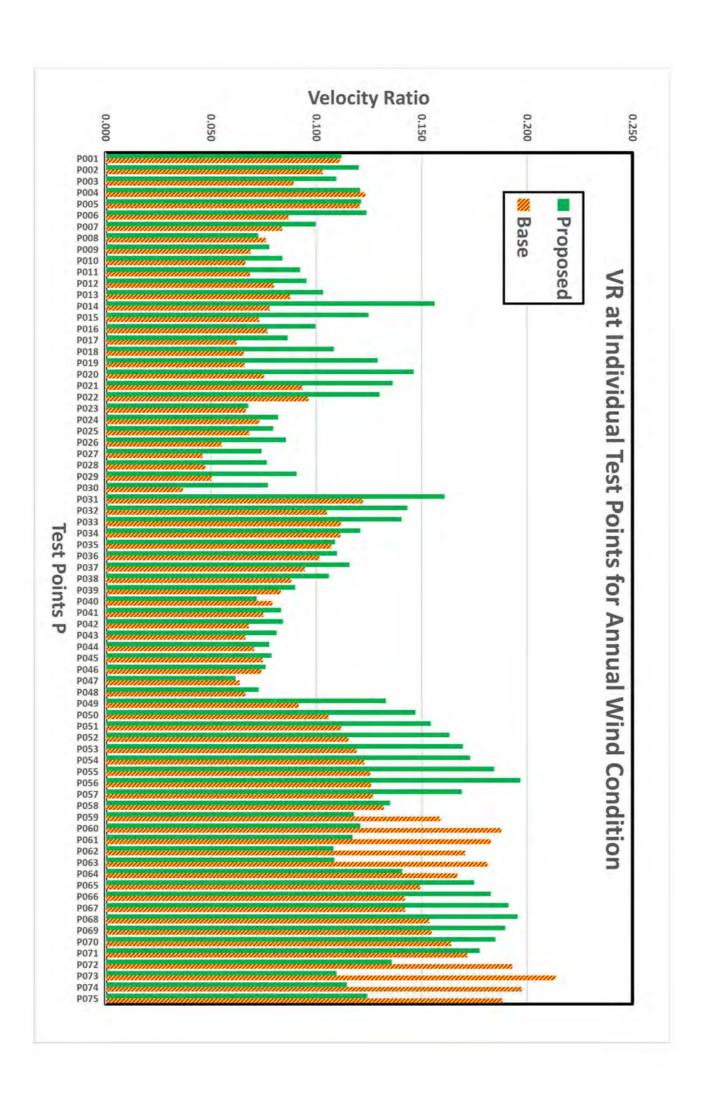
Wind	Velocit	y Ratio,	Proposed Case													
	Tes Point		Wind direction (Degree) Wind direction	A5 NE	67.5 ENE	90 E	112.5 ESE	135 SE	157.5 SSE	180	202.5 55W	225 SW	247.5 WSW	5um	Average	Average
			Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6.5%	4.9%	4.5%	6.7%	6.8%	WSW	83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)	11070		8.3%	9.7%	7,6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	T	(Committee)
0241	833866.22	822391.65		0.072	0.106	0.062	0.019	0.082	0.126	0.031	0.014	0.049	0.014		0.062	0.046
0242	833851.35	822407,57		0.110	0.134	0.054	0.037	0.059	0.097	0.080	0.105	0.087	0.084		0.080	0.078
0243	833827.89	822398.95		0.062	0.089	0.057	0.011	0.015	0.024	0.065	0.114	0.108	0.090	\vdash	0.059	0.069
0244	833804.30 833780.78	822390.67		0.051	0.105	0.058	0.016	0.011	0.073	0.054	0.138	0.109	0.118		0.066	0.080
0245	833757.33	822382.18 822373.51		0.040	0.079	0.047	0.012	0.020	0.102	0.036	0.126	0.104	0.130	$\overline{}$	0.037	0.077
0247	833734.04	822364.43		0.051	0.014	0.081	0.048	0.077	0.079	0.036	0.127	0.084	0.136		0.065	0.085
0248	833710.59	822355.78		0.055	0.055	0.079	0.046	0.083	0.070	0.012	0.127	0.074	0.143		0.068	0.080
0249	833687.02	822347.45	1	0.030	0,139	0,067	0,036	0.086	0.069	0,029	0.150	0,126	0.167		0.081	0,097
0250	833663.42	822339.18		0.169	0.213	0.067	880.0	0.101	0.094	0.105	0.180	0.166	0.182		0.124	0.130
0251	833639.95	822330.58		0.196	0.224	0.030	0.019	0.073	0.042	0.109	0.231	0.211	0.201		0.111	0,131
0252	833616.38	822322.23		0.179	0.210	0.037	0.057	0.074	0.037	0.118	0.276	0.253	0.224	-	0.123	0.156
O253	833593.28 833569.92	822312.67 822303.77		0.205	0.168	0.027	0.029	0,058	0.037	0,129	0,297	0.281	0.248		0.115	0.163
0255	833546.38	822295.35		0.201	0.219	0.054	0.035	0.035	0.080	0.135	0.032	0.042	0.212		0.091	0.070
0256	833522.92	822286.72		0.209	0.212	0.035	0.067	0.057	0.075	0.145	0.035	0.057	0.220		0.094	0.079
0257	833499.46	822278.09		0.190	0.227	0.029	0.023	0.067	0.080	0.130	0.244	0.201	0.268		0.115	0.144
0258	833475.98	822269.49	d.	0.220	0.160	0.016	0.011	0.043	0.045	0.108	0.257	0.217	0.279		0.100	0.139
0259	833452.58	822260.70		0.243	0.185	0.021	0.046	0.064	0.053	0.062	0.253	0.212	0.289		0.111	0.141
0260	833429.26	822251.69	ii-	0.273	0.205	0.024	0.129	0.119	0.087	0.014	0.238	0.197	0.292	-	0.131	0.148
O261 O262	833405.77 833381.89	822243.13 822234.73		0.248	0.173	0.006	0.170	0.142	0.092	0.068	0.120	0.153	0.286		0.117	0,130
0263	833661.30	822392.32		0.100	0.104	0.015	0.034	0.014	0.039	0.058	0.231	0,068	0.067	$\overline{}$	0.051	0.049
0264	833639.45	822380.18	1	0.177	0.207	0.034	0.011	0.023	0.034	0.051	0.109	0,048	0.029		0.076	0.048
0265	833617.91	822367.49	7	0.201	0.241	0.048	0.090	0.062	0.077	0.055	0.047	0.057	0.031		0.101	0.058
0266	833594.76	822358.04		0.191	0.247	0.077	0.127	0.107	0.110	0.055	0.146	0.100	0.043		0.130	0.100
0267	833571.50	822348.88	1,	0.176	0,076	0,064	0.118	0.079	0.094	0.056	0.114	0.079	0.078		0.092	0.087
0268	833548.06	822340.20		0.118	0.048	0.088	0.138	0.091	0.095	0.048	0.163	0.134	0.052		0.100	0,109
0269	833524.81	822331.01		0.174	0.091	0.096	0.130	0.070	0.061	0.015	0.163	0.173	0.091	-	0.110	0.112
0270	833501.49 833471.89	822321.99 822335.41		0.214	0.130	0.079	0.099	0.033	0.019	0.029	0.152	0.189	0.170		0.107	0.109
0271	833448.29	822335.41		0.073	0.096	0.018	0.082	0.075	0.077	0.066	0.067	0.096	0.238		0.056	0.087
0272	833425.53	822318.81		0.091	0.055	0.023	0.013	0.047	0.051	0.090	0.260	0.249	0.322		0.071	0.150
0274	833401.62	822309.78		0.186	0.183	0.030	0.022	0.017	0.021	0.098	0.322	0.270	0.330		0.111	0.163
0275	833378.55	822301.33		0.333	0.309	0.034	0.030	0.023	0.026	0.120	0.378	0.349	0.355		0.158	0.196
0276	833677.38	821849.60	J	0.063	0.117	0.131	0.104	0.248	0.129	0.196	0.336	0,156	0.118		0.150	0.185
0277	833693.33	821868.85		0.057	0.052	0.032	0.082	0.160	0.114	0.139	0.250	0.179	0.241		0.095	0.158
0278	B33709.27	821888.11		0.074	0.069	0.052	0.057	0.156	0.119	0.112	0.206	0.185	0.290		0,096	0.152
0279	833725.22	821907.36		0.090	0.086	0.029	0.032	0.160	0.138	0.131	0.219	0.185	0.317		0.093	0,156
O280 O281	833741.17 833757.11	821926.61 821945.87		0.113	0.104	0.038	0.066	0.167	0.168	0.163	0.241	0.192	0.351	\vdash	0.112	0,177
0282	833773.06	821965.12	1	0.145	0.132	0.048	0.100	0.079	0.067	0.069	0.292	0.131	0,392		0.121	0.152
0283	833789.01	821984.38		0.148	0.134	0.043	0.083	0.045	0.075	0.070	0.291	0.043	0.369		0.095	0.127
0284	633804.95	822003.63	\$	0.143	0.141	0.049	0.082	0.060	0.029	0.030	0.272	0.126	0.345		0.099	0.132
0285	833820.90	822022.88		0,129	0,135	0,031	0.098	0.051	0.082	0,069	0,203	0,191	0,312		0,099	0.140
0286	833658.41	821865.88	1	0.092	0.073	0.137	0.107	0.186	0.128	0.196	0.222	0.109	0.290		0.130	0.167
0287	833674.35	821885,13		0.077	0.051	0.052	0.095	0.195	0.130	0.200	0.289	0.123	0.297		0.109	0.174
0288	833690.30 833706.25	821904.38		0.065	0.080	0.045	0.044	0.185	0.145	0.178	0.282	0.108	0.314	-	0.100	0.162
O289 O290	833722.19	821923.64 821942.89	1	0.058	0.101	0.055	0.029	0.198	0.160	0.164	0.249	0.118	0.327		0.102	0.160
0291	833738.14	821962.15	1	0.077	0.121	0.082	0.097	0.197	0.175	0.165	0.251	0.176	0.324		0.130	0.184
0292	833754.09	821981.40		0.090	0.112	0.091	0.102	0.163	0.117	0.110	0.260	0.138	0.300		0.121	0.162
0293	833770.03	822000.65		0.102	0.099	0.094	0.081	0.110	0.057	0.057	0.275	0.048	0.288		0.101	0.126
0294	833785.98	822019.91		0.115	0.077	0.094	0.048	0.081	0.066	0,062	0.279	0.114	0.277		0.099	0.134
0295	833801.93	822039.16		0.118	0,065	0.060	0.047	0,109	0.160	0,136	0.257	0.190	0.240	$\overline{}$	0.104	0,160
0296	833639.43 833655.38	821882.15	i.e	0.124	0.065	0.139	0.125	0.118	0.107	0.140	0.099	0.106	0.308	\vdash	0.115	0.134
O297 O298	833671.33	821901.41 821920.66		0.112	0.049	0.086	0.106	0.162	0.122	0.195	0.161	0.068	0.301		0.104	0.141
0299	833687.27	821939.92		0.096	0.082	0.125	0.043	0.207	0.170	0.207	0.260	0.092	0.276		0.125	0.167
0300	833703.22	821959.17	-	0.057	0.085	0.154	0.073	0.230	0.193	0.201	0.253	0.050	0.210		0.133	0.162
0301	833719.17	821978.42		0.037	0.078	0.165	0.102	0.232	0.204	0.197	0.247	0.122	0.138		0.143	0.174
0302	833735.11	821997.68	7	0.036	0.067	0.160	0.107	0.216	0.186	0.182	0.243	0.117	0.109		0.137	0.165
0303	833751.06	822016.93		0.040	0,066	0.144	0.085	0.172	0.111	0.116	0.241	0.039	0.146		0.112	0.129
0304	833767.01 833782.95	822036.18	-	0.037	0.070	0.132	0.041	0.096	0.080	0.054	0.242	0.090	0.147		0.096	0.116
O305	833782.95	822055.44 821898.43		0.061	0.066	0.109	0.022	0.110	0.167	0.147	0.234	0.152	0.124	\vdash	0.104	0.141
0307	833636.40	821917.69		0.139	0.031	0.119	0.107	0.127	0.100	0,129	0.047	0,055	0.254		0.096	0.107
0308	833652.35	821936.94		0.132	0.044	0.165	0.098	0,150	0.130	0.179	0.103	0.141	0.223		0.125	0.143
0309	833668.30	821956.19		0.133	0.052	0.204	0.079	0.184	0.160	0,209	0.179	0.098	0.171		0.142	0.154
0310	833684.24	821975.45		0.081	0.049	0.216	0.089	0.223	0.188	0.221	0.229	0.045	0.090		0.146	0.154
0311	833700.19	821994.70		0.056	0.039	0.193	0.108	0.245	0.208	0.218	0.232	0.085	0.097		0.146	0.167
0312	833716.14	822013.95	1	0.055	0.043	0.155	0.108	0.242	0.205	0.207	0.227	0.074	0.128		0.134	0.162
0313	833732.08 833748.03	822033.21 822052.46		0.053	0.060	0.129	0.085	0.216	0.164	0.174	0.215	0.054	0.167		0.117	0.143
0314	833763.98	822052.46		0.049	0.082	0.117	0.044	0.163	0.074	0.086	0.202	0.069	0.194		0.097	0.117
0316	833601.30	821914.50		0.171	0.022	0.087	0.107	0.194	0.162	0.154	0.097	0.057	0.133		0.102	0.114
0317	833617.25	821933.75		0.152	0.033	0.175	0.141	0.165	0.126	0.155	0.081	0,076	0.164		0.126	0.125
0318	833633.19	821953.00		0.151	0.042	0.215	0.143	0.139	0.111	0.138	0.037	0.160	0.165		0.138	0.133
0319	833649.14	821972.26		0.158	0.046	0.230	0.128	0.144	0.129	0.149	0.056	0.071	0.122	-	0.137	0.118
0320	833665.09	821991.51		0.044	0.043	0.192	0.134	0.191	0.172	0.195	0.111	0.089	0.131		0.132	0.142
0321	833681.03	822010.77		0.034	0.034	0.115	0.124	0.233	0.206	0.227	0.167	0.094	0.178		0.120	0.159
0322	833696.98	822030.02 822049.27		0.042	0.021	0.089	0.107	0.251	0.217	0.234	0.171	0.074	0.210	1	0.111	0.158
0324	833712.93 833728.87	822049.27		0.050	0.058	0.075	0.078	0.244	0.200	0.216	0.174	0.050	0.229		0,103	0.148
0325	833598.23	821949.98		0.127	0.057	0.076	0.206	0.216	0.200	0.172	0.174	0.030	0.171		0.133	0.124
0326	833614.17	821969.23		0.156	0.072	0.135	0.198	0.159	0.140	0.114	0.122	0,184	0.220		0.154	0.164
0327	833630.12	821988.48		0.175	0.058	0.179	0.143	0.114	0.084	0.064	0.042	0.023	0.066		0.115	0.079
0328	833705.99			0.048	0.049	0.035	0.015	0.067	0.063	0.078	0.189	0.019	0.100		0.053	0.073
0329	833853.65	821865.50		0.086	0.053	0.068	0.026	0.060	0.117	0.082	0.085	0.331	0.158		0.087	0.134
0330	833840.40	821873,52		0,069	0,050	0.082	0.051	0,082	0,200	0,156	0,090	0,397	0,214	1	0.109	0.177
	833849.95	821885.09		0.109	0,067	0.095	0.048	0.049	0.171	0.146	0.090	0.329	0.220		0.107	0.158
0331		821896.66	1	0.083	0.061	0.124	0.059	0.019	0.092	0.115	0.035	0.215	0.122	-	0.091	0.105
0332	833859.49			8.000												
O332 O333	833829.02	821883.22		0.062	0.021	0.081	0.056	0.111	0.218	0.172	0.050	0.318	0.160		0.099	0.155
0332				0.062 0.095 0.111	0.021 0.046 0.081	0.081 0.058 0.143	0.056	0.052	0.218	0.177	0.050	0.318 0.307 0.351	0.160 0.182 0.186		0.099 0.097 0.126	0.151

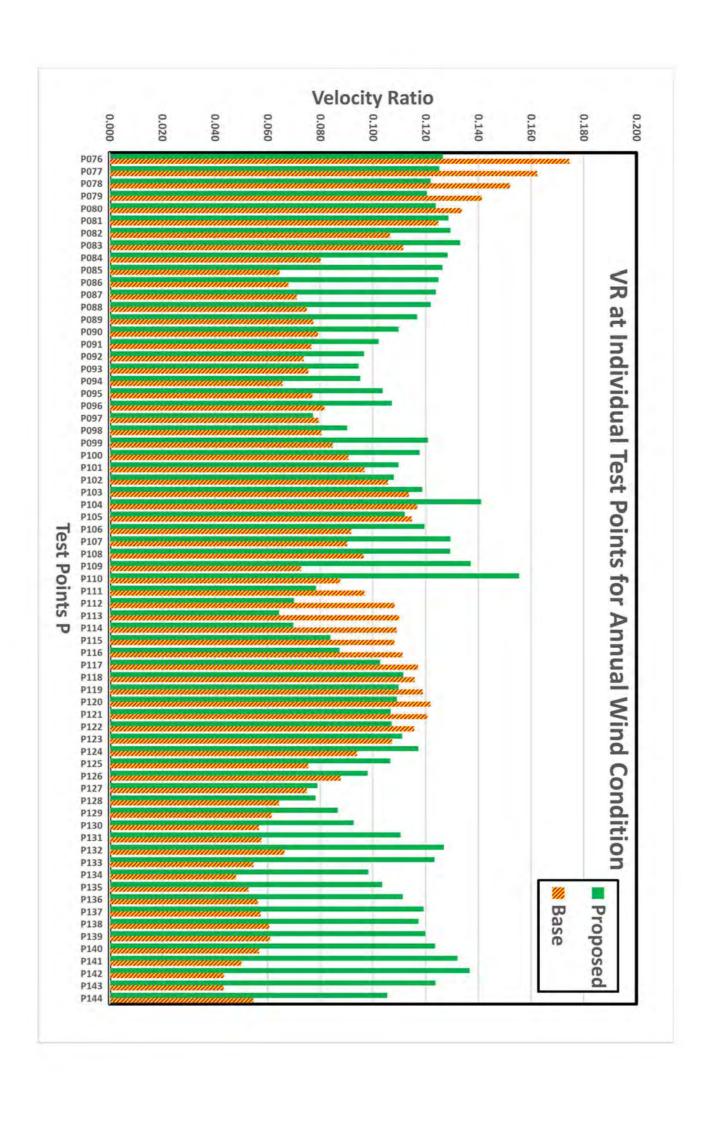
wind	velocit	y Ratio,	Proposed Case Wind direction (Degree)	45	67.5	90	112.5	135	157.5	180	202.5	225	247.5			
	Tes Point	t.	Wind direction	NE.	ENE	. E	ESE	SE	SSE	5	55W	SW	247.5 WSW	5um	Average	Average
ID	Easting (m)	Northing (m)	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	5,5%	4.9%	4.5%	6.7%	6.8%		83.6%	(Annual)	(Summer)
0337	2017/2010	821901.13	Probability (Summer)	0.044	0.011	0.056	9,7%	0.047	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	0.062	0.005
0338	833828.51 833932.47	821892.35		0.240	0.013	0.036	0.024	0.047	0.151	0.125	0.071	0.159	0.085		0.062	0.095
0339	833941.87	821904.03		0.204	0.144	0.190	0.074	0.058	0.096	0.074	0.033	0.036	0.053		0.120	0.069
0340	833951.27	821915.72		0.124	0.083	0.091	0.078	0.103	0.115	0.080	0.033	0.018	0.041		0.082	0.062
0341	833919.84	821903.19		0.196	0.138	0.187	0.122	0.142	0.028	0,024	0.018	0,022	0,035		0.122	0.063
O342 O343	833929.72 833939.60	821914.47 821925.76		0.171	0.117	0.181	0.122	0.114	0.072	0.075	0.030	0.048	0.038		0.122	0.078
0344	833900.99	821917.58		0.108	0.088	0.097	0.050	0.093	0.036	0.056	0.031	0.106	0.096		0.079	0.071
0345	833910,39	821929,27		0.077	0,073	0,055	0,076	0,132	0,068	0,069	0,023	0,158	0,108		0,076	0,088
0346	833919.79	821940.96	1	0.052	0.078	0.045	0.064	0,128	0.056	0.056	0.016	0.168	0.115		0.069	0.084
O347 O348	833929.19 833938.59	821952.65 821964.34		0.049	0.068	0.072	0.048	0.087	0.036	0.033	0.039	0.159	0.082		0.067	0.076
0349	833890.50	821926.82		0.098	0.067	0.090	0.092	0.139	0.138	0.140	0.146	0.218	0,093		0.112	0.142
0350	833900.14	821938.31		0.081	0.034	0,123	0,078	0,136	0,165	0,163	0.148	0.164	0,056		0.110	0.134
0351	833909.78	821949.80		0.070	0.040	0.089	0.049	0.121	0.176	0,169	0.149	0.142	0.053		0.095	0.123
O352	833919.42 833929.07	821961.29 821972.79	-	0.074	0.062	0.064	0.038	0.092	0.182	0.165	0.163	0.105	0.051		0.086	0.111
0354	834031.20	822022.99		0.139	0.166	0.132	0.056	0.054	0.065	0.139	0.147	0.015	0.020		0.109	0.078
0355	834044.19	822038.46		0.072	0.059	0.083	0.027	0.045	0.115	0.110	0.100	0.030	0.025		0.067	0.065
0356	833968.40	822059.06		0.147	0.103	0.096	0.049	0.079	0.054	0.066	0.099	0.088	0.185		0.089	880.0
0357	833978.02	822070.57	-	0.158	0.098	0.042	0.017	0.070	0.030	0.116	0.087	0.068	0.157		0.068	0.072
0358	833987.63 833997.25	822082.09 822093.60		0.151	0.082	0,080	0.032	0.043	0.065	0.103	0.079	0.056	0.182		0.069	0.074
0360	834006.87	822105.11		0.039	0.041	0.083	0.058	0.031	0.071	0.073	0.074	0,028	0.164		0.058	0.067
0361	833959.48	822066.78		0.097	0.113	0.063	0.041	0.085	0.037	0.092	0.125	0.084	0.180		0.079	0.089
0362	833969.16	822078.24		0.122	0.123	0.028	0.019	0.088	0.052	0.078	0.105	0.061	0.150		0.067	0.072
O363	833978.84 833988.52	822089.70 822101.16		0.107	0,116	0,063	0.037	0.062	0.076	0.093	0,081	0.049	0.163		0.074	0.074
0365	833998.20	822112.62		0.056	0.040	0.080	0.059	0.019	0.084	0.109	0.075	0.030	0.156		0.060	0.068
0366	833947.28	822077.33		0.077	0.129	0.081	0.067	0.095	0.060	0.149	0.164	0.066	0.153		0.095	0.104
0367	833957.20	822088.58		0.099	0.141	0.064	0.065	0.102	0.070	0.120	0.142	0.054	0.132		0.090	0.092
O368	833967.11 833977.03	822099.84 822111.09		0.094	0.132	0.092	0,084	0.093	0.089	0,124	0.137	0,045	0.129		0.098	0.096
0370	833986.95	822111.09		0.072	0.034	0.068	0.045	0.036	0.083	0.132	0.147	0.064	0.134		0.100	0.089
0371	833898.29	822137.37		0.066	0.064	0.073	0.064	0.059	0.122	0.155	0.081	0.094	0.067		0.078	0.090
0372	833908.77	822148,17		0.043	0.034	0,040	0.036	0.063	0.122	0.175	0.077	0.088	0.060		0.059	0,083
0373	833870.30	822151.60		0.059	0.073	0.033	0.049	0.037	0.067	0.080	0.038	0.070	0.110		0.052	0.060
0374	833880.63 833856.97	822162,47 822161,59		0.034	0.026	0.023	0.030	0.035	0.091	0.078	0.039	0.044	0.033		0,036	0.046
D376	833867.44	822172.33		0.040	0,031	0.013	0.047	0.026	0.082	0.054	0.033	0.039	0.032		0.034	0.040
0377	833611.59	822332,37		0.083	0.092	0,046	0.081	0.077	0.065	0,022	0.099	0,072	0,036		0.070	0.066
0378	833635.20	822340.59		0.160	0.180	0.065	0.074	0.111	0.099	0.028	0.155	0.138	0.117		0.109	0.105
D379 D360	833658.54 833675.53	822349.55 822355.49		0.124	0.168	0.077	0.115	0.101	0.097	0.050	0.112	0.120	0.131	_	0.108	0.102
0381	833668.22	822374.10		0,056	0,068	0.025	0.038	0.036	0.037	0.065	0.044	0,056	0.068		0,042	0.044
0382	833645.34	822364.03		0.134	0.177	0.064	0.083	0.049	0.047	0.016	0.106	0.102	0.055		0.092	0.072
0383	833622.17	822354.63		0.154	0.184	0.063	0.099	0.084	0.087	0.033	0.097	0.080	0.035		0.100	0.075
D001	833605.61 833820.29	822348,74 822111.30		0.097	0.135	0.052	0.090	0.076	0.077	0.031	0.107	0.070	0.021		0.082	0.069
D002	833812.49	822117.56		0.183	0.161	0.137	0.044	0.130	0.191	0,198	0.229	0,207	0.248		0.150	0.178
D003	833804.69	822123.81		0.120	0.138	0.048	0.030	0.110	0.130	0.149	0.205	0.185	0.207		0.104	0.142
D004	833826.88	822118.83		0.019	0,019	0.009	0.029	0.045	0.100	0.099	0.159	0.043	0.091		0.042	0.075
D005	833819.07 833811.27	822125.08 822131.34		0.159	0.151	0.137	0.046	0.127	0.195	0.181	0.304	0.058	0.107		0.140	0.146
D007	833825.66	822132.61		0.106	0,138	0.126	0.037	0.050	0.038	0,104	0.075	0.125	0.147		0.095	0.090
D008	833817.85	822138.87		0.164	0.167	0.066	0.036	0.164	0.208	0.163	0.355	0.054	0.068		0.129	0.145
D009	833832.24	822140.14		0.066	0.103	0.091	0.019	0.033	0.062	0.158	0.092	0.129	0.097		0.080	0.090
D010 D011	833824.43 833838.82	822146.39 822147.67		0.162	0.162	0.115	0.024	0.194	0.221	0.131	0.372	0.064	0.036		0.142	0.151
D011	833831.02	822153.92		0.127	0.137	0.105	0.008	0.201	0.228	0.159	0.342	0.097	0.016		0.133	0.152
D013	833845.40	822155.20		0.108	0.124	0.069	0.033	0.074	0.038	0.117	0.170	0.058	0.119		0.084	0.087
D014	833837.60	822161.45		0.094	0.068	0.048	0.055	0.200	0.252	0.139	0.306	0.019	0.049		0.103	0.132
D015 D016	833899.34 833891.53	822107.40 822113.66		0.114	0.064	0.052	0.111	0,060	0.188	0.184	0.201	0.047	0.076		0.095	0.115
D017	833883.73	822119.91		0.030	0.042	0.026	0.046	0.105	0.257	0.285	0.135	0.059	0.073		0.036	0.117
D018	833875.93	822126.16		0.056	0.042	0.015	0.040	0.094	0.239	0.256	0.086	0.075	0.098		0,069	0.107
D019	833868.12	822132,42		0.052	0.047	0.021	0.035	0.064	0,156	0,166	0.027	0,090	0,072		0.055	0.076
D020	833614.22 833625.42	822011.42 822023.08		0.117	0.076	0.135	0.173	0.111	0.114	0.073	0.051	0.038	0.020		0.109	0.083
D021	833625.42	822023.08		0.043	0.080	0.163	0.159	0.130	0.122	0.125	0.054	0.048	0.031		0.114	0.096
D023	833634.39	822032.59		0.071	0.110	0.197	0.180	0.205	0.203	0.227	0.067	0.048	0.061		0.150	0.134
D024	833643.45	822044,01		0.101	0.078	0.106	0.087	0.191	0.200	0,233	0.188	0.055	0.069		0.120	0.135
D025	833653.10	822055.85		0.118	0.081	0.078	0.082	0.225	0.239	0.277	0.185	0.046	0.080		0.120	0.143
D026	833638.45 833662.47	822059.59 822068.39		0.078	0.047	0.040	0.066	0.095	0.084	0.051	0.096	0.020	0.076		0.059	0.063
D028	833647.41	822072.72		0.128	0.031	0.039	0.089	0.058	0.076	0.130	0.133	0.025	0.072		0.068	0.077
D029	833632.58	822075.81		0.061	0.031	0.021	0.054	0.108	0.091	0.079	0.033	0.020	0.090		0.046	0.055
D030	833672.90	822082.91		0.166	0.108	0.064	0.061	0.215	0.214	0.260	0.214	0.018	0.026		0.119	0.128
D031	833658.24 833643.46	822085.88 822088.68		0.155	0.046	0.042	0.087	0.137	0.162	0.214	0.148	0.012	0.040		0.089	0.100
D033	833628.53	822090.95		0.070	0,026	0.026	0.093	0.003	0.073	0.085	0.053	0.026	0.075		0.052	0.060
D034	833818.77	822061.95		0.076	0.069	0.068	0.028	0.206	0.190	0.181	0.210	0.215	0.123		0.110	0.161
D035	833809.59	822067.11		0.154	0.100	0.067	0.020	0.184	0.182	0.176	0.225	0.178	0.104		0,116	0.150
D036 D037	833799.96 833770.99	822072.88 822080.33		0,107	0.095	0.080	0.014	0.135	0.150	0,149	0.210	0.085	0.097		0.098	0.117
D037	833765.27	822090.10		0.030	0.112	0.076	0.046	0.030	0.071	0,103	0.161	0.123	0.114		0.079	0.101
D039	833751.16	822091.77		0.038	0.071	0.084	0.052	0.125	0.067	0.104	0.139	0.093	0.131		0.082	0.100
D040	833736.50	822092.92		0.043	0.035	0.079	0.045	0.171	0.094	0.122	0.139	0.070	0.115		0.079	0.102
D041	833721.74	822093.94		0.063	0.032	0.063	0.038	0.149	0.135	0.166	0.159	0.051	0.084		0.078	0.103
D042 D043	833705,95 833688,13	822094.71 822096.51		0.126	0.074	0.054	0.029	0,080	0,076	0,099	0.180	0.041	0.051	-	0.074	0.080
D043	833688.13 833673.32	822098.89		0.1//	0.090	0.040	0.041	0.177	0.174	0.205	0.183	0.037	0.073		0.119	0.118
D045	833658.51	822101.28		0.151	0.057	0.035	0.075	0.138	0.161	0.212	0.072	0.079	0.066		0,086	0,100
D046	833643.70	822103.66	1	0.133	0.042	0.035	0.098	0.119	0.142	0,126	0.036	0,096	0.092		0.077	0.089
D047	833628.89	822106.04		0.118	0.046	0.036	0.114	0.128	0.142	0.044	0.053	0.115	0.087		0.078	0.089
D048	833614.39	822102.19	Li.	0.094	0.048	0.040	0.105	0.135	0.138	0.079	0.060	0.055	0.062	_	0.074	0,079

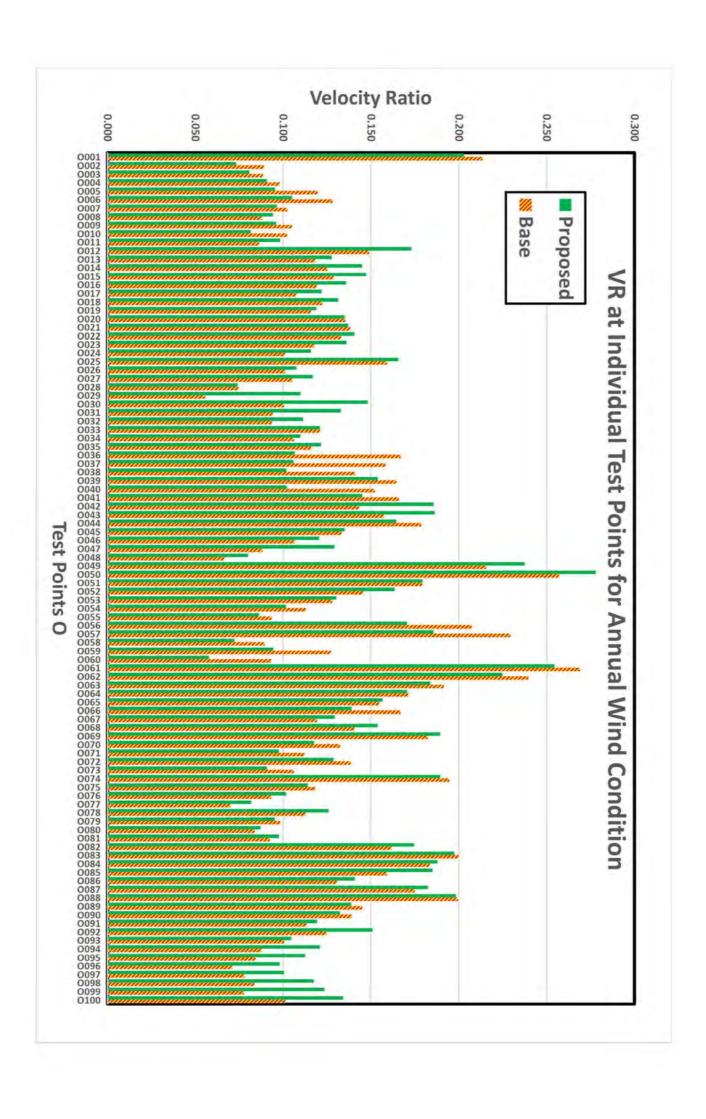
	Tes Point		Wind direction (Degree)	45	67.5	90	112.5	135	157.5	180	202.5	225	247.5	*****		
	res Point		Wind direction	NE	ENE	E	ESE	SE	SSE	5	SSW	SW	WsW	Sum	Average	Average
in		No Selection	Probability (Annual)	7.6%	12.4%	21.8%	12.4%	6,5%	4.9%	4.5%	6.7%	5.8%		83.6%	(Annual)	(Summer)
ID	Easting (m)	Northing (m)	Probability (Summer)	III 200		8.3%	9.7%	7.6%	8.2%	9.2%	14.2%	16.9%	7.6%	81.7%	100	15000
D049	833599.89	822098.34	4	0.069	0.029	0.028	0.067	0.108	0.098	0.070	0.094	0.057	0.065		0.058	0.073
D050	833585.40	822094.49		0.054	0:019	0.045	0.042	0.061	0.061	0.043	0.101	0.051	0.063		0.048	0.060
D051	833776.49	822095.36		0.021	0.122	0.080	0.034	0.011	0.058	0.046	0.050	0.141	0.187		0.068	0.079
D052	833761.81	822098.45		0.030	0.087	0.093	0.056	0.060	0.068	0.088	0.101	0.138	0.212		0.081	0.104
D053	833747.13	822101.53		0.044	0.042	0.098	0.066	0.127	0,075	0,109	0.113	0.125	0.206		0.085	0.114
D054	833732.45	822104.61	T.	0.078	0.020	0.091	0.064	0.148	0.102	0.131	0.125	0.122	0.197		0.088	0.121
D055	833717.77	822107.70		0.128	0.055	0.077	0.060	0.104	0.114	0.145	0.126	0.132	0.190		0.092	0.119
D056	633703.09	822110.78		0.156	0.107	0.080	0.054	0.106	0.099	0.133	0.102	0.162	0.197		0.101	0.119
D057	833688,41	822113.86	9	0,152	0,105	0.075	0.042	0.146	0,134	0.181	0.092	0.203	0.210		0,108	0.137
D058	833673.73	822116.95	1	0.148	0.082	0.042	0.034	0.149	0.152	0.209	0.105	0.252	0.247		0.102	0.154
D059	833659.05	822120.03		0,145	0.062	0.027	0.042	0.138	0.155	0.212	0.148	0.306	0.298		0.104	0.177
D060	833644.37	822123.11	, i	0.145	0.052	0.027	0.060	0.129	0.152	0.189	0.221	0.354	0.344		0.112	0.202
D061	833663.64	822132.67		0.133	0.062	0.062	0.040	0.130	0,136	0.197	0.241	0,389	0,386		0.123	0.217
D062	833825.69	822190.69		0,102	0.087	0,100	0.115	0,121	0,040	0,113	0.068	0.112	0.068		0.098	0.093
D063	833832.10	822198.36		0.041	0.090	0.091	0.111	0.122	0.061	0.147	0.120	0.125	0.057		0.098	0.108
D064	833838.51	822206.04		0.024	0.098	0.081	0.099	0.142	0.087	0.163	0.152	0.123	0.065		0.100	0.118
D065	833844.92	822213.71		0.104	0.109	0.075	0.087	0.154	0.123	0.164	0.186	0.094	0.042		0.109	0.119
D066	833851.33	822221.39	A .	0.145	0.107	0.061	0.060	0.151	0.134	0.156	0.212	0.050	0.078		0.103	0.113
D067	833817.23	822197.22		0.098	0.071	0.071	0.103	0.122	0.134	0.086	0.115	0.120	0.066		0.094	0.105
D068	833823.77	822204.78		0.015	0.068	0.069	0.100	0.034	0.115	0.051	0.019	0.113	0.054	-	0.067	0.071
D069	833830.31	822212.35		0.032	0.060	0.036	0.061	0.093	0.038	0.057	0.029	0.059	0.034		0.050	0.050
D070	833836.85	822219.91		0.046	0.089	0.064	0.083	0.145	0.079	0.131	0.046	0.045	0.028		0.077	0.072
D071	833843.39	822227.48		0,150	0.109	0.095	0,104	0,160	0,131	0.183	0.097	0,057	0.067		0.112	0.106
D072	833835.66	822233.82		0.138	0.086	0.137	0.137	0.121	0.150	0.182	0.029	0.074	0.063		0.118	0.103
D073	833827.93	822240.17		0.120	0.051	0.140	0.147	0.077	0.142	0.132	0.049	0.074	0.061	-	0.108	0.097
D074	833820.21	822246.51		0.102	0.032	0.124	0.134	0.047	0.121	0.101	0.060	0.069	0.057		0.093	0.086
D075	833812.48	822252.86	1	0.077	0,037	0,109	0.120	0.028	0,101	0,065	0.044	0.067	0.057		0.079	0.072
D076	833805.65	822257.88		0.047	0.057	0.095	0.103	0.020	0.085	0.038	0.025	0.076	0.075		0.069	0.063
D077	833772.09	822234.97		0.111	0.076	0.114	0.131	0.073	0.045	0.049	0.084	0.079	0.109		0.095	0.085
D078	833778.67	822242.50		0.114	0.089	0.036	0.037	0.019	0.017	0.029	0.025	0.039	0.034		0.048	0.030
D079	833785.26	822250.02		0.122	0.098	0.057	0.033	0.013	0.022	0.042	0.027	0.098	0.077		0.060	0.050
D080	833791.84	822257.55		0.090	0.087	0.021	0,038	0.024	0.015	0,044	0.026	0.101	0.088		0.048	0.049
D081	833798.42	822265.08		0.079	0.066	0.091	0.083	0.033	0.078	0.055	0.050	0.096	0.079		0.075	0.072

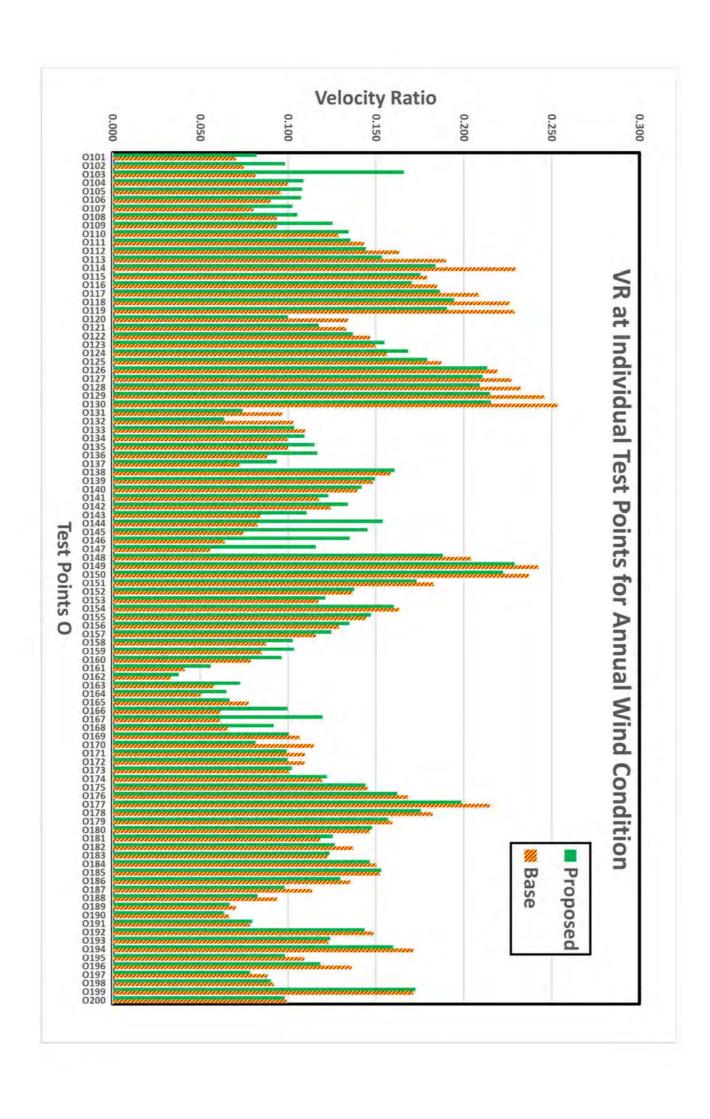
Summary of Spatial Averaged Velocity Ratio

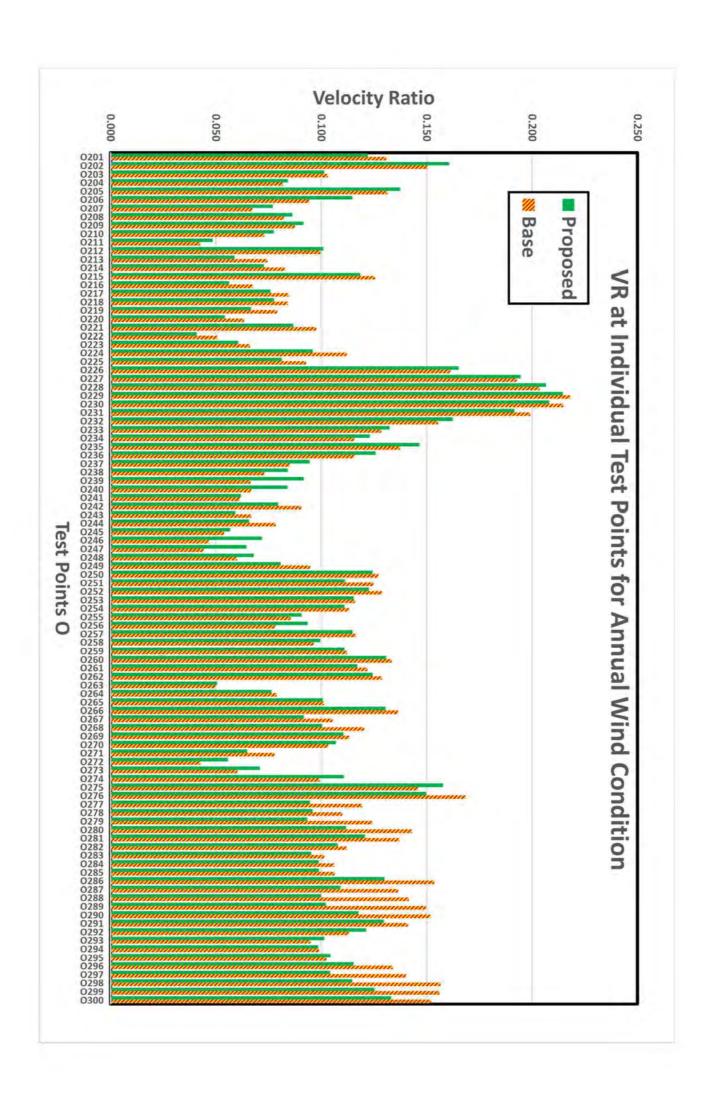
ID	Location	В	Base		Proposed	
	Overall	Annual	Summer	Annual	Summer	
SVR	Site Air Ventilation Assessment (SVR) (All P Points)	0.098	0.121	0.115	0.143	
	Site A (P001 - P030)	0.076	0.105	0.103	0.140	
	Site B (P031 - P104)	0.115	0.141	0.125	0.161	
	SSP-017 (P105 - P144)	0.082	0.095	0.108	0.111	
LVR	Local Air Ventilation Assessment (LVR) (All P & O Points)	0.112	0.130	0.117	0.137	
	Road Sections	Annual	Summer	Annual	Summer	
R001	Hing Wah Street (0001 - 0012)	0.114	0.143	0.107	0.142	
R002	Hing Wah Street (0013 - 0027)	0.122	0.127	0.132	0.149	
R003	Cheung Wah Street (O028 - O035)	0.095	0.112	0.116	0.143	
R004	Cheung Sha Wan Path (O036 - O044)	0.159	0.157	0.139	0.140	
R005	Kwong Cheung Street (0045 - 0048)	0.099	0.123	0.116	0.159	
R006	Tai Nan West Street (O049 - O060)	0.156	0.185	0.146	0.175	
R007	Lai Chi Kok Road (O061 - O069)	0.182	0.169	0.178	0.165	
R008	Fortune Street (O070 - O073)	0.122	0.145	0.109	0.143	
R009	Hang Cheung Street (0074 - 0079)	0.115	0.132	0.118	0.132	
R010	Cheung Sha Wan Road (O080 - O091)	0.148	0.183	0.153	0.191	
R011	Cheung Sha Wan Road (O092 - O108)	0.088	0.160	0.114	0.181	
R012	Cheung Sha Wan Road (O109 - O130)	0.184	0.271	0.169	0.270	
R013	Fuk Wa Street (0131 - 0137)	0.096	0.098	0.096	0.090	
R014	Fuk Wing Street (O138 - O142)	0.137	0.129	0.142	0.133	
R015	Fuk Wing Street (O143 - O147)	0.072	0.078	0.132	0.141	
R016	Un Chau Street (O148 - O160)	0.148	0.114	0.149	0.121	
R017	Castle Peak Road (O161 - O182)	0.108	0.124	0.111	0.124	
R018	Cheung Yue Street (O183 - O191)	0.109	0.109	0.105	0.109	
R019	Un Chau Street (O192 - O196)	0.138	0.108	0.129	0.090	
R020	Cheung Fat Street (O197 - O199)	0.117	0.097	0.114	0.090	
R021	Hing Wah Street (O200 - O205)	0.116	0.112	0.117	0.116	
R022	Cheung Wah Street (O206 - O208)	0.081	0.075	0.093	0.101	
R023	Tsap Fai Street (O209 - O211)	0.068	0.057	0.072	0.067	
R024	Fuk Wa Street (O212 - O214)	0.086	0.079	0.078	0.073	
R025	Yu Chau West Street (O215 - O220)	0.084	0.076	0.075	0.069	
R026	Tai Nan West Street (O221 - O226)	0.097	0.116	0.088	0.115	
R027	Castle Peak Road (O227 - O239)	0.147	0.114	0.152	0.122	
R028	Kwong Shing Street (O240 - O241)	0.064	0.065	0.073	0.058	
R029	Wing Hong Street (O242 - O262)	0.096	0.106	0.096	0.115	
R030	Wing Ming Street (0263 - 0270)	0.101	0.091	0.096	0.084	
R031	King Lam Street (0271 - 0275)	0.085	0.125	0.092	0.141	
INDEX	Open Area	Annual	Summer	Annual	Summer	
Z001	Sham Shui Po Sports Ground (O276 - O328)	0.127	0.153	0.115	0.145	
Z002	Hang Chun Court (0329 - 0337)	0.096	0.141	0.094	0.138	
Z003	S.K.H. Kei Fook Primary School – Middle (O338 - O343)	0.119	0.076	0.119	0.077	
Z004	S.K.H. Kei Fook Primary School – West (O344 - O353)	0.100	0.116	0.092	0.110	
Z005	Un Chau Estate (O354 - O355)	0.089	0.072	0.032	0.072	
Z006	Hing Wah Street Playground (O356 - O370)	0.072	0.072	0.033	0.072	
Z007	Cheung Sha Wan Catholic Secondary School (O371 - O376)	0.048	0.055	0.052	0.062	
Z008	Wing Hong Street Rest Garden (O377 - O384)	0.087	0.077	0.032	0.002	
2000	Open Area - Within Scheme Boundary	Annual	Summer	Annual	Summer	
A001	Site A – Setback Areas in West (D001 - D014)	0.072	0.103	0.104	0.123	
A002	Site A – North-East Area (D015 - D019)	0.051	0.049	0.076	0.123	
A003	Site B – Open Area (D020 - D061)	0.109	0.049	0.090	0.107	
A003	SSP-017 - Setback Area in West (D062 - D076)	0.109	0.113	0.090	0.110	
A004	SSP-017 - Setback Area in West (D002 - D076) SSP-017 - SW/NE pedestrian pathway (D077 - D081)		-55	0.032	0.092	

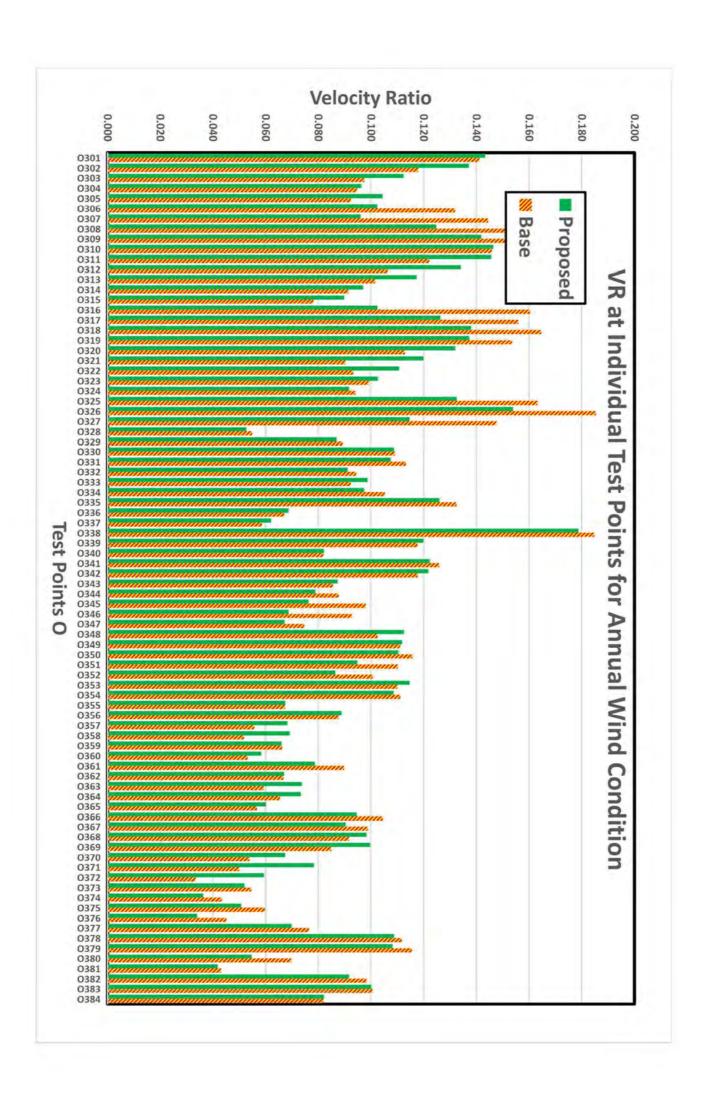


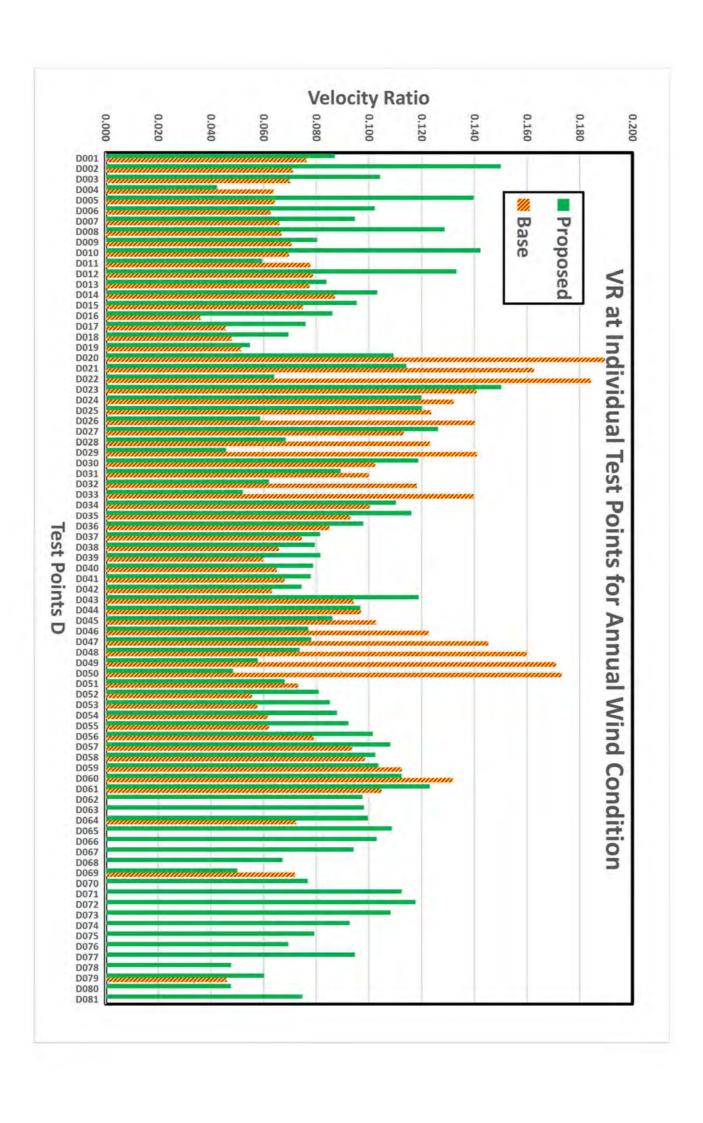


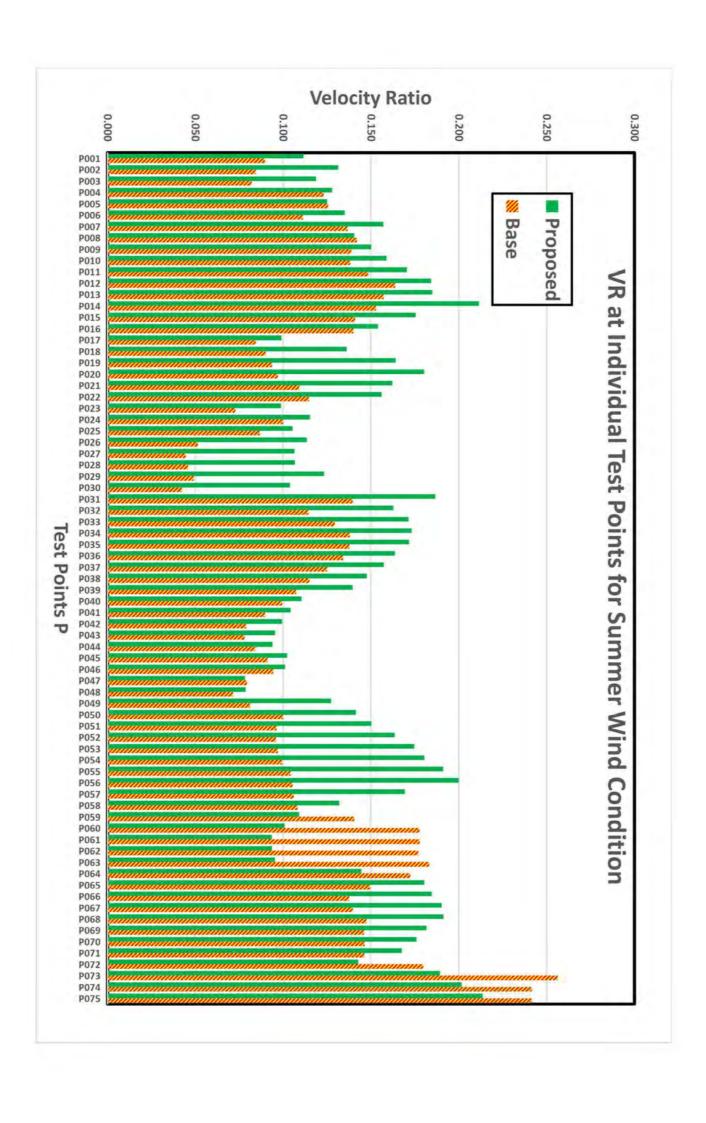


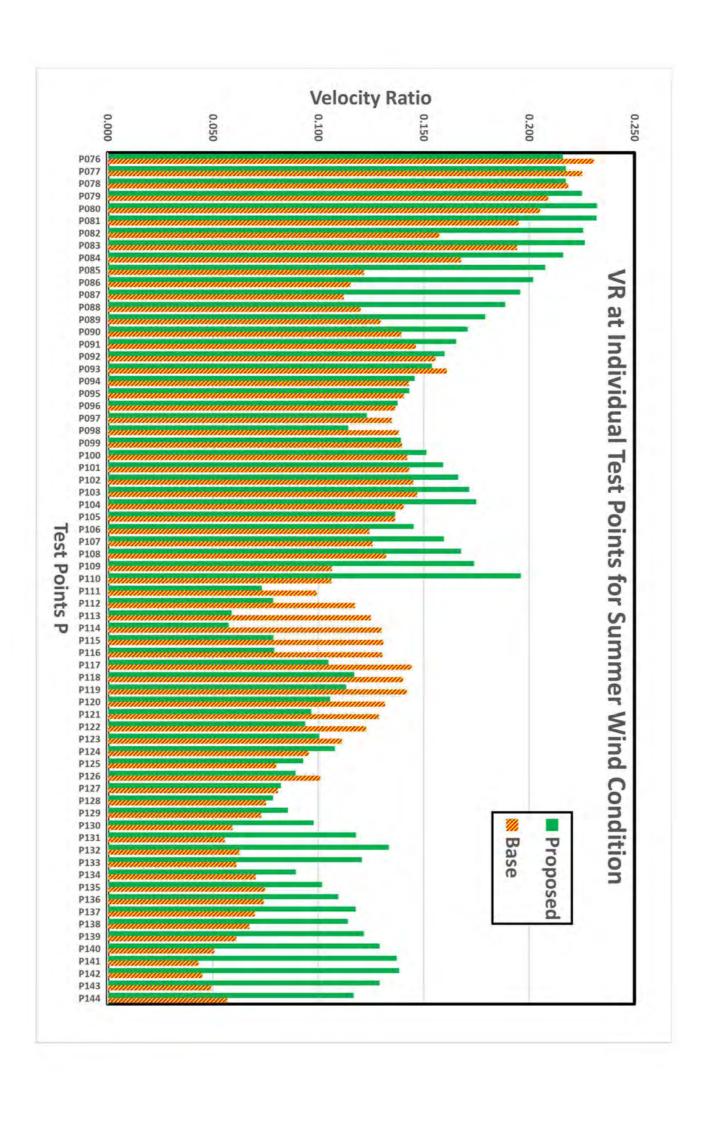


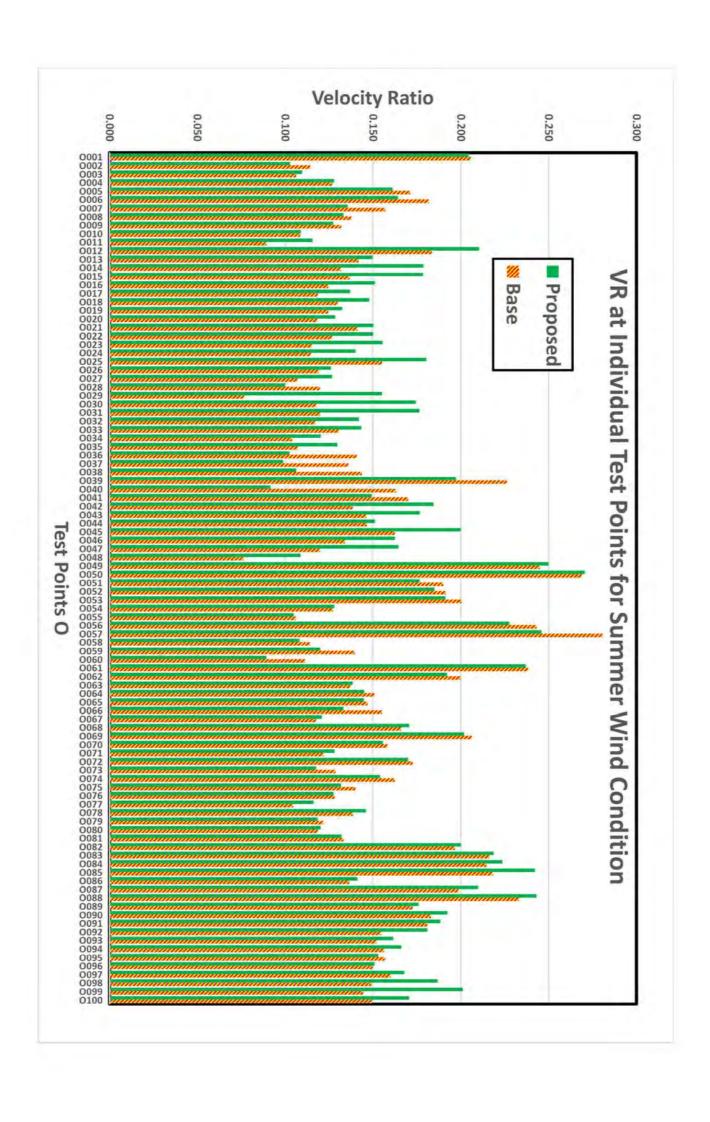


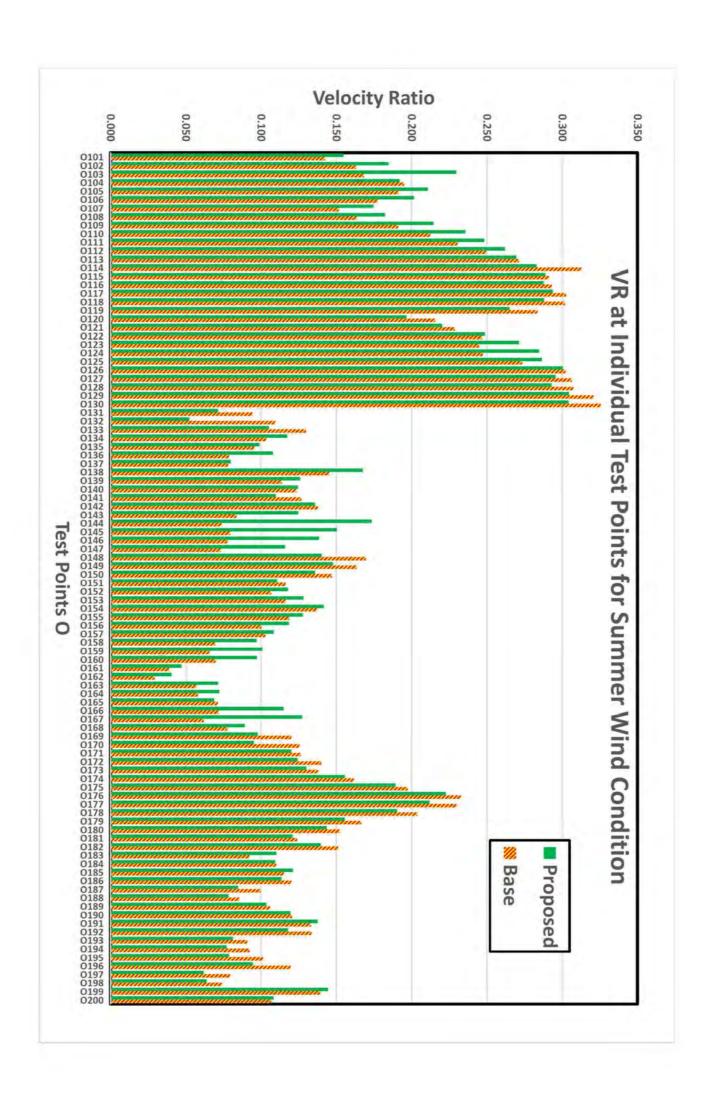


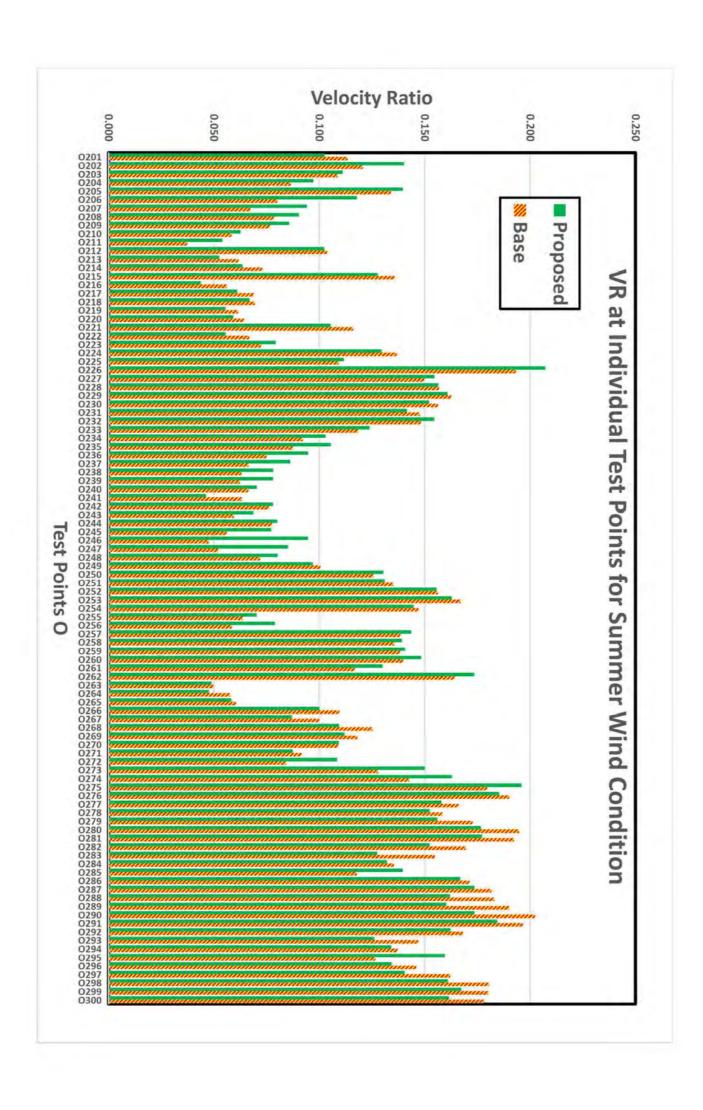


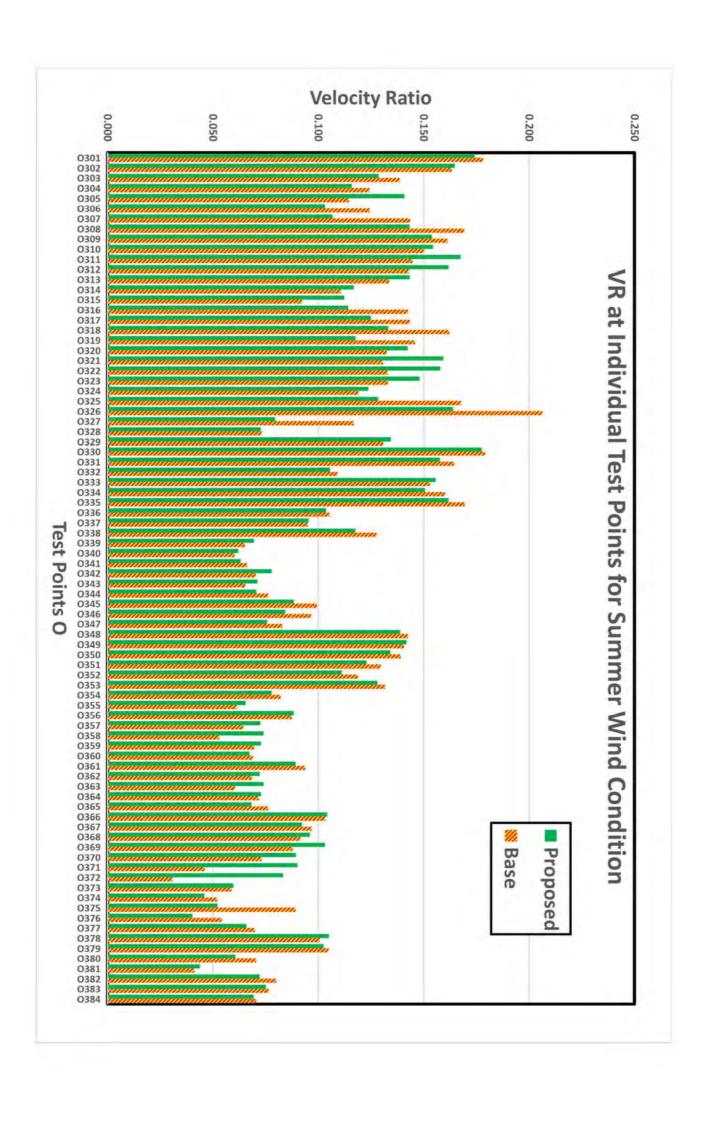


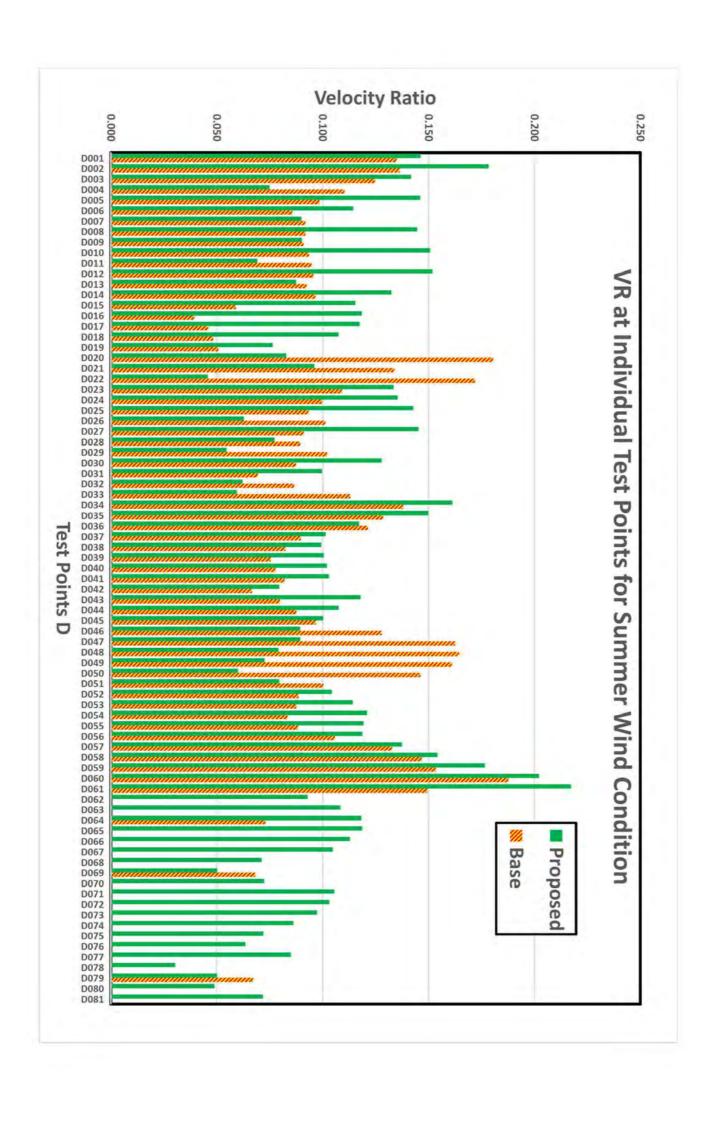




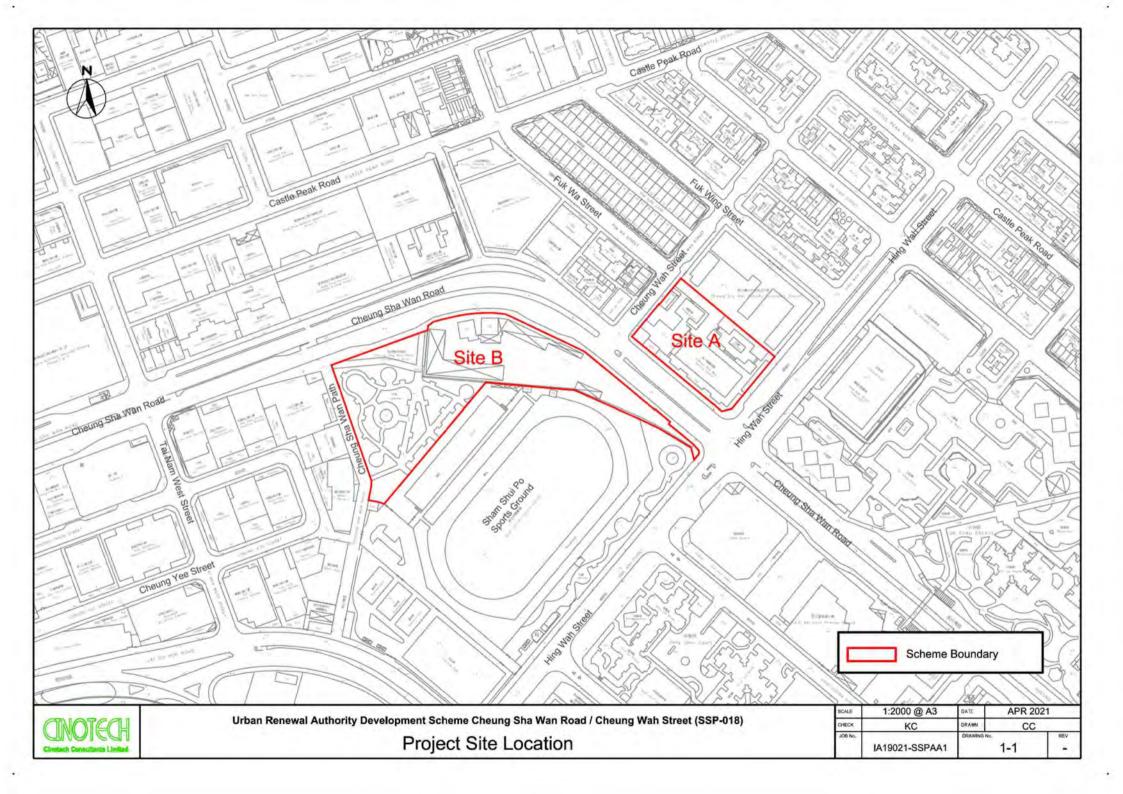


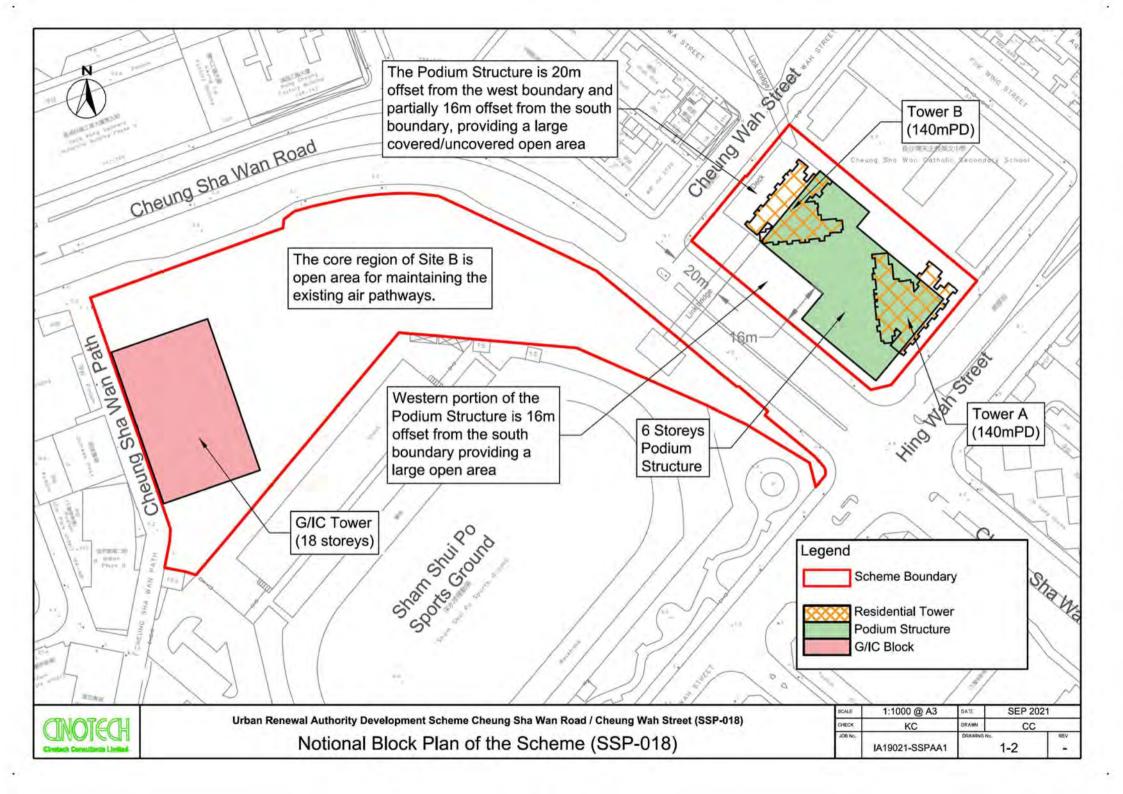


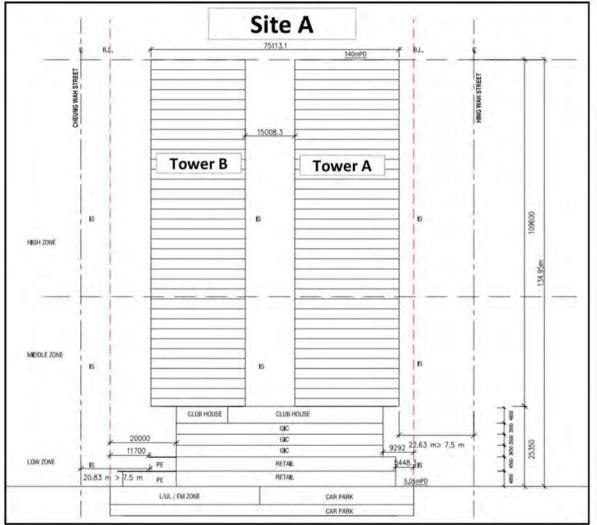


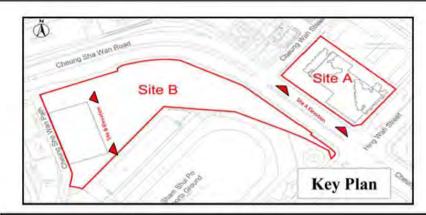


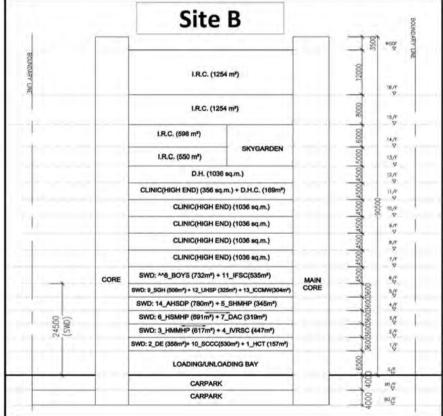












Remark:

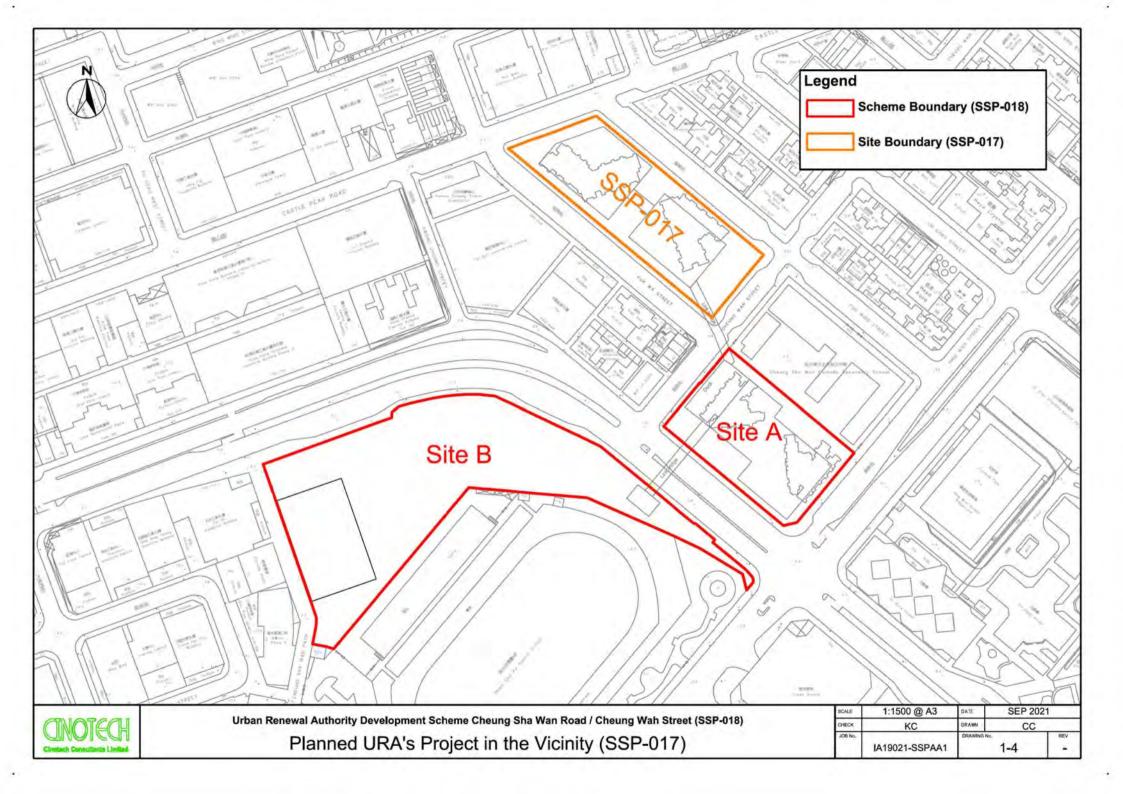
Notional Design subject to change at detailed design stage

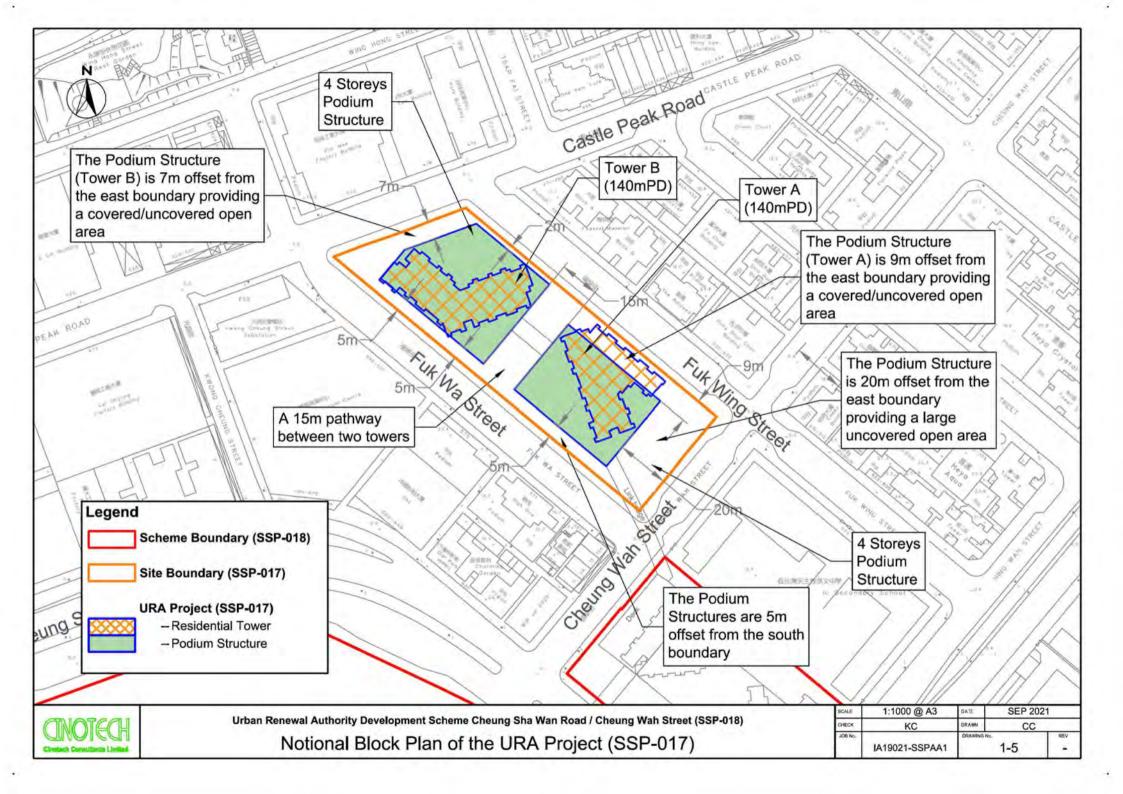


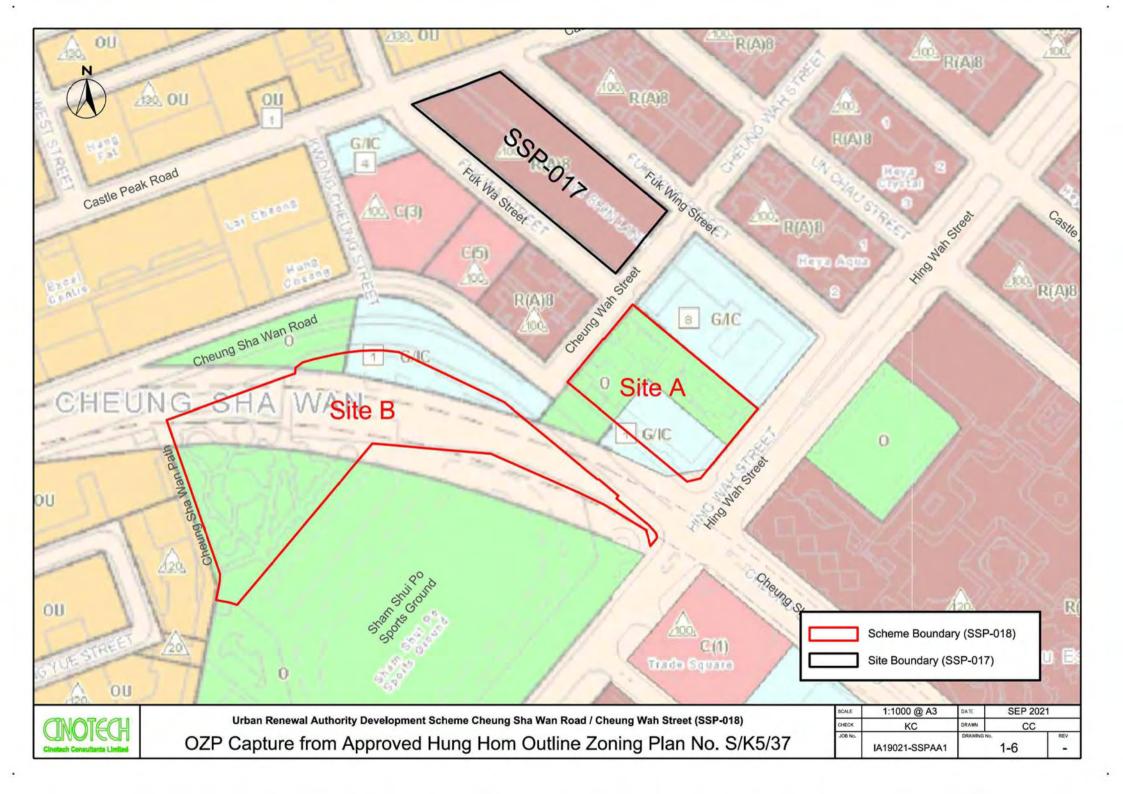
Urban Renewal Authority Development Scheme Cheung Sha Wan Road / Cheung Wah Street (SSP-018)

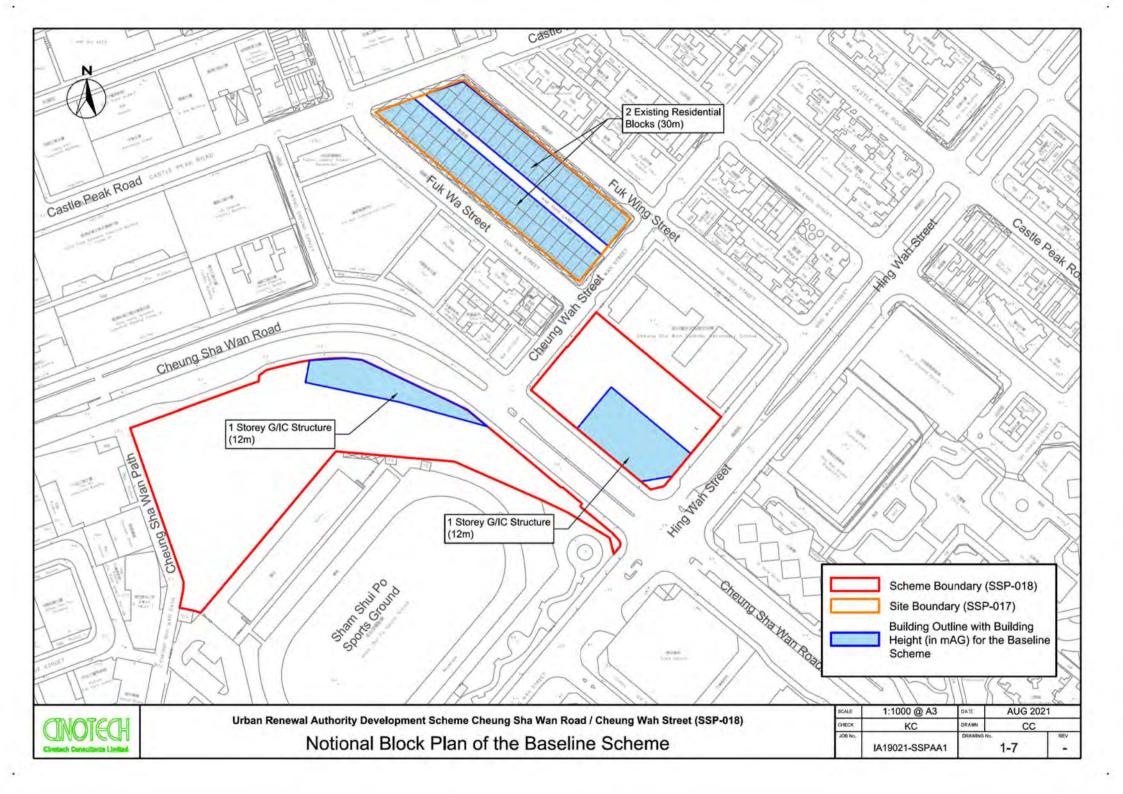
Notional Section Plan of the Scheme

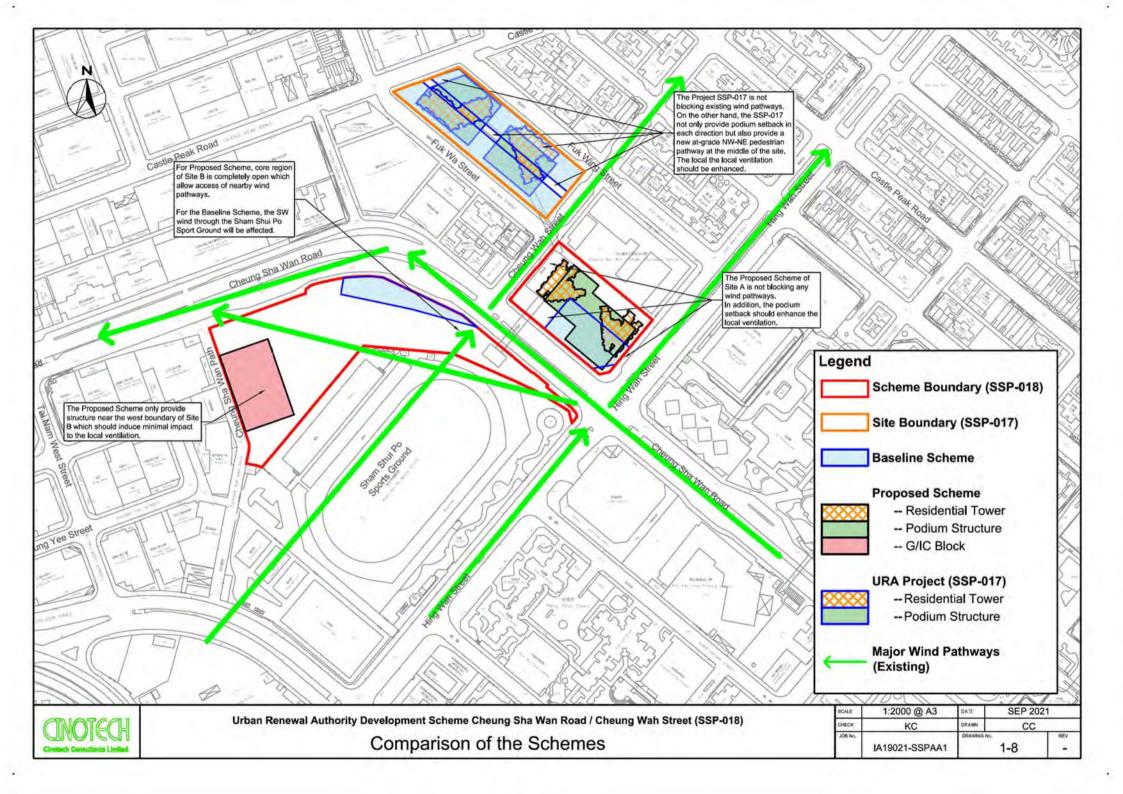
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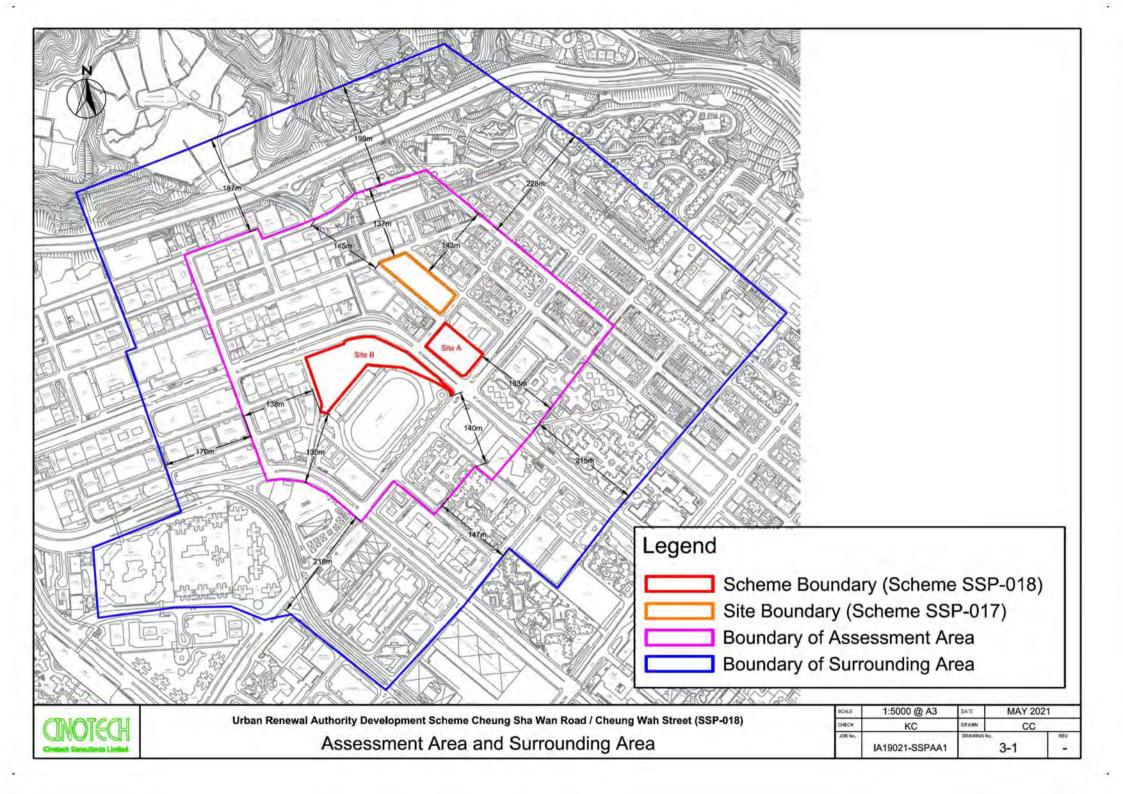


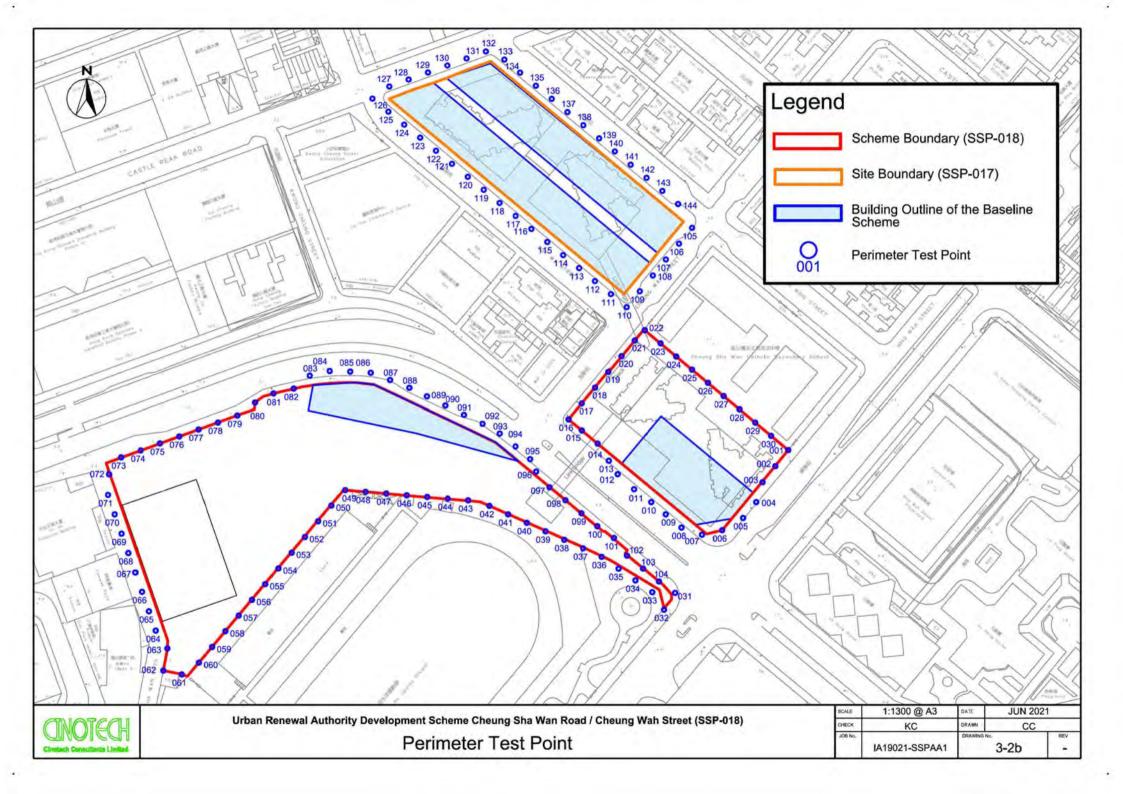


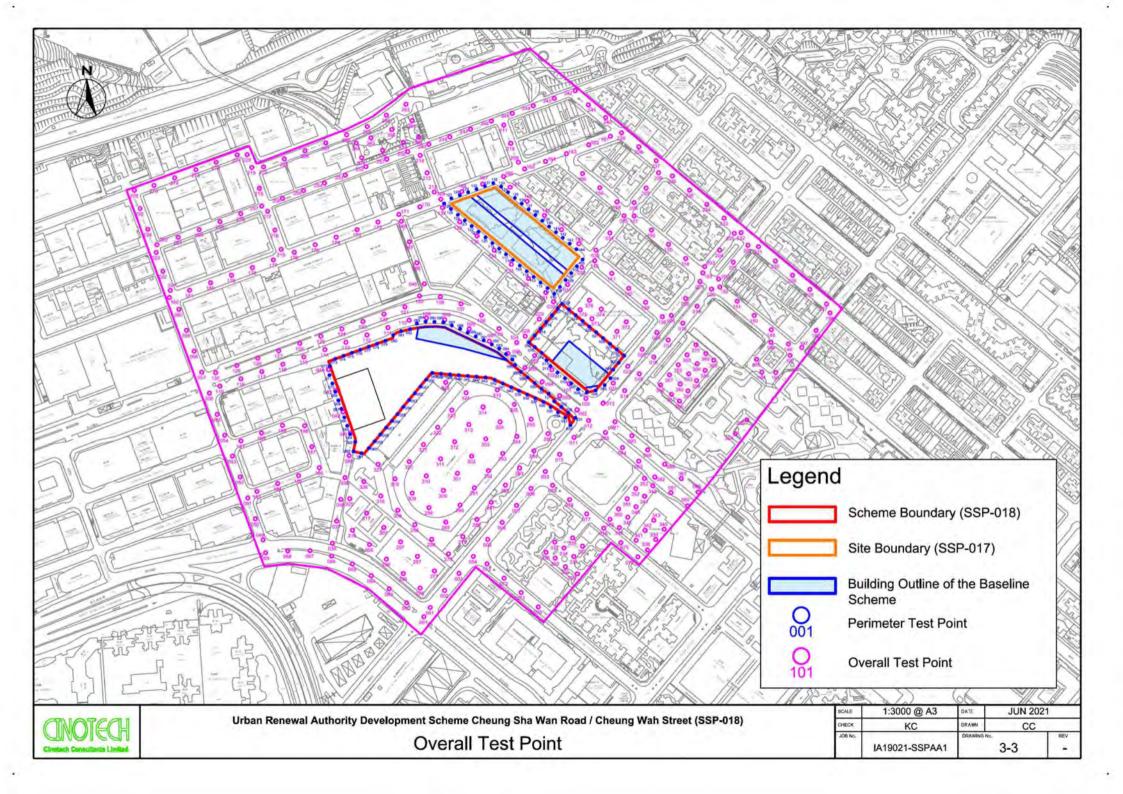


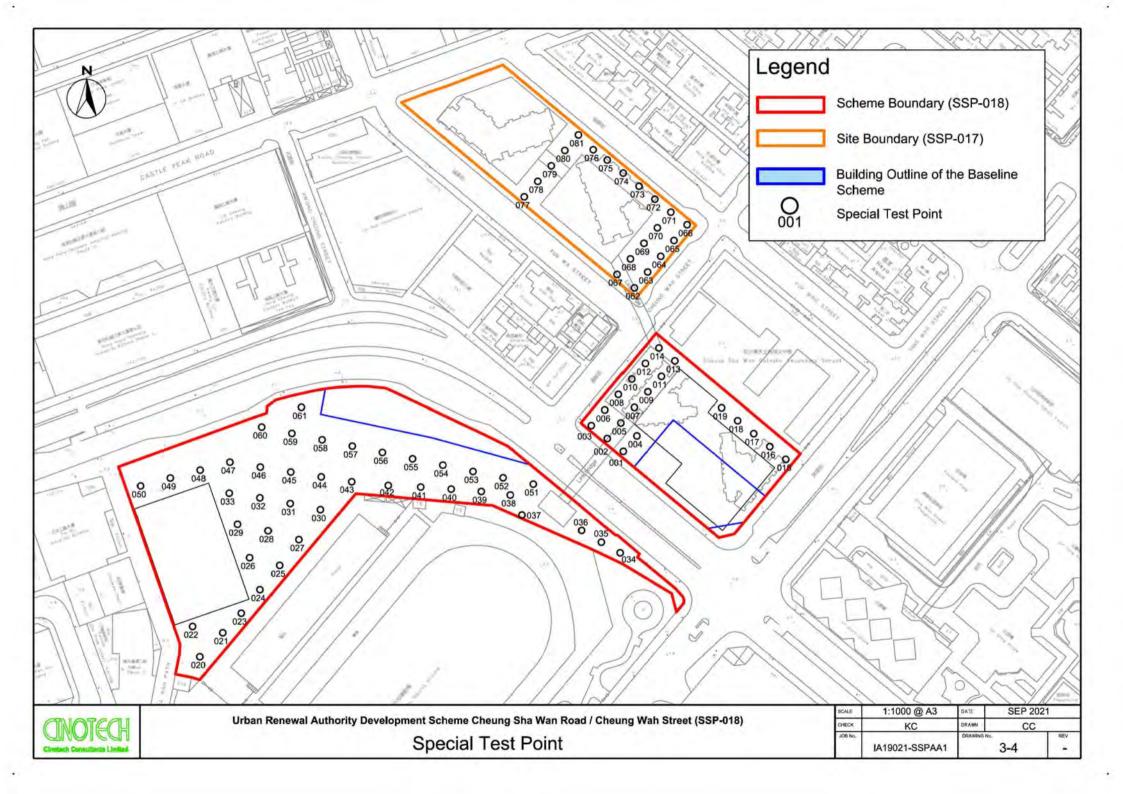


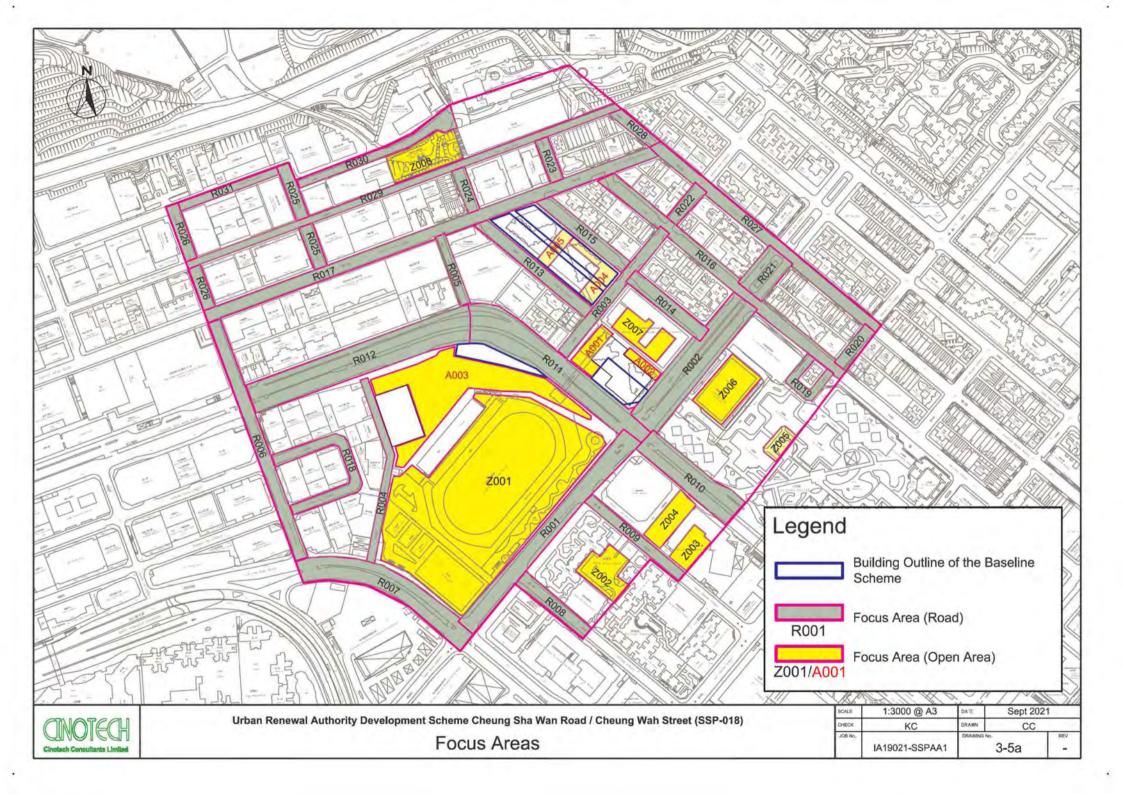


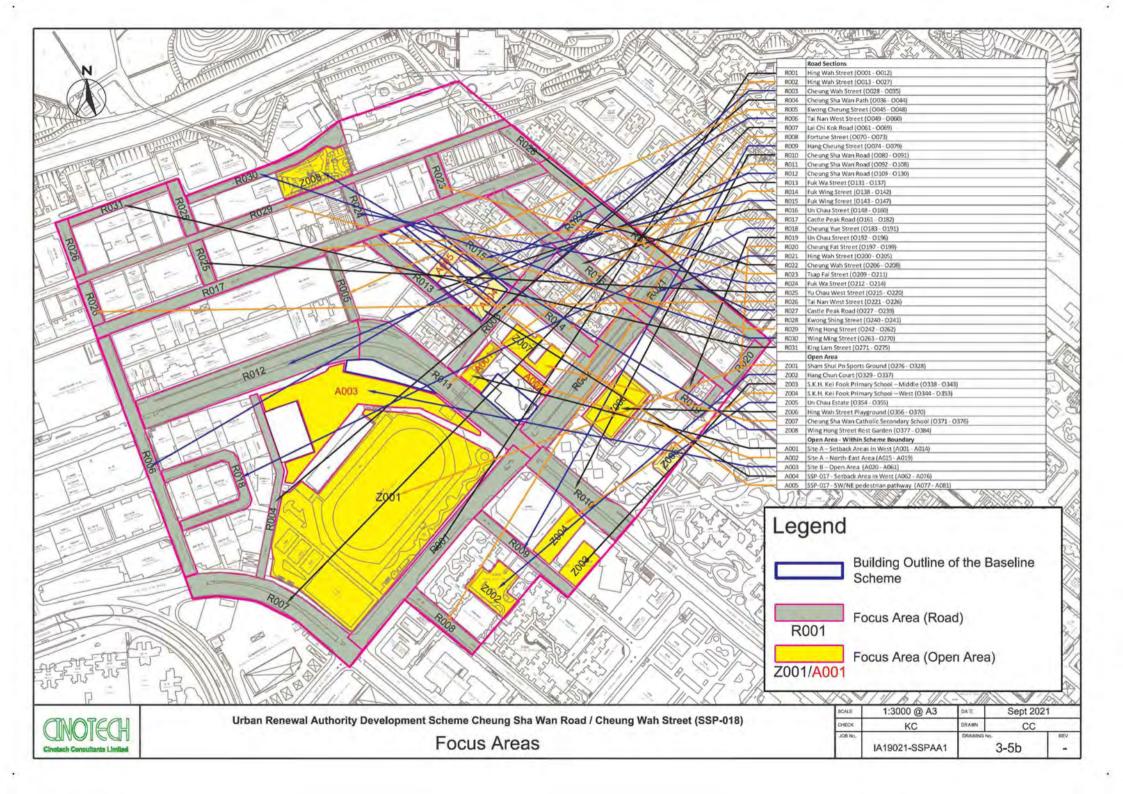


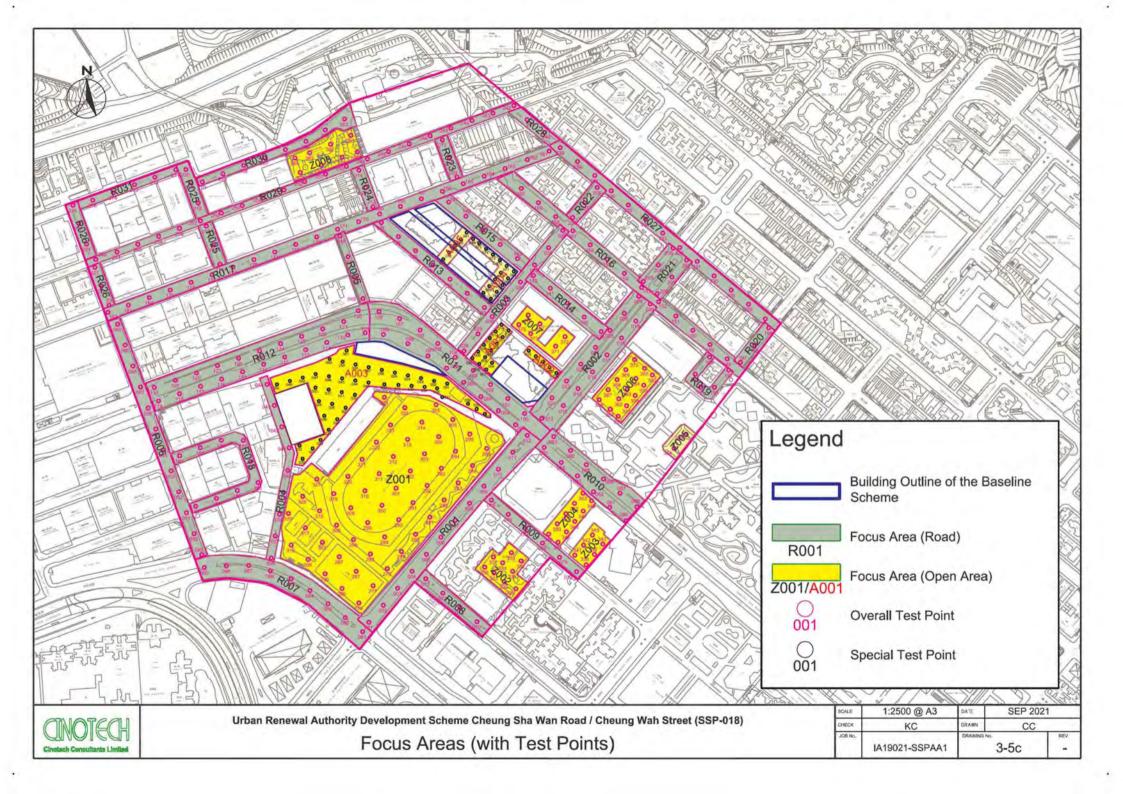


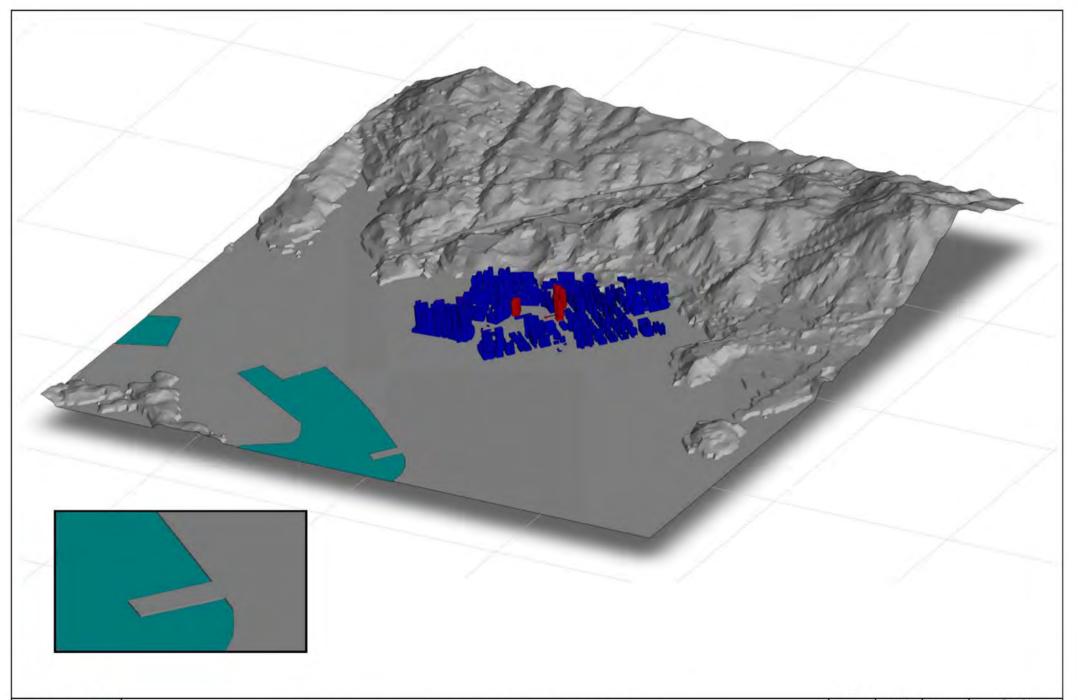




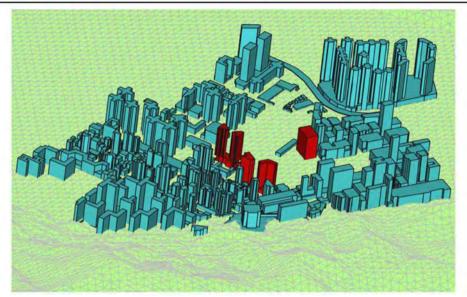


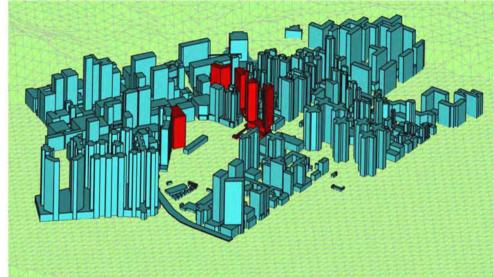






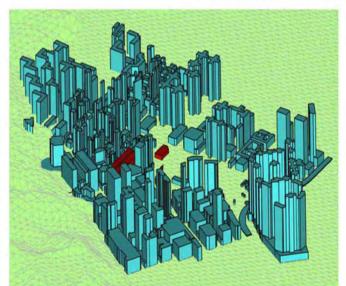




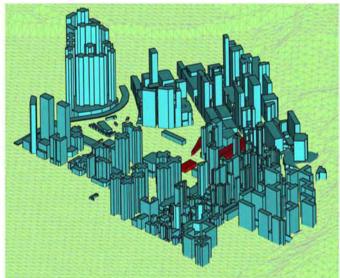


View from North

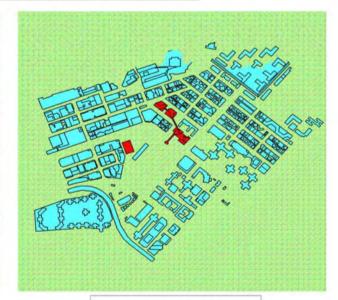
View from South







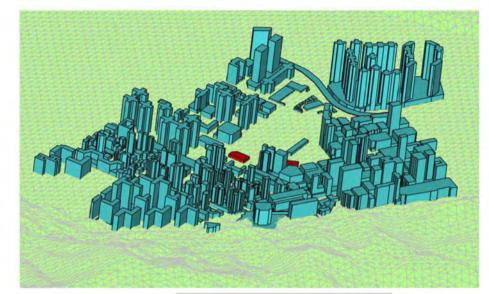
View from East



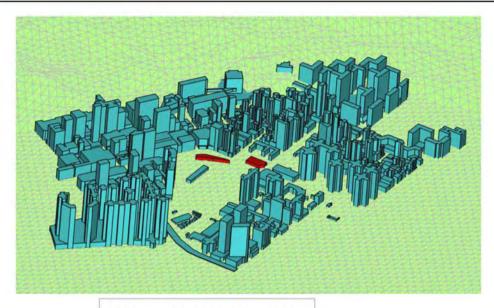
Top View



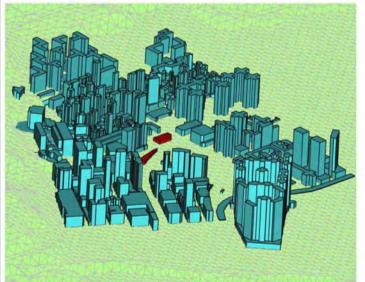
JOB NO.	IA9021/KC-AA1-01	FIGURE NO.	3-6b	REV.
CHECK	KC	DRAWN		CC
SCALE	N.T.S.	DATE	Sep-21	



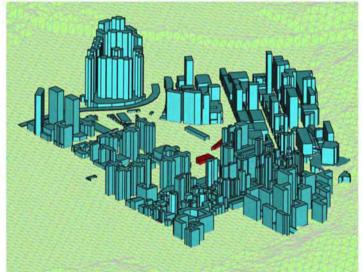
View from North



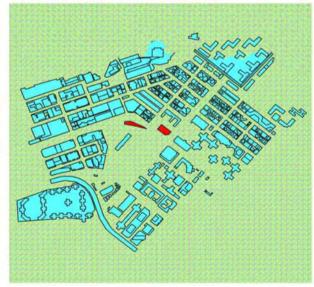
View from South



View from West



View from East



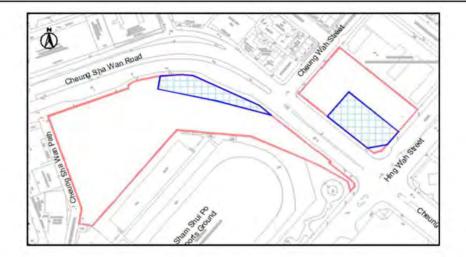
Top View

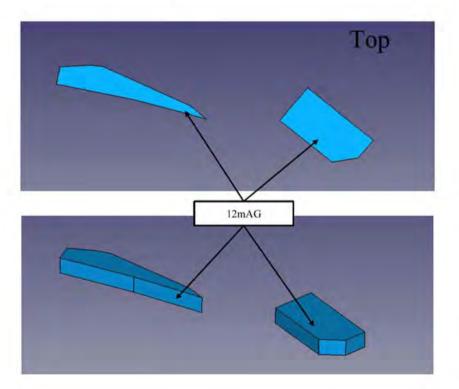


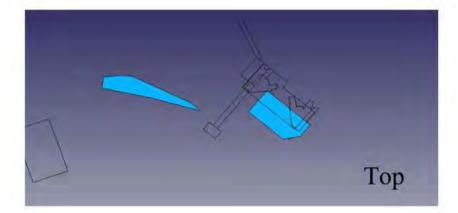
Urban Renewal Authority Development Scheme Cheung Sha Wan Road / Cheung Wah Street (SSP-018)

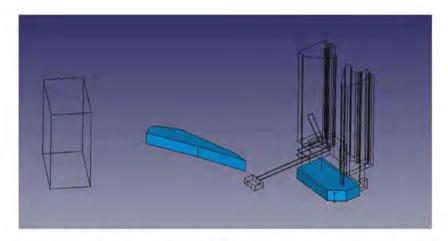
Buildings Included in the CFD Models - Proposed Model

SCALE	N.T.S.	DATE		Sep-21
CHECK	KC	DRAWN		CC
JOB NO.	IA9021/KC-AA1-01	FIGURE NO.	3-6c	REV.





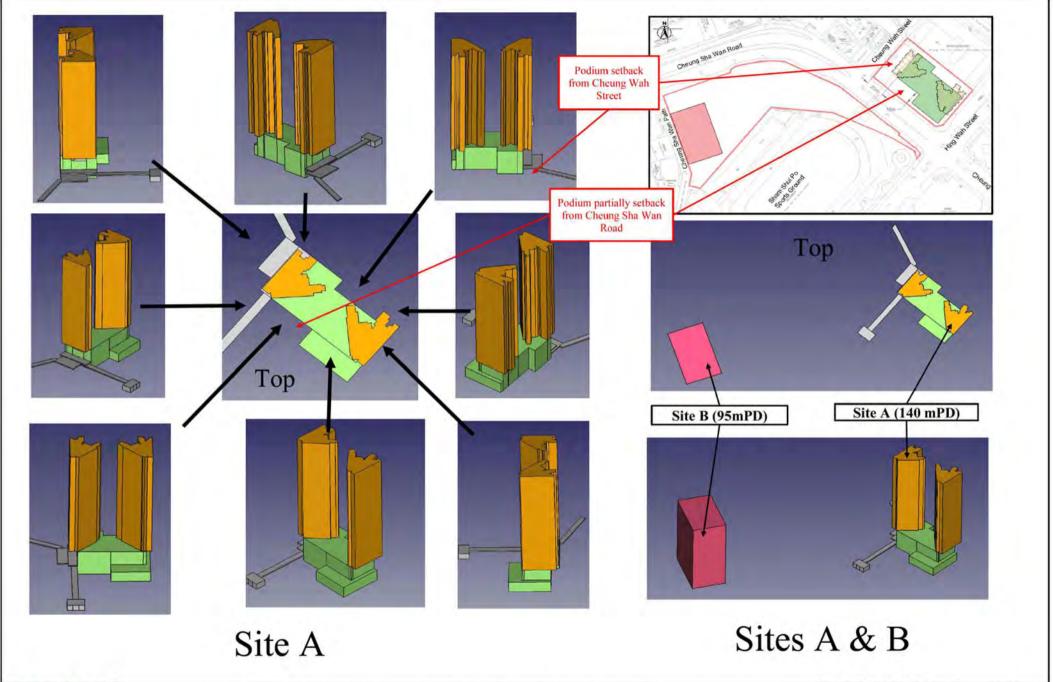




With the Outline of the Propsoed Buildings



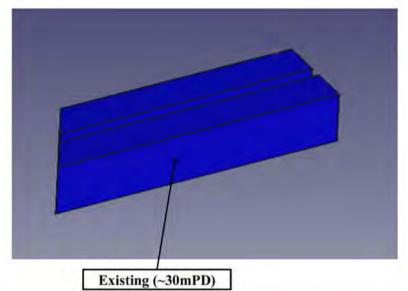
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CHECK	KC	DRAWN		CC
SCALE	N.T.S.	DATE	Jul-21	

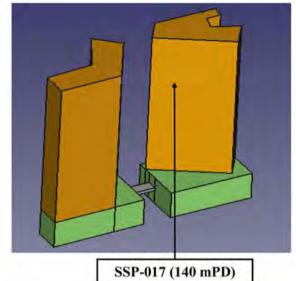


CINOTECH Second Consultants limited

SCALE	N.T.S.	DATE	Jul-21		
CHECK	KC	DRAWN		CC	
JOB NO.	IA9021/SSPAA1	FIGURE NO.	3-7b	REV.	
				7	

Baseline Model

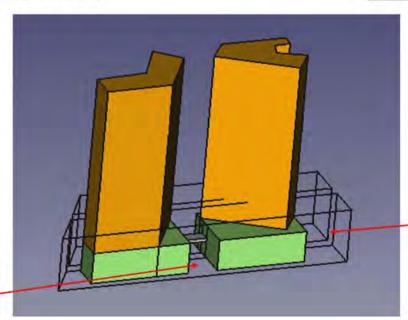




Proposed Model

Comparison

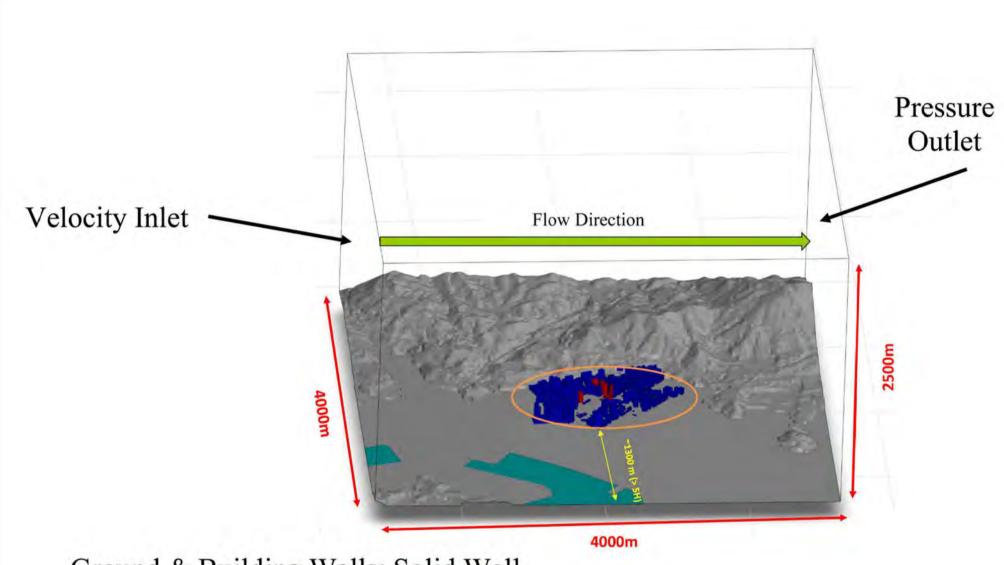
New 15m SW-NE pedestrian pathway



20m Building Setback



SCALE	N.T.S.	DATE	Sep-21	
CHECK	KC	DRAWN	CC	
JOB NO.	IA9021/SSPAA1	FIGURE NO.	3-7c	REV.
30B 140.	MANUFACTION PACE	FIGURE NO.	3-70	IXEV.



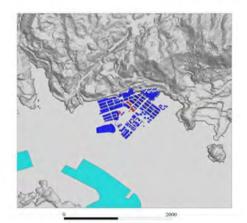
Ground & Building Walls: Solid Wall

* Setting for 270 deg Wind is adopted in this example # Height of Highest building within Assessment Area, h = 135 m; h = 5 x 135 = 675 m ## Height of Highest building in Computation Domin, H = 180 m; H = 5 x 180 = 900 m

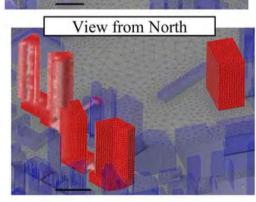


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CHECK	KC	DRAWN	CC	
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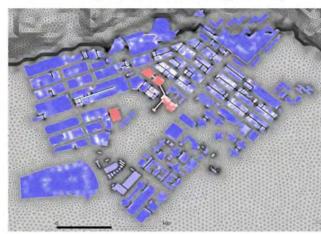
Top (Full View)

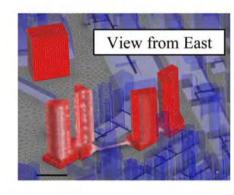


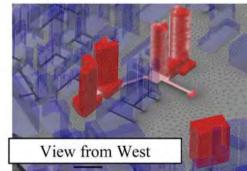
View from South



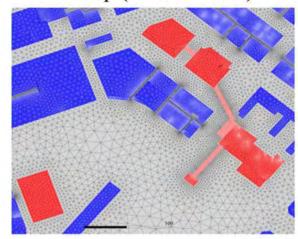
Top (Surrounding Aera)

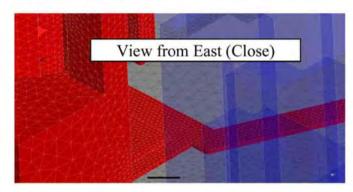


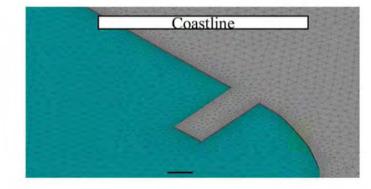




Top (Scheme Aera)



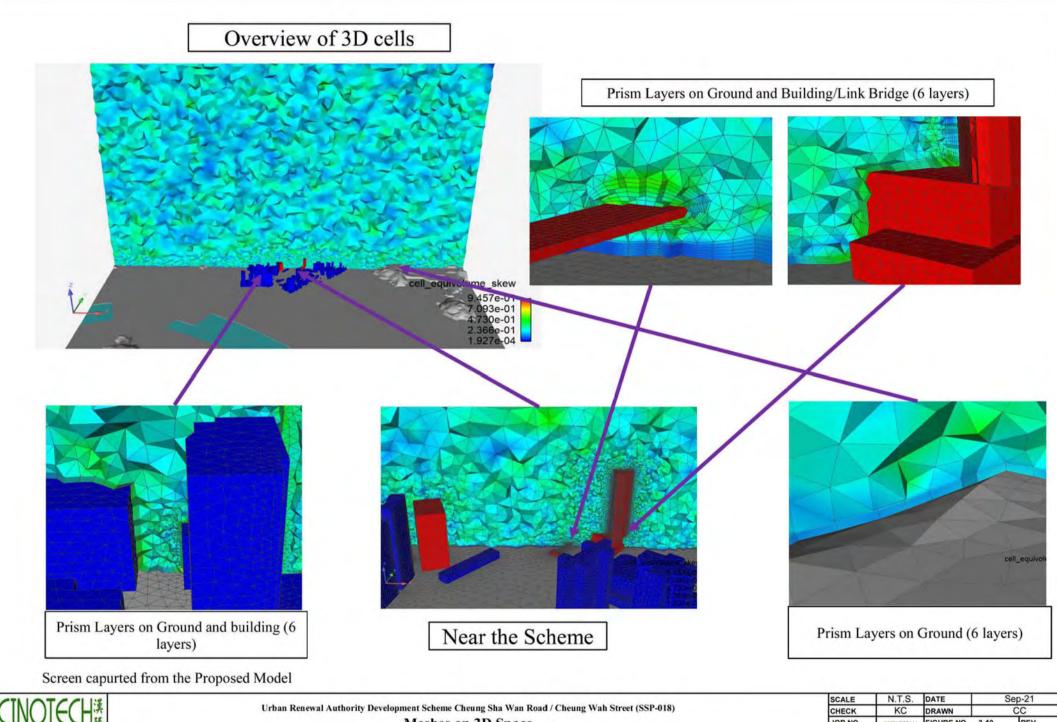




Screen capurted from the Proposed Model

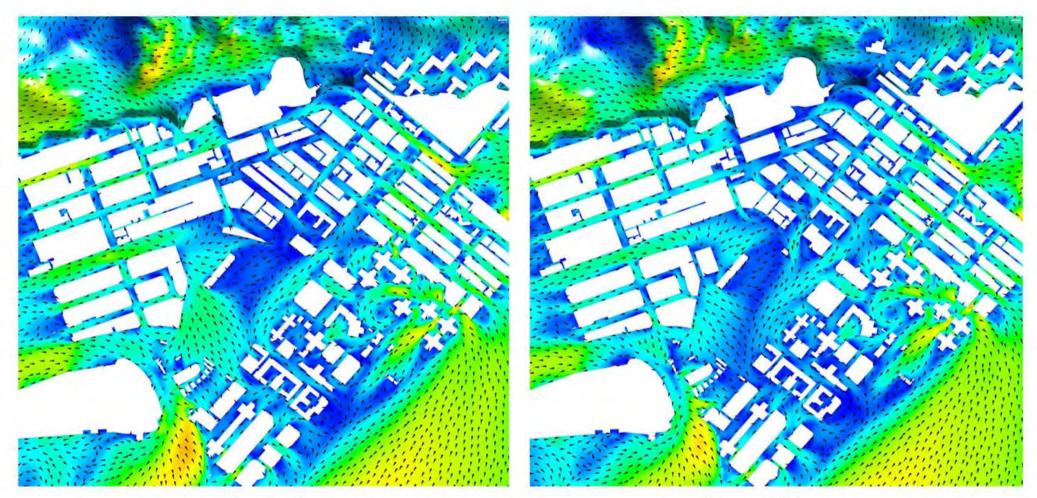


SCALE	N.T.S.	DATE		Sep-21
CHECK	KC	DRAWN		CC
JOB NO.	IA9021/SSPAA1	FIGURE NO.	3-9	REV.



JOB NO. FIGURE NO. 3-10 REV.

Velocity Ratio



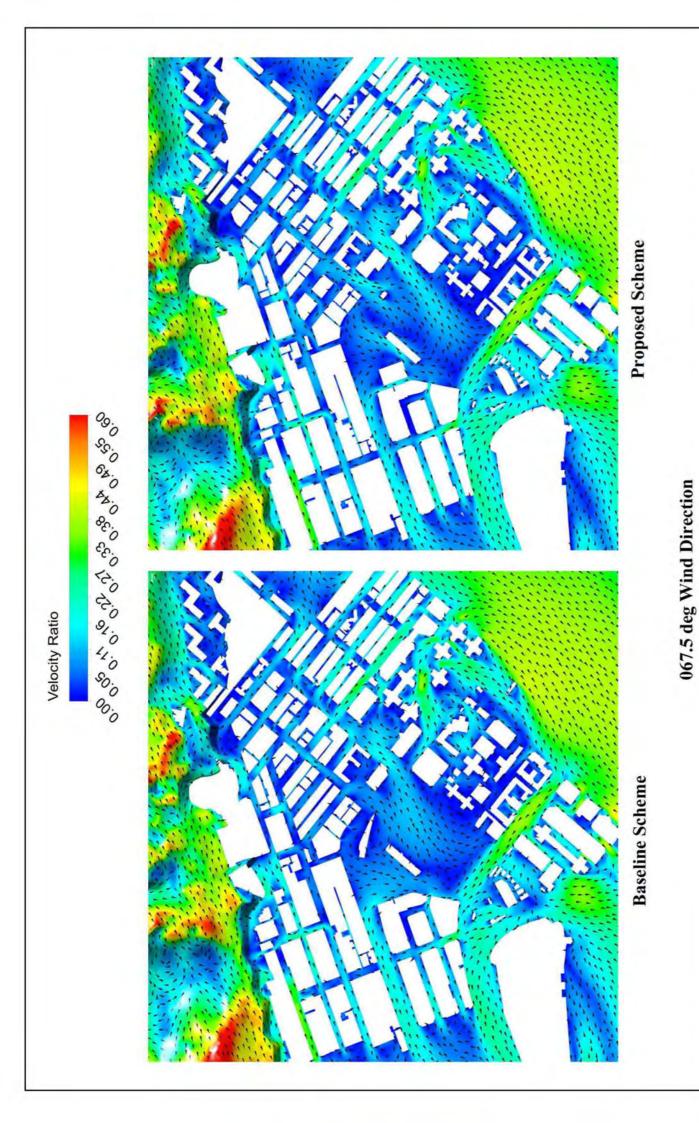
Baseline Scheme

Proposed Scheme

045 deg Wind Direction

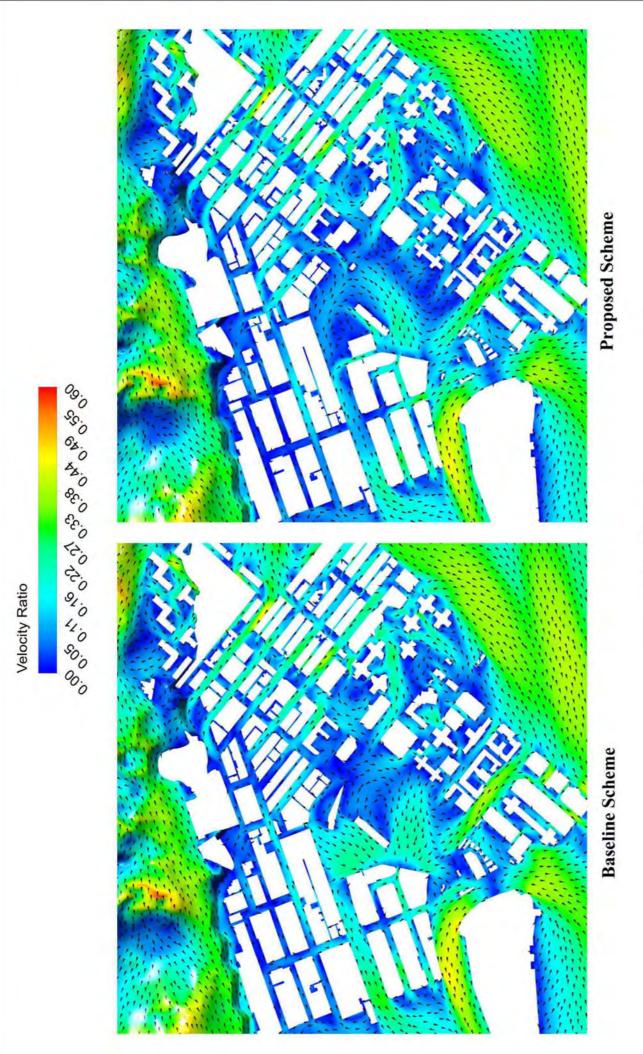


SCALE	N.T.S.	DATE	Sep-21	
CHECK	KC	DRAWN		CC
JOB NO.	IA19021/SSPAA1	FIGURE NO.	4-1a	REV.
				-





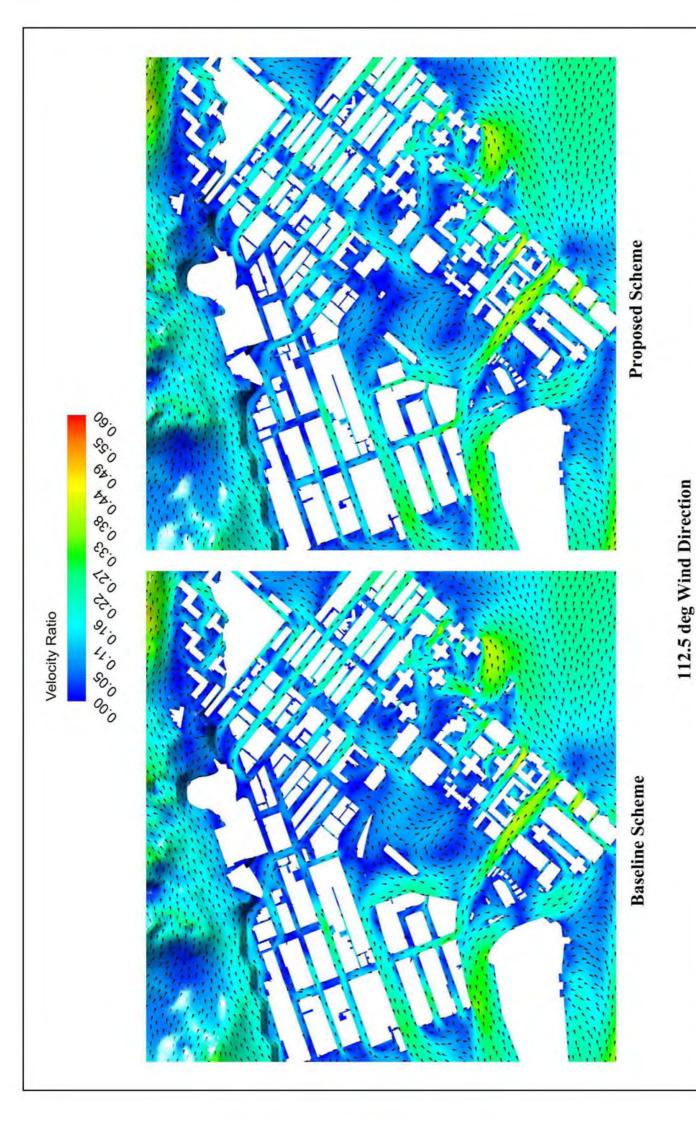
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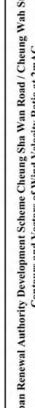




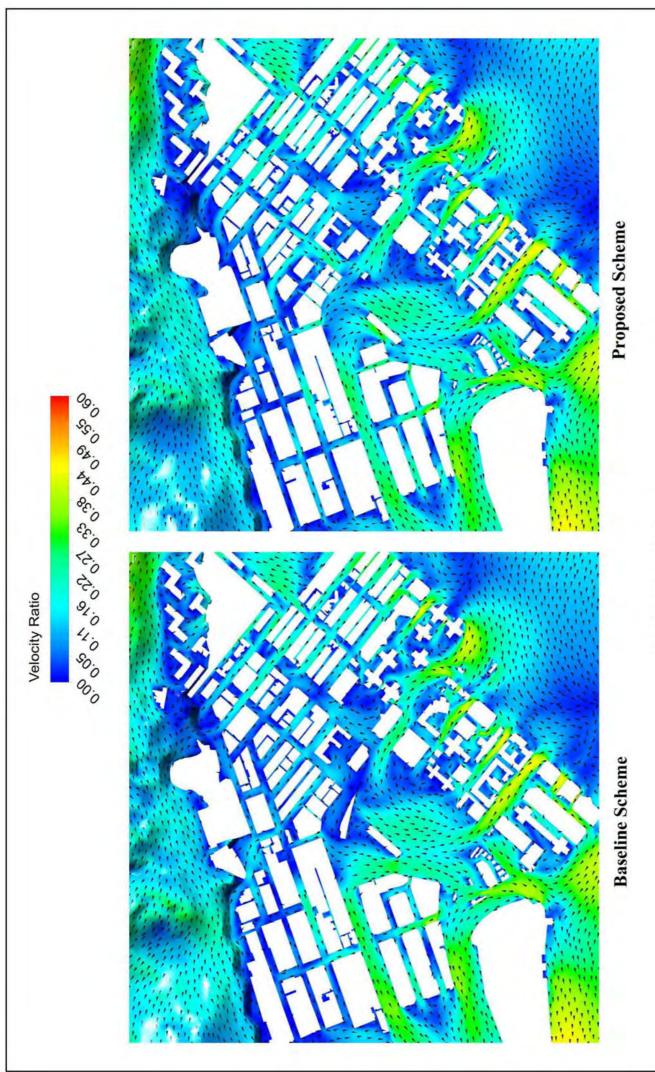
g Wah Street (SSP-018)	
Urban Renewal Authority Development Scheme Cheung Sha Wan Road / Cheu	Contours and Vectors of Wind Velocity Ratio at 2mAC







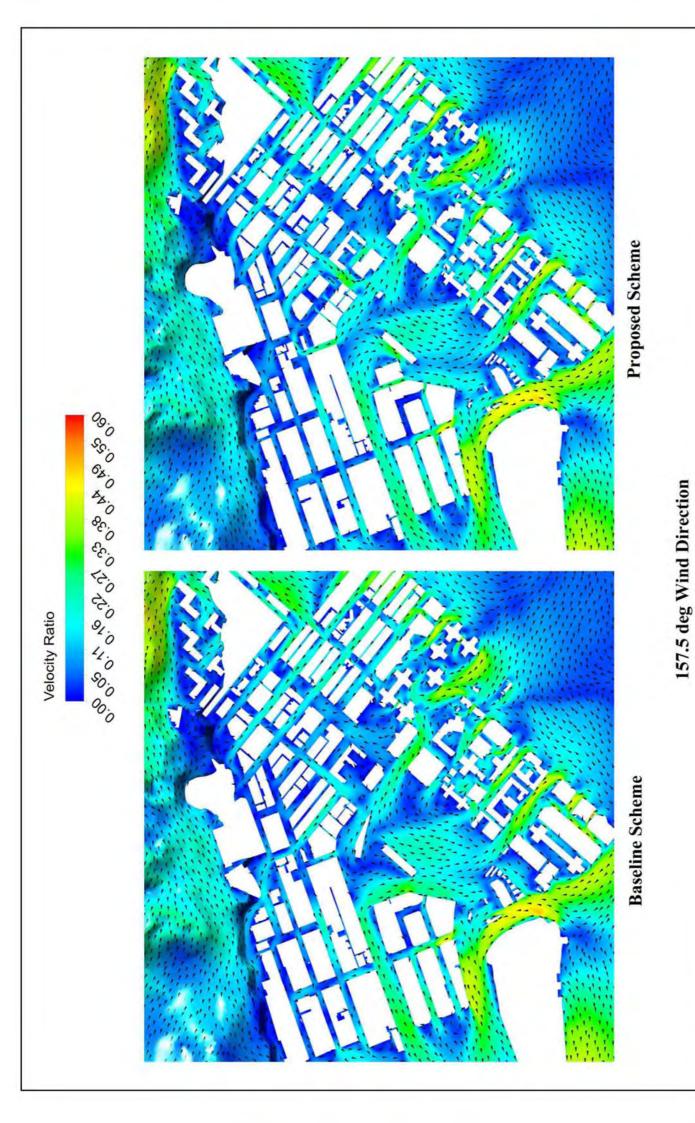


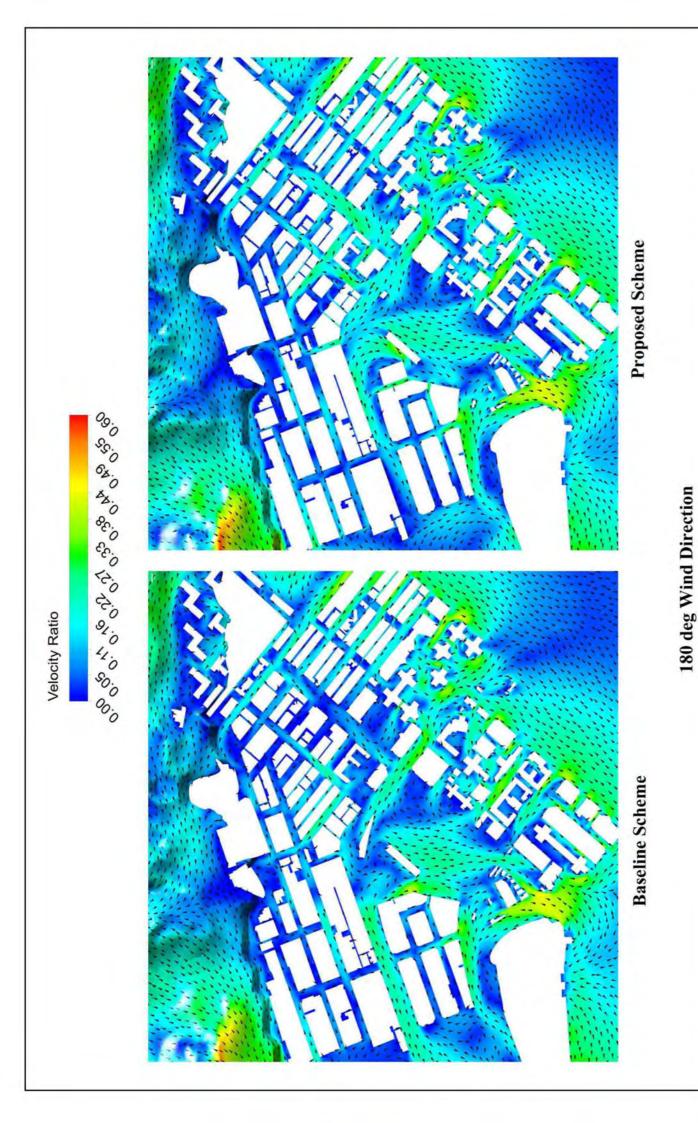


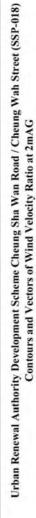
135 deg Wind Direction



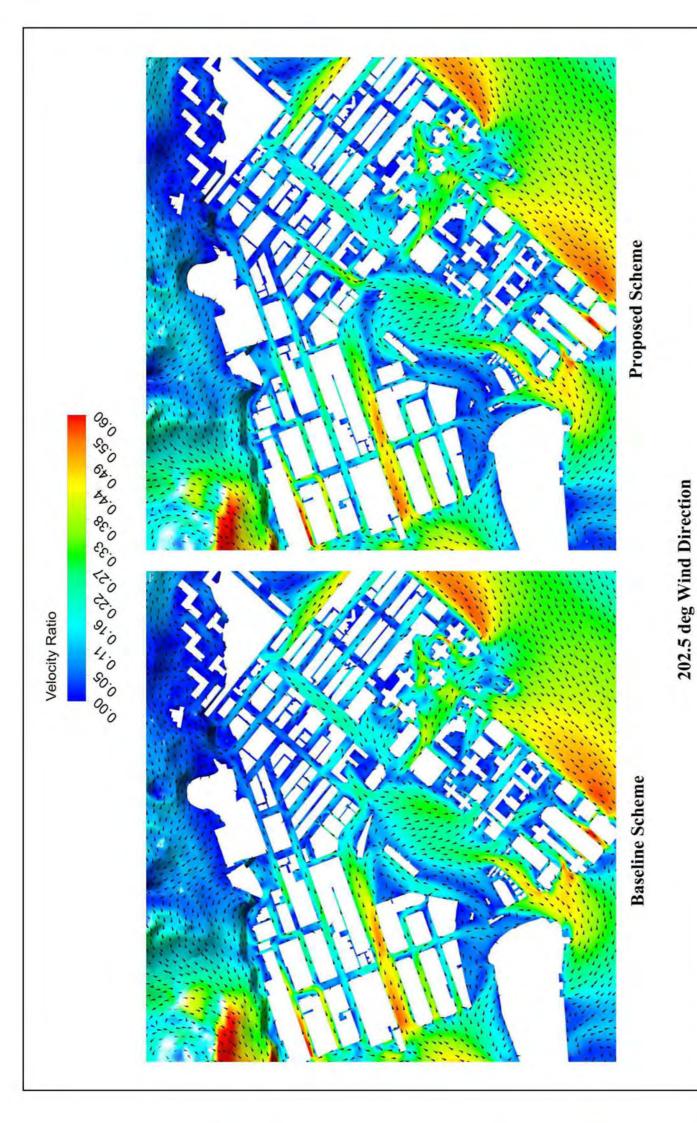
ig Wah Street (SSP-018)	
/ Cheur	2mAG
Sha Wan Road / Che	Ratio at
Sha Wa	elocity
Cheung	Wind V
Scheme (ectors of
lopment	rs and V
y Deve	Conton
Authori	
Renewal	
Urban	

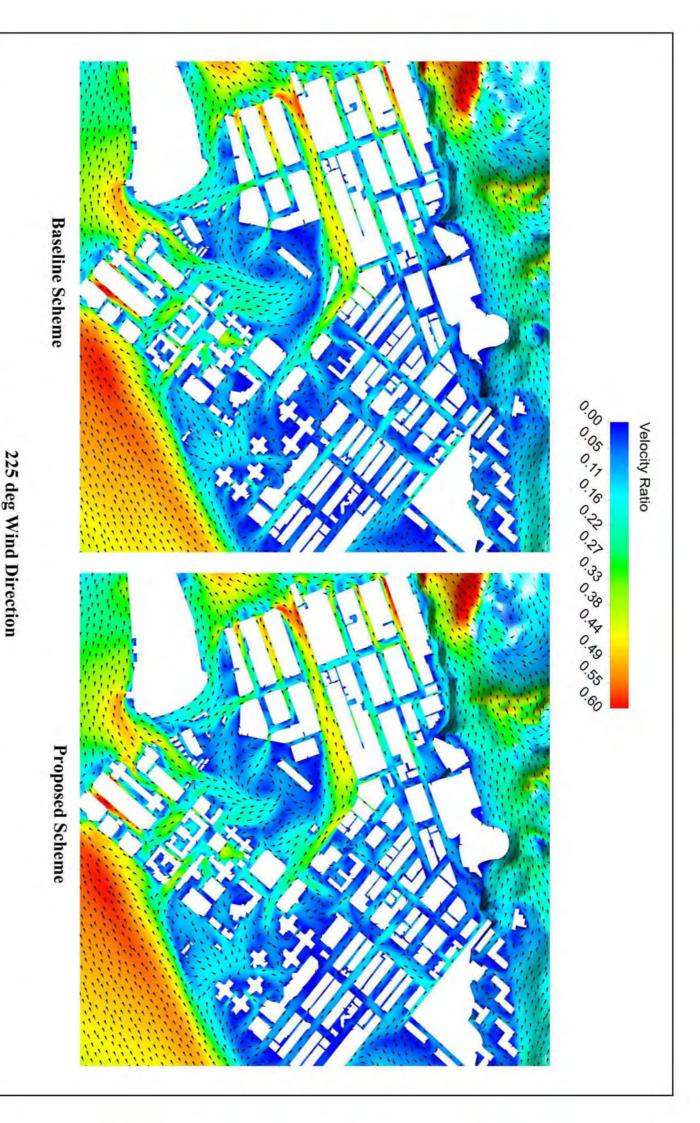






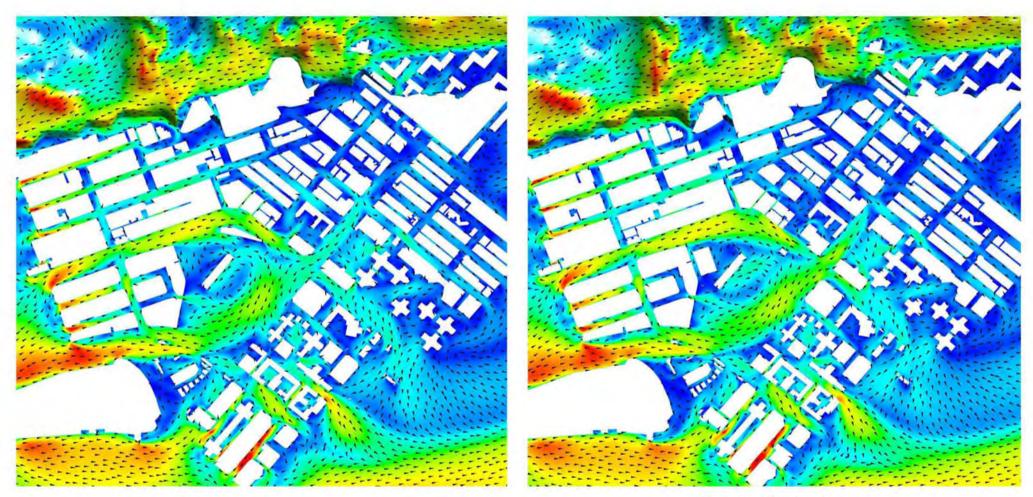








Velocity Ratio



Baseline Scheme

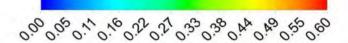
Proposed Scheme

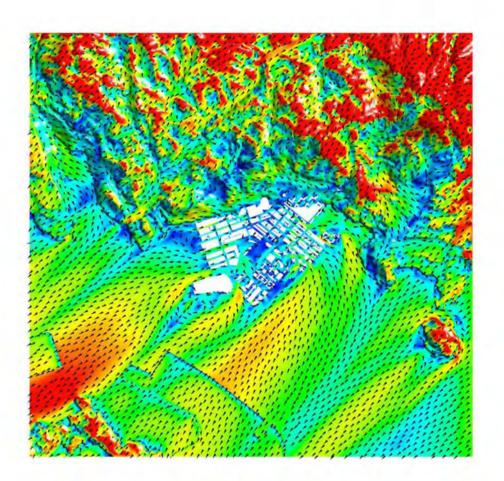
247.5 deg Wind Direction

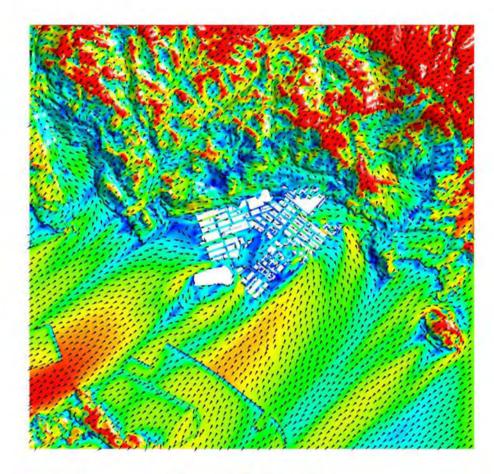


SCALE	N.T.S.	DATE	Sep-21	
CHECK	KC	DRAWN		CC
JOB NO.	IA19021/SSPAA1	FIGURE NO.	4-1j	REV.

Velocity Ratio







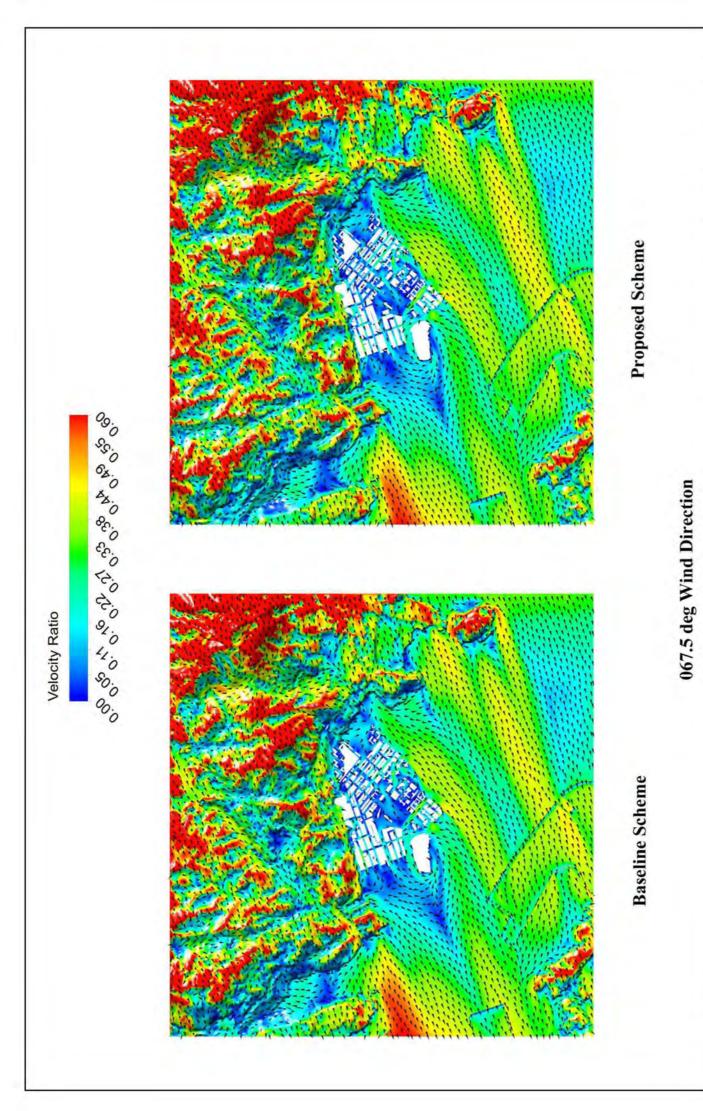
Baseline Scheme

Proposed Scheme

045 deg Wind Direction

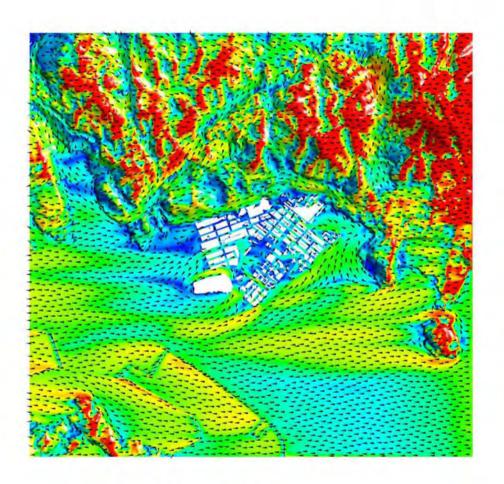


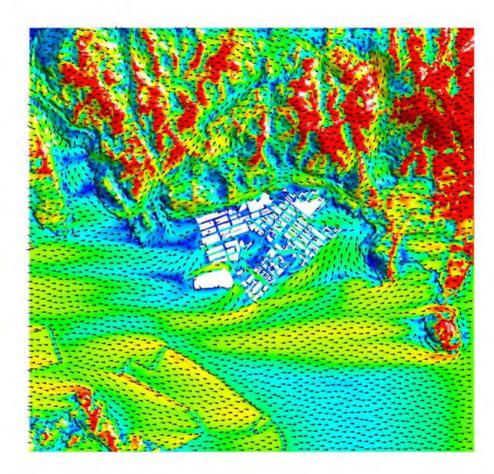
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	CHECK	KC	DRAWN	CC	
	JOB NO.	IA19021/SSPAA1	FIGURE NO.	4-2a	REV.





Velocity Ratio





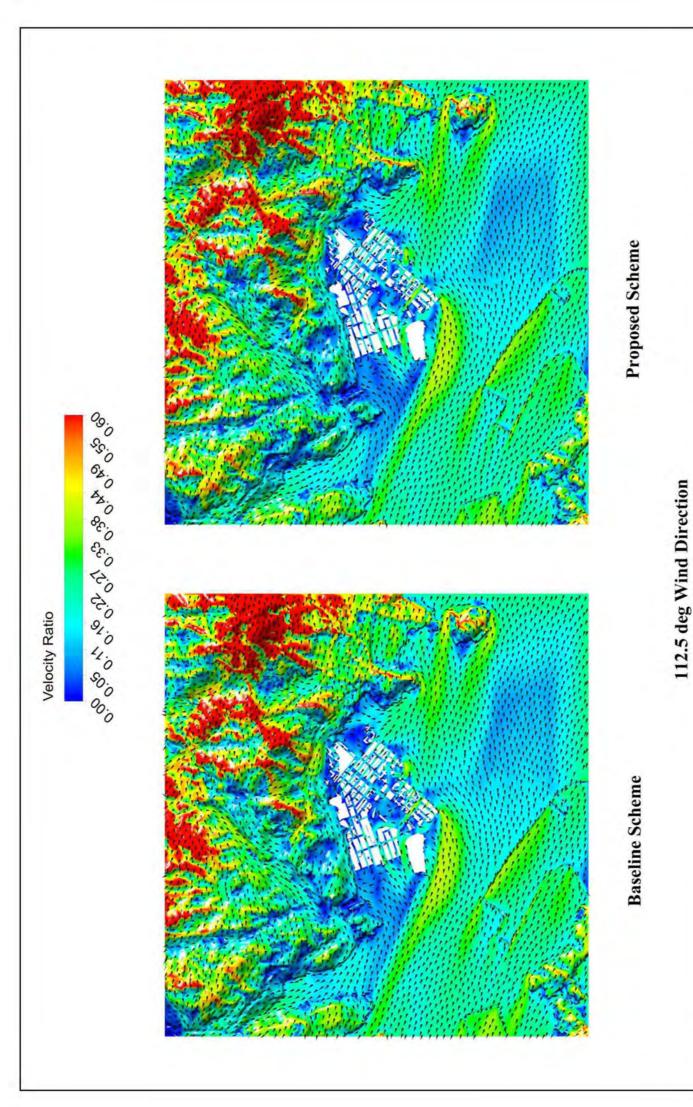
Baseline Scheme

Proposed Scheme

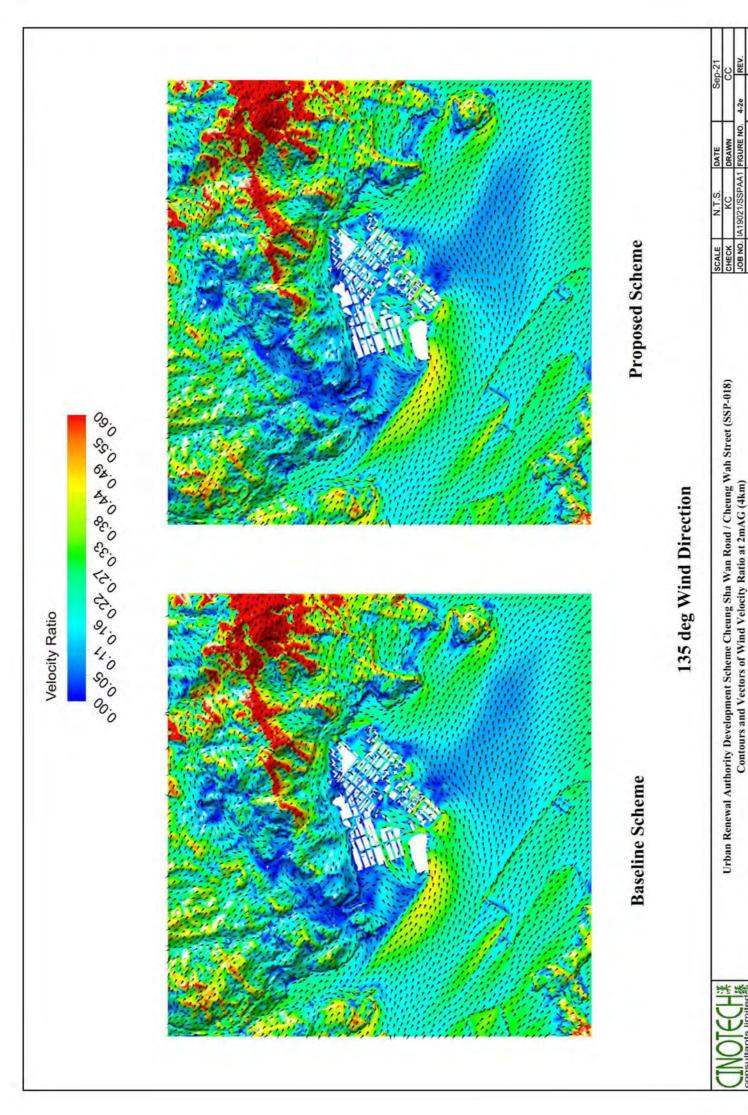
090 deg Wind Direction

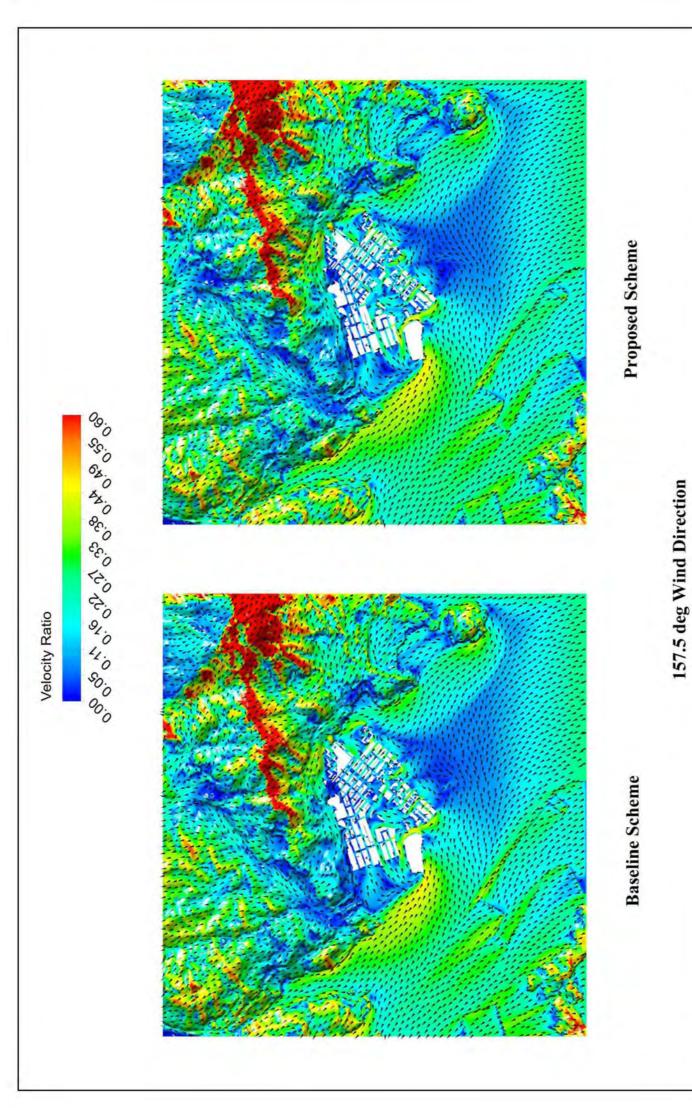


SCALE	N.T.S.	DATE DRAWN	Sep-21	
CHECK	KC			CC
JOB NO.	IA19021/SSPAA1	FIGURE NO.	4-2c	REV.
				-

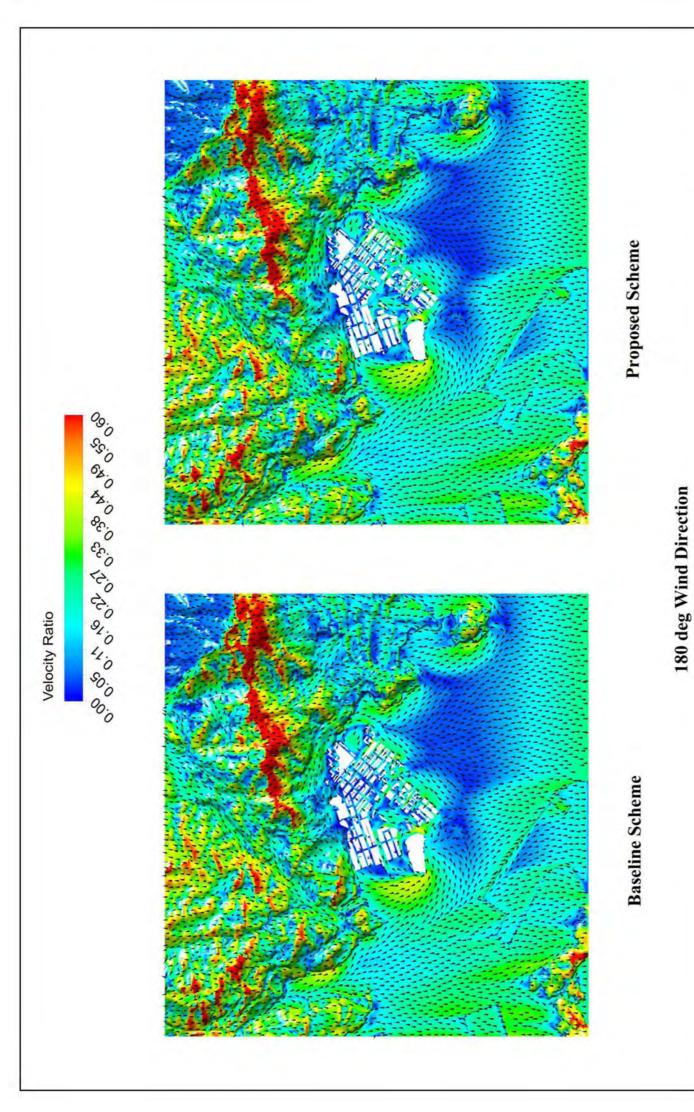


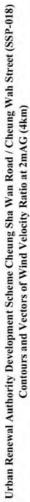




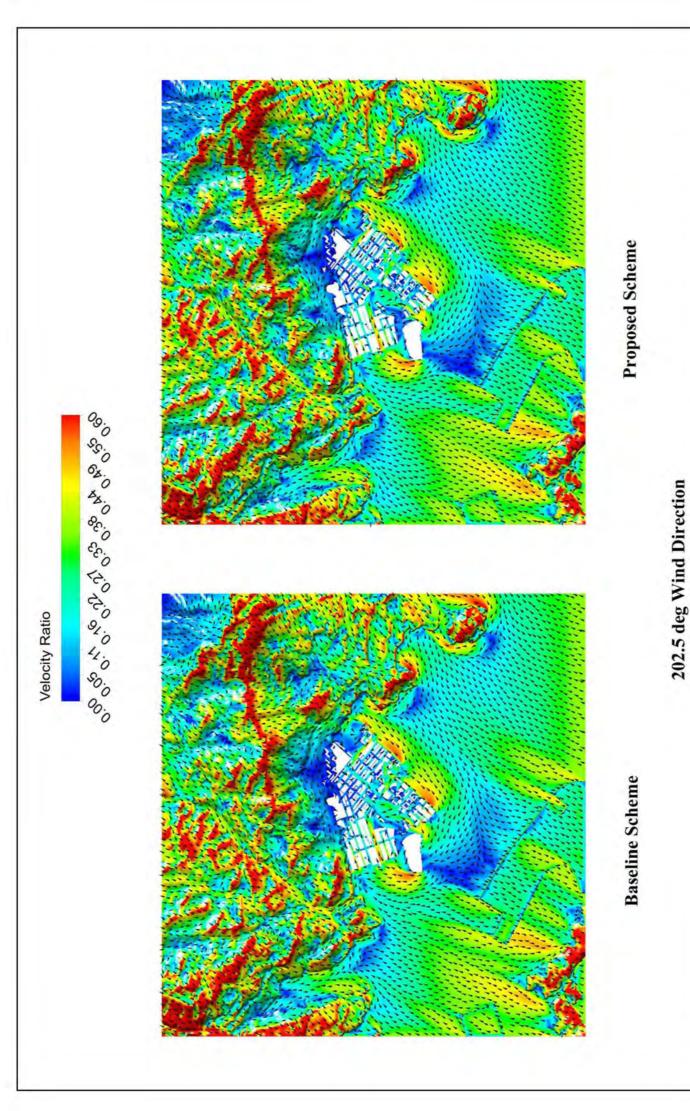


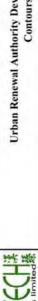


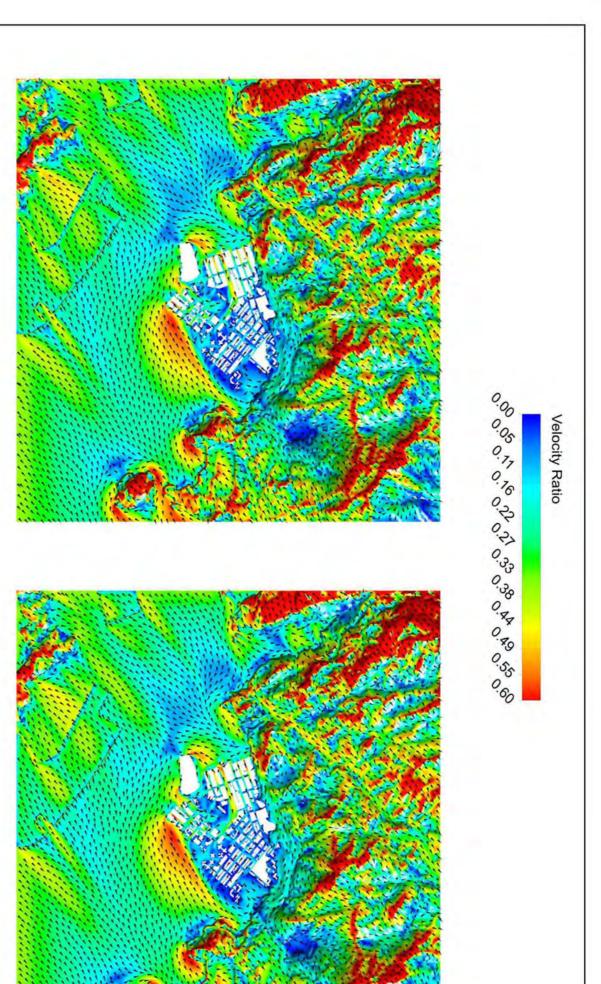














Baseline Scheme

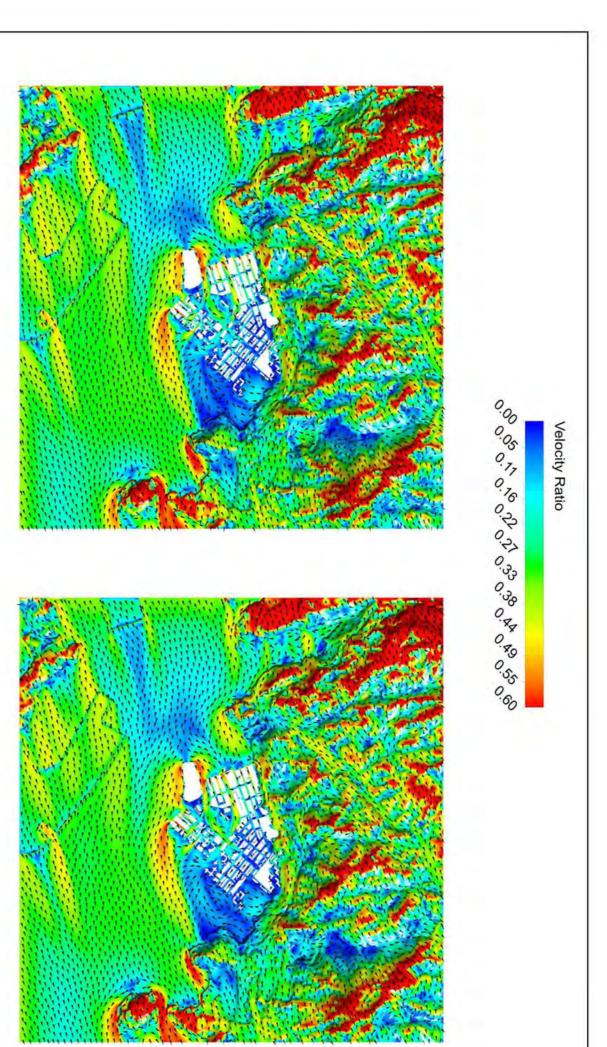
Urban Renewal Authority Development Scheme Cheung Sha Wan Road / Cheung Wah Street (SSP-018)

Contours and Vectors of Wind Velocity Ratio at 2mAG (4km)

225 deg Wind Direction

Proposed Scheme

	JOB NO.	CHECK	SCALE		
	IA19021/SSPAA1 FIGURE NO.	KC	N.T.S.		
	FIGURE NO.	DRAWN	DATE		
	4-21				
,	REV.	CC	Sep-21		





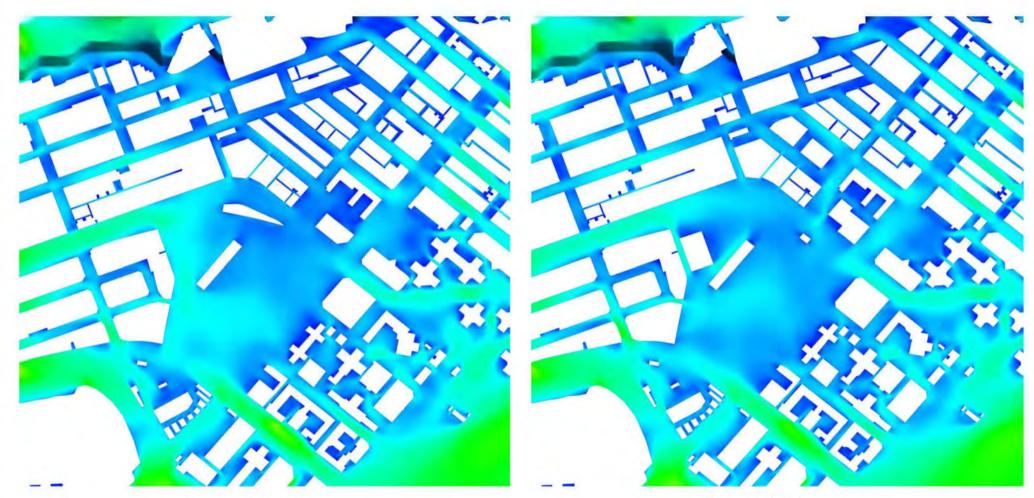
Proposed Scheme

247.5 deg Wind Direction





Velocity Ratio



Baseline Scheme

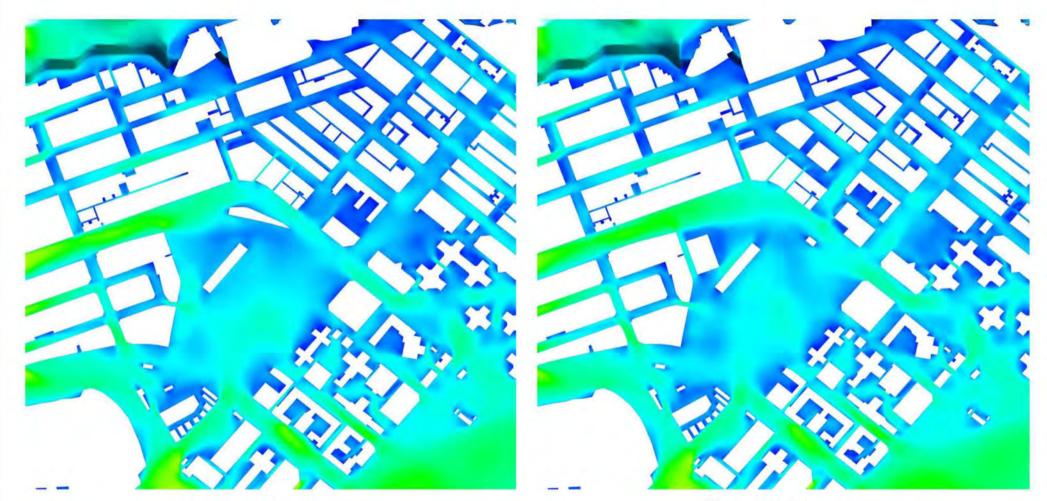
Proposed Scheme

Annual



SCALE	N.T.S.	DATE		Sep-21
CHECK	KC	DRAWN		CC
JOB NO.	IA19021/SSPAA1	FIGURE NO.	4-3a	REV.

Velocity Ratio



Baseline Scheme

Proposed Scheme

Summer



SCALE	N.T.S.	DATE		Sep-21
CHECK	KC KC	DRAWN		CC
JOB N	o. IA19021/SSPAA	1 FIGURE NO.	4-3b	REV.

Appendix 8

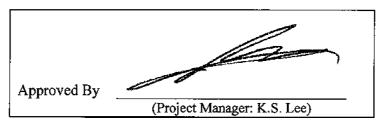
Drainage & Sewerage Impact Assessment (DSIA) Report

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Drainage Impact Assessment

(V1.0)

September 2021



REMARKS:

The information supplied and contained within this report is, to the best of our knowledge, correct at the time of printing.

CINOTECH accepts no responsibility for changes made to this report by third parties.

CINOTECH CONSULTANTS LIMITED

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Email: info@cinotech.com.hk

Prepared by	Colman Wong	Colman	23 September 2021
Checked by	Karina Chan		23 September 2021

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3	DRAINAGE IMPACT ASSESSMENT	4
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3.3	DRAINAGE DISCHARGE FROM PROJECT TO PUBLIC DRAINAGE SYSTEM	5
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1 INTRODUCTION

1.1 Background

- 1.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). This Drainage Impact Assessment (DIA) is to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.2 Cinotech Consultants Limited was commissioned by URA to carry out a Drainage Impact Assessment (DIA) to assess and envisage any potential drainage impact on the implementation of the proposed development of the Scheme and to recommend necessary pipe upgrading/diversion as necessary.

2 DESCRIPTION OF THE ENVIRONMENT

2.1 Existing Environment

- 2.1.1 The Scheme SSP-018 consists of Sites A and B. Site A is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the south-western boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary (Figure 2-1). The proposed gross site areas of the Site A & Site B are 5,197m² and 13,857m² respectively, subject to site survey and detailed design.
- 2.1.2 Currently, the Site A comprises a single storey Cheung Sha Wan Sports Centre and its associate outdoor garden and playground. The Site B comprises a government land lot (GLA-TNK 1723) which currently is an open area with a few 1-2 storeys temporary structures, Cheung Sha Wan Path Sitting-out Area, and a garden associated with Sham Shui Po Sports Ground.
- 2.1.3 According to the Approved Cheung Sha Wan Outline Zoning Plan (OZP) No. S/K5/37, the Site A consists of Open Space, G/IC (1 storey), and small portion of road zone. Similarly, the Site B also consists of Open Space, G/IC (1 storey), and road zone.
- 2.1.4 Based on the best available information, the stormwater from Site A is currently discharged via public storm water manholes SMH4061013, SMH4061014, SMH4010597, SMH4010598, to the box culvert SBP4001321 in the east. While stormwater from Site B is either discharged via storm water manhole SMH4010820 to box culvert SBP4001323 in the east, or discharged via storm water manhole SMH4010081 to the decked nullah SDP4000306 in the far west. An overview of the existing drainage pipes in the vicinity is provided in Figure 2-2.

2.2 The Proposed Development

- 2.2.1 The entire Site A is proposed to rezone to "R(A)" and redevelop the area for high-density residential development, with non-domestic uses always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of a building. The proposed development on Site A consists of a 2 floors of basement carpark, a 5 storeys podium (GFA: 5,197m² for retails; 5,197m² for G/IC) and two 34 storeys residential towers (838 flats).
- 2.2.2 Western part of the Site B is proposed to rezone to G/IC and provide a G/IC complex with GFA of 33,696 m² for community and amenity. The rest of the Site B of about 9,645 m², is proposed to be public open space.
- 2.2.3 The proposed notional scheme is shown in Appendix I. The notional design is subject to change at detailed design stage.
- 2.2.4 It should be noted that public storm water manholes SMH4061013, SMH4061014, SMH4010597, SMH4010598 are within the boundary of Site A (Figure 2-2). Those manholes as well as their connecting drainage pipes will be removed. As those public storm water manholes are not only serving the Site A but also for upstream catchments, re-diversion of the existing drainage pipes is necessary.

2.2.5 An existing public storm water manhole SMH4010820 is current in Site B. The manhole together with it associated pipe will be removed. As the manhole should only serve the Site B, no re-diversion is necessary.

3 DRAINAGE IMPACT ASSESSMENT

3.1 Catchments in the Vicinity

- 3.1.1 Stormwater Drainage Manual Planning, Design and Management", fifth edition, January 2018, (hereafter called "the DSD Manual") prepared by the DSD provides guidelines for the design of the drainage system. According to Table 10 of the DSD Manual, the recommended design return period based on flood levels is 50 years ("main rural catchment drainage channels") for conservative purpose.
- 3.1.2 The runoff coefficients of each zone are summarized in Table 3-1.

Table 3-1 Runoff Coefficients

Type of Area	Run-off Coefficient [1]
Grass	0.19
Paved/Concrete	0.90

Note:

3.1.3 A hydraulic calculation has been performed on the peak flows from a 1:50 year rainstorm with rainfall intensity according to the DSD Manual. The increase of 10.4% in rainfall for 2041-2060 is also incorporated into the calculation. The catchments are shown in Figure 3-1 and Figure 3-2a to Figure 3-2f. The volumes of stormwater runoff of each zone are summarized in Table 3-2. The detailed calculations are shown in Appendix II.

Table 3-2 Comparison of Drainage Discharge from the Site and Vicinities

Catchments	Total Drainage Discharge (L/s)
Project site A	304.9
Project Site B (POS)	442.9
Project Site B (G/IC)	220.9
A1	181.3
A2	190.5
B1	196.5
B2	75.1
B3	268.1
B4	620.6

Note:

[1] Detailed calculations are shown in Appendix II.

3.2 Impact to Existing Public Drainage System

3.2.1 The runoff from Site A and the Site B (POS) will be directed to the nearest section of box culvert in the east (SBP4001321 & SBP4001322), without via existing public drainage pipes. The runoff from the Site B (G/IC) will be directed to the nearest existing manhole (SMH4010052). The hydraulic calculations of the full capacities for the existing pipes

The runoff coefficients are extracted from Section 7.5.2 of "Stormwater Drainage Manual – Planning, Design and Management", fifth edition, January 2018.

^[2] Paved and unpaved area for the proposed development subject to minor changes in detailed design stage.

connecting to the public drainage system are summarized in **Table 3-3**. The detailed calculation can be found in Table A in **Appendix III.**

Table 3-3 Capacities of Existing Drainage Pipes

Drainage Pipe	Upstream Manhole no.	Downstream Manhole no.	Full Capacity ^[1] (L/s)	Catchment	Peak Flow (L/s)	Percentage
PS B01	SMH4010052	SMH4010053	1750	Project site B (G/IC) + B1 +B2 +B3 +B4	1381.1	79%
PS B02	SMH4010053	SMH4010054	2021	Project site B (G/IC) + B1 +B2 +B3 +B4	1381.1	68%
PS B03	SMH4010054	SMH4010055	1976	Project site B (G/IC) + B1 +B2 +B3 +B4	1381.1	70%

Note:

3.2.2 From the calculation detailed in Table A of Appendix III, the downstream drainage pipes PS B01 – PS B03 can cater the stormwater discharge from Site B (G/IC). Therefore, no upgrading works for those pipes are required.

3.3 Drainage Discharge from Project to Public Drainage System

Site A (Composite Development)

3.3.1 Stormwater from Project Site A will be collected by a new terminal manhole (STMH-A01) then discharged via a new proposed pipe (PP A01) to the box culvert (SBP4001321) (2440mm×2440mm) along Hing Wah Street. The diameter and slope of the proposed pipe PP A01 are φ600mm and 1:100 respectively.

Re-diversion of Existing Drainage Pipe due to Site A

- 3.3.2 As the existing public stormwater manholes SMH4061013, SMH4061014, SMH4010597, SMH4010598 together with their associated drainage pipes will be removed due to the Site A, new stormwater manhole and drainage pipes will be required to re-divert the stormwater from upstream catchments to the box culvert SBP4001324 along Hing Wah Street (Figure 3a).
- 3.3.3 Five new manholes (STMH-A02 STMH-A06) and six new drainage pipes (PP A02 PP A07) have been proposed for the re-diversion. The diameter and slope of those proposed pipes are φ600mm and 1:100 respectively.

Site B (POS)

3.3.4 Stormwater from Project Site B (POS) will be collected by a new terminal manhole (STMH-B01) then discharged via a new pipe (PP B01) to the box culvert (SBP4001323) (2440mm×2440mm) along Hing Wah Street (Figure 3-3b). The diameter and slope of the proposed pipe PP B01 are φ600mm and 1:100 respectively.

^[1] Calculated by Colebrook-White Equation. The detailed calculation is shown in Appendix III.

Site B (G/IC Complex)

3.3.5 Stormwater from Project Site B (G/IC) will be collected by a new terminal manhole (STMH-B02) then discharged via a new pipe (PP B02) to the existing manhole (SMH4010052) along Cheung Sha Wan Road (Figure 3-3c). The diameter and slope of the proposed pipe PP B02 are φ600mm and 1:100 respectively.

Details of the Proposed Pipes

- 3.3.6 The proposed new pipes are summarised in **Table 3-4 & Table 3-5** and illustrated in **Figure 3-3a to Figure 3-3c**. Detailed calculation is presented in Table B of **Appendix III**.
- 3.3.7 It should be noted that the proposed new drainage pipe PP A02 will cross over with existing public sewer FWD4011891. FWD4011891 is a 750mm pipe with invert level of 1.02-1.06mpD, while PP A02 is having invert level of 3.50-3.62mPD. Similarly, the proposed new drainage pipe PP A04 (invert level of 3.05-3.26mPD) will cross over the proposed new sewer for Site A (~1.0 mPD, please refer to the SIA report for details). As there are significant vertical distances in between the pipes, no conflict of the pipes is anticipated.
- 3.3.8 The calculation shows that capacities of the proposed pipes are sufficient to cater the peak stormwater flow. Therefore, no adverse drainage impact is anticipated if the proposed new stormwater manholes and drainage pipes are implemented properly.

Table 3-4 Capacities of Proposed Drainage Pipes

Drainage Pipe	Upstream Manhole no.	Downstream Manhole no.	Diameter (mm)	Full Capacity ^[1] (l/s)	% of full capacity
		Projec	t Site A		
PP A01	STMH-A01	SBP4001321	600	556	55%
		Project Site A	- Re-diversion		
PP A02	SMH4061012	STMH-A02	600	556	67%
PP A03 STMH-A02		STMH-A03	600	548	68%
PP A04 STMH-A03		STMH-A04	600	548	68%
PP A05	STMH-A04	STMH-A05	600	548	68%
PP A06	STMH-A05	STMH-A06	600	548	68%
PP A07	STMH-A06	SBP4001321	600	548	68%
		Project Si	te B (POS)		
PP B01	STMH-B01	SBP4001323	600	556	80%
		Project Si	te B (G/IC)		
PP B02	STMH-B02	SMH4010052	600	556	40%

Note:

^[1] Calculated by Colebrook-White Equation. The detailed calculation is shown in Appendix III.

Table 3-5 Details of Proposed Drainage Pipes

Drainage	Upstream	Downstream	Diameter	Invert level (mP.D.) [1]		Slope [1]
Pipe	Manhole no.	Manhole no.	(mm)	Upstream	Downstream	
			Project Site A			
PP A01	STMH-A01	SBP4001321	600	2.86	2.68	0.01
		Project	Site A - Re-d	iversion		
PP A02	SMH4061012	STMH-A02	600	3.62	3.50	0.01
PP A03	STMH-A02	STMH-A03	600	3.50	3.26	0.01
PP A04	STMH-A03	STMH-A04	600	3.26	3.05	0.01
PP A05	STMH-A04	STMH-A05	600	3.05	2.70	0.01
PP A06	STMH-A05	STMH-A06	600	2.70	2.32	0.01
PP A07	STMH-A06	SBP4001321	600	2.32	2.00	0.01
		Pre	oject Site B (P	OS)		
PP B01	STMH-B01	SBP4001323	600	1.84	1.70	0.01
		Pro	oject Site B (G	/IC)		
PP B02	STMH-B02	SMH4010052	600	4.26	4.00	0.01

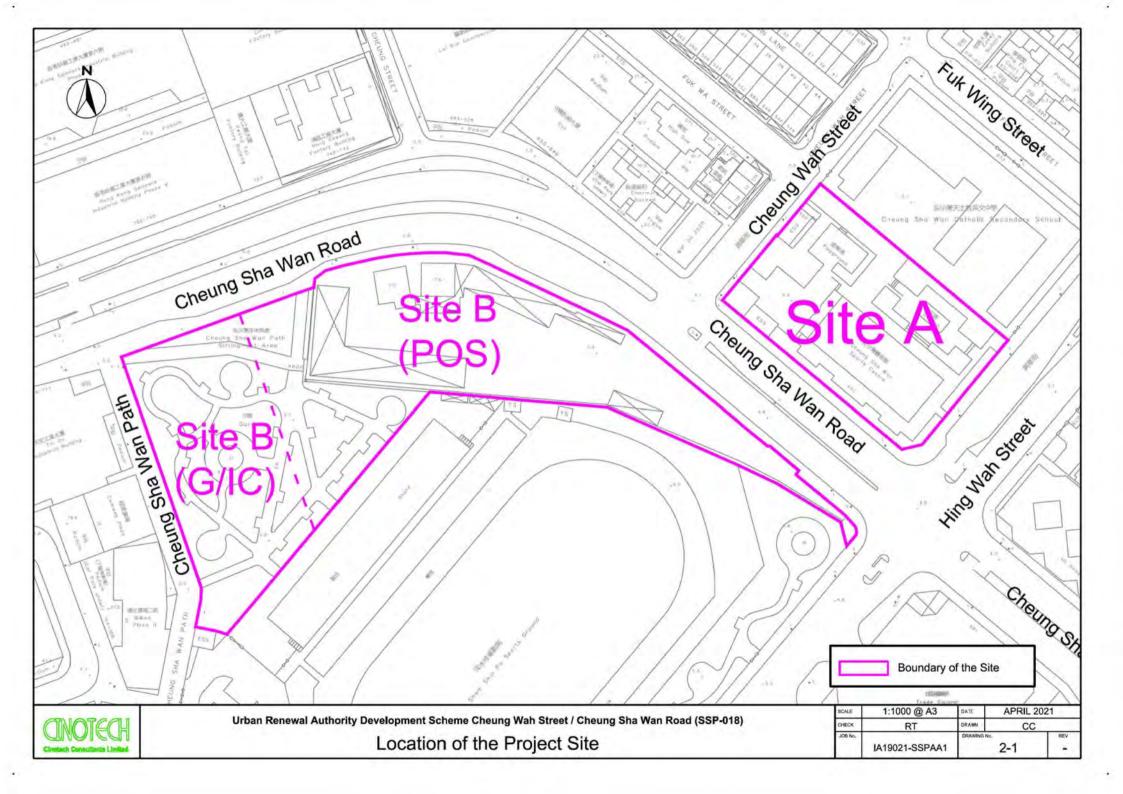
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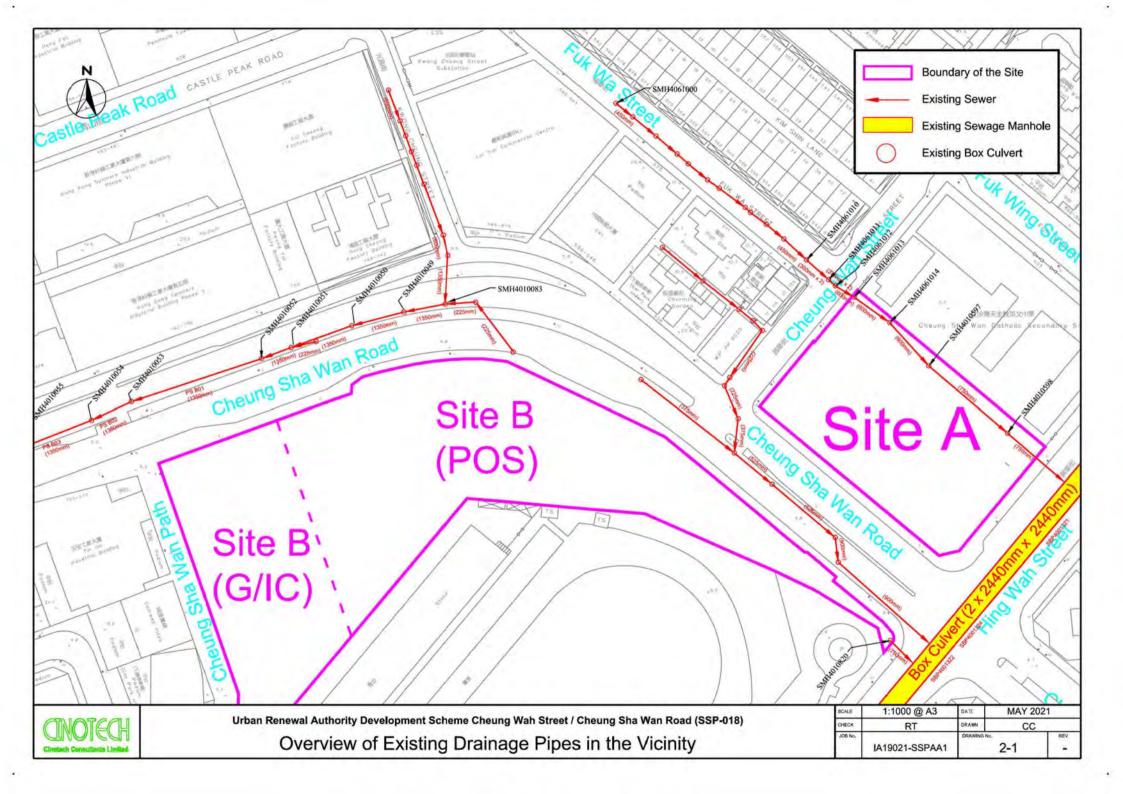
^[1] The Invert level and slope of the proposed upgrade pipes subject to detail design.

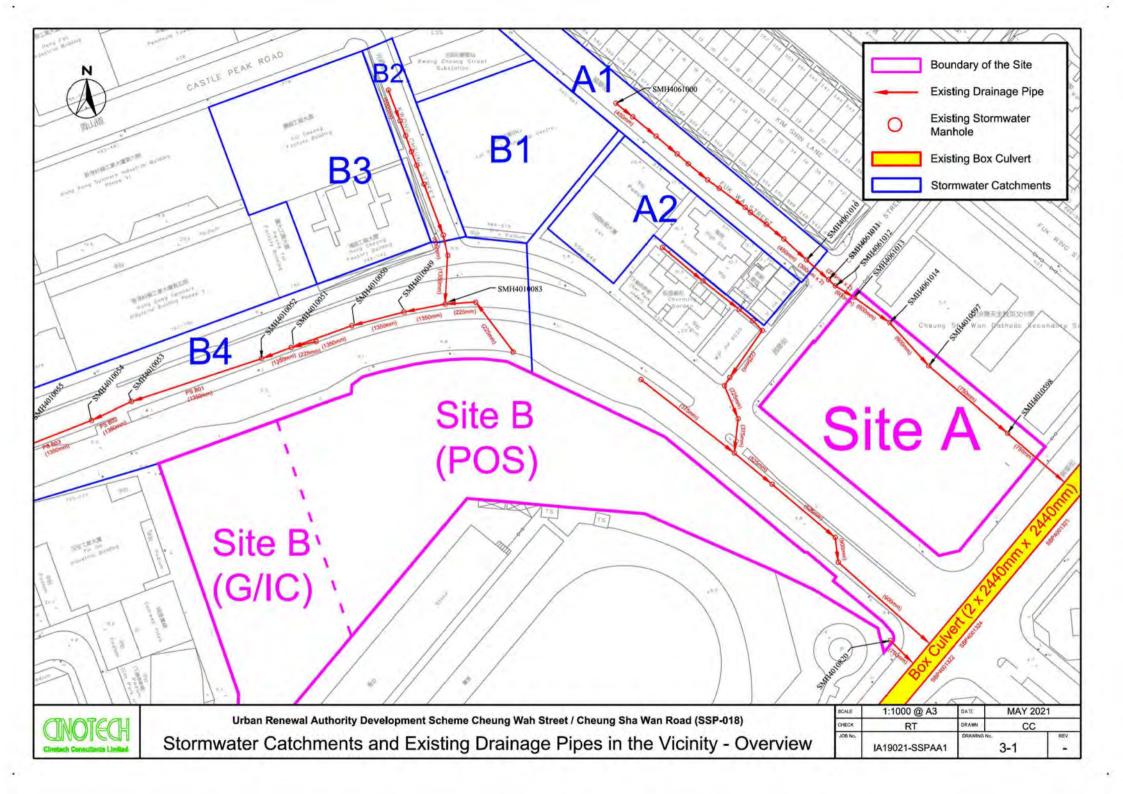
4 CONCLUSION

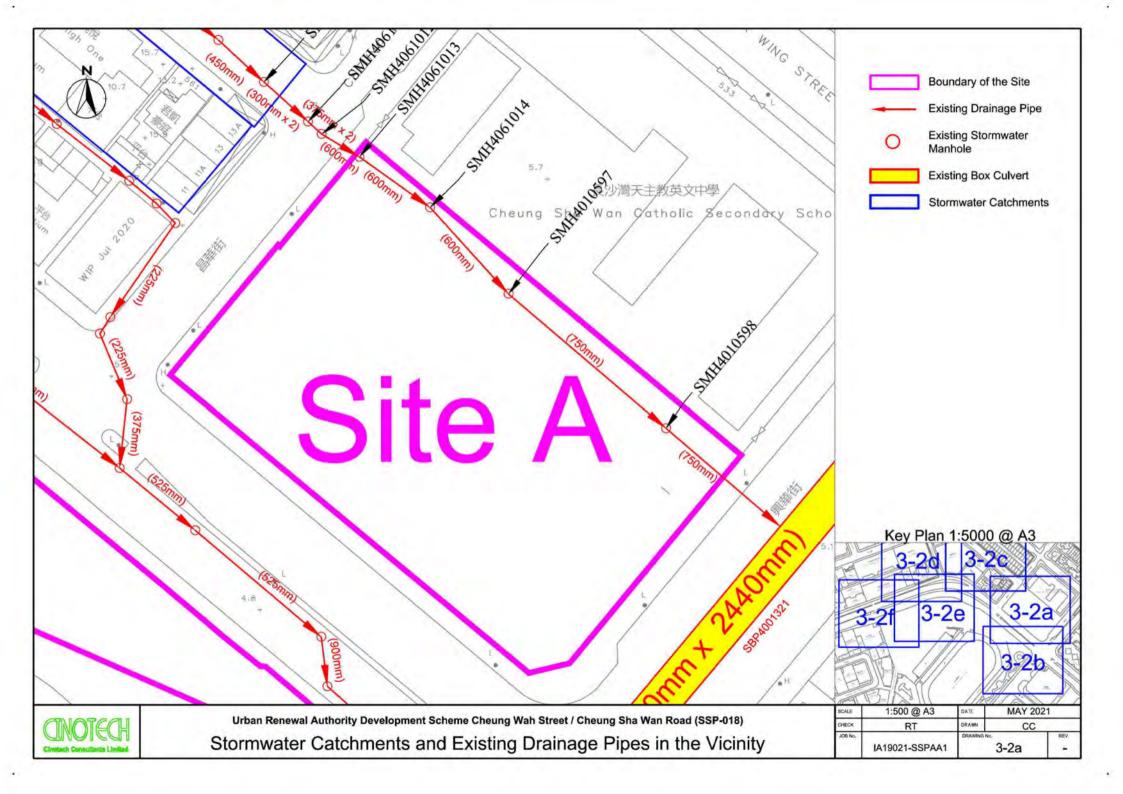
- 4.1.1 The Development Scheme proposes to redevelop a composite development at Site A, which consists of 2 residential towers which providing about 838 flats, 2 floors of basement carpark, as well as a 5 storeys podium with ~5,197m² of G/C area and ~5,197m² of retail area; The Development Scheme also proposes a G/IC complex with GFA of ~33,696 m² for G/IC facilities at Site B.
- 4.1.2 For Site A, a new manhole (STMH-A01) is proposed to cater the drainage from the new development and then discharge via a new 600mm pipe (PP A01) to the nearby box culvert (SBP4001321).
- 4.1.3 The existing pipes and manholes (from existing manhole SMH4061012 to the box culvert SBP4001321) which are located within the boundary of Site A, will be replaced by new manholes (STMH-A02 STMH-A06) and new pipes (from PP A02 to PP A07) to cater the stormwater from upstream catchments and then discharge to the box culvert (SBP4001324).
- 4.1.4 For Site B (POS), the existing manhole (SMH4010820) will be removed. A new terminal manhole (STMH-B01) will to collect the drainage discharge from Site B (POS), then discharged via a new 600mm pipe (PP B01) to the box culvert (SBP4001323).
- 4.1.5 A new manhole (STMH-B02) is proposed to cater the drainage from Site B (G/IC) and discharge via a new 600mm pipe (PP B02) to the existing manhole (SMH4010052).
- 4.1.6 Actual layout and invert levels of the proposed pipes are subject to detail design.
- 4.1.7 The new pipes would have sufficient capacity to cater for the stormwater discharge from the proposed development and surrounding catchments; therefore, no adverse drainage impact on the public drainage system is expected.

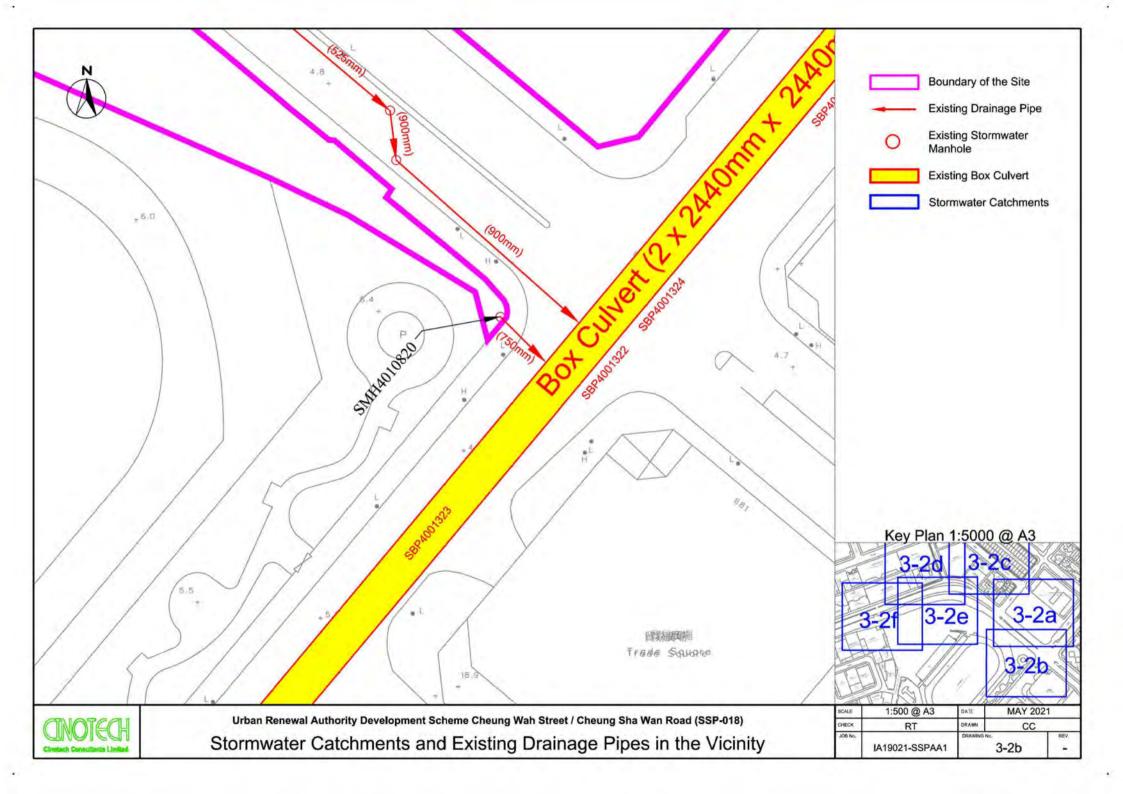
FIGURES

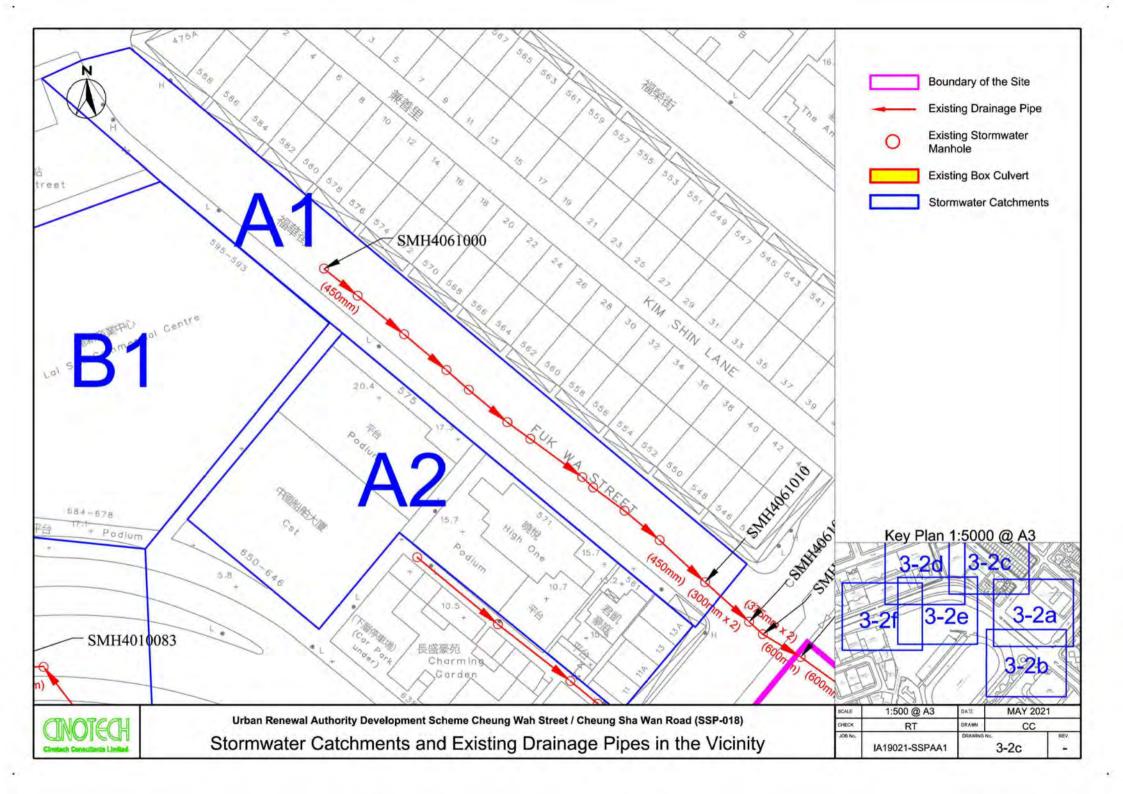


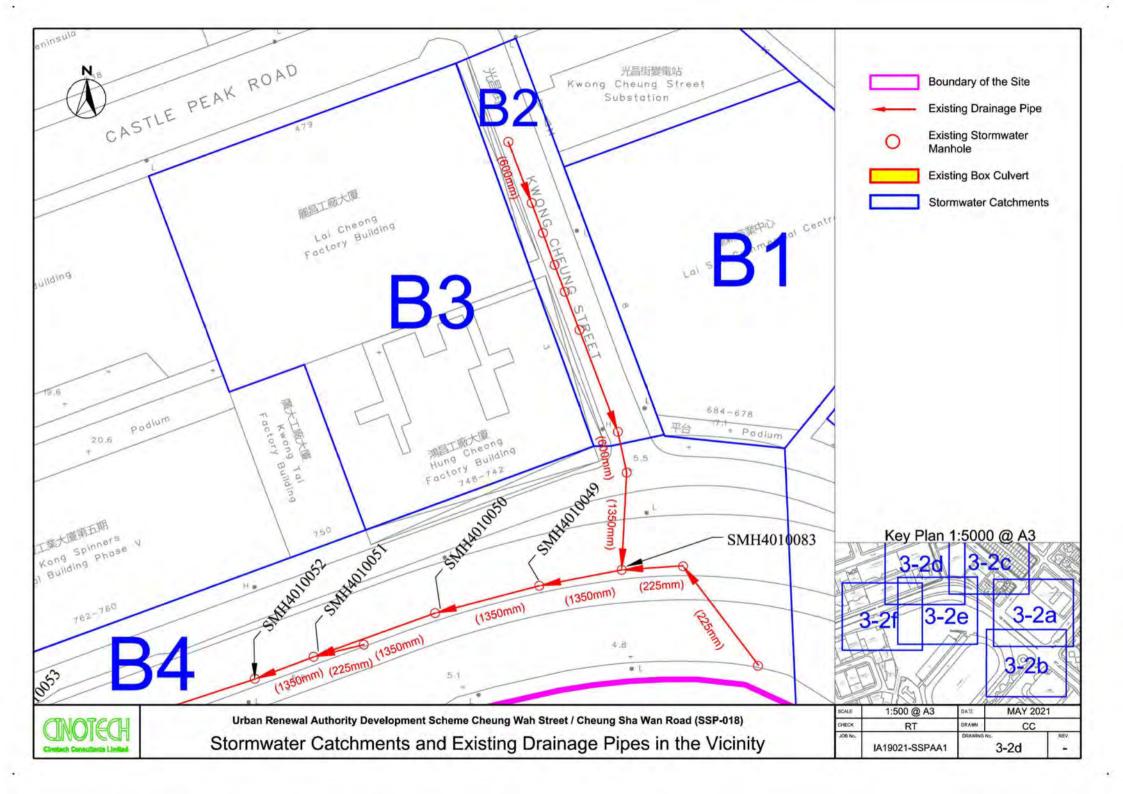


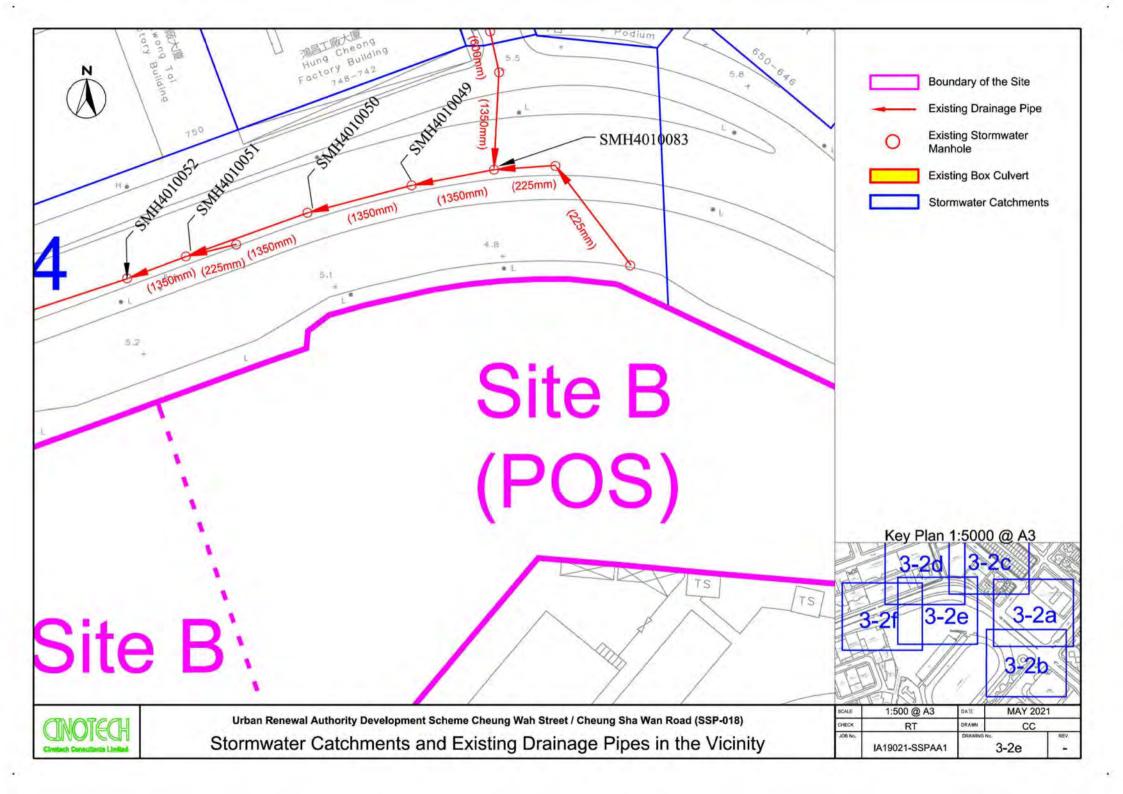


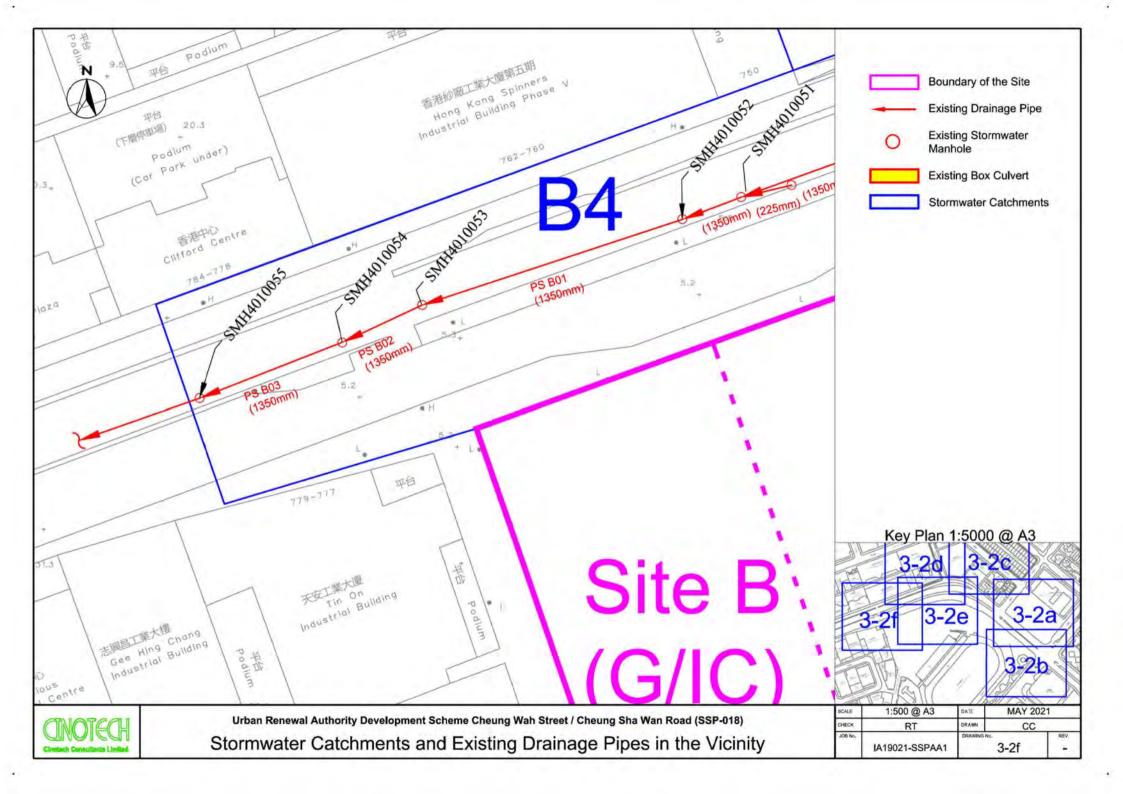


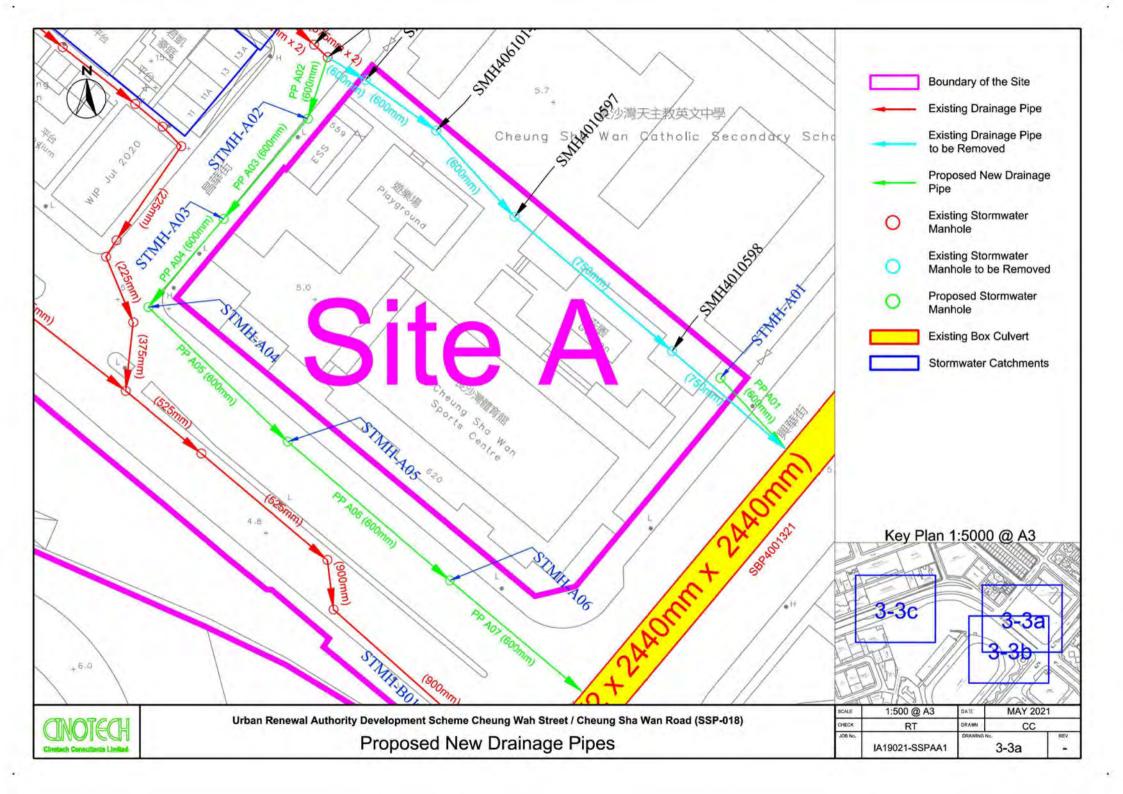


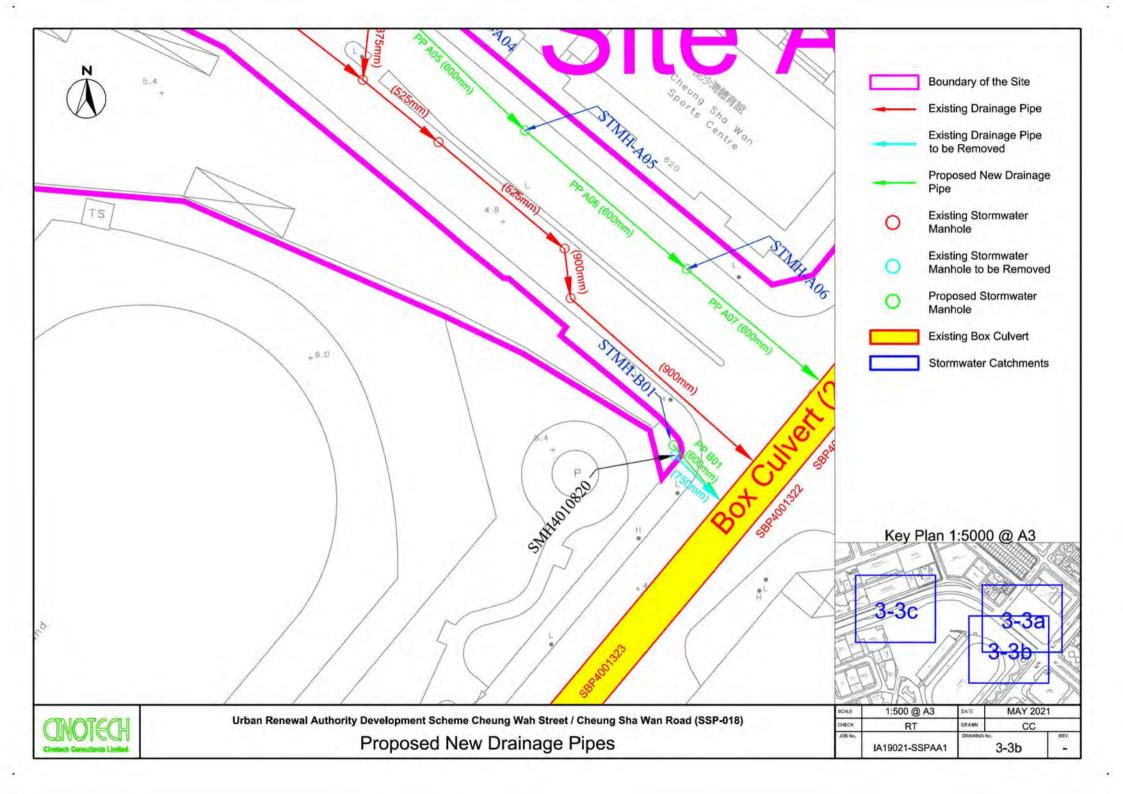


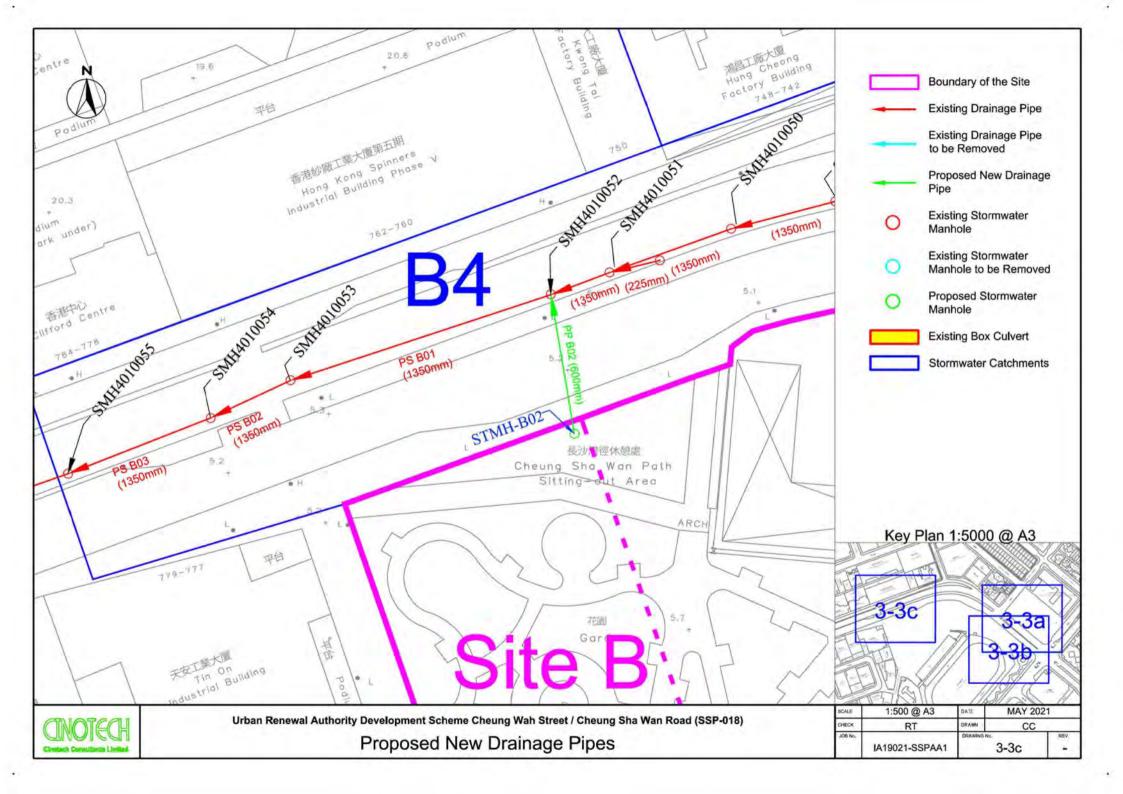




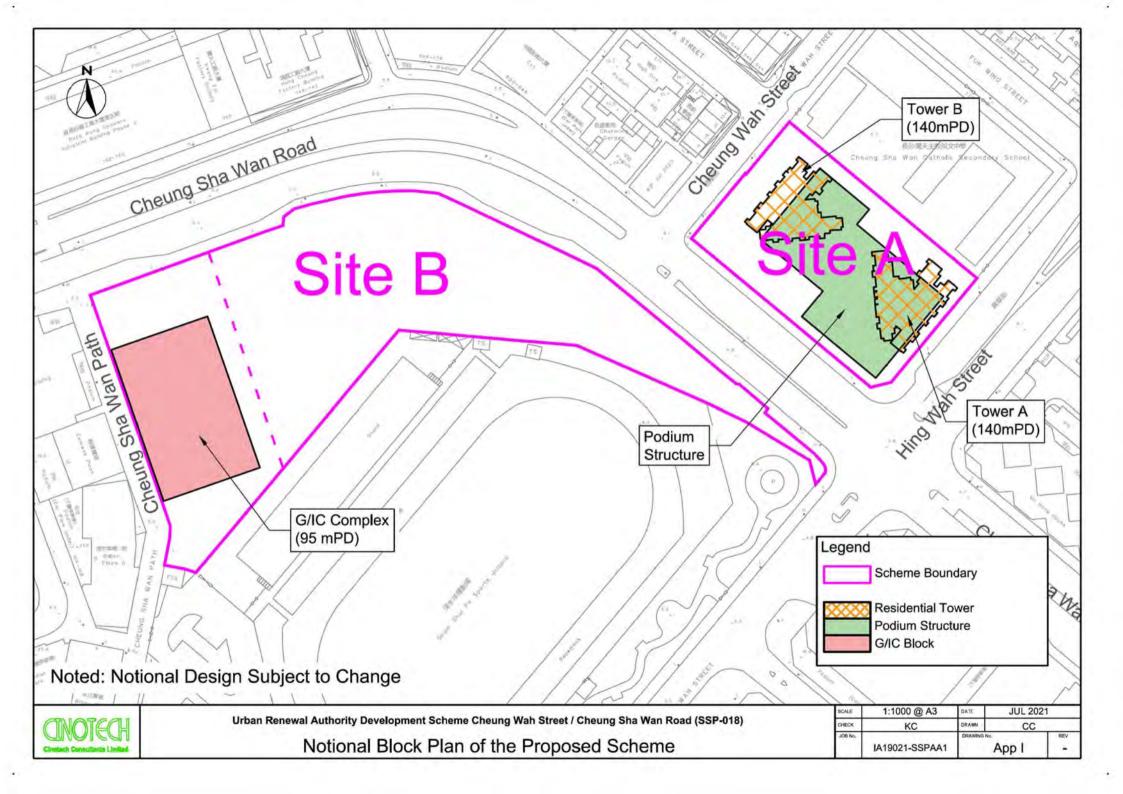


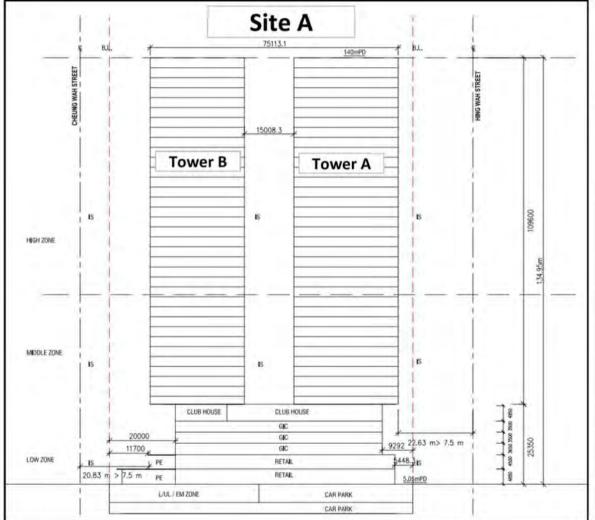


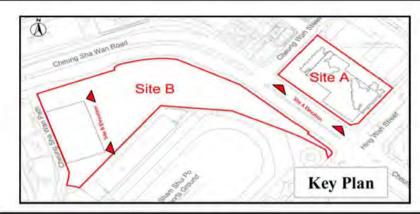


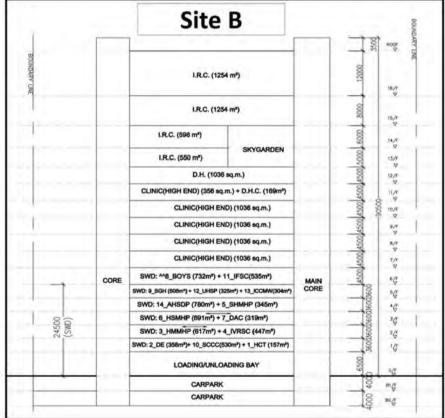


APPENDIX I Notional Block Plan of the Proposed Scheme









Remark:

Notional Design subject to change at detailed design stage



Urban Renewal Authority Development Scheme Cheung Wah Street/ Cheung Sha Wan (SSP-018)

Notional Section Plan of the Proposed Scheme

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APPENDIX II Drainage From Catchment Zone

Appendix II - Drainage from Catchment Zone

Catchment Zone	Project Site A	Project Site B (POS)	Project Site B (G/IC)	A1	A2	B1	B2	В3	B4
Description	Proposed Development	Proposed Development	Proposed Development	Fuk Wa Street	Existing Buildings	Existing Buildings	Kwong Cheung Street	Existing Buildings	Cheung Sha Wan Road
Catchment Area (m²)	5197	9645	4212	2389	2603	3158	982	4135	8540
Slope (m per 100m) ^[1]	0,40	0.40	0.40	0.18	0.40	0.40	0,30	0,40	0.16
L (m)	93.0	243.0	140,0	20.0	30.0	70.0	20,0	60,0	30,0
TOC (min)	6,9	16.9	10.6	1:9	2.4	5.4	1.8	4.5	2.5
Runoff intensity (mm/hr) ^[2]	212.4	166.3	189.8	274.8	264.9	225.3	276.9	234.7	263.1
Paved area (m²)	5197	9645	4212	2389	2603	3158	982	4135	8540
Runoff coefficient (paved)	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9
Drainage discharge (L/s)	276.2	401.2	200,1	164.2	172.5	178.0	68.0	242.8	562.1
Unpaved area (m ²) ^[3]	Ó	0	0	0.0	0.0	0.0	0.0	0.0	0.0
Runoff coefficient (unpaved)	0.19	0.19	0.19	0.19	0.19	0.19	0.19	0.19	0.19
Drainage discharge (L/s)	0,0	0.0	0.0	0,0	0.0	0.0	0.0	0,0	0.0
Total Drainage discharge (L/s)	276.2	401.2	200.1	164.2	172,5	178.0	68.0	242.8	562.1
Rainfall increased for 2041-2060	10.4%	10.4%	10.4%	10.4%	10.4%	10.4%	10.4%	10.4%	10.4%
Total Drainage discharge with Rainfall increased (L/s)	304.9	442.9	220.9	181.3	190,5	196.5	75.1	268.1	620.6

Note:
[1] A slope of 1:250 is assumed for flat catchment area.
[2] The run-off intensity is calculated by the equation in Section 4.3.3 of the Drainage Manual:

$$i = \frac{a}{(t_a + b)^a}$$

[2] The run-off intensity is some $i=\frac{a}{(t_d+b)^c}$ where Table 3a - Storm Constants for 50 years return period of HKO Headquarters are adopted. a=451.3

$$a = 451.3$$

$$b = 2.46$$

$$c = 0.337$$

[3] There is no unpaved area in the study area.

APPENDIX III Detailed Calculation of Pipe Capacities

Appendix III - Detailed Calculation of Pipe Capacities

Table A - Caculation of Existing Pipe

Pipe No.	Upstream Manhole No.	Downstream Manhole No.	Upstream invert level (mP.D.)	Downstream invert level (mP.D.)	Leugth (m)	Diameter (m)	Area (m³)	Hydraulic Radius (m)	Slope	Kinenmtic Viscosity (m²/s)	Hydraulic Pipeline Roughness (m)	Velocity (m/s)	Full Capacity (L/s)	Catchment	Peak Flow (L/s)	% of fall capacity
							Exis	ting Pipes								
PS B01	SMH4010052	SMH4010053	2.64	2.57	51.2	1.350	1.431	0.338	0.001	I.14E-06	0,003	1,22	1750	Project site B (G/IC) ± B1 +B2 +B3 +B4	1381.1	79%
PS B02	SMH4010053	SMI14010054	2.57	2.54	16.5-	1.350	1.431	0.338	0.002	1.14E-06	0.003	1:41	2021	Project site B (G/IC) + B1 +B2 +B3 +B4	1381.1	68%
PS B03	SM014010054	SMH4010055	2.54	2.49	28.7	1.350	1.431	0.338	0.002	1.14E-06	0.003	1.38	1976	Project site B (G/IC) + B1 +B2 +B3 +B4	1381.)	70%

[11] The roughness coefficient for slimed concrete sewer under poor condition is adopted; the ks values are 3mm for velocities greater than 1.2m/s, otherwise 6mm.

Table B - Calculation of Proposed New Pipe

Pipe No.	Upstream Manhole No.	Downstream Manhole No.	Upstream invert level (mP.D.)	Downstream invert level (mP.D.)	Length (m)	Diameter (m)	Area (m²)	Hydraulic Radius (m)	Slope	Kinematic Viscosity (m²/s)	Hydraulic Pipeline Roughness (m)	Velocity (m/s)	Full Capacity (L/s)	Catchment	Peak Flow	% of full capacity
				•			Propos	d New Pipes								
							Proj	ect Site A							v	
PP A01	STMH-A01	SBP4001321	2.86	2.68	18.2	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.97	556	Project site A	304.9	55%
							Project Site	A - Re-diversi	m							
PP A02	SMH4061012	STMH-A02	3.62	3,50	12.1	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.97	556	A1 ± A2	371.8	67%
PP A03	STMH-A02	STMH-A03	3.50	3,26	24.5	0,600	0.283	0.150	0.010	1.14E-06	0.003	1.94	548	A1 + A2	371.8	68%
PP A04	STMH-A03	STMH-A04	3.26	3.05	21.7	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.94	548	A1+A2	371,8	68%
PP A05	STMH-A04	STMH-A05	3.05	2.70	36.2	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.94	548	A1 + A2	371.8	68%
PP-A06	STMH-A05	STMH-A06	2.70	2.32	39.9	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.94	548	A1 ± A2	371.8	68%
PP A07	STMH-A06	SBP4001321	2.32	2,00	32.6	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.94	548	A1 ± A2	371.8	68%
							Project	Site B (POS)								
PP B01	STMH-B01	SBP4001323	1.84	1.70	13.5	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.97	556	Project site B (POS)	442.9	80%
							Project	Site B (G/IC)								
PP B02	STMH-B02	SMH4010052	4.26	4.00	26.0	0.600	0.283	0.150	0.010	1.14E-06	0.003	1.97	556	Project site B (G/IC)	220.9	40%

^[1] The roughness coefficient for slimed concrete sewer under poor condition is adopted; the ks values are imm for velocities greater than 1.2m/s, otherwise forum.

[2] The upstream and downstream level of proposed pipes will be contirmed by pipe survey in detail design stage.

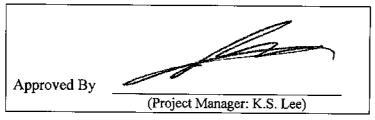
[3] The location of the terminal manhole within the Site is subject to detail design.

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Sewerage Impact Assessment

(V1.0)

September 2021



REMARKS:

The information supplied and contained within this report is, to the best of our knowledge, correct at the time of printing.

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1 INTRODUCTION

1.1 Background

- 1.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). This Sewerage Impact Assessment (SIA) is to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.2 Cinotech Consultants Limited was commissioned by URA to carry out a Sewerage Impact Assessment (SIA) to assess and envisage any potential sewerage impact on the implementation of the proposed development of the Scheme and to recommend necessary pipe upgrading/diversion as necessary.

2 DESCRIPTION OF THE ENVIRONMENT

2.1 Existing Environment

- 2.1.1 The Scheme SSP-018 consists of Sites A and B. Site A is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the south-western boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary (Figure 2-1). The proposed gross site areas of the Site A & Site B are 5,197m² and 13,857m² respectively, subject to site survey and detailed design.
- 2.1.2 Currently, the Site A comprises a single storey Cheung Sha Wan Sports Centre and its associate outdoor garden and playground. The Site B comprises a government land lot (GLA-TNK 1723) which currently is an open area with a few 1-2 storeys temporary structures, Cheung Sha Wan Path Sitting-out Area, and a garden associated with Sham Shui Po Sports Ground.

2.2 The Proposed Development

- 2.2.1 The entire Site A is proposed to rezone to "R(A)" and redevelop the area for high-density residential development, with non-domestic uses always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of a building. The proposed development on Site A consists of a 2 floors of basement carpark, a 5 storeys podium (GFA: ~5,197m² for G/IC area, and ~5,197m² for Commercial area) and two 34 storeys residential towers (838 flats).
- 2.2.2 Western part of the Site B is proposed to rezone to G/IC and provide a G/IC complex with GFA of 33,696 m² for community and amenity. The rest of the Site B of about 9,645 m², is proposed to be public open space.
- 2.2.3 The proposed notional scheme is shown in Appendix I. The notional design is subject to change at detailed design stage.

3 SEWERAGE IMPACT ASSESSMENT

3.1 Sewage Discharge from the Scheme

3.1.1 Based on the population by-census 2016, the average domestic household size in Sham Shui Po District Council Constituency Area is 2.6 persons, therefore the design residential population is about 1928 persons (838 flats × 2.6). The population of restaurant, retail and G/IC are estimated according to the usable floor area (UFA) per person and the worker density from Figure 9 of Commercial and Industrial Floor Space Utilization, published by Planning Department. **Table 3-1** indicates the population calculation of the Site A and Site B. It should be note that GFA ratio of *Clubhouse : Retails : Restaurant* is assumed to be 10%: 45%: 45%. As the sewage discharge per unit area for restaurant is much higher than the other two and the assumed ratio of restaurant is on high side, this assumption is considered conservative.

Table 3-1 Estimation of Population

Section		Non-	Population Factor		Population		
	No. of Flat [1]	residential GFA (m²)	No. of person per flat [3]	Residential Population	Worker Density (worker/100 m²)	No. of Employee	
			Site A				
Residential	838		2.6	2179	-		
Restaurant	-	2338.65			5.1	119	
Retail		2338.65	-	1 3 4 1 M	3.5	82	
Clubhouse		519.7	H - H	- 2 - 4	3.3	17	
G/IC	-	5197			3.3	172	
			Site B				
G/IC	-	33733			3.3	1113	

[1] No. of flats and GFA are provided by URA

3.1.2 The estimated contributing population, sewage flow rate and peak flow from Site A and Site B are summarised in Table 3-2. The peak flow are 59.2 L/s and 21.7 L/s for Site A and Site B respectively, applying the peaking factor including stormwater allowance of 6 for the contribution population between 1,000 to 5,000.

^[2] It is assumed that the GFA ratio of Clubhouse : Retails : Restaurant = 10% : 45% : 45%.

^[3] The average domestic household size is 2.6 persons for Sham Shui Po, according to Population By-census 2016. Source from (http://www.bycensus2016.gov.hk/en/bc-dp.html).

^[4] The worker densities for different sections are from Figure 9 of Commercial and Industrial Floor Space Utilization Survey.

Table 3-2 Calculation of Sewage Discharge

Occupant Type	Unit Flow Factors [1] [4] (m3/day/person)	No. of Occupants / Employee	Flow Rate (m³/day)	Contributing population [2]	Peak Factor	Peak Flow (L/s)				
		Site A								
Residential	0.27	2179	588.3		- 2	-				
Restaurant	1.58	119	188.0	-	4.	-				
Retail	0.28	82	23.0	-	+	-				
Clubhouse	0.28	17	4.8	7-	-	-				
G/IC	0.28	172	48.2		-	4				
Total		1-0	852.2	3157	6	59.2				
	Site B									
G/IC	0.28	1113	311.6	F						
Total	1 2 5 - 4	- 5 E	311.6	1155	1 1	21.7				

EPD's Guidelines for Estimating Sewage Flows for Infrastructure Planning defining sewage flow parameter.

3.2 Sewage Discharge from the Vicinity

- 3.2.1 The surrounding developments near the Scheme is sectioned into different catchments based on the existing sewerage system. The sewage catchment areas in the vicinity are shown in Figure 3-1 & Figures 3-2a 3-2f and the estimated sewage discharges from each catchment are summarised in Table 3-3. The population and detailed calculation of flow rate is presented in Appendix II.
- 3.2.2 It should be noted that the actual sewage discharge route of Cheung Sha Wan Catholic Secondary School (Catchment A), as well as Gee Hing Chang Industrial Building and Precious Industrial Centre (Catchment E) are uncertain due to the lack of information in the relevant record plans. Based on the best available information, assumption has been made that Catchment A discharged to sewer manhole FMH4009911 (upstream of Site A) and two developments in Catchment E discharged to sewer manhole FMH4009982 (downstream of Site B, upstream of PS B02). The said proposal will be subject to change upon verification of the sewerage discharge route of the above developments at subsequent detailed design stage.

^[2] The contribution population for Site A is 852.2 (m³/day) / 0.27(m³/day/person) = 3157 and the contribution population for Site B is 311.6 (m³/day) / 0.27(m³/day/person) = 1155

^[3] Peaking Factor of 6 and 8 for contributing population 1,000-5,000 and <1,000 respectively and the operation hour is assumed to be 24 hours. The peak flow is the sum of flow rate of each occupant type x peaking factor.

^[4] The Unit Flow Factors are 0.27, 1.58, 0.28, 0.28, m3/day/head for Residential, Restaurant, Retail and Clubhouse respectively.

Table 3-3 Sewage Discharge from Surrounding Catchments

Catchment ID	Development	Total Flowrate / catchment (m³/day)	
A	Cheung Sha Wan Catholic Secondary School	38.6	
В	Fuk Wing Street (Cheung Wah Street to Castle Peak Road) & Fuk Wa Street (Cheung Wah Street to Castle Peak Road)	1168.6	
	571 Fuk Wa Street		
	561 Fuk Wa Street		
	11-13A Cheung Wah Street		
C	Charming Garden (長盛豪苑) (638 Cheung Wah Street)	361.5	
	Furture development on Land Slot NKIL 2197 RP		
D	650-646 Cheung Wah Street (Tower)	272.5	
D	650-646 Cheung Wah Street (Podium)	372.5	
D.	Gee Hing Chang Industrial Building	169.7	
E	Precious Industrial Centre	168.7	

^{*} The calculation is detailed in Appendix II.

3.3 Review Sewerage System

- 3.3.1 Since the sewage discharge from the Scheme is expected to increase after the development, the downstream sewers shall be checked for sufficient capacities to cater sewerage discharge.
- 3.3.2 The capacities of the downstream foul sewer pipe sections (PS A01 PS A10 and PS B01 PS B06, Figure 3-1, & Figures 3-2a 3-2f) are calculated by Colebrook-White Equation and listed in Table 3-4. The detailed calculation is shown in Table A of Appendix III.

Table 3-4 Capacity of Existing Foul Sewers

Pipe Section	Upstream Manhole	Downstream Manhole	Full Capacity (L/s	
	Sit	e A		
PS A01	FMH4009914	FMH4009915	339.4	
PS A02	FMH4009915	Unknown	449.4	
PS A03	Unknown	FMH4009917	293.0	
PS A04	FMH4009917	FMH4009918	355.9	
PS A05	FMH4009918	FMH4009919	404.7	
PS A06	FMH4009919	FMH4010450	384.5	
PS A07	FMH4010450	FMH4010451	377.1	
PS A08	FMH4010451	FMH4010452	362.6	
PS A09	FMH4010452	FMH4010453	1224.1	
PS A10	FMH4010453	FMH4010454	3640.3	
	Sit	e B		
PS B01	FMH4009981	FMH4009982	1559.7	
PS B02	FMH4009982	FMH4009983	1077.5	
PS B03	FMH4009983	FMH4009984	1431.9	
PS B04	FMH4009984	FMH4009985	1431.9	
PS B05	FMH4009985	FMH4009986	1431.9	
PS B06	FMH4009986	FMH4009987	1431.9	
	Upstream P	ipe Sections		
US 01	FMH4009910	FMH4009911	343.2	
US 02	FMH4045944	FMH4045945	791.9	
US 03	FMH4009974	FMH4009975	600.4	

^[1] The Manhole ID of the sewage manhole between sewers PS A02 & PS A03 is not available.

- 3.3.3 The utilization calculation adopts the following assumptions/configurations:
 - The Upstream Pipes US 01, US02 & US03 is assumed to be fully utilized (Figures 3-1, 3-2a & 3-2c).
 - For the calculation of peak flow of PS A01 PS A10, 100% of the discharge from Catchments C & D are included for conservative assessment (Figure 3-2a).
 - For the calculation of peak flow of PS B01 PS B06, 100% of the discharge Upstream
 Pipe US 03 are included for conservative assessment (Figure 3-2d).
 - No sewage flow is anticipated along the 2 x 300m sewers between FMH4009977 & FMH4009979 (Figure 3-2d, in the south of catchment D) under normal condition. It is because their invert level (up to 3.96mPD) are more than 1m higher than the other connected sewers. Therefore, only discharge from Upstream Pipe US 03 and Site B will reach PS B01. The potential discharge from Catchments C & D (and other upstream areas) can only reach PS B01 via Upstream Pipe US 03.
 - The sewage from Site A & Site B will discharge to FMH4009914 & PMH4009981 respectively, the details will be provided in later sections.
- 3.3.4 Table 3-5 shows a summary of the proportion of peak flow to full capacity from surrounding catchment areas to each segment of existing pipe sections. The detailed calculation is shown in Tables B of Appendix III.

^[2] The invert level between FMH4009984 and FMH4009986 (Downstream of PS B03 to Upstream of PS B06) are not available. Average slope has been adopted.

Table 3-5 Proportion of Peak Flow to Full Capacity (Existing Pipes)

able 5-5 I roportion of a care a row to a unit capacity (Existing a specify						
Full Capacity (L/s)	Total Peak Flow (L/s)	Total Discharge Loading to Pipe Capacity (%)				
	Site A					
339.4	511.3	151%				
449.4	511.3	114%				
293.0	511.3	175%				
355.9	511.3	144%				
404.7	511.3	126%				
384.5	511.3	133%				
377.1	511.3	136%				
362.6	511.3	141%				
1224.1	511.3	42%				
3640.3	1303.2	36%				
	Site B					
1559.7	628.5	40%				
1077.5	643.7	60%				
1431.9	643.7	45%				
1431.9	643.7	45%				
1431.9	643.7	45%				
1431.9	643.7	45%				
	Full Capacity (L/s) 339.4 449.4 293.0 355.9 404.7 384.5 377.1 362.6 1224.1 3640.3 1559.7 1077.5 1431.9 1431.9	Full Capacity (L/s) Total Peak Flow (L/s) Site A 339.4 511.3 449.4 511.3 293.0 511.3 355.9 511.3 404.7 511.3 384.5 511.3 377.1 511.3 362.6 511.3 1224.1 511.3 3640.3 1303.2 Site B 1559.7 628.5 1077.5 643.7 1431.9 643.7 1431.9 643.7 1431.9 643.7				

^{*} Bold for surcharged pipe.

- 3.3.5 For Site A, PS A01 PS A08 are required to be upgraded due to that the capacity are more than 100% full with the proposed redevelopment. PS A01 PS A08 are proposed to be upgraded to 900mm. Upon this chance, the slope of each sewer segment can also be even out.
- 3.3.6 For Site B, the full capacities of each sewer segment are far from fully utilized and therefore there is no sewer pipe need to be upgraded.
- 3.3.7 The discharge loading and capacity of the upgrading pipe sections are shown in **Table 3-6** and the detailed calculation can be found in **Appendix IV**.

Table 3-6 Proportion of Peak Flow to Full Capacity after Upgrading

Segment	Full Capacity (L/s)	Total Peak Flow (L/s)	Total Discharge Loading to Pipe Capacity (%)
PS A01	627.6	511.3	81%
PS A02	627.6	511.3	81%
PS A03	627.6	511,3	81%
PS A04	627.6	511.3	81%
PS A05	627.6	511.3	81%
PS A06	627.6	511.3	81%
PS A07	627.6	511.3	81%
PS A08	627.6	511.3	81%

3.3.8 The sewage discharge from Site A is proposed to be collected by a terminal manhole (FTMH01) and discharged via proposed pipe (PP01) to existing manhole FMH4009914. For Site B, the sewage discharge is proposed to be collected by a new terminal manhole (FTMH02) and discharged via proposed pipe (PP02) to existing manhole (FMH4009981). The diameter and slope of both PP01 & PP02 are 300mm and 1:100 respectively. The proposed new pipe is presented in **Table 3-7**. The location of the proposed upgrade and new

pipes are shown in Figures 3-3a - 3-3c, the exact location of the new manholes and invert level will subject to future detail design.

Table 3-7 Proportion of Peak Flow to Full Capacity (Proposed New Pipes)

Segment		Proposed New Pipe [1]		Full	Total	Total Discharge	
	Catchment	Upstream Invert Level (mPD)	Downstream Invert Level (mPD)	Diameter (mm)	Capacity (L/s)	Peak Flow (L/s)	Loading to Pipe Capacity (%)
PP01	Site (A)	1.10	1.00	300	87.9	76.9	88%
PP02	Site (B)	2.15	1.95	300	87.9	28.1	32%

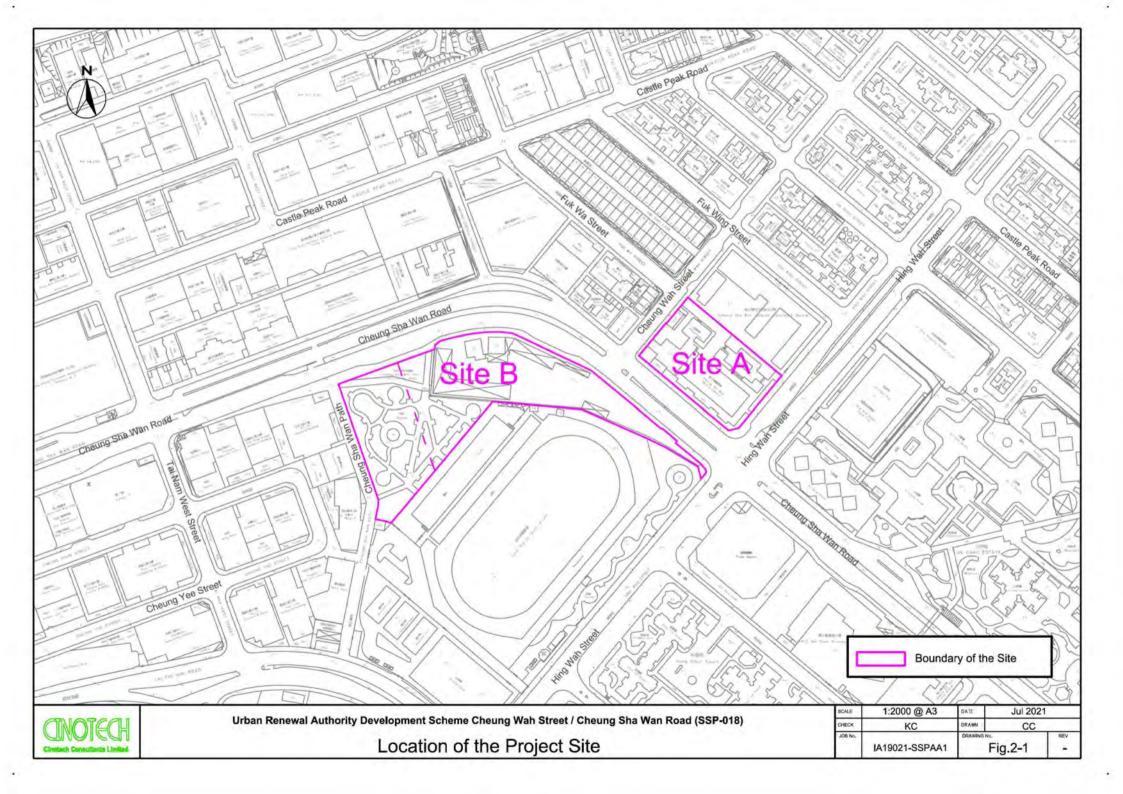
^[1] The upstream and downstream level of proposed pipes will be subject to detail design.

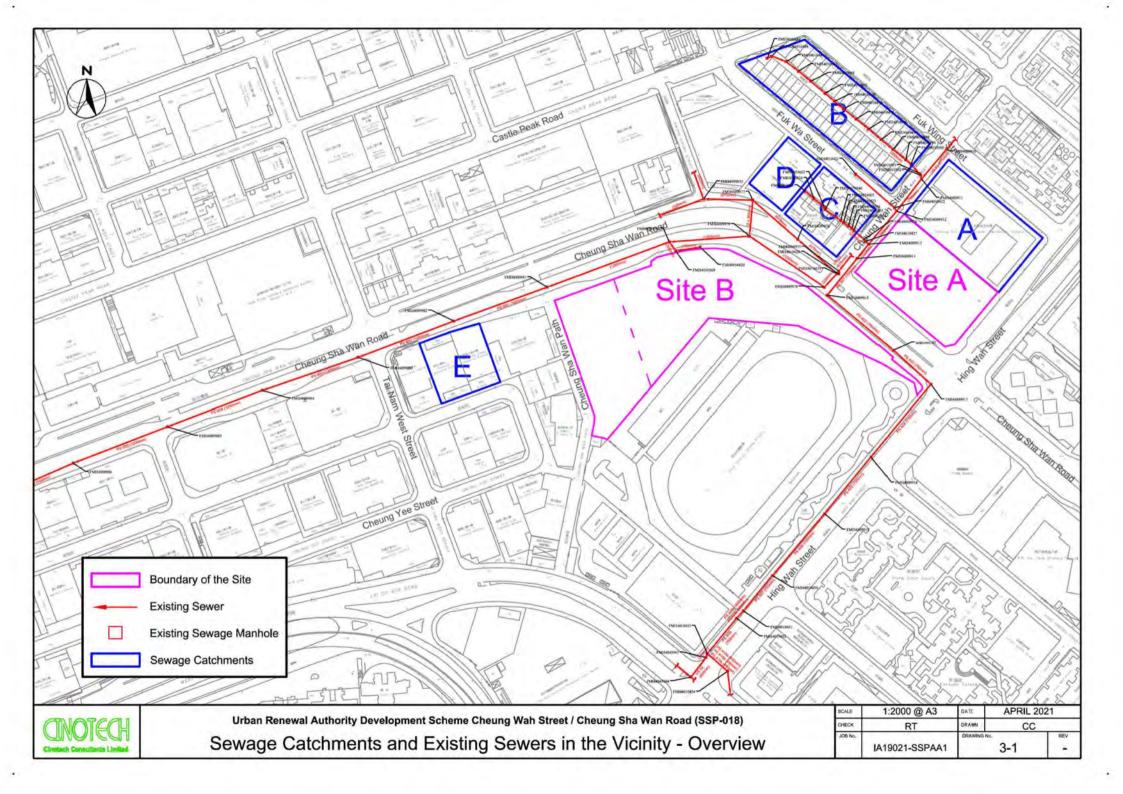
3.3.9 The project proponent (URA) will be responsible for all of the sewers laying and upgrading works related to the Scheme, including the aforementioned proposed new/upgrade sewers.

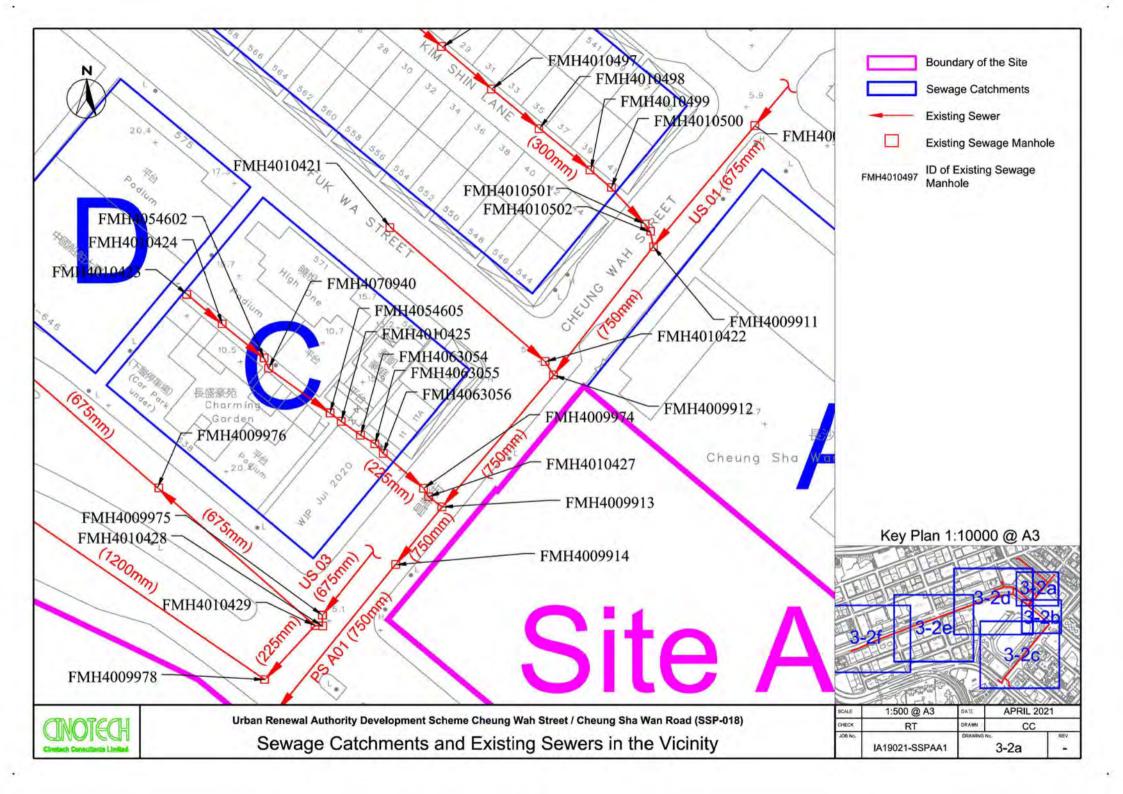
4 CONCLUSION

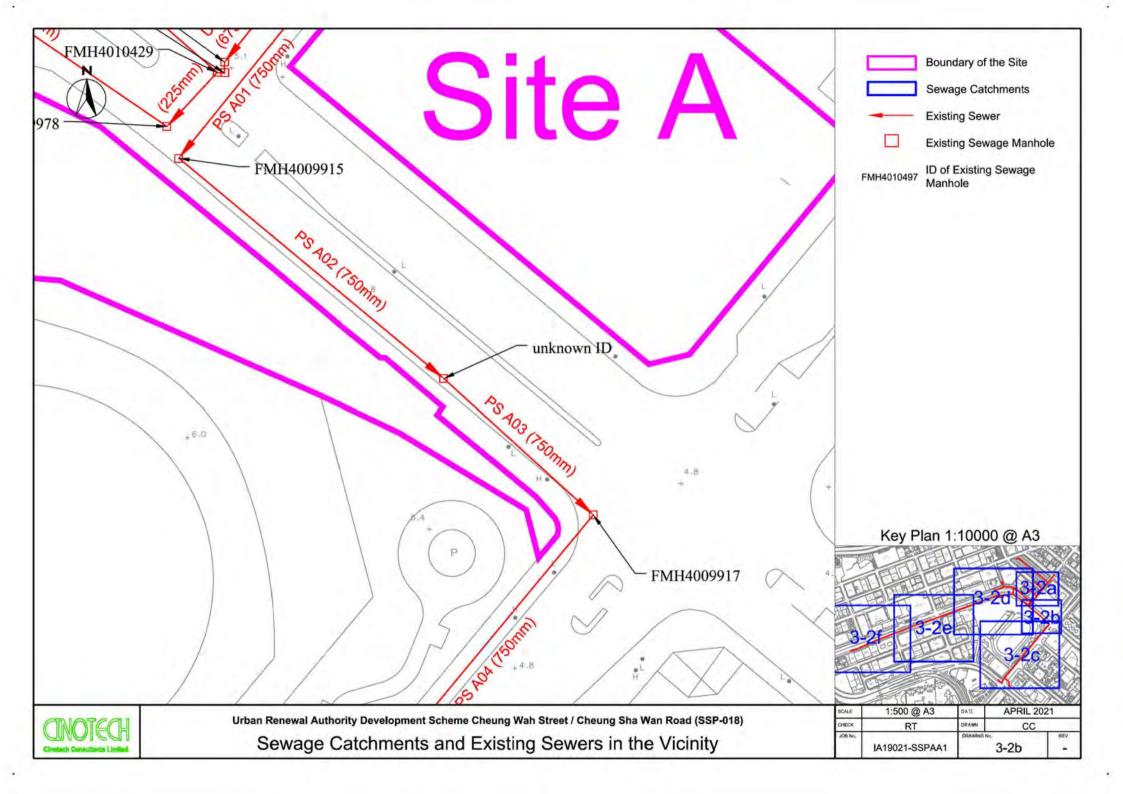
- 4.1.1 The Development Scheme proposes to redevelop a composite development at Site A, which consists of 2 residential towers which providing about 838 flats, 2 floors of basement carpark, as well as a 5 storeys podium with ~5,197m² for G/IC area, and ~5,197m² for Commercial area. The Development Scheme also proposes a G/IC complex with GFA of ~33,733 m² for G/IC facilities at Site B.
- 4.1.2 The estimated daily sewage discharge from the proposed the composite development at Site A and G/IC complex at Site B are 852.2 m³/day and 311.6 m³/day respectively. The sewage effluent from the proposed Site A will be collected by the terminal manhole FTMH01 and ultimately discharge to the public sewer at manhole FMH4009914. Terminal manhole FTMH02 will collect the sewage effluent from the proposed Site B and connect to the public sewage at manhole FMH4009981. Two pipes (PP01 and PP02) are proposed to cater the sewage discharge of the proposed development in the Scheme. The diameters of the proposed pipes are both 300mm (Figures 3-3a & 3-3c refers). The slopes of both proposed pipes are 1:100. Eight existing sewers between manhole FMH4009914 & FMH4010452 are proposed to be upgraded from 750mm to 900mm, with average slope of ~0.0018 to cater the peak sewage flow (Figures 3-3a & 3-3b refers). Actual layout and inverts levels of the proposed pipes are subject to detail design.
- 4.1.3 With the proposed new and upgraded sewers, the sewage network is considered to have sufficient capacities to cater the expected sewage flows from the proposed development of the Scheme and the surrounding catchments. Therefore, no adverse sewerage impact on the public sewerage system is expected from the proposed development.

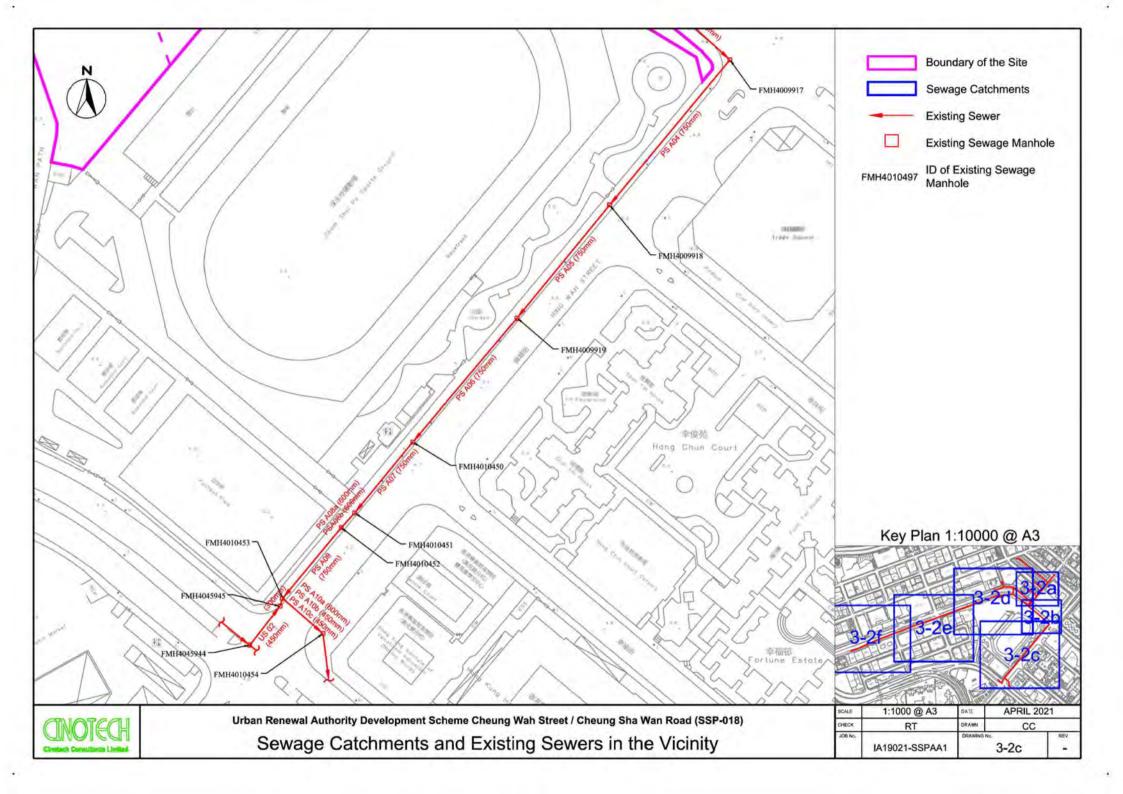
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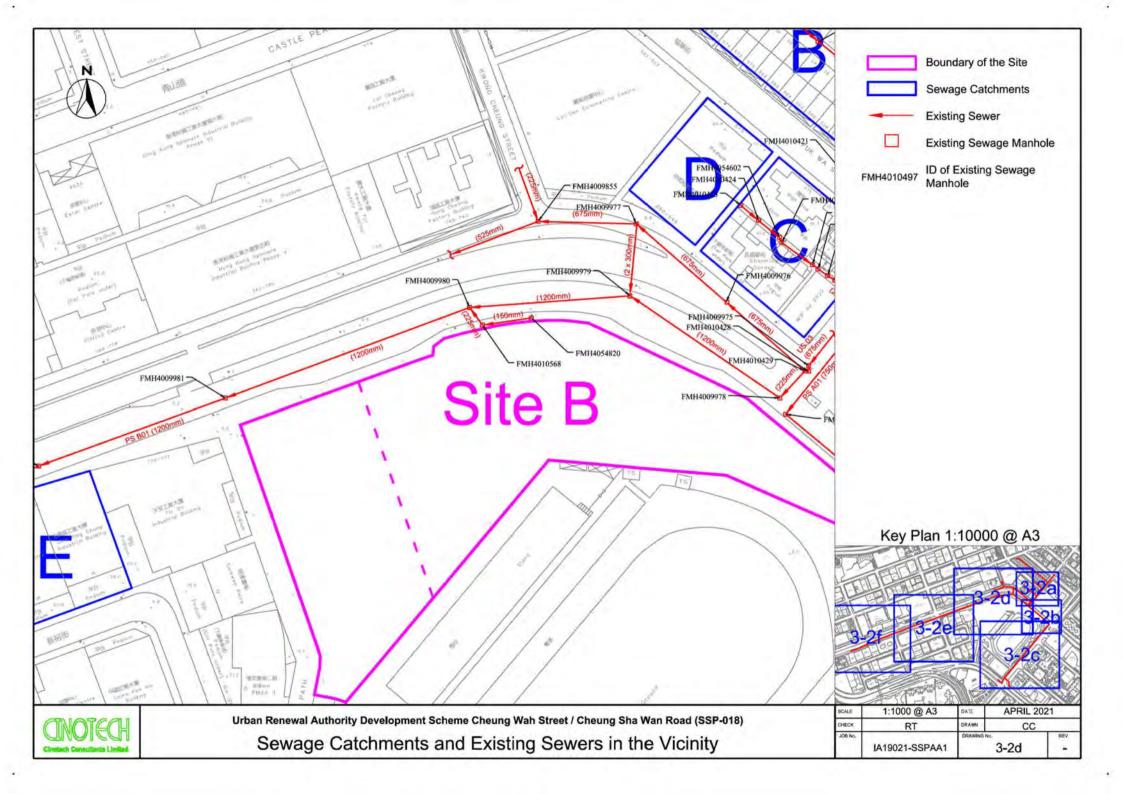


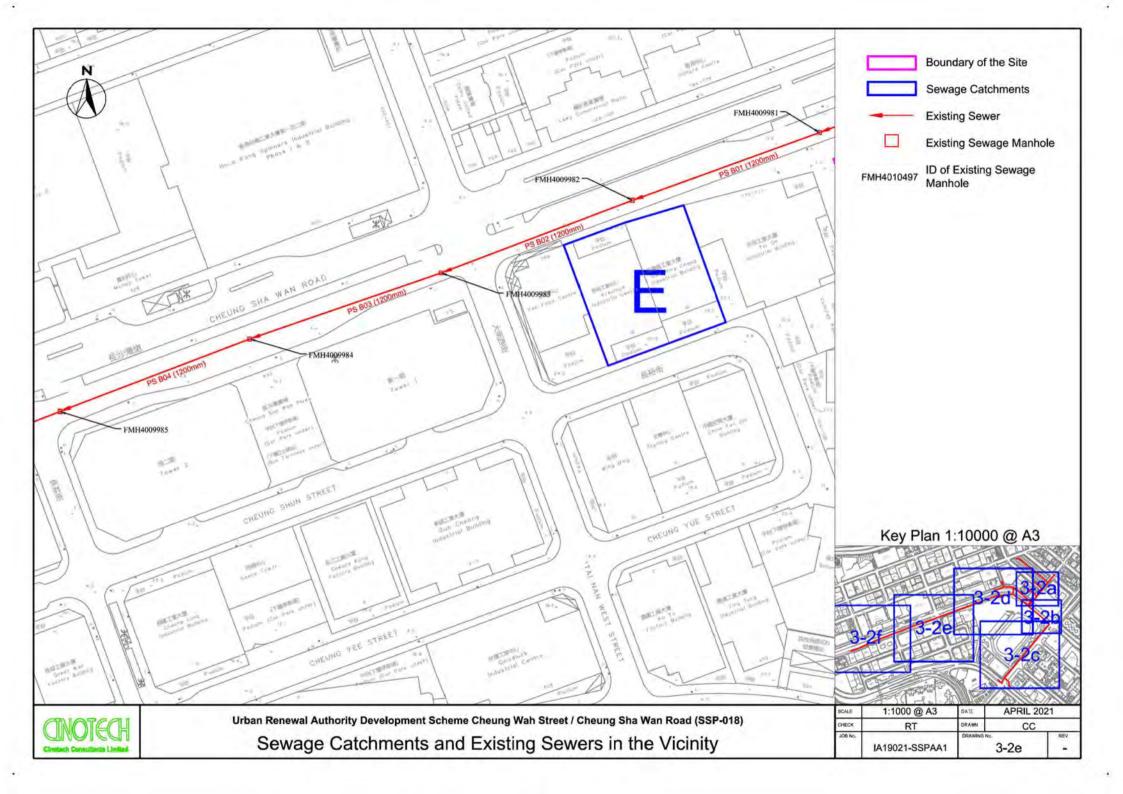


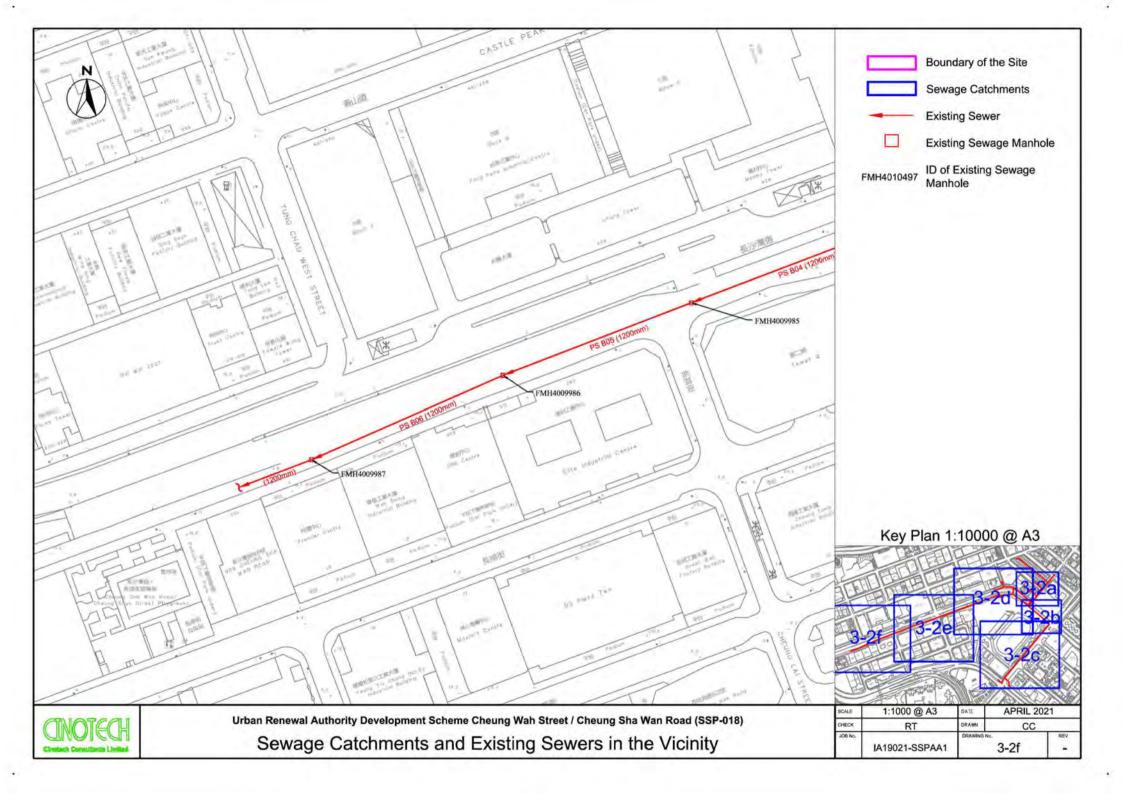


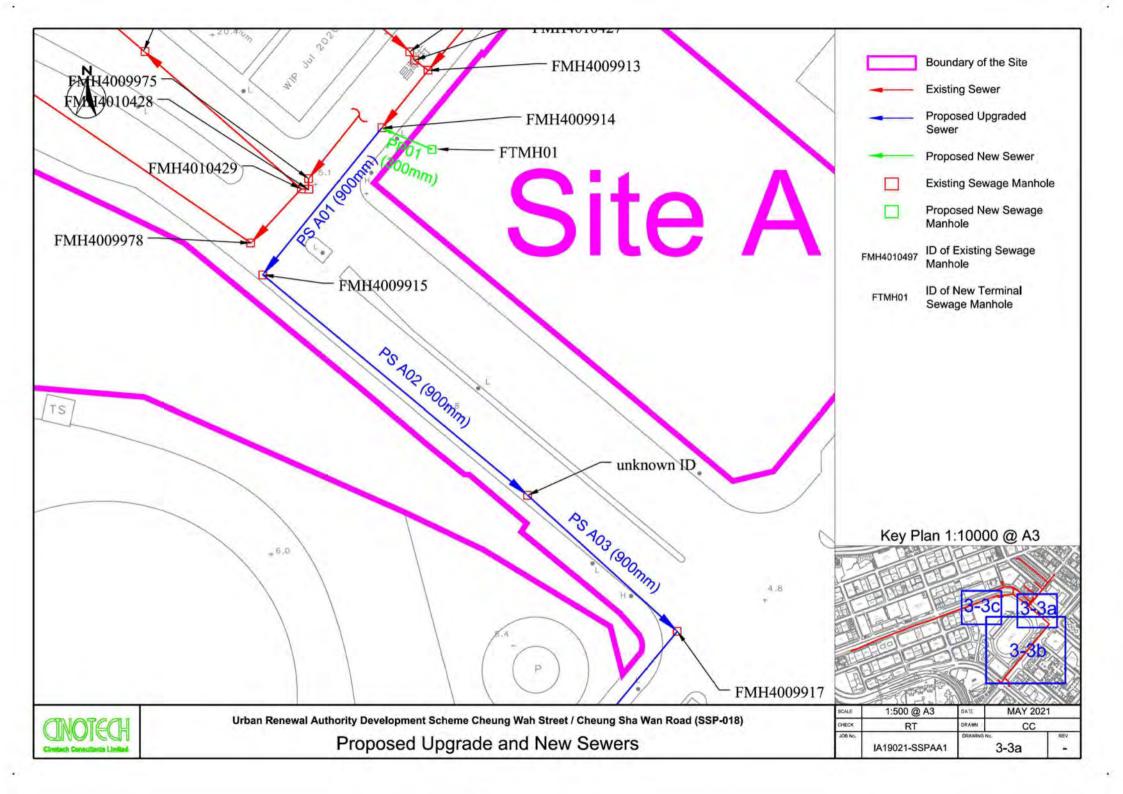


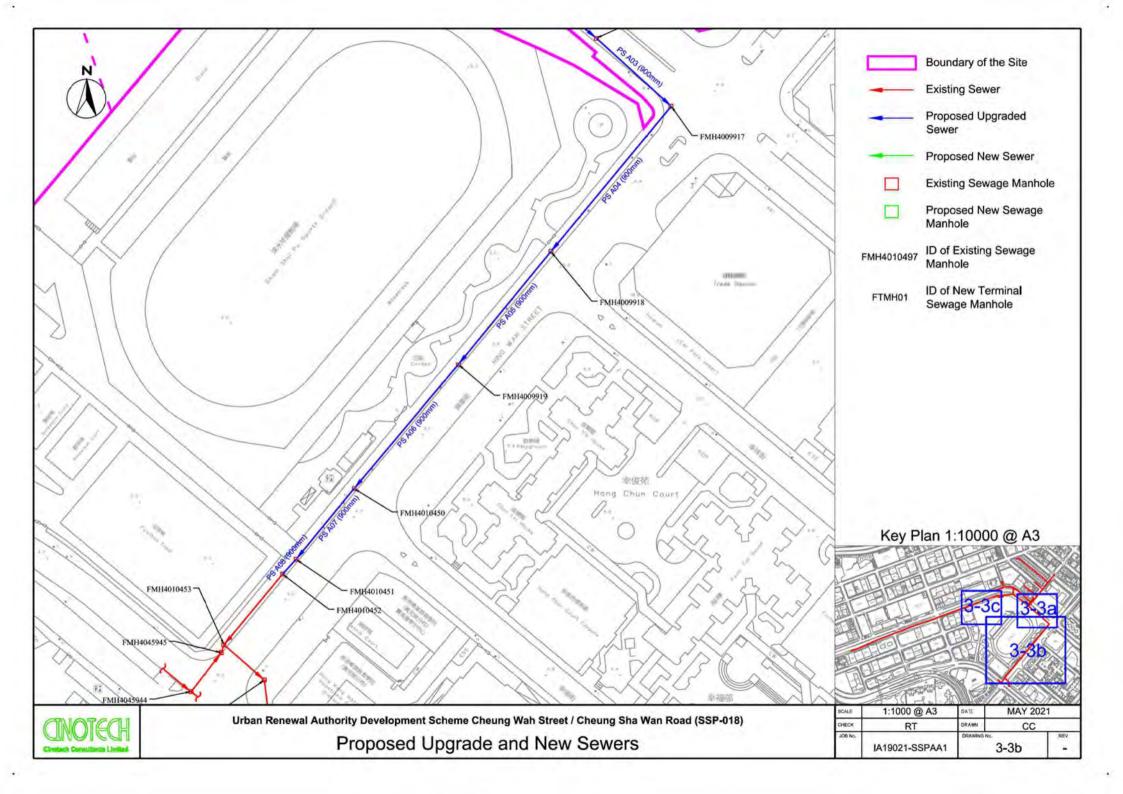


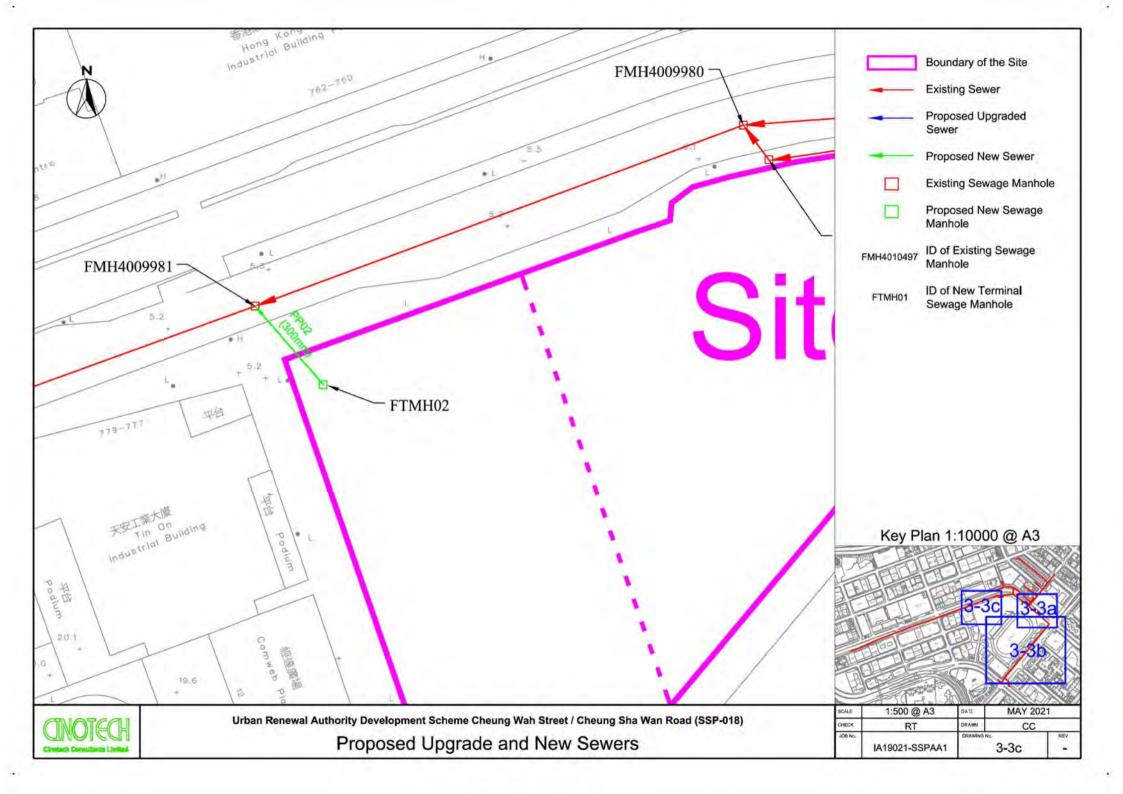




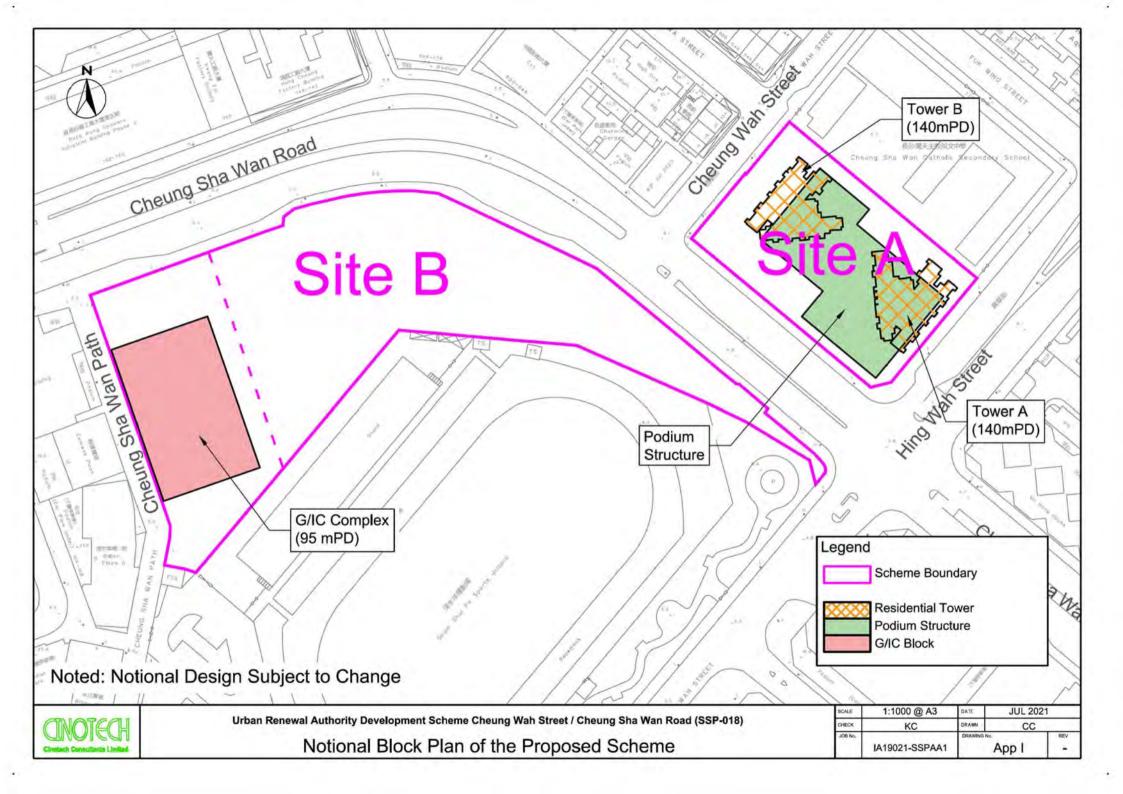


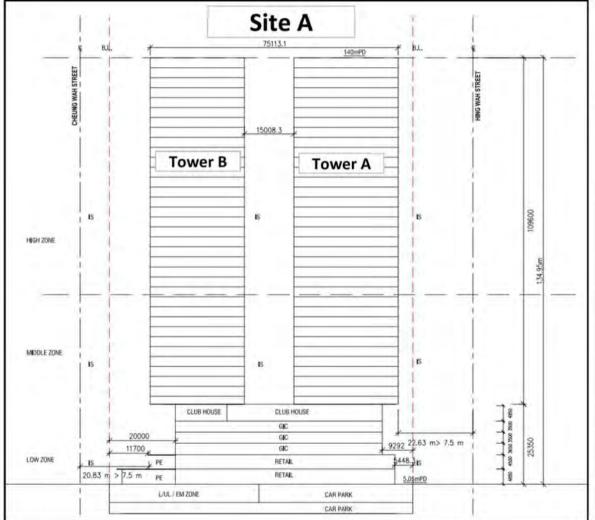


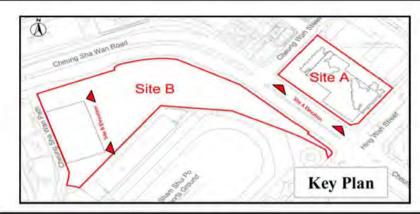


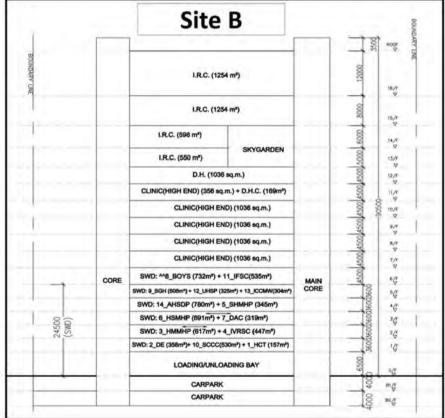


Appendix I Notional Block Plan of the Proposed Scheme









Remark:

Notional Design subject to change at detailed design stage



Urban Renewal Authority Development Scheme Cheung Wah Street/ Cheung Sha Wan (SSP-018)

Notional Section Plan of the Proposed Scheme

SCALE	N.T.S.	DATE	Jun-21				
CHECK	KC	DRAWN		CC			
JOB NO.	IA9021-5SPAA1	FIGURE NO.	APP I	REV.			

Appendix II
Sewage Discharge from Surrounding Catchments

Appendix II: Sewage Discharge from Surrounding

													Pepulation				
Catchment ID	Building	No. of Flats	Ne of Sheps	No. ef Restaurants	Retail Area (m²) ^[1]	Restaurant Area (m²) ⁽ⁱ⁾	Commercial Area (m²) ⁽³⁾	ledestrial Area (m²) ⁽ⁱ⁾	Residential (वेहन	Retall/ Shop (Staff) ⁽⁴⁾	Restaurants (Staff) ^[4]	School (Staff) ⁽⁵⁾	School (Student) ⁽⁶⁾	Retall (staff) ^[6] by worker density	Restaurant (staff) ¹⁴ by worker density	Commercial (Staff) ^M by worker density	Industrial (Stuff) ^[6] by worker density
A	Cheung Sha Wan Catholic Secondary School	-	-		-	-	•	-		-	-	61	842	-	•	•	-
В	Fuk Wing Street (Cheung Wah Street to Castle Peak Road) & Fuk Wa Street (Cheung Wah Street to Castle Peak Road) [3]	[3]	40	24	-	-	-	-	3543	80	120	-	-	-	-	-	
	571 Fuk Wa Street	187	-	-	•	-	•	-	486	•	5	•	-	•			-
	561 Fuk Wa Street	21	-	ı	-	-	-	-	55	-	5	-	-	-	-	-	-
С	11-13A Cheung, Wah Street	20	3	2	-	-		-	52	6	10	·	-	-			-
	Charming Garden (長盛豪苑) (638 Cheung Wah Street)	112	2	2	-	-	-	-	291	4	10	-	-	-	-	-	-
	Furture development on Land Slot NKIL 2197	78	-	-	202.5	202.5		-	203	-	-	-	-	7	10	-	-
	650-646 Cheung Wah Street (Tower)	-	-	-	-	-	11172	-	-	-	-	-	-	-	-	659	-
D	650-646 Cheung Wah Street (Podium)	-	-	-	-	2327.5		-		-	-	-	-	-	119		-
F.	Gee Hing Chang Industrial Building	-	1	-	-	-	-	6768.3	-	2	-	-	-	-	-	-	156
E	Precious Industrial Centre	-	3	-	-	-	-	6860.7	-	6	-	-	-	-	•	-	158

Notes:

- [1] Estimated value
- [2] The average domestic household size is 2.6 persons for Sham Shui Po, according to Population By-census 2016. Source from (http://www.bycensus2016.gov.hk/en/bc-dp.html).
- [3] The population for Large Street Block Groups (No: 26123) is reference to Population By-census 2016. Source from (http://www.bycensus2016.gov.hk/en/bc-dp.html).
- [4] The density of 2 employees per a retail/shop and 5 employees per a restaurant is based on site survey.
- [5] The number of teacher and student of Cheung Sha Wan Catholic Secondary School are reference to School Annual School Report 2019-2020
- The worker density for Commercial Area (5.9 employee per 100 m²), Restaurant Area (5.1 employee per 100 m²), Retail Area (3.5 employee per 100 m²) and Industrial Area (2.3 employee per 100 m²) are from Figure 9 and 10 of Commercial and Industrial Floor Space Utilization Survey 2005.
- [7] The Unit Flow Factors are 0.27, 0.28, 0.04, 1.58 and 0.53 m³/day/head for residential use, retail/office/commercial/School(Staff), School Student, restaurants and industrial use, respectively.
- [8] Number of flats are reference to Centaline Property https://hk.centanet.com/estate/.
- [9] Number of flats are reference to Midland Realty /https://www.midland.com.hk/en/
- [10] It is assumed that the Furture development on Land Slot NKIL 2197 RP consists of 26 storeys of residential tower with 3 flats per floor. The non-residential area is estimated by allowable the plot ratio according to OZP (1.5 for non-residential).

Appendix II: Sewage Discharge from Surrounding

	in. Bewage Discharge i]	Howrate (m³/da	y) ^[7]					
Catchment ID	Building	Residential UFF=0,27	Retail/Shop UFF=0.28	School (Staff) UFF=0.28	School (Student) UFF=0.04	Restaurants UFF=1,58	Commercial UFF=0.28	Industrial UFF=0.53	Flowrate / catchment (m³/day)	Total Flowrate / catchment (m³/day)	Reference
A	Cheung Sha Wan Catholic Secondary School		-	4.9	33.7	-		-	38.6	38.6	•
В	Fuk Wing Street (Cheung Wah Street to Castle Peak Road) & Fuk Wa Street (Cheung Wah Street to Castle Peak Road) [3]	956.6	22.4		•	189.6		-	1168.6	1168.6	
	571 Fuk Wa Street	131.2	-	-	-	7.9		-	139.1		Centaline Property ^[8]
	561 Fuk Wa Street	14,9	-	-	-	7,9	-	-	22.8		Centaine Property
с	11-13A Cheung Wah Street	14.0	1.7	-		15.8		-	31.5	361.5	1612 15 1 91
	Charming Garden (長盛豪苑) (638 Cheung Wah Street)	78.6	1.1	-	-	15.8	-	-	95.5		Midland Realty ^[9]
	Furture development on Land Slot NKIL 2197 RP [10]	54.8	2.0	-	-	15.8		-	72.6		
D	650-646 Cheung Wah Street (Tower)	-	-	-	-	-	184.5	-	184.5	372.5	
D D	650-646 Cheung Wah Street (Podium)		-	-	-	188.0		-	0.881	312.5	-
TC.	Gee Hing Chang Industrial Building		0.6	-	-	-	-	82.7	83.2	160.7	
E	Precious Industrial Centre	-	1.7	-	-	-	-	83.7	85.4	168.7	•

Notes:

[2]

[6]

[1] Estimated valu

The average domestic household size is 2.6 persons for Sham Shui Po, according to Population By-census 2016. Source from (http://www.bycensus2016.gov.hk/en/bc-dp.html).

[3] The population for Large Street Block Groups (No: 26123) is reference to Population By-census 2016. Source from (http://www.bycensus2016.gov.hk/en/bc-dp.html).

[4] The density of 2 employees per a retail/shop and 5 employees per a restaurant is based on site survey.

[5] The number of teacher and student of Cheung Sha Wan Catholic Secondary School are reference to School Annual School Report 2019-2020

The worker density for Commercial Area (5.9 employee per 100 m2), Restaurant Area (5.1 employee per 100 m2), Retail Area (3.5 employee per 100 m2) and Industrial Area (2.3 employee per 100 m2) are from Figure 9 and 10 of Commercial and Industrial Floor Space Utilization Survey 2005.

[7] The Unit Flow Factors are 0.27, 0.28, 0.04, 1.58 and 0.53 m3/day/head for residential use, retail/office/commercial/School(Staff), School Student, restaurants and industrial use, respectively.

[8] Number of flats are reference to Centaline Property https://hk.centanet.com/estate/.

[9] Number of flats are reference to Midland Realty /https://www.midland.com.hk/en/

[10] It is assumed that the Furture development on Land Slot NKIL 2197 RP consists of 26 storeys of residential tower with 3 flats per floor. The non-residential area is estimated by allowable the plot ratio according to OZP (1.5 for non-residential).

Appendix III

Detailed Calculation of Existing Sewage Discharge

Appendix III: Calculation of Existing Pipe Capacity

Table A - Pipe Capacity Calculation

Segment	Upstream Manhole	Downstream Manhole	Upstream Invert Level (mPD)	Downstream Invert Level (mPD)	Length (m)	Diameter (mm)	Diameter (m)	Area (m²)	Hydraulic Radius (m)	Slope	Kinematic Viscosity (m ² /s)	Hydraulic Pipeline Roughness (m) ^[1]	Velocity (m/s)	Full Capacity (1/8)	Remark
	*				Existin	g Pipes									
							Site A								
PS A01	FMH4009914	FMH4009915	1	0.95	35.3	750	0.75	0,442	0.1875	0.0014	0.00000114	0.006	0.77	339,4	
PS A02	FMH4009915	Unknown	0.95	0.79	64.5	750	0.75	0.442	0.1875	0.0025	0.00000114	0.006	1.02	449.4	p =
PS A03	Unknown	FMH4009917	0.79	0.75	37.8	750	0.75	0.442	0.1875	_0.0011	0.00000114	0.006	0.66	293.0	1.
PS A04	FMH4009917	FMH4009918	0.75	0.64	70.6	750	0.75	0.442	0.1875	0.0016	0.00000114	0.006	0.81	355,9	
PS A05	FMH4009918	FMH4009919	0.64	0.53	54.6	750	0.75	0.442	0.1875	0.0020	0.00000114	0.006	0.92	404.7	
PS A06	FMH4009919	FMH4010450	0,53	0.42	60.5	750	0,75	0,442	0.1875	0.0018	0.00000114	0.006	0.87	384.5	
PS A07	FMH4010450	FMH4010451	0.42	0.36	34.3	750	0.75	0.442	0.1875	0.0017	0.00000114	0.006	0,85	377,1	
PS A08	FMH4010451	FMH4010452	0.34	0,33	7.5	114		55		4			1.0	362,6	PS A08 consists of two pipes: PS A08a and A08b
PS A09	FMH4010452	FMH4010453	0.33	-0.18	34.3	750	0.75	0.442	0.1875	0.0149	0.00000114	0.003	2.77	1224.1	
PS A10	FMH4010453	FMH4010454	100	8	20,1	94	14	*		101	in.	127	-	3640.3	PS A10 consists of three pipes: P A10a, A10b & A10c
	*						Site B								
PS B01	FMH4009981	FMH4009982	1.95	1.8	74.3	1200	1.2	1.131	0.3	0.0020	0.00000114	0.003	1.38	1559.7	
PS B02	FMH4009982	FMH4009983	1.8	1.71	76.6	1200	1,2	1.131	0.3	-0.0012	0.00000114	0.006	0.95	1077,5	
PS B03	FMH4009983	EMH4009984	1.71	1.58	75.8	1200	1.2	1.131	0.3	0.0017	0.00000114	0.003	1.27	1431.9	
PS B04	FMH4009984	FMH4009985	1.58	1.45	76.0	1200	1.2	1.131	0.3	_0.0017	0.00000114	0.003	1.27	1431.9	i t
PS B05	FMH4009985	FMH4009986	1.45	1.32	75.5	1200	1.2	1.131	0,3	0.0017	0.00000114	0.003	1,27	1431.9	
PS B06	FMH4009986	FMH4009987	1.32	1.19	78.3	1200	1.2	1.131	0.3	0.0017	0.00000114	0.003	1.27	1431.9	1
	A COLUMN TO STATE OF THE PARTY					Upstr	eam Pipe Se	ections				- A- 6			
US 01	FMH4009910	FMH4009911	1.36	1.28	29.5	675	0.675	0.358	0.16875	0.0025	0.00000114	0.006	0.96	343.2	
US 02	FMH4045944	EMH4045945	1.65	-0.10	18.8	450	0.45	0.159	0.1125	0.0933	0.00000114	0.003	4.98	791.9	
US 03	FMH4009974	FMH4009975	3.2	3.01	30.4	675	0.675	0.358	0.16875	0.0063	0.00000114	0.003	1.68	600.4	10
						Sub-P	pe for A08								
PS A08a	FMH4010451	FMH4010452	0.34	0.33	7.5	600	0.6	0,283	0.15	0.0013	0.00000114	0.006	0.64	181.3	
PS A08b	FMH4010451	FMH4010452	0.34	0,33	7.5	600	0.6	0,283	0.15	0.0013	0.00000114	0.006	0.64	181,3	
PS A10a	FMH4010453	FMH4010454	-0.2	-2.8	20.1	600	0.6	0.283	0.15	0.1296	0.00000114	0.003	7.09	2003.3	to an analysis of the second
PS A10b	FM114010453	FMH4010454	-0.2	-2.2	20.1	450	0.45	0.159	0.1125	0.0997	0.00000114	0.003	5.15	818.5	1
PS A10c	FMH4010453	FMH4010454	-0.2	-2.2	20.1	450	0.45	0.159	0.1125	0.0997	0.00000114	0.003	5.15	818.5	I .

Note:

^[1] The roughness coefficient for slimed concrete sewer under poor condition is adopted; the ks values are 3mm for velocities greater than 1.2m/s, otherwise 6mm.

^[2] The Manhole ID of the sewage manhole between Pipe PS A02 & PS A03 is not available.

^[3] The invert level between FMH4009984 and FMH4009986 (Downsmeam of PS B03 to Upstream of PS B06) are not available. Average slope has been adopted.

Appendix 111: Calculation of Existing Pipe Capacity

Table B: Proportion of Peak Flow to Full Capacity

Segment	Upstream Manhole	Downstream Manhole	Full Capacity (L/s)	Catchment	Total catchment discharge (m²/day) [1]	Contribution Population ^[2]	Peaking Factor ^[3]	Catchment Inflow Factors, P _{CIP} (4)	Peak Flow ^[5] (L/s)	Total Peak Flow ^{[6][7]} (L/s)	% of full capacity
		•		Existing Pipes				l .			
	T			Site A Upstream Pipe Section 01 + project(A) + A + B + C				T			
PS A01	FM114009914	FM134009915	339.4	+ D	2793.4	10346	4	1.3	168.1	511.3	151%
P\$ A02	FMH4009915	Unknown	449.4	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	114%
PS A03	Unknown	FM114009917	293.0	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168,1	511.3	175%
PS A04	FMH4009917	FMH4009918	355.9	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1,3	168.1	511.3	144%
PS A05	FM114009918	FM114009919	404.7	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	126%
PS A06	FMH4009919	FMH4010450	384.5	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	133%
PS A07	FM114010450	FM114010451	377.1	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	136%
PS A08	FMH4010451	FMH4010452	362.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	141%
PS A09	FM114010452	FM114010453	1224.1	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168,1	511.3	42%
PS A10	FMH4010453	FMH4010454	3640.3	Upstream Pipe Section 01 + Upstream Pipe Section 02 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	1303.2	36%
	,	•		Site B						•	
PS B01	FMH4009981	FMH4009982	1559.7	Upstream Pipe Section 03 + project(B)	311.6	1154	6	1.3	28.1	628.5	40%
PS B02	FM114009982	FM114009983	1077.5	Upstream Pipe Section 03 + project(B) + E	480.3	1779	6	1.3	43.4	643.7	60%
PS B03	FMH4009983	FMH4009984	1431.9	Upstream Pipe Section 03 + project(B) + E	480.3	1779	6	1.3	43.4	643.7	45%
PS B04	FM114009984	FM114009985	1431.9	Upstream Pipe Section 03 + project(B) + E	480.3	1779	6	1.3	43.4	643.7	45%
PS B05	FMH4009985	FMH4009986	1431.9	Upstream Pipe Section 03 + project(B) + E	480.3	1779	6	1.3	43.4	643.7	45%
PS B06	FM114009986	FM114009987	1431.9	Upstream Pipe Section 03 + project(B) + E	480.3	1779	6	1.3	43.4	643.7	45%

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Note:

- [1] The discharge from Upstream Pipes US 01, US 02 & US 03 are not included.
- [2] The contribution population = total catchment discharge (m³/day) / 0.27(m³/day/person)
- [3] Peaking Factor of 8 for contribution population < 1,000,6 for contribution population of 1000 5000,5 for contribution population of 5000-10000 and 4 for contribution population of 10000-50000 are adopted.
- [4] Catchment Inflow Factors of North West Kowloon (=1.3) has been adopted
- [5] Peak Flow = Daily average dry weather flow × Peaking Factor (including stormwater allowance) × Catchment Inflow Factor / 24 / 3600, the operation hour is assumed to be 24 hours.
- [6] Full pipe capacity of US 01 is added to the peak flow of PS A01-PS A10, and full pipe capacity of US 02 is added to the peak flow of PS A10.
- [7] Full pipe capacity of US 02 is added to the peak flow of PS B01- PS B06.

Appendix IV

Capacity Calculation of Proposed Pipes and Upgraded Pipes

Appendix IV: Calculation of Proposed Pipe Capacity

Table A - Pine Canacity Calculation

Segment	Upstream Manhole	Downstream Manhole	Upstream Invert Level (mPD) [1]	Downstream Invert Level (mPD) [1]	Length (m)	Diameter (mm)	Diameter (m)	Area (m²)	Hydraulic Radius (m)	Slope	Kinematic Viscosity (m²/s)	Hydraulic Pipeline Roughness (m) ^[2]	Velocity (m/s)	Full Capacity (1/s)
	Proposed New Pipe													
PP01	FTMH01	FMH4009914	1.10	1.00	10.0	300	0.3	0.071	0.075	0.0100	0.00000114	0.003	1.24	87.9
PP02	FTM1102	FMH4009981	2.15	1.95	20.0	300	0.3	0.071	0.075	0.0100	0.00000114	0.003	1.24	87.9
	Proposed Upgrading Pipe													
P\$ A01	FMH4009914	FMH4009915	L	0.94	35.3	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A02	FMH4009915	Unknown	0.94	0.82	64.5	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A03	Unknown	FM134009917	0.82	<u>0.75</u>	37.8	<u>900</u>	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A04	FMH4009917	FMH4009918	0.75	0.62	70.6	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A05	FMH4009918	FMH4009919	0.62	0.52	54.6	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A06	FMH4009919	FMH4010450	0.52	0.41	60.5	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
P\$ A07	FMH4010450	FMH4010451	0.41	<u>0.34</u>	34.3	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6
PS A08	FMH4010451	FMH4010452	0.34	0.33	7.5	900	0.9	0.636	0.225	0.0018	0.00000114	0.006	0.99	627.6

^[1] The upstream and downstream level of proposed pipes will be subject to detail design.
[2] The roughness coefficient for slimed concrete sewer under poor condition is adopted; the ks values are 3mm for velocities greater than 1.2m/s, otherwise 6mm.

Appendix IV: Calculation of Proposed Pipe Capacity

Table B: Proportion of Peak Flow to Full Capacity after Upgrading

Segment	Upstream Manhole	Downstream Manhole	Full Capacity (L/s)	Catchment	Total catchment discharge (m²/day) [1]	Contribution Population ⁽²⁾	Peaking Factor ^[3]	Catchment Inflow Factors, P _{CIP} (4)	Peak Flow ⁽⁵⁾ (L/s)	Total Peak Flow ^{[6][7]} (L/s)	% of full capacity
				Proposed New Pipes							
PPOI	FTMH01	FMH4009914	87.9	Project (A)	852.2	3156	6	1.3	76.9	76.9	88%
PP02	FTMH02	FMH4009981	87.9	Project (B)	311.6	1154	6	1.3	28.1	28.1	32%
				Proposed Upgrading Plan							
P\$ A01	FMH4009914	FMH4009915	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A02	FM114009915	Unknown	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A03	Unknown	FMH4009917	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A04	FM114009917	FMH4009918	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A05	FMH4009918	FMH4009919	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A06	FM114009919	FMH4010450	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A07	FMH4010450	FMH4010451	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%
PS A08	FM114010451	FMH4010452	627.6	Upstream Pipe Section 01 + project(A) + A + B + C + D	2793.4	10346	4	1.3	168.1	511.3	81%

Note:

- [1] The discharge from Upstream Pipes US 01, US 02 & US 03 are not included.
- The contribution population = total catchment discharge (m³/day) / 0.27(m³/day/person)
- Peaking Factor of 8 for contribution population < 1,000, 6 for contribution population of 1000 5000, 5 for contribution population of 5000-10000 and 4 for contribution population of 10000-50000 are adopted.
- Catchment Inflow Factors of North West Kowloon (=1.3) has been adopted
- Peak Flow = Daily average dry weather flow × Peaking Factor (including stormwater allowance) × Catchment Inflow Factor / 24 / 3600, the operation hour is assumed to be 24 hours.
- Full pipe capacity of US 01 is added to the peak flow of PS A01-PS A10, and full pipe capacity of US 02 is added to the peak flow of PS A10.
- [2] [3] [4] [5] [6] [7] Full pipe capacity of US 02 is added to the peak flow of PS B01- PS B06.

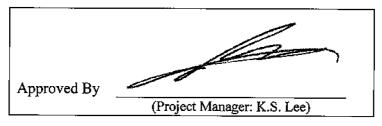
Appendix 9 Water Supply Impact Assessment (WSIA) Report

Urban Renewal Authority Development Scheme Cheung Wah Street / Cheung Sha Wan Road (SSP-018)

Water Supply Impact Assessment Report

(V1.0)

September 2021



REMARKS:

The information supplied and contained within this report is, to the best of our knowledge, correct at the time of printing.

CINOTECH accepts no responsibility for changes made to this report by third parties.

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Figure 2-1 Location of the Project Site

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Appendix I Notional Block Plan of the Proposed Scheme Appendix II Fresh Water Mains Record Plan

Appendix III Salt Water Mains Record Plan

Appendix IV Detailed Water Demand Calculation

1 INTRODUCTION

1.1 Background

- 1.1.1 The Urban Renewal Authority (URA) has proposed a Cheung Wah Street / Cheung Sha Wan Road Development Scheme (SSP-018) (the Scheme) under section 25 of the Urban Renewal Authority Ordinance (URAO). This Water Supply Impact Assessment (SIA) is to support the submission of a draft Development Scheme Plan (DSP) with its planning proposal to the Town Planning Board (TPB) for consideration.
- 1.1.2 Cinotech Consultants Limited was commissioned by URA to conduct this to assess any potential water impact brought by the proposed development. Architectural drawings and technical information of the subject site were largely provided by the project architect and other project team members.

2 DESCRIPTION OF THE ENVIRONMENT

2.1 Existing Environment

- 2.1.1 The Scheme SSP-018 consists of Sites A and B. Site A is bounded by Hing Wah Street on the south-eastern boundary, Cheung Sha Wan Road on the south-western boundary, Cheung Wah Street on the north-western boundary, and Cheung Sha Wan Catholic Secondary School on the north-eastern boundary. Site B is bounded by Cheung Sha Wan Road to the north, Cheung Sha Wan Path to the west, and Sham Shui Po Sports Ground on the south-eastern boundary (Figure 2-1). The proposed gross site areas of the Site A & Site B are 5,197m² and 13,857m² respectively, subject to site survey and detailed design. The location of the site is shown in Figure 2-1.
- 2.1.2 Currently, the Site A comprises a single storey Cheung Sha Wan Sports Centre and its associate outdoor garden and playground. The Site B comprises a government land lot (GLA-TNK 1723) which currently is an open area with a few 1-2 storeys temporary structures, Cheung Sha Wan Path Sitting-out Area, and a garden associated with Sham Shui Po Sports Ground.

2.2 The Proposed Development

- 2.2.1 The entire Site A is proposed to rezone to "R(A)" and redevelop the area for high-density residential development, with non-domestic uses always permitted on the lowest three floors of a building or in the purpose-designed non-residential portion of a building. The proposed development on Site A consists of a 2 floors of basement carpark, a 5 storeys podium (GFA: 5,197m² for retails; 5,197m² for G/IC) and two 34 storeys residential towers (838 flats).
- 2.2.2 Western part of the Site B is proposed to rezone to G/IC and provide a G/IC complex with GFA of 33,696 m² for community and amenity. The rest of the Site B of about 9,645 m², is proposed to be public open space.
- 2.2.3 The proposed notional scheme is shown in Appendix I. The notional design is subject to change at detailed design stage.

3 WATER SUPPLY IMPACT ASSESSMENT

3.1 Existing Freshwater Supply

- 3.1.1 According to the Fresh Water Mains Record Plans and reply letter from Water Supplies Department (WSD), the Scheme Area is currently served by Shek Kip Mei No.2 Fresh Water Service Reservoir (Shek Kip Mei No.2 FWSR; Capacity: 40,000 m³) and Shek Kip Mei No.3 Fresh Water Service Reservoir (Shek Kip Mei No.3 FWSR; Capacity: 48,188 m³).
- 3.1.2 Site A is currently served by a 40/80 mm branch from a 200mm main along Cheung Wah Street which is origin from a 450mm main along Castle Peak Road.
- 3.1.3 Site B is currently served by a 150mm main along Cheung Sha Wan Path, which is connected to a 30" Steel pipe along Lai Chi Kok Road.
- 3.1.4 The WSD Fresh Water Mains Record Plan is provided in Appendix II.

3.2 Freshwater Supply Impact

3.2.1 The calculations for the water demand for the existing and future scenarios and existing spare capacities at different reservoirs are included in **Appendix IV**, together with comparisons with the existing supply facilities. The fresh water demand is expected to increase from 1.31 m³/day to 748.77 m³/d (an increase of 747.46 m³/day, or 0.747 MLD) as a result of the proposed development.

Shek Kip Mei No.2 FWSR & Shek Kip Mei No.3 FWSR

3.2.2 As shown in Appendix IV, there is substantially greater spare capacity (27 MLD) in Shek Kip Mei No.2 FWSR & Shek Kip Mei No.3 FWSR. The expected increase in demand can therefore be accommodated by the existing Fresh Water Service Reservoir. No adverse impact to Fresh Water Service Reservoir is anticipated.

Fresh Water Mains (Site A)

- 3.2.3 Currently, the fresh water of the Site A and Cheung Sha Wan Catholic Secondary School (the School) are sharing the same branch from the 200mm main along Cheung Wah Street. The School is in upstream location and having two 100mm pipes from the 200mm main; while the Site A is located at downstream of the School with only a 40/80mm pipe.
- 3.2.4 With assuming a maximum sustained flow velocity of 2.0m/s, which is 2/3 of the maximum flow velocity (3m/s) suggested in Departmental Instruction (DI) No. 1309 "Design Criteria", the capacity of 40mm, 80mm, 100mm and 200mm mains are 217 m³/day, 869 m³/day, 1357 m³/day, and 5429 m³/day respectively.
- 3.2.5 Assuming the development of Site A is using the existing fresh water pipe to the site, the total fresh water capacity of the Site A and the School is 2714 m³/day (2 x 100mm pipe), while the fresh water capacity of 80mm/40mm branch for the Site A is only 869/217 m³/day.
- 3.2.6 Three time the estimated mean daily fresh water demand of the Proposed Development Site A is ~2,230m³/day. As the water consumption of the School is far less than the residential towers, and the water supply capacity of the School and Site A are more than three time of the estimated mean daily fresh water demand of the Proposed Development (Site A), no fresh water supply impact to the School is anticipated. However, the branch reaching Site A is

- only a 40/80mm pipe which is insufficient. In addition, a two-end feed fresh water supply network is preferred for the proposed development. New fresh water pipes and upgrade of existing fresh water pipes are required.
- 3.2.7 It is proposed to upgrade the existing 40/80mm pipe to 100mm pipe. In addition, it is proposed to provide a new 100mm fresh water pipe connect to the 300mm fresh water main along Lai Chi Kok Road. With the proposed water pipes implemented properly, the fresh water capacity of the Site A is 2714 m³/day (2 x 100mm pipe) with both-end feed supply network thus no adverse fresh water supply impact is anticipated for Site A. The alignment and connection points of the proposed new/upgraded water pipes subject to detail design. The suggested upgrade and new fresh water mains are illustrated in Appendix II.

Fresh Water Mains (Site B)

3.2.8 Three time the estimated mean daily fresh water demand of the Proposed Development Site A is ~20m³/day, which is far below the water capacity of the 150mm fresh water main along Cheung Sha Wan Path (3054 m³/day). No adverse fresh water supply impact is anticipated for Site B.

3.3 Existing Saltwater Supply

- 3.3.1 According to the Fresh Water Mains Record Plans and reply letter from Water Supplies Department (WSD), the Scheme Area is currently served by Cheung Sha Wan Salt Water Pumping Station (Cheung Sha Wan SWPS) (Capacity 96 mld).
- 3.3.2 Site A is currently served by a 150mm main along Cheung Wah Street and Cheung Sha Wan Road.
- 3.3.3 There is no WSD salt water supply main connected to the Site B. The nearest salt water mains are the 6" (~150mm) salt water main along Cheung Sha Wan Road, and a 200mm salt water main along Hing Wah Street. There is also a 50mm branch near the eastern boundary of Site B.
- 3.3.4 The WSD Salt Water Mains Record Plan is provided in Appendix III.

3.4 Salt Water Supply Impact

3.4.1 The calculations for the water demand for the existing and future scenarios and existing spare capacities at different reservoirs are included in **Appendix IV**, together with comparisons with the existing supply facilities. The salt water demand is expected to increase from 0.46 m³/day to 160.28 m³/d (an increase of 159.82 m³/day, or 0.160 MLD) as a result of the proposed development.

Cheung Sha Wan SWPS

3.4.2 As shown in Appendix IV, there is substantially greater spare capacity (24 MDL) in Cheung Sha Wan SWPS. The expected increase in demand can therefore be accommodated by the existing Cheung Sha Wan SWPS. No adverse impact to Cheung Sha Wan SWPS is anticipated.

Salt Water Mains (Site A)

- 3.4.3 With assuming a maximum sustained flow velocity of 2.0m/s, which is 2/3 of the maximum flow velocity (3m/s) suggested in Departmental Instruction (DI) No. 1309 "Design Criteria", the capacity of 150mm mains is 3054m³/day.
- 3.4.4 As the Site A is served by a 150mm main, which making the theoretical total salt water capacity of the Scheme Area and the surrounding area to ~3054 m³/day. The 150mm salt water main has far more than sufficient capacity to maintain three time the estimated mean daily salt water demand of the Site A (~474m³/day), the expected increase in demand of the Site A should not has any adverse impact to the existing salt water mains and downstream areas.

Salt Water Mains (Site B)

- 3.4.5 Three time the estimated mean daily salt water demand of the Site B (~7m³/day) is small compare to the capacity of 150mm mains. However, there is no salt water pipe connected to the west portion of site B, where the proposed G/IC complex located. New salt water pipes are required.
- 3.4.6 It is proposed to provide a new 80mm salt water pipe connect to the 150mm salt water main along Cheung Sha Wan Road. With the proposed water pipe implemented properly, the salt water capacity of the Site B is 869 m³/day thus no adverse salt water supply impact is anticipated for Site B. The alignment and connection points of the proposed new/upgraded water pipes subject to detail design. The suggested new salt water mains are illustrated in Appendix III.

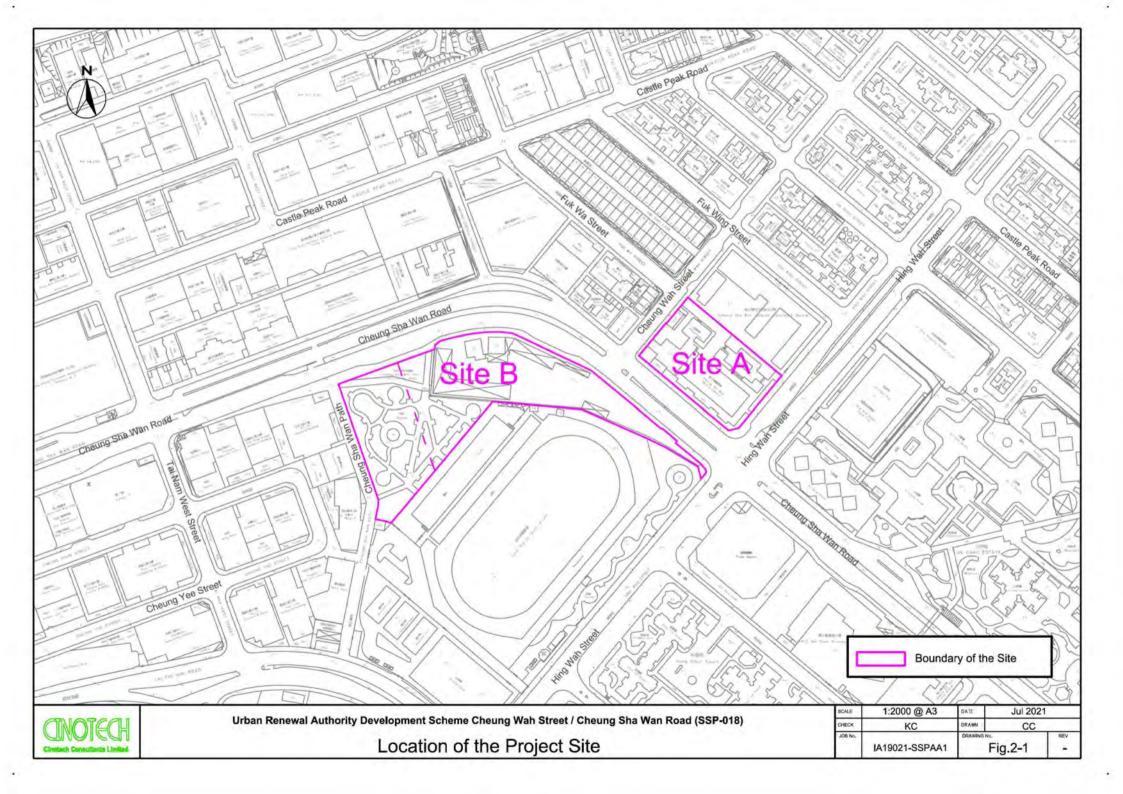
3.5 Construction and Maintenance

- 3.5.1 Responsibilities for the investigation, design, construction, repair and maintenance of the internal water supply facilities and connection to the main water system(s) will be discussed among URA/its joint venture partners/its assignees and relevant Government departments in detailed design stage.
- 3.5.2 The detailed connection arrangements for the Scheme Area and the local water mains will be reviewed in later stages during implementation of the Scheme. Local upgrading and/or realignment may be implemented if necessary.

4 CONCLUSION

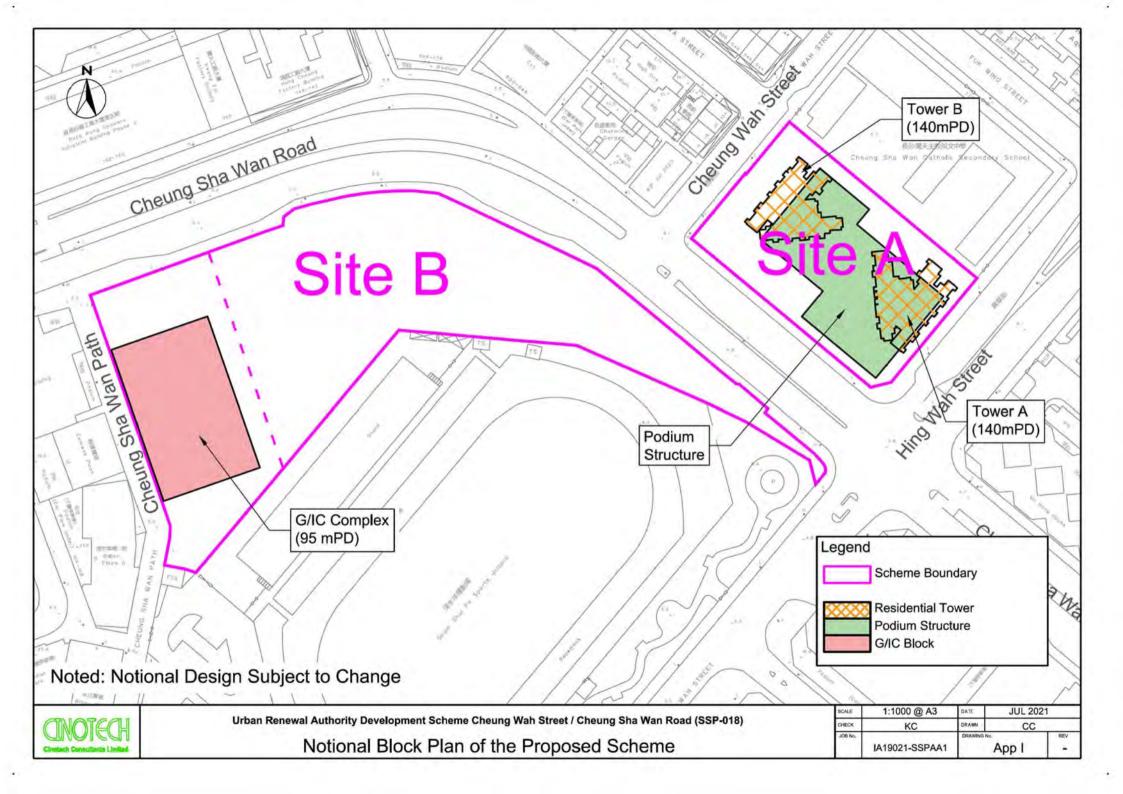
4.1.1 The water supply impact due to the proposed Scheme has been reviewed. Although the proposed Scheme at the Site will result in increases in both the fresh and salt water demands, the increases can be accommodated by the existing main supply facilities and the proposed new/upgraded pipes. Therefore, no adverse water supply impact is anticipated from the proposed development.

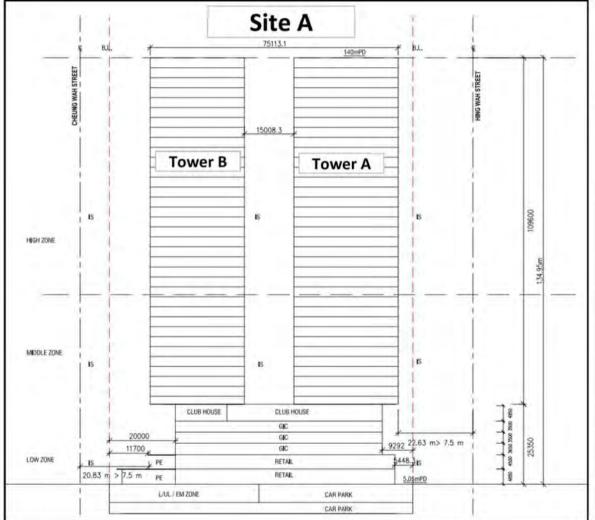
Figure			

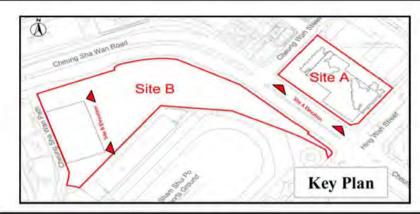


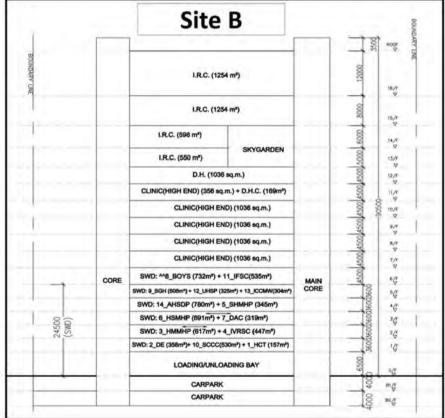
Appendix I

Notional Block Plan of the Proposed Scheme









Remark:

Notional Design subject to change at detailed design stage

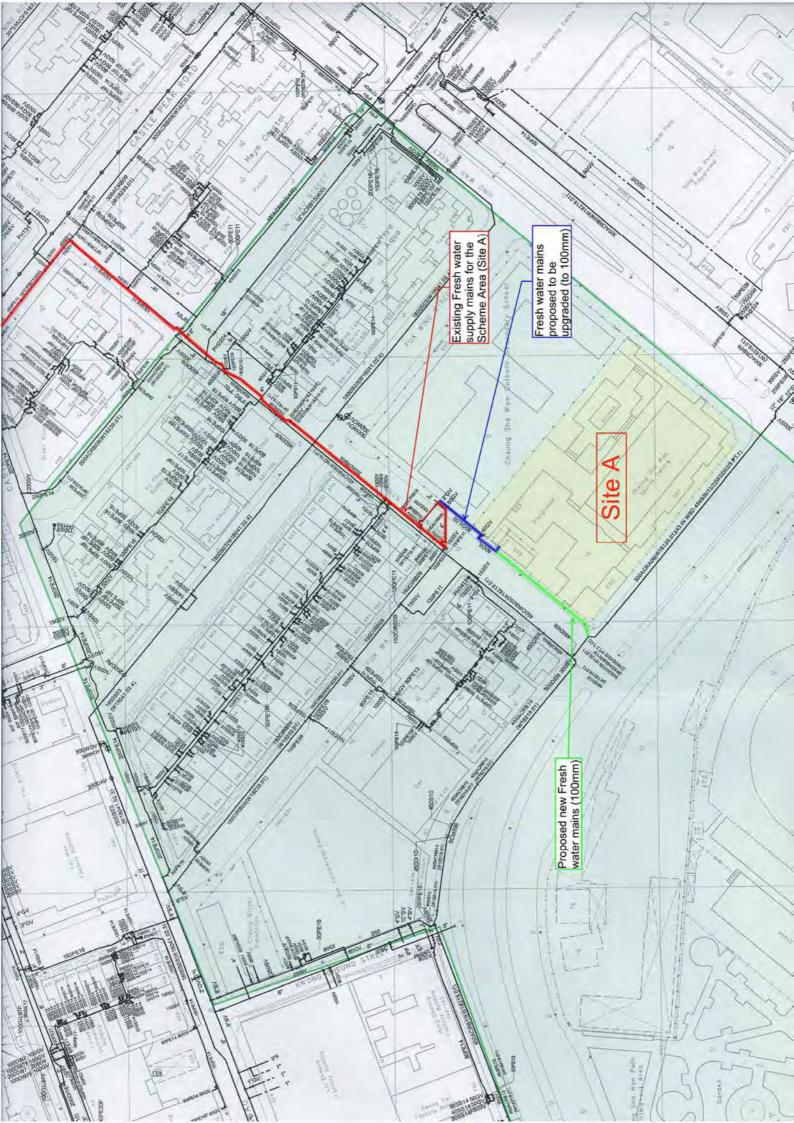


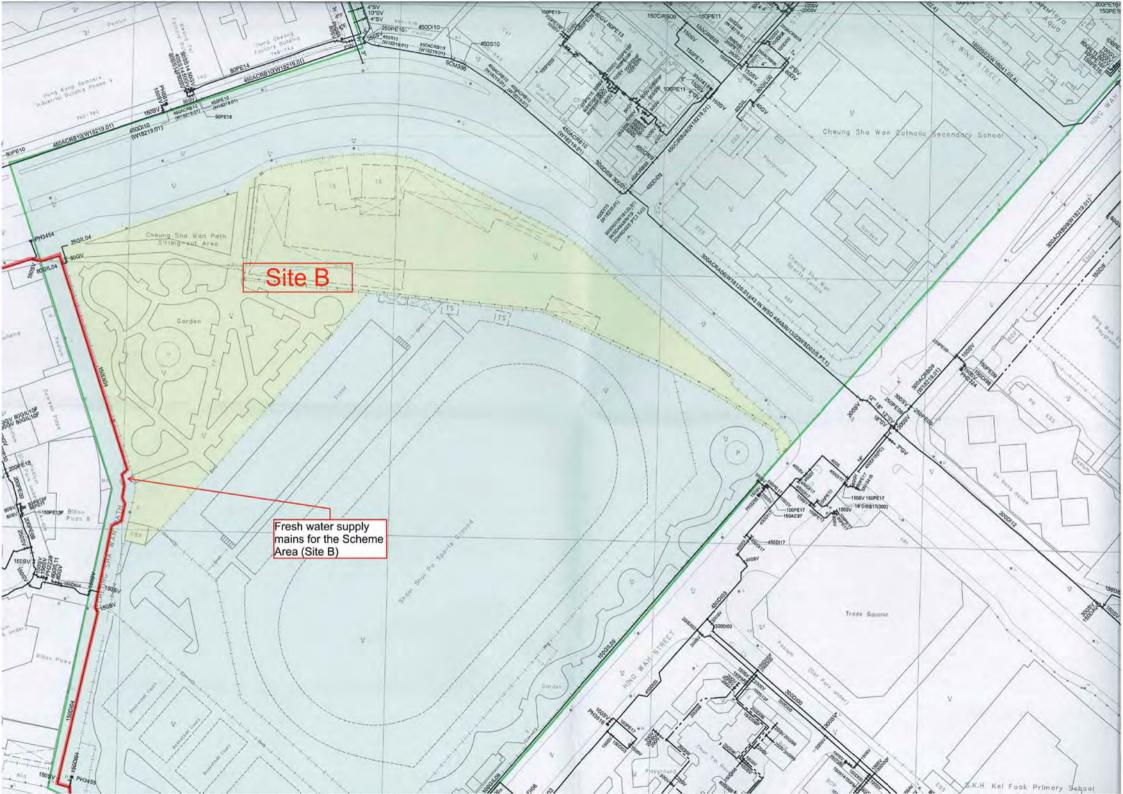
Urban Renewal Authority Development Scheme Cheung Wah Street/ Cheung Sha Wan (SSP-018)

Notional Section Plan of the Proposed Scheme

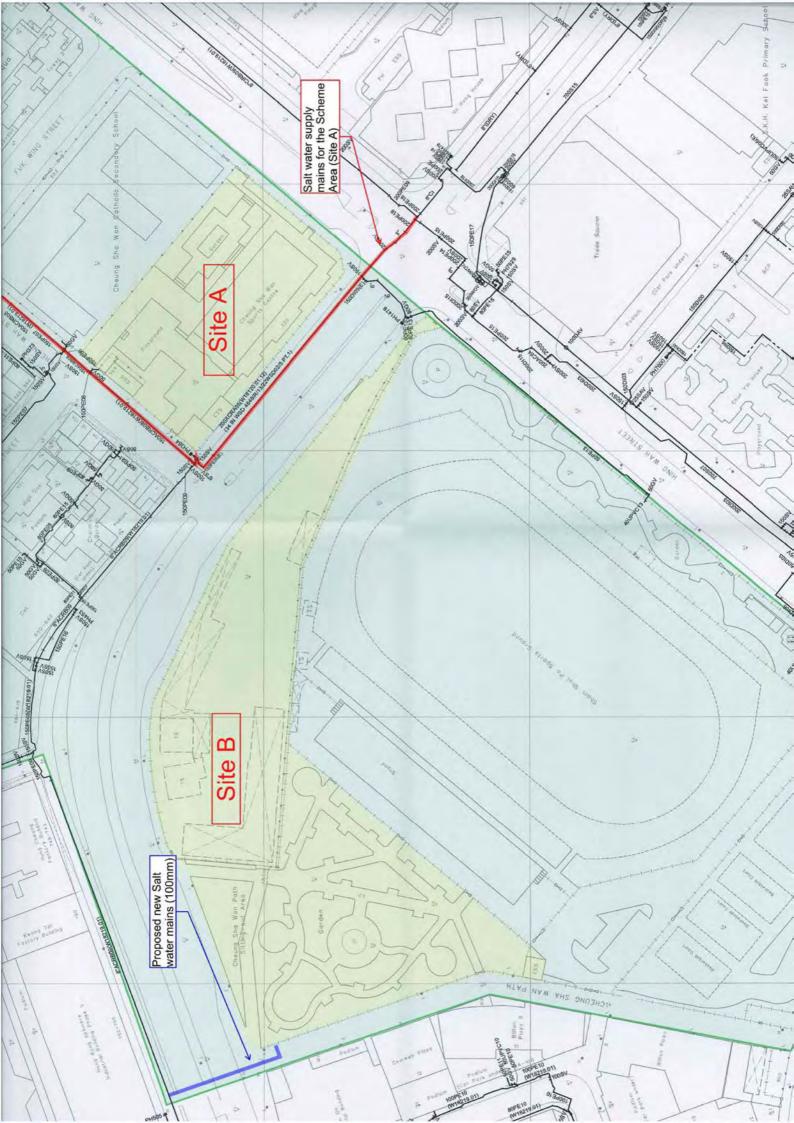
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Appendix II
Fresh Water Mains Record Plan





Appendix III
Salt Water Mains Record Plan



Appendix IV

Detailed Water Demand Calculation

Existing Water Demands

Floor Area (Site A - Cheung Sha Wan Sports Centre)

 $\underline{\text{UFA (m}^2)} [1] \qquad \underline{\text{UFA (ha)}}$

Cheung Sha Wan Sports Centr 6565 m² 6.565 ba

Note [1] - Estimated value.

Site B - Cheung Sha Wan Sports Centre

UFA (m²) UFA (ha)

None [1] ---

Note [1] - There is currently no facility with significant water demand in Site B

Water Demands

Refer to WSD Departmental Instruction 1309

Site A - Commercial & G/IC

	Category	UFA (ha)	Unit Demand Fresh Water	Unit Demand Salt Water (m3/ha/day)	Daily Demand Fresh Water	,
			(m²/ha/day)	(m.ə/navuay)	(m²/d)	(m²/d)
Government, Institution/Community	G/IC	6.6	0.2	0.070	1.31	0.46

<u>Total</u>		
	Daily Demand Fresh Water	Daily Demand Salt Water
	(m³/d)	(m³/d)
Site A	1.31	0.46
Site B	_	1
T1	1.71	0.46

Predicted Water Demands

Populations (Site A - Residiential)

	<u>Units [1]</u>	PPF [2]	Popn.	
Residential Accommodation (R2 & Service Trade)	838	2.6	2,179	Persons
Management/Club House Staff (Service Trade)			20	Persons

Note [1] - The development profile is provided by URA based on the latest Scheme.

Note [2] - The average domestic household size is 2.4 persons for Lai Chi Kok North District Council Constituency Area according to Population By-census 2016.

Floor Area (Site A - Commercial & G/IC)

	<u>UFA (m²) [1]</u>		<u>UFA (ha)</u>	
Commercial (C/R)	5,197	m²	5.197	bя
Government, Institution/Community (G/IC)	5,197	m²	5.197	ba

Note [1] - The development profile is provided by URA based on the latest Scheme.

Floor Area (Site B - G/IC)

 UFA (m²)
 UFA (m²)
 UFA (ha)

 Government, Institution/Community (G/IC)
 33,696
 m²
 33.696

Note [1] - The development profile is provided by URA based on the latest Scheme.

Water Demands

Refer to WSD Departmental Instruction 1309

Site A - Residiential

	Category	Population	Unit Demand Fresh Water	Unit Demand Salt Water	Daily Demand Fresh Water	Daily Demand Salt Water	
	Category	ropusios	(m³/kead/day)	(m³/head/day)	(m³/d)	(m³/d)	
Residential Accommodation	R2	2,179	0.300	0.070	653.64	152.52	
Residential Accommodation	Service Trade	2,179	0.035	0.000	76.26	0.00	
Management and Club House Staff	Service Trade	20	0.035	0.070	0.70	1.40	

ha

Site A - Commercial & G/IC

	Category	UFA (ha)	Unit Demand Fresh Water (m³/ha/day)	Unit Demand Salt Water (m3/ha/day)	Daily Demand Fresh Water (m³/d)	Daily Demand Salt Water (m³/d)
Commercial	C/R	5.2	2	0.700	10.39	3.64
Government, Institution/Community	G/IC	5.2	0.2	0.070	1.04	0.36

Site 8 - G/IC

	Category	UFA (ha)	Unit Demand Fresh Water (m3/ha/day)	Unit Demand Salt Water (m3/ha/day)	Daily Demand Fresh Water (m³/d)	Daily Demand Salt Water (m ³ /d)
Government, Institution/Community	G/IC	33.7	0,2	0.070	6.74	2.36

Tota.

TOTAL		
	Daily Demand Fresh Water	Daily Demand Salt Water
	(m ³ /d)	(m³/d)
Site A	742.03	157.92
Site B	6.74	2.36
Total	748.77	160.28

Summary of Water Demands

Scenario	Daily Demand - Fresh Water	Daily Demand - Salt Water
	(m³/d)	(m³/d)
Existing (Site A only)	1.31	0.46
Future (Site A)	742.03	157.92
Future (Site B)	6.74	2.36
Future (Total)	748.77	160.28
la avana	747.46	159.82
Increase	0.747 (MLD)	0.160 (MLD)

Fresh Water Reservoir Capacity

Reservoir	Capacity {x 1,000 m³)	Supply Capacity @ Capacity Factor = 0.8 (MLD)	Existing Daily Consumption (MLD)	Spare Capacity (MLD)	Remarks
Shek Kip Mei No.2 FWSR	40.000	50.000	83	27	>> 0.747 MLD Additional Demand
Shek Kip Mei No.3 FWSR	48.188	60.235	03	21	from Development

Salt Water Pumping Capacity

Pumping Station	Design Pumping Capacity (MLD)	Existing Daily Consumption (MLD)	Spare Capacity (MLD)	Remarks			
Cheung Sha Wan SWPS	96	72	l 24	>> 0.160 mLD Additional Demand from Development			

Appendix 10

Tentative Implementation Programme

SSP-018 URA Cheung Wah Street / Cheung Sha Wan Road Development Scheme Tentative Implementation Programme

	11.7	Year	1	Т	- 1	ear 2	-11		Year	-3		Y	ear 4			Yea	r 5			Year	6	Т	Y	ear 7	v F		Yea	8.1			Year	9		Y	ear l	0		Ye	ar 11			Year	12		Y	ear	13
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Gazettal of commencement of SSP-018																						I																									
TPB consideration and deemed draft DSP suitable for exhibition																																															
Exhibition of draft DSP for public inspection				1																																											
Processing of representations under s.6 of TPB						ŀ																T						1													1						
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SSP-018 Site B Design, Construction and Completion				1	1					7		-	F								ļ	ļ	ļ						1				1		T												
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